





# The Power to Build







# For nearly 60 years, Simpson Strong-Tie has focused on providing powerful solutions to meet our customers' needs.

We offer a full array of anchoring systems for residential, commercial, infrastructure and industrial uses – from anchoring adhesives and mechanical anchors for anchoring applications in concrete and masonry to direct fastening solutions for attachments to concrete, steel, CMU, or metal deck.

The innovative products featured in this catalog are the result of more than 40 years of research and development, and have passed the rigorous quality-assurance testing you have come to expect from Simpson Strong-Tie. With our expanding lines of high-performance anchoring products, engineering and field support, product testing and training, we are committed to giving you the power to build.







# SIMPSON Strong-Tie

#### **Anchor Product Selection Guide**

		_	Tested Base Materials and Code Listings					<u> </u>	8		
	Pro	duct	Page No.	Cracked	rete Uncracked	Concrete on Metal	CN Grout-Filled	1U Hollow	Unreinforced Clay Brick	Other	Other Listings
				Gracked	Uliciackeu	Deck		HOHOW	Masonry		
	AT-XP®		20	ER-263, F FL-16	ER-263, RR25960, FL-16230.1		ER-281, RR25966, FL-16230.1	_	_	_	NSF/ANSI Std 61, DOT
	SET-XP®		38	ESR-2508, FL-17	RR25744, 449.2	_	ER-265, RR25965, FL-16230.3	ER-265	_	_	NSF/ANSI Std 61, DOT
Adhesive Anchors	ET-HP®		62	ESR-3 FL-17	3372, 449.1	_	ER-241 FL-16230.2	_	ESR-3638, RR25120	_	DOT
Adhesive	AT		86	_	Non-IBC	_	Non-IBC	Non-IBC	ESR-1958	_	DOT
	SET		102	_	Non-IBC	_	Non-IBC	Non-IBC	ESR-1772, FL-15730.5	_	NSF/ANSI Std 61, DOT
	EDOT	1	122	_	Non-IBC	_	_	_	_	_	DOT
	Torq-Cut <sup>™</sup>		138	ESR-2705, RR25946, FL-15731.3		_	_	_	_	_	_
	Strong-Bolt® 2	•	144	ESR-3037, FL-15	RR25891, 731.2	ESR-3037 RR25891 FL-15731.2	ER-240, RR25936 FL-16230.4	_	_	_	UL, FM, DOT
	Wedge-All <sup>®</sup>		164	_	Non-IBC	Non-IBC	ESR-1396, FL-15730.7	_	_	_	UL, FM, DOT
ors	Easy-Set		179	_	Non-IBC	_	_	_	_	_	_
Mechanical Anchors	Sleeve-All®		180	_	Non-IBC	_	Non-IBC	_	_	_	UL, FM, DOT
Me	Titen HD®		184	ESR-2713, RR257 FL-15730.6		<sup>7</sup> 41,	ESR-1056, RR25560, FL-15730.6	IBC	_	_	FM, DOT
	Titen®	***************************************	203	_	FL-2355.1	_	FL-23	355.1	_	_	_
	Titen HD® Rod Hanger		208	ESR-2713, FL-15	RR25741, 730.6	ESR-2713 RR25741	_	_	_	_	FM
	Wood Rod Hanger	***************************************	212	_	_	_	_	_	_	IBC (Wood)	UL, FM

#### **Anchor Product Selection Guide**



			Tested Base Materials and Code Listings						· · · · · · · · · · · · · · · · · · ·		
	Product		Page No.	Con	ncrete Concrete on Metal		Clay Bric		Unreinforced Clay Brick	ed k Other	Other Listings
				Cracked	Uncracked	Deck	Grout-Filled	Hollow	Masonry	Othor	
	Blue Banger Hanger®		214	ESR-	3707	ESR-3707	_	_	_	IBC (Steel Roof Deck)	UL,FM
	Drop-In (DIAB)		224	_	Non-IBC	Non-IBC	_	_	_	_	UL, FM
	Drop-In (DIA)		229	_	Non-IBC	Non-IBC	_	_	_	Non-IBC (Hollow Core Panel)	UL, FM, DOT
	Hollow Drop-In		236	_	Non-IBC	_	_	IBC	_	_	UL,FM
ors	Zinc Nailon™	-	241	_	Non-IBC	_	_	_	_	_	_
Mechanical Anchors	Lag Screw Expansion Shield	CARROLD CO.	239	_	Non-IBC	_	_	_	_	_	_
Me	Expansion Screw Anchor		240	_	Non-IBC	_	_	_	_	_	_
	Crimp Drive®		242	_	Non-IBC	Non-IBC	_	_	_	_	FM
	Split Drive		244	_	Non-IBC	_	_	_	_	_	_
	Tie-Wire		177	_	Non-IBC	Non-IBC	_	_	_	_	_
	Sure Wall	<b>Apply and Apply and Apply apply</b>	245	_	_	_	_	_	_	Drywall	_
Direct Fastening	Powder-Actuated Fasteners		266	_	ESR-2138, RR25469, FL-15730.3, FL-15730.4	ESR-2138, RR25469, FL-15730.3, FL-15730.4	ESR-2138, RR25469, FL-15730.3, FL-15730.4	ESR-2138, RR25469, FL-15730.3, FL-15730.4	_	Steel ESR-2138, RR25469, FL-15730.3, FL-15730.4	FM
Direct Fa	Gas-Actuated Fasteners	*********	249	_	ESR-2811, RR25837, FL-15730.1 FL-15730.2	ESR-2811, RR25837, FL-15730.1 FL-15730.2	ESR-2811, RR25837, FL-15730.1 FL-15730.2	ESR-2811, RR25837, FL-15730.1 FL-15730.2	_	Steel, ESR-2811, FL-15730.1, FL-15730.2	_

ESR or ER – ICC-ES or IAPMO UES code report available.

 $\ensuremath{\mathsf{RR}}-\ensuremath{\mathsf{City}}$  of Los Angeles research report available.

FL - Florida building code approval available.

 $\ensuremath{\mathsf{IBC}}$  – Load data is available in this catalog intended for use under  $\ensuremath{\mathsf{IBC}}$  , but code listings are not available.

Non-IBC – Load data is available in this catalog, but it is outside the scope of the current IBC. May be permitted for non-IBC applications.

UL - Underwriters Laboratories listing available.

FM – Factory Mutual listing available.

DOT – Various departments of transportation listings available. See www.strongtie.com/DOT for details.

# C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

#### **Table of Contents**

## **SIMPSON** Strong-Tie

#### **Adhesive Anchors**

	Adhesive Accessories	128
	Adhesive Anchoring Installation Instructions	124
	Adhesive Retaining Caps	132
	Adhesive Shear Tubes	135
	AT Acrylic Adhesive	86
鹹	. AT-XP® Acrylic Adhesive	20
	EDOT Adhesive	122
	ET-HP® Adhesive	62
	Hole-Cleaning Brushes	135
	Steel Adhesive Anchoring Screen Tubes	133
	Opti-Mesh Adhesive Anchoring Screen Tubes	134
鹹	Piston Plug Delivery System	130
	Retrofit Bolt	135
	SET Epoxy Adhesive	102
	SET-XP® Epoxy Adhesive	38

#### **Direct Fastening**

Extension Tools	273 249 248 266 253
Gas-Actuated Fasteners and Accessories  GCN-MEP Concrete Nailer  Powder-Actuated Fasteners  Powder-Actuated Tool/Load/Fastener Matrix  Powder-Actuated Tool Matrix  Powder Loads  PTP-27L / PTP-27LMAGR  PTP-27S / PTP-27SMAGR	249 248 266 253
GCN-MEP Concrete Nailer	248 266 253
Powder-Actuated Fasteners  Powder-Actuated Tool/Load/Fastener Matrix  Powder-Actuated Tool Matrix  Powder Loads  PTP-27L / PTP-27LMAGR  PTP-27S / PTP-27SMAGR  PT-27HDA	266 253
Powder-Actuated Tool/Load/Fastener Matrix  Powder-Actuated Tool Matrix  Powder Loads  PTP-27L / PTP-27LMAGR  PTP-27S / PTP-27SMAGR  PT-27HDA	253
Powder-Actuated Tool Matrix  Powder Loads  PTP-27L / PTP-27LMAGR  PTP-27S / PTP-27SMAGR  PT-27HDA	
Powder Loads PTP-27L / PTP-27LMAGR PTP-27S / PTP-27SMAGR PT-27HDA	254
PTP-27L / PTP-27LMAGR PTP-27S / PTP-27SMAGR PT-27HDA	
PTP-27S / PTP-27SMAGR	265
PT-27HDA	256
	258
DT 07	260
F I-27	261
PT-22A	262
PT-22HA	263
PT-22P	

#### **Mechanical Anchors**

	Blue Banger Hanger® Threaded Insert	.214
凾	Crimp Drive® Anchor	.242
鹹	Drop-In Internally Threaded Anchor (DIAB)	.224
	Drop-In Internally Threaded Anchor (DIA)	.229
	Easy-Set Pin-Drive Anchor	.179
	Expansion Screw Anchor	.240
NEW	Hollow Drop-In Anchor	
9	LSES Lag Screw Expansion Shield	
	Sleeve-All® Sleeve Anchor	
	Split-Drive Anchor	
	Strong-Bolt® 2 Wedge Anchor	
	Sure Wall Drywall Anchor	
NEW	Tie-Wire Anchor	
9	Titen HD® Screw Anchor	
	Titen® Screw	
	Titen® Stainless-Steel Screw	
	Titen HD® Rod Hanger	
	Titen HD® Rod Coupler	
	Torq-Cut™ Self-Undercutting Anchor	
	Wedge-All® Wedge Anchor	
<u>a</u> i		
NEW	Wood Rod Hanger	
	Zinc Nailon™ Pin Drive Anchor	.241

#### **Restoration Solutions**

	Crack Injection Guide	293
	Crack-Pac® Flex-H <sub>2</sub> 0™	288
	Crack-Pac® Injection Epoxy	286
	Crack Repair Accessories	289
	Epoxy Injection Guide	296
	ETI Injection Epoxy	284
N	Heli-Tie™ Helical Stitching Tie	292
	Heli-Tie™ Helical Wall Tie	290

#### **Carbide Drill Bits and Accessories**

"A" Taper Drill Bits	306
Core Bits	313
Demolition Bits	310
Rebar Cutter	308
Rebar Cutter Adaptors	309
SDS-MAX® Drill Bits	304
SDS-PLUS® Drill Bits	302
Spline/Straight Shank Drill Bits	305

#### **Additional Information**

Allowable Stress Design Method	322
Alphabetical Index of Products	335
Anchor Selection Guide	4
Corrosion Information	316
Example Design Calculations	324
General Instructions for the Designer	15
General Instructions for the Installer	13
Glossary of Common Terms	332–334
Strength Design Method	322
Suggested General Notes for Anchor Products	331
Supplemental Topics for Anchors	316–318
Table Icons	12



New products are shown with the symbol.



### Simpson Strong-Tie Company Inc.



18-135

136-245

246-281

Product Identification Key

general categories, identified by

tabs along the page's outer edge.

Products and additional informationare divided into eight

**Adhesive Anchors** 

**Mechanical Anchors** 

**Direct Fastening** 

For nearly 60 years, Simpson Strong-Tie has focused on creating structural products that help people build safer and stronger homes and buildings. A leader in structural systems research and technology, Simpson Strong-Tie is one of the largest suppliers of structural building products in the world. The Simpson Strong-Tie commitment to product development, engineering, testing and training is evident in the consistent quality and delivery of its products and services.

For more information, visit the company's website at www.strongtie.com.

#### The Simpson Strong-Tie Company Inc. "No Equal" pledge includes:

- Quality products value-engineered for the lowest installed cost at the highest-rated performance levels
- Most thoroughly tested and evaluated products in the industry
- · Strategically located manufacturing and warehouse facilities
- · National code agency listings
- · Largest number of patented connectors in the industry
- · Global locations with an international sales team
- In-house R&D and tool and die professionals
- · In-house product testing and quality control engineers
- Support of industry groups including AISI, AITC, ASTM, ASCE, AWC, AWPA, ACI, AISC, CSI, CFSEI, ICFA, NBMDA, NLBMDA, SDI, SETMA, SFA, SFIA, STAFDA, SREA, NFBA, TPI, WDSC, WIJMA, WTCA and local engineering groups.

# The Simpson Strong-Tie Quality Policy

We help people build safer structures economically. We do this by designing, engineering and manufacturing "No Equal" structural connectors and other related products that meet or exceed our customers' needs and expectations. Everyone is responsible for product quality and is committed to ensuring the effectiveness of the Quality Management System.



# Getting Fast Technical Support

When you call for engineering technical support, we can help you quickly if you have the following information at hand. This will help us to serve you promptly and efficiently.

- Which Simpson Strong-Tie catalog are you using? (See the front cover for the form number.)
- Which Simpson Strong-Tie product are you using?
- What are the design requirements (i.e., loads, anchor diameter, base material, edge/spacing distance, etc.)?

#### We Are ISO 9001-2008 Registered

Simpson Strong-Tie is an ISO 9001-2008 registered company. ISO 9001-2008 is an internationally recognized quality assurance system that lets our domestic and international customers know they can count on the consistent quality of Simpson Strong-Tie® products and services.



800-999-5099

www.strongtie.com

# **Restoration Solutions** 282-297 **Carbide Drill Bits** 298-313 314-331 **Appendix** 332-334 **Glossary of Terms** Alphabetical Index 335-340 of Products

#### **New Products**





# AT-XP® High-Strength Acrylic Adhesive

Formulated for high-strength anchorage of threaded rod and rebar into concrete (cracked or uncracked) and masonry under a wide range of conditions, AT-XP dispenses easily in cold or warm environments and, when mixed, is a dark teal color for easy identification.

See page 20 for more information.



# Adhesive Piston Plug Delivery System

The Simpson Strong-Tie® Adhesive Piston Plug Delivery System facilitates consistent dispensing of anchoring adhesives in any installation orientation. The matched tolerance design between the piston plug and the drilled hole virtually eliminates the formation of voids and air pockets during adhesive dispensing.

See page 130 for more information.



# Battery-Powered Dispensing Tool for Acrylic Adhesives

The ADTA30CKT offers power dispensing of 30 oz., 10:1-ratio, dual-cartridge adhesives without the need for a hose or compressor. Tool comes complete with two 18V lithium-ion battery packs and a charger.

See page 128 for more information.



# Battery-Powered Dispensing Tool for Epoxy Adhesives

The EDTA22CKT offers power dispensing of 22 oz., 1:1-ratio, dual-cartridge adhesives without the need for a hose or compressor, and may be easily converted to dispense 16.5 oz., 2:1-ratio, dual-cartridge adhesives (conversion parts included). Tool comes complete with two 18V lithium-ion battery packs and a charger.

See page 128 for more information.



#### Titen HD® 1/4" Screw Anchor

The new ¼" Titen HD Screw Anchor (THDB25) offers the same self-undercutting, non-expansion characteristics as the popular Titen HD anchor and is code listed for use in cracked and uncracked concrete.

See page 184 for more information.

# c (U) us APPROVED

## Hollow Drop-In Anchor

The Simpson Strong-Tie® Hollow Drop-In Anchor (HDIA) is an internally threaded, flush-mount expansion anchor for use in hollow materials such as CMU and hollow-core plank, as well as in solid base materials.

See page 236 for more information.



# Drop-In Internally Threaded Anchor (DIAB)

The redesigned drop-in internally threaded expansion shell anchors set easily by driving the expansion plug towards the bottom of the anchors using the specially designed SDS or hand-drive setting tool. A positive-set indicator shows when the plug is fully set and the anchor has properly expanded.

See page 224 for more information.



# Heli-Tie<sup>™</sup> Helical Stitching Tie

The Simpson Strong-Tie® helical stitching tie provides a unique solution for the preservation and repair of damaged brick and masonry structures. The stitching tie is grouted across the crack to reconnect and distribute the loads over a large surface area while providing an inconspicuous repair that preserves and maintains the appearance of the structure.

See page 292 for more information.



# Wood Rod Hanger

The new wood rod hanger is a one-piece fastening system for suspending ¼" or %" threaded rod from wood members. Both vertical and horizontal rod hangers provide attachment points for use in pipe hanging, fire protection and cable-tray applications. The Type-17 point provides for fast starts with no pre-drilling required.

See page 212 for more information.



## PT-27HDA

The PT-27HDA is a low-velocity, heavy-duty powder-actuated tool designed for installing fasteners into poured and precast concrete, grout-filled concrete masonry block, horizontal mortared joints and structural steel.

See page 260 for more information.



## Tie-Wire Anchor

A wedge-style expansion anchor for use in normal-weight concrete or concrete over metal deck. Offers a tri-segmented, dual-embossed clip.

See page 177 for more information.



# Crimp Drive® Countersunk

The Crimp Drive countersunk anchor is an easy-to-install expansion anchor for use in concrete and grout-filled CMU. The product design helps speed up anchor installation and reduce overall cost.

See page 242 for more information.



# SDS Stop Bit

The fixed-depth drill bit – designed to meet the hole-depth specifications of most drop-in style anchors, including the DIA and DIAB series anchors – takes the guesswork out of drilling to correct depth, saving time and bit life.

See pages 225 or 303 for more information.

#### How to Use This Catalog

# SIMPSON Strong-Tie

# Using Data Tables and Load Tables

This catalog contains both strength design data tables and allowable load tables. Some allowable load tables for concrete were established under old qualification standards that are no longer valid under the IBC. The following icons indicate whether or not a given table is intended to be used under the IBC (or under other building codes that use the IBC as their basis):

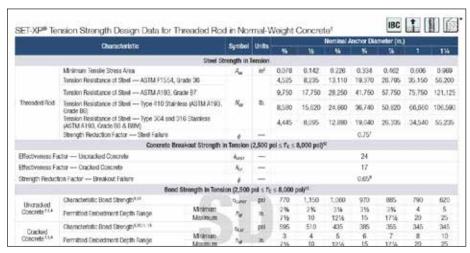




Tables that are "not valid for International Building Code" may be used where the designer determines that other building codes or regulations permit it — for example, under AASTHO or temporary construction.

#### Strength Design Data Tables

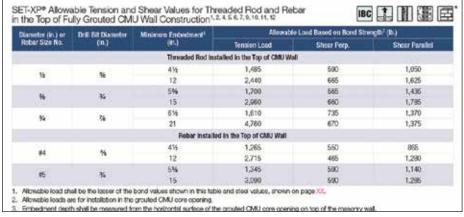
Under the IBC, strength design (see page 322) must be used for cast-in-place and post-installed mechanical and adhesive anchors that are installed into concrete. The design data from these tables are to be used with the design provisions of ACI 318 Appendix D, IBC Chapter 19 and the respective ICC-ES Acceptance Criteria. Strength design data tables are watermarked with the letters "SD." Given the complexity of strength design calculations, designers may find Simpson Strong-Tie<sup>®</sup> Anchor Designer™ software (www.strongtie.com/software) to be a great time saver for computing anchor design strengths using the tabulated design data.



Example Strength Design Data Table

#### Allowable Load Tables

Under the IBC, allowable stress design (see page 322) maybe used for cast-in-place and post-installed adhesive and mechanical anchors installed into masonry or for gas/powder-actuated fasteners installed into concrete, masonry or steel.



Example Allowable Load Table



Under the IBC, allowable stress design may only be used for cast-in-place and post-installed mechanical and adhesive anchors installed into concrete if the allowable loads are converted from strength design calculations. Converted allowable loads are very specific to the design assumptions described in the tables.

	O psi) — Static  Nominal Embed. Depth (in.)		mensions for	Minimum Dir	nensions for	Allowable T	ension Load Ba	sed on Concrete o	r Bond (lb.)
Rod Dis. (dl.)		Nominal Embed: Unwendered		Cracked (in.)		Edge distances = c on all sides		Edge Distances = 1 %" on or side and C <sub>ac</sub> on three sides	
	3000	- b <sub>a</sub>	Cat	No.	Est	Uncracked	Cracked	Uncracked	Cracked
	2%	4 1/4 57/4	314 316	-	-	845		480 570	-
	3	4% 7%	5 435	4%	3%	1,070	820	455 630	555
74	416	6% 10%	8% 6%	6%	3%	1,605	1,230	420 630	830
	6	7%	1116	7%	4%	2,140	1,645	405 630	1,110
	7%	9%	14%	9%	5%	2,675	2,055	400 630	1,390
	2%	514 6%	5% 5%	-	-	1,950	_	1,050 1,050 1,000 1,380 930 1,380 900	-
	4	616	7% 6	616	5%	2.840	1,255	1,000	675
.%:	6	1416	12%	816	516	4,255	1,880	930	1,015
	8	10%	1776 12	10%	5%	5,680	2,505	1,380	1,350
	10	1216 24	22 1/4 15	12%	6%	7,095	3,135	1,380	1,690
	3%	614 716	6% 6%	-	32	2,555	_	1,290	~
	5	814	916 716	814	6%	4,095	1,670	1,340	840
79	716	10%	15% 11%	10%	6%	6,140	2,500	1,245	1,260
	1216	15%	26% 18%	15%	7%	10.230	4,165	1,180 1,850 1,515	2,105
	316	714 816	7% 7%	(80)	-	3,130	-	1,515	-
22.00	. 6	9%	11	9%	7%	5,370	2,145	1,670	1,035
94	9	12%	17%	12%	7%	8.055	3.215	1,555	1,555

**Example Converted Allowable Load Table** 

## Table Icon System

In order to facilitate easier identification of performance data, the following icon system has been incorporated into the sections of the catalog with multiple load tables. These icons will appear in the heading of the table to promote easier visual identification of the type of load, insert type and substrate addressed in the table. Icons are intended for quick identification. All specific information regarding suitability should be read from the table itself.



Normal-Weight Concrete







**Lightweight Concrete** over Metal Deck

















Valid for International **Building Code** 



**Building Code** 

12



## **General Notes**

These general notes are provided to ensure proper installation of Simpson Strong-Tie Company Inc. products and must be followed fully.

- Simpson Strong-Tie Company Inc. reserves the right to change specifications, designs, and models without notice or liability for such changes.
- Unless otherwise noted, dimensions are in inches and loads are in pounds.
- c. Do not overload, which will jeopardize the anchorage. Service loads shall not exceed published allowable loads. Factored loads shall not exceed design strengths calculated in accordance with published design data.
- d. Some hardened fasteners may experience premature failure if exposed to moisture. These fasteners are recommended to be used in dry interior applications.
- Do not weld products listed in this catalog. Some steel types have poor weldability and a tendency to crack when welded.

#### General Instructions for the Installer

These general instructions for the installer are provided to ensure the proper selection and installation of Simpson Strong-Tie products and must be followed carefully. They are in addition to the specific design and installation instructions and notes provided for each particular product, all of which should be consulted prior to and during the installation of Simpson Strong-Tie products.

- Do not modify Simpson Strong-Tie products as the performance of modified products may be substantially weakened. Simpson Strong-Tie will not warrant or guarantee the performance of such modified products.
- Do not alter installation procedures from those set forth in this catalog.
- c. Drill holes for post-installed anchors with carbide-tipped drills meeting the diameter requirements of ANSI B212.15 (shown in the table to the right). A properly sized hole is critical to the performance of post-installed anchors. Rotary-hammered drills with light, high-frequency impact are recommended for drilling holes. When holes are to be drilled in archaic or hollow base materials, the drill should be set to "rotation only" mode.
- d. For mechanical anchors requiring specific installation torque: Failure to apply the recommended installation torque can result in excessive displacement of the anchor under load or premature failure of the anchor. These anchors will lose pre-tension after setting due to pre-load relaxation. See page 316 for more information.
- e. Do not disturb, bolt up, or apply load to adhesive anchors prior to the full cure of the adhesive.
- f. Use proper safety equipment.

Finished Diameters for Rotary and Rotary-Hammer Carbide-Tipped Concrete Drills per ANSI B212.15

Nominal Drill Bit Diameter (in.)	Tolerance Range Minimum (in.)	Tolerance Range Maximum (in.)
1/8	0.134	0.140
5/32	0.165	0.171
3/16	0.198	0.206
7/32	0.229	0.237
1/4	0.260	0.268
5⁄16	0.327	0.335
3/8	0.390	0.398
7/16	0.458	0.468
1/2	0.520	0.530
9⁄16	0.582	0.592
5%	0.650	0.660
11/16	0.713	0.723
3/4	0.775	0.787
13/16	0.837	0.849
27/32	0.869	0.881
7/8	0.905	0.917
15/16	0.968	0.980
1	1.030	1.042
11/8	1.160	1.175
1 3/16	1.223	1.238
11/4	1.285	1.300
1 5/16	1.352	1.367
1%	1.410	1.425
1 7/16	1.472	1.487
1 1/2	1.535	1.550
1 %16	1.588	1.608
15%	1.655	1.675
13⁄4	1.772	1.792
2	2.008	2.028



# Additional Instructions for the Installer for Gas- and Powder-Actuated Fastening

Before operating any Simpson Strong-Tie gas- or powder-actuated tool, you must read and understand the Operator's Manual and be trained by an authorized instructor in the operation of the tool. Simpson Strong-Tie recommends you read and fully understand the safety guidelines of the tool you use. To become a Certified Operator of Simpson Strong-Tie gas- and powder-actuated tools, you must pass a test and receive a certified operator card. Test and Operator's Manual are included with each tool kit. Extra copies may be obtained by contacting Simpson Strong-Tie at (800) 999-5099.

To avoid serious injury or death:

- a. Always make sure that the operators and bystanders wear safety glasses. Hearing and head protection is also recommended.
- b. Always post warning signs within the area when gas- or powderactuated tools are in use. Signs should state "Tool in Use."
- Always store gas- and powder-actuated tools unloaded. Store tools and powder loads in a locked container out of reach of children.
- d. Never place any part of your body over the front muzzle of the tool, even if no fastener is present. The fastener, pin or tool piston can cause serious injury or death in the event of accidental discharge.

- e. Never attempt to bypass or circumvent any of the safety features on a gas- or powder-actuated tool.
- f. Always keep the tool pointed in a safe direction.
- g. Always keep your finger off the trigger.
- h. Always keep the tool unloaded until ready to use.
- Always hold the tool perpendicular (90°) to the fastening surface to prevent ricocheting fasteners. Use the spall guard whenever possible.
- j. Never attempt to fasten into soft, thin, brittle or very hard materials such as drywall, light-gauge steel, glass, tile or cast iron as these materials are inappropriate. Conduct a pre-punch test to determine base material adequacy.
- k. Never attempt to fasten into soft material such as drywall or wood. Fastening through soft materials into appropriate base material may be allowed if the application is appropriate.
- I. Never attempt to fasten to a spalled, cracked or uneven surface.



# General Instructions for the Designer

These general instructions for the designer are provided to ensure the proper selection and installation of Simpson Strong-Tie® products and must be followed carefully. They are in addition to the specific design and installation instructions and notes provided for each particular product, all of which should be consulted prior to and during the design process.

- The term "Designer" used throughout this catalog is intended to mean a licensed/certified building design professional, a licensed professional engineer or a licensed architect.
- b. All connected members and related elements shall be designed by the Designer and must have sufficient strength (bending, shear, etc.) to resist the loads imposed by the anchors.
- c. When the allowable allowable stress design method is used, the design service load shall not exceed the published allowable loads reduced by load-adjustment factors for temperature, spacing and edge distance. Where stated in this catalog, allowable loads may be increased 331/8% when permitted by code. In general, this is permissible only when the alternative basic load combinations of the IBC are used.
- d. When the strength design method is used, the factored loads shall not exceed the design strengths calculated in accordance with the published design data.
- e. Simpson Strong-Tie strongly recommends the following addition to construction drawings and specifications: "Simpson Strong-Tie products are specifically required to meet the structural calculations of plan. Before substituting another brand, confirm load capacity based on reliable published testing data or calculations. The Engineer/Designer should evaluate and give written approval for substitution prior to installation."
- f. Where used in this catalog, "IBC" refers to the 2012 International Building Code, and "ACI 318" refers to ACI 318-11 Building Code Requirements for Structural Concrete. Local and/or regional building codes may require meeting special conditions. Building codes often require special inspection of anchors. For compliance with these requirements, contact the local building authority. Except where mandated by code, Simpson Strong-Tie products do not require special inspection.
- g. Allowable loads and design strengths are determined from test results, calculations and experience. These are guide values for sound base materials with known properties. Due to variation in base materials and site conditions, site-specific testing should be conducted if exact performance in a specific base material at a specific site must be known.
- h. Unless stated otherwise, tests conducted to derive performance information were performed in members with minimum thickness equal to 1.5 times the anchor embedment depth. Anchoring into thinner members requires the evaluation and judgment of a qualified Designer.
- i. Tests are conducted with anchors installed perpendicular (±6° from a vertical reference) from a vertical reference to the surface of the base material. Deviations can result in anchor bending stresses and reduce the load-carrying capacity of the anchor.
- Allowable loads and design strengths do not consider bending stresses due to shear loads applied with large eccentricities.

- k. Metal anchors and fasteners will corrode and may lose loadcarrying capacity when installed in corrosive environments or exposed to corrosive materials. See page 316.
- I. Mechanical anchors should not be installed into concrete that is less than 7 days old. The allowable loads and design strengths of mechanical anchors that are installed into concrete less than 28 days old should be based on the actual compressive strength of the concrete at the time of installation.
- m. Nominal embedment depth ("embedment depth") is the distance from the surface of the base material to the installed end of the anchor and is measured prior to application of an installation torque (if applicable). Effective embedment depth is the distance from the surface of the base material to the deepest point at which the load is transferred to the base material.
- n. Drill bits shall meet the diameter requirements of ANSI B212.15. For adhesive anchor installations in oversized holes, see page 318. For adhesive anchor installations into core-drilled holes, see page 319.
- Threaded-rod inserts for adhesive anchors shall be oil-free UNC fully threaded steel. Bare steel, zinc plating, mechanical galvanizing or hot-dip galvanizing coatings are acceptable.
- p. Allowable loads and design strengths are generally based on testing of adhesive anchors installed into dry holes. For installations into damp, wet and submerged environments, see page 319.
- ACI 318 states that adhesive anchors should not be installed into concrete that is less than 21 days old. For information on adhesive anchors installed into concrete less than 21 days old, see page 318.
- q. Adhesive anchors can be affected by elevated base material temperature. See page 319.
- r. Anchors are permitted to support fire-resistant construction provided at least one of the following conditions is fulfilled: (a) anchors are used to resist wind or seismic forces only; (b) anchors that support gravity-load-bearing structural elements are within a fire-resistive envelope or a fire-resistive membrane, are protected by approved fire-resistive materials, or have been evaluated for resistance to fire exposure in accordance with recognized standards; or (c) anchors are used to support non-structural
- s. Exposure to some chemicals may degrade the bond strength of adhesive anchors. Refer to the product description for chemical resistance information or refer to see page 320.

# SIMPSON Strong-Tie

#### **Important Information and General Notes**

## Limited Warranty

Simpson Strong-Tie Company Inc. warrants catalog products to be free from defects in material or manufacturing. Simpson Strong-Tie Company Inc. products are further warranted for adequacy of design when used in accordance with design limits in this catalog and when properly specified, installed and maintained. This warranty does not apply to uses not in compliance with specific applications and installations set forth in this catalog, or to non-catalog or modified products, or to deterioration due to environmental conditions.

Simpson Strong-Tie® anchors, fasteners and connectors are designed to enable structures to resist the movement, stress and loading that results from impact events such as earthquakes and high-velocity winds. Other Simpson Strong-Tie products are designed to the load capacities and uses listed in this catalog. Properly installed Simpson Strong-Tie products will perform in accordance with the specifications set forth in the applicable Simpson Strong-Tie catalog. Additional performance limitations for specific products may be listed on the applicable catalog pages.

Due to the particular characteristics of potential impact events, the specific design and location of the structure, the building materials used, the quality of construction, and the condition of the soils involved, damage may nonetheless result to a structure and its contents even if the loads resulting from the impact event do not exceed Simpson Strong-Tie catalog specifications and Simpson Strong-Tie connectors are properly installed in accordance with applicable building codes.

All warranty obligations of Simpson Strong-Tie Company Inc. shall be limited, at the discretion of Simpson Strong-Tie Company Inc., to repair or replacement of the defective part. These remedies shall constitute the sole obligation of Simpson Strong-Tie Company Inc. and the sole remedy of purchaser under this warranty. In no event will Simpson Strong-Tie Company Inc. be responsible for incidental, consequential, or special loss or damage, however caused.

This warranty is expressly in lieu of all other warranties, expressed or implied, including warranties of merchantability or fitness for a particular purpose, all such other warranties being hereby expressly excluded. This warranty may change periodically – consult our website **www.strongtie.com** for current information.

#### Terms and Conditions of Sale

#### **Product Use**

Products in this catalog are designed and manufactured for the specific purposes shown, and should not be used with other connectors not approved by a qualified Designer. Modifications to products or changes in installations should only be made by a qualified Designer. The performance of such modified products or altered installations is the sole responsibility of the Designer.

#### Indemnity

Customers or Designers modifying products or installations, or designing non-catalog products for fabrication by Simpson Strong-Tie Company Inc. shall, regardless of specific instructions to the user, indemnify, defend and hold harmless Simpson Strong-Tie Company Inc. for any and all claimed loss or damage occasioned in whole or in part by non-catalog or modified products.

#### Non-Catalog And Modified Products

Consult Simpson Strong-Tie Company Inc. for applications for which there is no catalog product, or for connectors for use in hostile environments, with excessive wood shrinkage, or with abnormal loading or erection requirements.

Non-catalog products must be designed by the customer and will be fabricated by Simpson Strong-Tie in accordance with customer specifications.

Simpson Strong-Tie cannot and does not make any representations regarding the suitability of use or load-carrying capacities of non-catalog products. Simpson Strong-Tie provides no warranty, express or implied, on non-catalog products. F.O.B. Shipping Point unless otherwise specified.



# Warning

Simpson Strong-Tie Company Inc. anchors, fasteners and connectors are designed and tested to provide specified design loads. To obtain optimal performance from Simpson Strong-Tie products and to achieve maximum allowable design load, the products must be properly installed and used in accordance with the installation instructions and design limits provided by Simpson Strong-Tie. To ensure proper installation and use, designers and installers must carefully read the General Notes, General Instructions to the Installer and General Instructions to the Designer contained in this catalog, as well as consult the applicable catalog pages for specific product installation instructions and notes. Please always consult the Simpson Strong-Tie website at strongtie.com for updates regarding all Simpson Strong-Tie products.

Proper product installation requires careful attention to all notes and instructions, including the following basic rules:

- 1. Be familiar with the application and correct use of the anchor, connector or fastener.
- Follow all installation instructions provided in the catalog, website, *Installer's Pocket Guide* or any other Simpson Strong-Tie publication.
- Follow all product-related warnings provided in the catalog, website or any other Simpson Strong-Tie publication.
- 4. Install anchors, connectors and fasteners in accordance with their intended use.
- 5. Install all anchors, connectors and fasteners per installation instructions provided by Simpson Strong-Tie.
- 6. When using power tools to install fasteners: (a) use proper fastener type for direct fastening tool; (b) use proper powder or gas loads; and (c) follow appropriate safety precautions as outlined in this catalog, on the website or in the tool Operator's Manual.

In addition to following the basic rules provided above as well as all notes, warnings and instructions provided in the catalog, installers, designers, engineers and consumers should consult the Simpson Strong-Tie website at www.strongtie.com to obtain additional design and installation information, including:

- Instructional builder/contractor training kits containing an instructional video, an instructor guide and a student guide in both English and Spanish;
- Installer's Pocket Guide (form S-INSTALL; contact Simpson Strong-Tie for more information), which is designed specifically for installers and uses detailed graphics and minimal text in both English and Spanish to explain visually how to install many key products;

- Information on workshops Simpson Strong-Tie conducts at various training centers throughout the United States;
- Product-specific installation videos;
- · Specialty catalogs;
- Code reports Simpson Strong-Tie® Code Report Finder software:
- Technical fliers, bulletins and engineering letters;
- Master format specifications;
- Material safety data sheets;
- Corrosion information;
- · Adhesive cartridge estimator;
- Simpson Strong-Tie Anchor Designer<sup>™</sup> software;
- Simpson Strong-Tie AutoCAD® menu;
- Simpson Strong-Tie CFS Designer™ software;
- Simpson Strong-Tie Connector Selector<sup>™</sup> software;
- Connector selection guides for engineered wood products (by manufacturer);
- Simpson Strong-Tie Strong-Wall<sup>®</sup> Selector software;
- Simpson Strong-Tie Strong Frame® Selector;
- Simpson Strong-Tie Fastener Finder; and
- Answers to frequently asked questions and technical topics.

Failure to fully follow all of the notes and instructions provided by Simpson Strong-Tie may result in improper installation of products. Improperly installed products may not perform to the specifications set forth in this catalog and may reduce a structure's ability to resist the movement, stress and loading that occur from gravity loads as well as impact events such as earthquakes and high-velocity winds.

Simpson Strong-Tie Company Inc. does not guarantee the performance or safety of products that are modified, improperly installed or not used in accordance with the design and load limits set forth in this catalog.

# **Adhesive** Anchors







From rebar doweling on a high-traffic infrastructure retrofit project to do-it-yourself projects, Simpson Strong-Tie offers a wide variety of adhesive anchoring products to meet virtually any need.

Our strong, versatile epoxy-based adhesives are ideal for anchoring threaded rod, rebar and smooth dowels in an assortment of base materials. And our acrylic formulations deliver consistent performance for high-strength anchor grouting in a wide range of weather conditions — curing fast even in water-saturated concrete.







# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC

#### **AT-XP®** High-Strength Acrylic Adhesive

Strong

Cracked

Concrete

Formulated for high-strength anchorage of threaded rod and rebar into cracked and uncracked concrete and masonry under a wide range of conditions, AT-XP® adhesive dispenses easily in cold or warm environments and in below-freezing temperatures with no need to warm the cartridge. When mixed properly, this low-odor formula is a dark teal color for easy post-installation identification.

#### **Features**

- Passed the demanding ICC-ES AC308 adverse-condition tests pertaining to reduced and elevated temperatures and long-term sustained loads
- Code listed under the IBC/IRC for cracked and uncracked concrete per IAPMO UES ER-263 and City of L.A. RR25960
- · Code listed under the IBC/IRC for masonry per IAPMO UES ER-281 and City of L.A. RR25966
- 10:1 two-component high-strength, acrylic-based anchoring adhesive
- · Suitable for use under static and seismic loading conditions in cracked and uncracked concrete as well as masonry
- Easy hole-cleaning procedure no power-brushing required
- Suitable for use in dry or water-saturated concrete
- For best results, store between 14°F and 80°F
- Cures in substrate temperatures as low as 14°F (–10°C) in 24 hours or less
- Available in 9.4 oz., 12.5 oz. and 30 oz. cartridges for application versatility
- Volatile Orgainic Compound (VOC) 30 g/L
- Manufactured in the USA using global materials

#### **Applications**

- · Threaded rod anchoring and rebar doweling into concrete and masonry
- Suitable for horizontal, vertical and overhead applications

Codes: IAPMO UES ER-263 (concrete); IAPMO UES ER-281 (masonry); City of L.A. RR25960 (concrete), RR25966 (masonry); FL-16230.1; NSF/ANSI Standard 61 (43.2 in.<sup>2</sup>/1,000 gal.)

#### **Chemical Resistance**

See pages 320-321.

#### Installation and Application Instructions

(See also pages 124-127.)

- Surfaces to receive adhesive must be clean.
- Base material temperature must be 14°F or above at the time of installation. For best results, material should be 14-80°F at time of application.
- To warm cold material, store cartridges in a warm, uniformly heated area or storage container. Do not immerse cartridges in water to facilitate warming.
- Mixed material in nozzle can harden in 3-4 minutes at temperatures of 70°F and above.





#### **Design Example**

See page 328.

#### Suggested Specifications

See www.strongtie.com for more information.





#### AT-XP® Adhesive Cartridge System

Model No.	Capacity ounces (cubic in.)	Cartridge Type	Carton Qty.	Dispensing Tool	Mixing Nozzle
AT-XP10	9.4 (16.9)	Coaxial	6	CDT10S	
AT-XP13	12.5 (22.5)	Side-by-side	10	ADT813S	AMN19Q
AT-XP30	30 (54)	Side-by-side	5	ADT30S ADTA30P or ADTA30CKT	

- 1. Cartridge estimation guidelines are available at www.strongtie.com/apps.
- Detailed information on dispensing tools, mixing nozzles and other adhesive accessories is available on pages 128 through 135 or at www.strongtie.com.
- 3. Use only Simpson Strong-Tie® mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair AT-XP adhesive performance.
- 4. One AMN19Q mixing nozzle and one nozzle extension are supplied with each cartridge.

#### Cure Schedule

Base N Tempe	Cure Time		
°F	°C	(hrs.)	
14	-10	24	
32	0	8	
50	10	3	
68	20	1	
86	30	30 min.	
100	38	20 min.	

For water-saturated concrete, the cure times must be doubled.



AT-XP® Installation Information and Additional Data for Threaded Rod and Rebar in Normal-Weight Concrete<sup>1</sup>

[ ]	ि
整3	
群3	0.
<b>経</b> 3	ിരി





Charactaristic	Symbol	Units		N	ominal An	chor Dian	neter (in.)	/ Rebar Siz	ze	
Characteristic	บแล สิงเซาอเเง			% / #3	1/2 / #4	<b>5% / #5</b>	3/4 / #6	<sup>7</sup> /8 / # <b>7</b>	1 / #8	1¼/#10
	Installation Information									
Drill Bit Diameter for Threaded	d <sub>hole</sub>	in.	7/16	9/16	11/16	13/16	1	1 1/8	13/8	
Drill Bit Diameter for Rebar	d <sub>hole</sub>	in.	1/2	5/8	3/4	7/8	1	1 1/8	13/8	
Maximum Tightening Torqu	Maximum Tightening Torque			10	20	30	45	60	80	125
Parmitted Embadment Denth Dange?	Minimum	h <sub>ef</sub>	in.	23/8	23/4	31/8	3 zz2	3¾	4	5
Permitted Embedment Depth Range <sup>2</sup>	Maximum	h <sub>ef</sub>	in.	71/2	10	12½	15	171/2	20	25
Minimum Concrete Thickness	SS	h <sub>min</sub>	in.	$h_{\rm ef} + 5d_{\rm o}$						
Critical Edge Distance <sup>2</sup>	Critical Edge Distance <sup>2</sup>				See foonote 2					
Minimum Edge Distance	C <sub>min</sub>	in.		1¾ 23						
Minimum Anchor Spacing		Smin	in.			,	3			6

<sup>1.</sup> The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.

 $[h/h_{ef}] \le 2.4$ 

 $\tau_{\textit{k.uncr}}$  = the characteristic bond strength in uncracked concrete, given in the tables that follow  $\leq k_{\textit{uncr}} ((\textit{hgt} \times \textit{f}'_{\textit{o}})^{0.5}/(\prod \times \textit{d}_{\textit{a}}))$ 

h = the member thickness (inches)

 $h_{ef}$  = the embedment depth (inches)

<sup>2.</sup>  $c_{ac} = h_{ef} (\tau_{k,uncr}/1160)^{0.4} \times [3.1 - 0.7(h/h_{ef})]$ , where:



**Adhesive** Anchors

#### AT-XP® Tension Strength Design Data for Threaded Rod in Normal-Weight Concrete<sup>1</sup>



	Chaustavistia		Cumbal	Unite			Nominal A	Anchor Dia	meter (in.)			
	Characteristic		Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	11/4	
		Ste	el Strength	in Tensio	on							
	Minimum Tensile Stress Area		A <sub>se</sub>	in. <sup>2</sup>	0.078	0.142	0.226	0.334	0.462	0.606	0.969	
	Tension Resistance of Steel — ASTM F155	54, Grade 36			4,525	8,235	13,110	19,370	26,795	35,150	56,200	
Threaded	Tension Resistance of Steel — ASTM A193	3, Grade B7			9,750	17,750	28,250	41,750	57,750	75,750	121,125	
Rod	Tension Resistance of Steel — Type 410 S (ASTM A193, Grade B6)	tainless	N <sub>sa</sub>	lb.	8,580	15,620	24,860	36,740	50,820	66,660	106,590	
	Tension Resistance of Steel — Type 304 and 316 Sta (ASTM A193, Grade B8 & B8M)				4,445	8,095	12,880	19,040	26,335	34,540	55,235	
	Strength Reduction Factor — Steel Failure			_				0.756				
	Concrete	Breakout Stren	gth in Tens	sion (2,50	00 psi ≤ f' <sub>c</sub>	≤ 8,000 p	si)					
Effectiveness Factor — Uncracked Concrete				_				24				
Effectiveness Factor — Cracked Concrete								17				
Strength Redu	ction Factor — Breakout Failure		φ	_				0.658				
	Во	nd Strength in	Tension (2,	500 psi ≤	$\leq f'_{\rm C} \leq 8,00$	0 psi)						
	Characteristic Bond Strength		$ au_{k,uncr}$	psi	1,390	1,590	1,715	1,770	1,750	1,655	1,250	
Uncracked Concrete 2,3,4	5	Minimum			2%	23/4	31/8	31/2	3¾	4	5	
OUTION	Permitted Embedment Depth Range	Maximum	h <sub>ef</sub>	in.	71/2	10	12½	15	17½	20	25	
	Characteristic Bond Strength <sup>9,10,11</sup>		$ au_{k,cr}$	psi	1,085	1,035	980	950	815	800	700	
Cracked Concrete 2,3,4		Minimum			3	3	31/8	31/2	3¾	4	5	
COTIOTOLO	Permitted Embedment Depth Range	Maximum	h <sub>ef</sub>	in.	7½	10	12½	15	17½	20	25	
	Bond Strength in Tension	n — Bond Strer	ngth Reduc	tion Fact	tors for Co	ntinuous S	pecial Ins	pection				
	Strength Reduction Factor — Dry Concrete		$\phi_{dry}$	_			$0.65^{7}$			0.	55 <sup>7</sup>	
Stre	ength Reduction Factor — Water-Saturated Cond	crete	$\phi_{sat}$	_				$0.45^{7}$				
Additional Factor for Water-Saturated Concrete				_	0.54 <sup>5</sup> 0.77 <sup>5</sup>			0.	965			
	Bond Strength in Tensi	on — Bond Str	ength Redu	ıction Fa	ctors for P	eriodic Sp	ecial Inspe	ection				
Strength Redu	ction Factor — Dry Concrete		$\phi_{drv}$	_			0.55 <sup>7</sup>			0.	45 <sup>7</sup>	
Strength Redu	ction Factor — Water-Saturated Concrete		$\phi_{sat}$	_				0.457				
Additional Fac	tor for Water-Saturated Concrete		K <sub>sat</sub>	_	0.	46 <sup>5</sup>		0.655		0.	0.815	

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- Temperature Range: Maximum short-term temperature of 180°F. Maximum long-term temperature of 110°F.
- Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term concrete temperatures are constant temperatures over a significant time period.
- 5. In water-saturated concrete, multiply  $\tau_{k,uncr}$  and  $\tau_{k,cr}$  by  $K_{sat}$ .
- 6. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 7. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 8. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition A are met, refer to Section D.400.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 9. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for  $\frac{1}{2}$ ",  $\frac{5}{4}$ ",  $\frac{9}{4}$ " and 1" anchors must be multiplied by  $\frac{2}{4}$ 0.85.
- 10. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for 11/4" anchors must be multiplied by  $\alpha_{N,seis} = 0.75$ .
- 11. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for  $\frac{7}{6}$ " anchors must be multiplied by  $\alpha_{N,seis} = 0.59$ .

<sup>\*</sup> See page 12 for an explanation of the load table icons.







#### AT-XP® Tension Strength Design Data for Rebar in Normal-Weight Concrete1

To reflect the regard being the being the beat and								Rebar Size			
	Characteristic		Symbol	ibol Units	#3	#4	#5	#6	#7	#8	#10
			Steel Stren	ath in Tei		<i>"</i> "4	#5	#10	#1	#0	#10
	Minimum Tensile	Stress Area	A <sub>se</sub>	in. <sup>2</sup>	0.11	0.2	0.31	0.44	0.6	0.79	1.27
	Tension Resistance of Steel — Rebar										
Rebar	(ASTM A615 G	N <sub>sa</sub>	lb.	9,900	18,000	27,900	39,600	54,000	71,100	114,300	
Hobai	Tension Resistance of (ASTM A706 G	r sa	ID.	8,800	16,000	24,800	35,200	48,000	63,200	101,600	
	Strength Reduction Fact	or — Steel Failure	φ	_				$0.75^{6}$			
	C	oncrete Breakout S	Strength in 1	Tension (2	2,500 psi ≤	$f_{C}^{\prime} \leq 8,000$	psi)				
Effectiveness	Factor — Uncracked Con-	crete	k <sub>uncr</sub>	_				24			
Effectivenes	s Factor — Cracked Conc	rete	k <sub>cr</sub>					17			
Strength Reduction Factor — Breakout Failure				_	0.658						
Bond Strength in Tension (2,500 psi $\leq$ f' <sub>c</sub> $\leq$ 8,000 psi)											
Uncracked Concrete <sup>2,3,4</sup>	Characteristic Bo	$ au_{k,uncr}$	psi	1,010	990	970	955	935	915	875	
	Permitted Embedment	Minimum	4	in	23/8	23/4	31/8	31/2	3¾	4	5
	Depth Range	Maximum	h <sub>ef</sub>	in.	71/2	10	12½	15	171/2	20	25
	Characteristic Bo	$ au_{k,cr}$	psi	340	770	780	790	795	795	820	
Cracked Concrete 2,3,4	Permitted Embedment	Minimum	h	in.	3	3	31/8	31/2	3¾	4	5
	Depth Range	Maximum	h <sub>ef</sub>	111.	71/2	10	12½	15	17½	20	25
	Bond Strength in	Tension — Bond S	Strength Re	duction F	actors for	Continuous	Special In	spection			
Strength Rec	luction Factor — Dry Cond	rete	$\phi_{dry}$	_			$0.65^{7}$			0.9	55 <sup>7</sup>
Strength Reduction	Factor — Water-Saturated	d Concrete	$\phi_{sat}$	_				0.457			
Additional Fac	tor for Water-Saturated Cor	ncrete	K <sub>sat</sub>	_	0.	54 <sup>5</sup>		0.775		0.9	96 <sup>5</sup>
	Bond Strength	in Tension — Bond	Strength F	Reduction	Factors fo	r Periodic S	Special Insp	ection			
Strength Reduction Factor -	— Dry Concrete		$\phi_{dry}$	_			0.55 <sup>7</sup>			0.4	45 <sup>7</sup>
Strength Reduction Factor -	— Water-Saturated Concre	te	$\phi_{sat}$	_				0.457		1	
Additional Factor for Water-	Saturated Concrete		K <sub>sat</sub>	_	0.4	46 <sup>5</sup>		0.655		0.815	

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- 2. Temperature Range: Maximum short-term temperature of 180°F. Maximum long-term temperature of 110°F.
- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term concrete temperatures are constant temperatures over a significant time period.
- 5. In water-saturated concrete, multiply  $\tau_{k,uncr}$  and  $\tau_{k,cr}$  by  $K_{sat.}$
- 6. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 7. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 8. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .

<sup>\*</sup> See page 12 for an explanation of the load table icons.

Shear Resistance of Steel — ASTM F1554, Grade 36

Shear Resistance of Steel — ASTM A193, Grade B7

Shear Resistance of Steel — Type 410 Stainless

Shear Resistance of Steel — Type 304 and 316

Reduction for Seismic Shear — ASTM F1554, Grade 36 Reduction for Seismic Shear — ASTM A193, Grade B7 Reduction for Seismic Shear — Type 410 Stainless

Stainless (ASTM A193, Grade B8 & B8M)

Reduction for Seismic Shear — Type 304 and 316

Stainless (ASTM A193, Grade B8 & B8M) Strength Reduction Factor — Steel Failure

Outside Diameter of Anchor

Load-Bearing Length of Anchor in Shear

Strength Reduction Factor — Breakout Failure

Coefficient for Pryout Strength

Strength Reduction Factor - Private Failure

Characteristic

Minimum Shear Stress Area

(ASTM A193, Grade B6)

(ASTM A193, Grade B6)

Threaded Rod



#### AT-XP® Shear Strength Design Data for Threaded Rod in Normal-Weight Cond

**Symbol** 

 $V_{sa}$ 

 $\alpha_{V,seis}$ 

do

 $k_{cp}$ 

Concrete Breakout Strength in Shear

Concrete Pryout Strength in Shear

in.

in.

Steel Strength in Shear

Units

lb.

0.078

2,260

4.875

4,290

2,225

0.85

0.85

0.375

ncrete	1		IBC	•		*
	Nominal A	Anchor Dia	meter (in.)			
1/2	5/8	3/4	7/8	1	11/4	
0.142	0.226	0.334	0.462	0.606	0.969	
4,940	7,865	11,625	16,080	21,090	33,720	
10,650	16,950	25,050	34,650	45,450	72,675	
9,370	14,910	22,040	30,490	40,000	63,955	
4,855	7,730	11,425	15,800	20,725	33,140	-
		0.85				<
		0.85				
		0.75			0.85	
	0.85	-				
		0.65 <sup>2</sup>				
0.5	0.625	0.75	0.875	1	1.25	
		h <sub>efi</sub>				

outengui neddeuoi i ryddi andre	
<ol> <li>The information presented in this table is to be used in conjunction with t design criteria of ACI 318-11.</li> </ol>	the

- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 3. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 4. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .

 $0.70^{3}$ 

1.0 for  $h_{ef}$  < 2.50"; 2.0 for  $h_{ef}$   $\geq$  2.50"

 $0.70^{4}$ 

5. The values of  $V_{\rm Sa}$  are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F,  $V_{sa}$  must be multiplied by  $\alpha_{V,seis}$  for the corresponding

<sup>\*</sup> See page 12 for an explanation of the load table icons.











#### AT-XP® Shear Strength Design Data for Rebar in Normal-Weight Concrete<sup>1</sup>

Characteristic		Cumbal	Units				Rebar Size				
	GHARACTERISTIC	Symbol	UIIILS	#3	#4	#5	#6	#7	#8	#10	
Steel Strength in Shear											
	Minimum Shear Stress Area	Ase	in. <sup>2</sup>	0.11	0.2	0.31	0.44	0.6	0.79	1.27	
	Shear Resistance of Steel — Rebar (ASTM A615 Grade 60)		lb.	4,950	10,800	16,740	23,760	32,400	42,660	68,580	
0.1	Shear Resistance of Steel — Rebar (ASTM A706 Grade 60)	V <sub>sa</sub>	10.	4,400	9,600	14,880	21,120	28,800	37,920	60,960	
Repar	Rebar Reduction for Seismic Shear — Rebar (ASTM A615 Grade 60)				0.56			0.80			
	Reduction for Seismic Shear — Rebar (ASTM A706 Grade 60)	$\alpha_{V,seis}^{5}$	_		0.56		0.80				
	Strength Reduction Factor — Steel Failure	φ		0.65 <sup>2</sup>							
	Conc	rete Breakou	t Strengt	h in Shear							
	Outside Diameter of Anchor	$d_o$	in.	0.375	0.5	0.625	0.75	0.875	1	1.25	
	Load-Bearing Length of Anchor in Shear	$\ell_e$	in.		$h_{ m ef}$						
Str	ength Reduction Factor — Breakout Failure	φ	_				$0.70^{3}$				
	Concrete Pryout Strength in Shear										
	Coefficient for Pryout Strength	k <sub>cp</sub>	_		1.0	0 for $h_{ef}$ <	2.50"; 2.0 fc	or $h_{ef} \ge 2.50$	)"		
	rength Reduction Factor — Pryout Failure	φ	_				0.704				

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 3. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 4. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 5. The values of  $V_{\rm Sa}$  are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F,  $V_{\rm Sa}$  must be multiplied by  $\alpha_{V_{\rm Seis}}$  for the corresponding anchor steel type.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

### AT-XP® Design Information — Concrete



AT-XP® Tension Design Strengths for Threaded Rod Anchors in Normal-Weight Concrete ( $f_c^1 = 2,500 \text{ psi}$ )

IDC	
IRC	





**Adhesive** Anchors

	Naminal	Minimum [	Dimensions	Minimum I	Tension Design Strength Based on Concrete or Bond (lb.)								
Rod Dia.	Nominal Embed.	for Unc	racked	for Cr	acked	Edge	Distances	= c <sub>ac</sub> on all s	ides	Edge	Distances =	= 1¾" on one three sides	e side
(in.)	Depth (in.)	(ir	1.)	(ii	1.)	SDC		SDC (		SDC	A-B <sup>6</sup>	SDC	C-F <sup>7,8</sup>
		ha	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	2%	4 1/4 5 3/4	4 <sup>3</sup> / <sub>4</sub> 4 <sup>1</sup> / <sub>4</sub>	_		2,140	_	1,605		1,115		935	_
	3	47/8 71/4	63/8 45/8	47/8	41/4	2,700	2,110	2,025	1,580	1,050 1,450	1,230	835 935 790 1,090	925
3/8	41/2	63/8 107/8	101/4 67/8	6%	51/4	4,055	3,165	3,040	2,375	975 1,450	1,845	1.090	1,385
	6	77/8 141/2	141/8 91/4	77/8	6	5,405	4,220	4,055	3,165	1,115 1,250 1,050 1,450 975 1,450 945 1,450	2,250	1.090	1,685
	71/2	9% 18	18 111/2	9%	6¾	6,755	5,275	5,065	3,955	925 1 450	2,585	695	1,935
	23/4	51/4 65/8	61/8 61/8	_	_	3,555	_	2,410	_	1,720 1,920	_	1,225 1,225	_
	3	5½ 7¼	61/8 61/8	5½	61/8	4,055	2,680	2,625	1,710	1,720 1,920 1,800 2,095	1,365	1,225 1,225 1,335 1,335	870
1/2	6	8½ 14½	14% 9%	81/2	7	8,240	5,365	5,255	3,420	1,755 2.605	2,700	1,120	1,740
	8	10½ 19¼ 12½ 24	14% 9¾ 19% 13	10½	81/2	10,990	7,155	7,005	4,560	1,755 2,605 1,695 2,605 1,665 2,605 2,180 2,405 2,965 4,095 2,780	3,425	1,000 1,080 1,660 1,060 1,660	2,320
	10	12½ 24	25¼ 16⅓	12½	93/4	13,735	8,940	8,755	5,700	1,665 2,605	4,070	1,060 1,660	2,895
	31/8	6½ 7½	77/8 77/8	61/4	7%	4,310	3,050	3,230	1,995	2,180 2,405	1,485	1,635 1,735 2,065 2,770 1,770	950
5/8	5	81/8 12	10½ 7%	81/8	77/8	8,720	5,285	5,905	3,370	2,965 4,095	2,485	2,065 2,770	1,585
78	71/2	105% 18 155%	1 2 3 %	10%	91/8	13,890	7,935	8,855	5,060	2,780 4,130	3,705	2.630	2,375
	12½	15% 30	32% 20%	15%	12½	23,150	13,230	14,760	8,435	2,610 4,090	5,620	1,665 2,605	3,960
	31/2	71/ <sub>4</sub> 81/ <sub>2</sub>	123/8 325/8 207/8 95/8 95/8	71/4	87/8	5,105	3,620	3,830	2,340	2,680 2,725	1,695	2,010 2,045	1,080
3/4	6	30 71/4 81/2 93/4 141/2 123/4 215/8 183/4	121/8 95/8	93/4	95/8	11,465	7,380	8,600	4,705	4,130 2,610 4,090 2,680 2,725 3,855 5,190 4,145 6,155 3,705 5,800 2,945 4,840 6,320 5,540 8,225 4,820 7,555 3,175 3,175 5,915 7,520 5,480 8,135	3,300	1,665 2,605 2,010 2,045 2,890 3,895 2,640 3,925 2,360	2,105
/4	9	12¾ 21%	95% 211/4 143/8 395/8 251/4 111/8	12¾	111⁄4	20,645	11,080	13,160	7,065	4,145 6,155	4,895	2,640 3,925	3,160
	15	18¾ 36 8⅓	39% 25¼	18¾	15¾	34,405	18,465	21,935	11,775	3,705 5,800	7,660	2,360 3,700	5,265
	3¾	9	11 1/8	81/8	10½	5,665	4,010	4,250	1,825	2,945 2,945	1,825	3,700 1,900 1,900 2,855	805
7/8	7	113/8 167/8 147/8	13¾ 11⅓ 24	11%	111/8	14,445	8,625	8,195	3,815	4,840 6,320	3,735	2,855 3,550	1,655
78	101/2	251/4	161/4	147/8	12½	26,540	12,940	12,295	5,725	5,540 8,225	5,605	3,550 2,450 3,640	2,480
	17½	217/8 42 9	46 29%	21 1/8	17½	46,300	21,565	20,490	9,540	4,820 7,555	8,840	2,135 3,345 2,380	4,130
	4	95%	46 29% 12% 12% 15% 15% 26% 18	9	12%	6,240	4,420	4,680	2,885	3,175 3,175	1,920	2,380 2,380	1,225
1	8	13 19¼ 17	15% 12%	13	12%	17,650	9,050	11,935	5,770	5,915 7,520	3,840	2,380 4,070 5,065	2,450
1	12	287/8	26¾ 18	17	12¾	28,075	13,570	17,900	8,650	5,480 8,135	5,760	3,495 5.185	3,670
	20	25 48	513/8 323/4 133/8 133/8	25	181⁄4	46,795	22,620	29,830	14,420	4,750 7,440	9,365	3,025 4,745	6,120
	5	11½ 12	13% 13%	111/4	13%	8,720	6,175	6,215	3,480	_	_	_	_
1 1/4	10	161/4	18¼ 15	161/4	13%	22,090	12,370	12,425	6,960	_	_	_	_
1 74	15	24 211/4 36	18¼ 15 32 22½	21 1/4	15¾	33,135	18,555	18,640	10,435	_	_	_	_
	25	31½ 60	57 <sup>3</sup> / <sub>8</sub> 37 <sup>1</sup> / <sub>2</sub>	31 1/4	22	55,225	30,925	31,065	17,395	_	_	_	_

Threaded Rod	Tension Design Strength of Threaded Rod Steel (lb.)									
Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M				
3/8	3,370	4,360	7,270	6,395	7,270	3,310				
1/2	6,175	7,990	13,315	11,715	13,315	6,070				
5/8	9,835	12,715	21,190	18,645	21,190	9,660				
3/4	14,530	18,790	31,315	27,555	31,315	14,280				
7/8	20,095	25,990	43,315	38,115	43,315	19,750				
1	26,365	34,090	56,815	49,995	56,815	25,905				
11/4	42.150	54.505	90.845	79.945	90.845	41.425				

- Tension design strength must be the lesser of the concrete, bond or threaded rod steel design strength.
- 2. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 180°F and long-term temperature of 110°F.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- \* See page 12 for an explanation of the load table icons.

- 6. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 7. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3. Design strengths in **Bold** indicate that the anchor ductility requirements of D.3.3.4.3 (a)1 to 3 are satisfied when using ASTM F1554 Grade 36 threaded rod. Any other ductility requirements must be satisfied.
- 8. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

### Design Information — Concrete



AT-XP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete  $(f'_{C} = 2,500 \text{ psi})$  — Static Load

IRC
-----

20		
<b>5</b> 6	200 200	

	Naminal Embad	Minimum Dimensions for			mensions for	Allowable T	ension Load Base		<del> </del>
Rod Dia. (in.)	Nominal Embed. Depth (in.)		acked n.)		cked n.)	Edge distances :	= c <sub>ac</sub> on all sides	Edge Distances side and c <sub>ac</sub> o	
	(,	h <sub>a</sub>	c <sub>ac</sub>	h <sub>a</sub>	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked
	23/8	4 ½ 5¾	43/ <sub>4</sub> 41/ <sub>4</sub>	_	_	1,530	_	795 895	_
	3	47/8 71/4	63/8 45/8	47/8	41/4	1,930	1,505	750 1,035	880
3/8	41/2	6% 10%	101/4 67/8	6%	51/4	2,895	2,260	695 1.035	1,320
	6	7% 14½	141/8 91/4	77/8	6	3,860	3,015	675 1,035	1,605
	71/2	9% 18	18 11½	9%	6¾	4,825	3,770	660 1.035	1,845
	23/4	51/4 65/8	61/8 61/8	_	_	2,540	_	1,230 1,370	_
	3	5½ 7¼	6 1/8 6 1/8	5½	61/8	2,895	1,915	1,285 1,495	975
1/2	6	8½ 14½	14% 9%	8½	7	5,885	3,830	1,255 1,860	1,930
	8	10½ 19¼	19% 13	10½	81/2	7,850	5,110	1,210 1,860	2,445
	10	12½ 24	25¼ 16⅓	12½	9¾	9,810	6,385	1,190 1,860	2,905
	31/8	6½ 7½	77/ <sub>8</sub> 77/ <sub>8</sub>	61/4	75/8	3,080	2,180	1,555 1,720	1,060
5/8	5	81/8 12	10½ 7%	81/8	77/8	6,230	3,775	2,120 2,925	1,775
/8	71/2	10% 18	18% 12%	10%	91/8	9,920	5,670	1,985 2,950	2,645
	12½	15% 30	32% 20%	15%	12½	16,535	9,450	1,865 2,920	4,015
	31/2	71/ <sub>4</sub> 81/ <sub>2</sub>	95% 95%	71/4	87/8	3,645	2,585	1,915 1,945	1,210
3/4	6	9¾ 14½	121/8 95/8	93⁄4	95/8	8,190	5,270	2,755 3,705	2,355
/4	9	12¾ 21¾	211/ <sub>4</sub> 143/ <sub>8</sub>	12¾	111/4	14,745	7,915	3,705 2,960 4,395	3,495
	15	18¾ 36	39% 25¼	18¾	15¾	24,575	13,190	2,645 4,145	5,470
	3¾	81/8 9	111/8 111/8	81/8	10½	4,045	2,865	2,105 2,105	1,305
7/8	7	11% 16%	13¾ 11⅓	11%	111/8	10,320	6,160	3,455 4,515	2,670
70	101/2	14% 25¼	24 161/4	147/8	12½	18,955	9,245	3,955 5,875	4,005
	17½	21% 42	46 29%	21%	17½	33,070	15,405	3,445 5,395	6,315
	4	9 9%	12% 12%	9	12%	4,455	3,155	2,270 2,270	1,370
1	8	13 19½	15% 12%	13	12%	12,605	6,465	4,225 5,370	2,745
,	12	17 28%	26¾ 18	17	12¾	20,055	9,695	3,915 5,810	4,115
	20	25 48	51% 32%	25	181⁄4	33,425	16,155	3,395 5,315	6,690
	5	111/4	13% 13%	111/4	13%	6,230	4,410	_	_
1 1/4	10	16¼ 24	18¼ 15	161⁄4	13%	15,780	8,835	_	_
1 /4	15	21¼ 36	32 22½	211/4	15¾	23,670	13,255	_	_
	25	31 ½ 60	57% 37½	311/4	22	39,445	22,090	_	_

Threaded Rod	Allowable Tension Load of Threaded Rod Steel (lb.)										
Dia. ASTM F1554 (in.) GR 36		ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M					
3/8	2,405	3,115	5,195	4,570	5,195	2,365	1				
1/2	4,410	5,705	9,510	8,370	9,510	4,335					
5/8	7,025	9,080	15,135	13,320	15,135	6,900					
3/4	10,380	13,420	22,370	19,680	22,370	10,200					
7/8	14,355	18,565	30,940	27,225	30,940	14,105					
1	18,830	24,350	40,580	35,710	40,580	18,505					
1 1/4	30,105	38,930	64,890	57,105	64,890	29,590	1				

<sup>\*</sup> See page 12 for an explanation of the load table icons.

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or threaded rod steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 180°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = 1.4$ . The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.



AT-XP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete ( $f_C' = 2,500~psi$ ) — Wind Load







$I_{C} = 2,500$		. Minimum Dimensions for		Minimum Di	mensions for	Allowable Te	ension Load Ba	sed on Concrete	or Bond (lb.)		
Rod Dia. (in.)	Nominal Embed. Depth (in.)	Uncracked (in.)		Cra	cked n.)		es = c <sub>ac</sub> on all les	Edge Distances side and cac o	= 1¾" on one		
	("".)	ha	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked		
	23/8	4 1/4 5 3/4	43/ <sub>4</sub> 41/ <sub>4</sub>	_	_	1,285	_	670 750	_		
	3	47/8 71/4	63/8 45/8	47/8	41/4	1,620	1,265	630 870	740		
3/8	41/2	6% 10%	101/4 67/8	6%	51/4	2,435	1,900	585 870	1,105		
	6	71/8 141/2	141/8 91/4	77/8	6	3,245	2,530	565 870	1,350		
	7½	9% 18	18 11½	9%	6¾	4,055	3,165	555 870	1,550		
	2¾	51/4 65/8	61/8 61/8	_	_	2,135	_	1,030 1,150	_		
	3	5½ 7¼	61/8 61/8	5½	61/8	2,435	1,610	1,080 1,255	820		
1/2	6	8½ 14½	14% 9%	81/2	7	4,945	3,220	1,055 1,565	1,620		
	8	10½ 19¼	19% 13	10½	81/2	6,595	4,295	1,015 1,565	2,055		
	10	12½ 24	25¼ 16%	12½	9¾	8,240	5,365	1,000 1,565	2,440		
	31/8	61/4 71/2	77/8 77/8	61/4	7%	2,585	1,830	1,310 1,445	890		
5/8	5	81/8 12	10½ 7%	81/8	77/8	5,230	3,170	1,780 2,455	1,490		
	7½	10% 18	18% 12%	10%	91/8	8,335	4,760	1,670 2,480	2,225		
	12½	15% 30	325/8 207/8 95/8	15%	12½	13,890	7,940	1,565 2,455 1,610	3,370		
	3½	71/4 81/2 93/4	9 <sup>5</sup> / <sub>8</sub> 12 <sup>1</sup> / <sub>8</sub>	71/4	87/8	3,065	2,170	1,635 2,315	1,015		
3/4	6	14½ 12¾	95/8 21 1/4	93/4	95/8	6,880	4,430	3,115 2,485	1,980		
	9	21 5/8 18 3/4	14% 39%	12¾	111/4	12,385	6,650	3,695 2,225	2,935		
	15	36 81/8	25 ½ 11 ½	18¾	15¾	20,645	11,080	3,480 1,765	4,595		
	3¾	9 11%	11 1/8 11 1/8 13 3/4	81/8	10½	3,400	2,405	1,765 1,765 2,905	1,095		
7/8	7	167/8 147/8	111/8	11%	111/8	8,665	5,175	3,790 3,325	2,240		
	10½	25½ 21%	16½ 46	147/8	12½	15,925	7,765	4.935	3,365		
	17½	42	29% 12%	21%	17½	27,780	12,940	2,890 4,535 1,905	5,305		
	4	95% 13	12% 15%	9	12%	3,745	2,650	1,905 3,550	1,150		
1	8	19¼ 17	12% 26¾	13	12%	10,590	5,430	4,510 3,290	2,305		
	12	287/s 25	18 51%	17	12¾	16,845	8,140	4,880 2.850	3,455		
	20	48 11 1⁄4	32¾ 13%	25	181/4	28,075	13,570	4,465	5,620		
	5	12 161⁄4	13% 18¼	111/4	13%	5,230	3,705	_	_		
1 1/4	10	24 21 1/4	15 32	161/4	13%	13,255	7,420	_	_		
	15	36 31 1/4	22½ 57¾	211/4	15¾	19,880	11,135	_	_		
	25	60	37 1/2	31 1/4	22	33,135	18,555	_	_		

Threaded Rod	Allowable Tension Load of Threaded Rod Steel (lb.)									
Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M	2			
3/8	2,020	2,615	4,360	3,835	4,360	1,985	7			
1/2	3,705	4,795	7,990	7,030	7,990	3,640				
5/8	5,900	7,630	12,715	11,185	12,715	5,795				
3/4	8,720	11,275	18,790	16,535	18,790	8,570				
7/8	12,055	15,595	25,990	22,870	25,990	11,850	3			
1	15,820	20,455	34,090	29,995	34,090	15,545	3			
1 1/4	25,290	32,705	54,505	47,965	54,505	24,855	4			

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or threaded rod steel load.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 180°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = \frac{1}{6.6} = 1.67$ . The conversion factor  $\alpha$  is bazsed on the load combination assuming 100% wind load.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

### Design Information — Concrete



AT-XP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete  $(f'_C = 2,500 \text{ psi})$  — Seismic Load

_		_
[]	lí	4
IRC:	ш	
IDU	li	350

(. C = , o	Embad			Minir	imum Allowable Tension Load Based on Concrete or Bond (lb.)								
Nom. Insert Dia.	Embed. Depth,	Minimum for Uncr	Dimensions acked (in.)	Dimensi	ons for	Edg	Edge Distances = $c_{ac}$ on all sides			Edge Distances = $1\frac{3}{4}$ " on one side and $c_{ac}$ on three sides			
(in.)	h <sub>ef</sub>	llef   Glo		Cracke	d (in.)	SDC		SDC		SDC	A-B <sup>5</sup>	SDC (	C-F <sup>6,7</sup>
	(111.)	ha	Cac	h <sub>a</sub>	Cac	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	2%	4 ½ 5¾	43/ <sub>4</sub> 41/ <sub>4</sub>	_	_	1,500	_	1,125	_	780 875	_	585 655	_
	3	47/8 71/4	63/8 45/8	47/8	41/4	1,890	1,475	1,420	1,105	735 1,015	860	555 765	650
3/8	41/2	7 ½ 63/8 107/8	10½ 6%	6%	51/4	2,840	2,215	2,130	1,665	685 1 015	1,290	515 765	970
	6	7 1/8 14 1/2	141/8 91/4 18	77/8	6	3,785	2,955	2,840	2,215	1,015	1,575	495 765	1,180
	7½	9% 18	11½	9%	6¾	4,730	3,695	3,545	2,770	650 1 015	1,810	485 765	1,355
	2¾	5½ 65%	61/8 61/8	_	_	2,490	_	1,685	_	1,205 1,345 1,260	_	860 860 935 935	_
	3	5½ 7¼ 8½	61/8 61/8	5½	61/8	2,840	1,875	1,840	1,195	1,260 1,465	955	935 935	610
1/2	6	141/2	143%	81/2	7	5,770	3,755	3,680	2,395	1,465 1,230 1,825 1,185 1,825 1,165 1,825 1,525 1,685 2,075 2,865	1,890	785 1.160	1,220
	8	10½ 19¼ 12½	9¾ 19⅙ 13	10½	81/2	7,695	5,010	4,905	3,190	1,185 1,825	2,400	755 1,160 740 1,160 1,145 1,215 1,445 1,940	1,625
	10	24	161/8	12½	9¾	9,615	6,260	6,130	3,990	1,165 1,825	2,850	740 1,160	2,025
	31/8	6½ 7½	7	61/4	7%	3,015	2,135	2,260	1,395	1,525 1,685	1,040	1,145 1,215	665
5/8	5	7½ 8½ 12	/ 1/8	81/8	77/8	6,105	3,700	4,135	2,360	2,075 2,865	1,740	1,445 1,940	1,110
78	71/2	10% 18	18% 12%	10%	91/8	9,725	5,555	6,200	3,540	1,945 2,890	2,595	1,240 1,840	1,665
	12½	15% 30	32% 20%	15%	12½	16,205	9,260	10,330	5,905	1,825 2,865	3,935	1,165 1,825	2,770
	31/2	7 1/4 8 1/2 9 3/4	95/8 95/8	71/4	8%	3,575	2,535	2,680	1,640	1,8/5	1,185	1,405 1,430	755
3/4	6	141/2	121/8	9¾	9%	8,025	5,165	6,020	3,295	2,700 3,635	2,310	2,025 2,725	1,475
/4	9	12 <sup>3</sup> ⁄ <sub>4</sub> 21 <sup>5</sup> ⁄ <sub>8</sub>	211/4 143/8	12¾	111/4	14,450	7,755	9,210	4,945	2,700 3,635 2,900 4,310	3,425	1,850 2,750	2,210
	15	18¾ 36	39% 251/4	18¾	15¾	24,085	12,925	15,355	8,245	2,595 4,060 2,060 2,060	5,360	1,650 2,590	3,685
	3¾	8 1/8 9	111/8	81/8	10½	3,965	2,805	2,975	1,280	2,060 2,060	1,280	1,165 1,825 1,405 1,430 2,025 2,725 1,850 2,750 1,650 2,590 1,330 1,330 2,000 2,485 1,715 2,550 1,495 2,340	565
7/8	7	11% 16%	13¾ 11⅓ 24	11%	111/8	10,110	6,040	5,735	2,670	3,390 4,425	2,615	2,000 2,485	1,160
/6	10½	147/8 251/4	161/4	147/8	12½	18,580	9,060	8,605	4,010	4,425 3,880 5,760	3,925	1,715 2,550	1,735
	17½	25½ 21½ 42	46 29% 12% 12%	21%	17½	32,410	15,095	14,345	6,680	3,375 5,290 2,225 2,225	6,190	1,495 2,340	2,890
	4	9 95%	12% 12%	9	12%	4,370	3,095	3,275	2,020	2,225 2,225	1,345	1,665 1,665	860
1	8	13 19¼ 17	15% 12%	13	12%	12,355	6,335	8,355	4,040	4,140 5,265	2,690	2,850 3,545	1,715
'	12	287/8	26¾ 18	17	12¾	19,655	9,500	12,530	6,055	3,835 5,695	4,030	2,445 3,630	2,570
	20	25 48	15% 12% 26% 18 51% 32%	25	181⁄4	32,755	15,835	20,880	10,095	3,325 5,210	6,555	2,340 1,665 1,665 2,850 3,545 2,445 3,630 2,120 3,320	4,285
	5	111/4	13%	111⁄4	13%	6,105	4,325	4,350	2,435	_	_	_	_
11/4	10	16¼ 24	18¼ 15	161⁄4	13%	15,465	8,660	8,700	4,870	_		_	_
1 /4	15	211/4	32 22½	211/4	15¾	23,195	12,990	13,050	7,305	_	_	_	_
	25	31 ½ 60	22½ 57¾ 37½	31 1/4	22	38,660	21,650	21,745	12,175	_	_	_	_

Threaded Rod Dia.	Allowable Tension Load of Threaded Rod Steel (lb.)										
(in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M					
3/8	2,360	3,050	5,090	4,475	5,090	2,315					
1/2	4,325	5,595	9,320	8,200	9,320	4,250					
5/8	6,885	8,900	14,835	13,050	14,835	6,760					
3/4	10,170	13,155	21,920	19,290	21,920	9,995					
7/8	14,065	18,195	30,320	26,680	30,320	13,825					
1	18,455	23,865	39,770	34,995	39,770	18,135					
1 1/4	29,505	38.155	63.590	55.960	63.590	29,000					

- 1. Allowable tension load must be the lesser of the concrete, bond or threaded rod
- 2. Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, shortterm temperature of 180°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = \%.7 = 1.43$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- \* See page 12 for an explanation of the load table icons.

- 5. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3. Design strengths in Bold indicate that the anchor ductility requirements of D.3.3.4.3 (a)1 to 3 are satisfied when using ASTM F1554 Grade 36 threaded rod. Any other ductility requirements must be satisfied.
- 7. Allowable tension loads in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.



AT-XP® Tension Design Strengths for Rebar in Normal-Weight Concrete (f'c = 2,500 psi)

	•	្តា	$\sim$
3C:		·	
-	580 582	of The	1000

								ension Design		sed on Concre	ete or Bond (				
Rebar	Nominal Embed.		Dimensions acked (in.)	Dimen	imum sions for	Edg	e Distances	= c <sub>ac</sub> on all si	des	Edge Dista		' on one side a	ınd c <sub>ac</sub> on		
Size	Depth (in.)	TOT OTICIE	ionou (III.)	Crack	ked (in.)	SDC	A-B <sup>6</sup>	SDC	C-F <sup>7,8</sup>	SDC		SDC (	C-F <sup>7,8</sup>		
	()	h <sub>a</sub>	c <sub>ac</sub>	ha	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked		
	2%	4 1/4 5 3/4	4 1/4 3 5/8	_	_	1,555	_	1,165	_	845 980	_	635 735	_		
	3	47/8 71/4	5 % 4 ½	47/8	35/8	1,965	660	1,470	495	795 1,100	415	600 825	310		
#3	41/2	6% 10%	9 6¾	6%	3%	2,945	990	2,210	745	740 1,100	625	555 825	470		
	6	7 1/8 14 1/2	12½ 9	71/8	3%	3,925	1,320	2,945	990	715 1,100	830	540 825	625		
	7½	9% 18	157/8 111/4	9%	3%	4,910	1,650	3,680	1,240	705	1,040	525	780		
	23/4	51/4 65/8	43/ <sub>4</sub> 43/ <sub>4</sub>	_	_	2,350	_	1,765	_	1,100 1,305 1,305	_	825 980 980	_		
	3	5½ 7¼	5 ½ 4¾	5½	43/4	2,565	1,995	1,925	1,495	1,320 1,425	1,105	990 1,070	830		
#4	6	8½ 14½	117/8	81/2	5%	5,130	3,990	3,850	2,995	1,140 1,690	2,085	855 1,265	1,565		
	8	10½ 19¼	16½ 12	10½	67/8	6,840	5,320	5,130	3,990	1,100 1,690	2,640	825 1,265	1,980		
	10	12½	21	121/2	8	8,555	6,650	6,415	4,990	1,080 1,690	3,175	810 1,265	2,380		
	31/8	6½ 7½	57/8 57/8	61/4	5%	3,275	2,630	2,455	1,975	1,675 1,675	1,350	1,260 1,260	1,010		
	5	8 1/8 12	9½ 7½	81/8	57/8	5,240	4,210	3,930	3,160	1,725 2,385	2,160	1,295 1,785	1,620		
#5	7½	10% 18	14 <sup>3</sup> ⁄ <sub>4</sub> 11 <sup>1</sup> ⁄ <sub>4</sub>	10%	75/8	7,855	6,320	5,890	4,740	1,605 2,385	2,995	1,205 1,785	2,245		
	121/2	15% 30	26 18¾	15%	10¾	13,095	10,530	9,820	7,895	1,520 2,385	4,615	1,140 1,785	3,460		
	3½	7 ½ 8½	7	71/4	7	4,330	3,585	3,250	2,685	2,100 2,100	1,735	1,575 1,575	1,300		
110	6	9¾ 14½	11 9	9¾	7½	7,425	6,145	5,570	4,605	2,310 3,190	2,935	1,730 2,395	2,200		
#6	9	12¾ 21%	17% 13½	12¾	97/8	11,140	9,215	8,355	6,910	2,150 3,190	4,135	1,610 2.395	3,105		
	15	18¾ 36	31 22½	18¾	13%	18,565	15,355	13,925	11,515	2,035 3,190	6,455	1,525 2,395	4,845		
	3¾	81/8 9	8 1/8 8 1/8	81/8	73/4	5,300	4,010	3,975	3,010	2,470 2,470	1,950	1,850 1.850	1,465		
#7	7	11% 16%	12% 10½	11%	91/4	9,895	8,415	7,420	6,310	2,950 4,075	3,805	2,210 3,055	2,855		
#1	101/2	14% 25¼	203/8 153/4	141/8	121/8	14,845	12,620	11,130	9,465	2,745 4,075	5,400	2,060 3,055 1,950 3,055	4,050		
	171⁄2	21% 42	35¾ 26¼	21%	17	24,740	21,035	18,555	15,775	2,600 4,075	8,495	1,950 3,055	6,370		
	4	9 9%	91/8 91/8	9	91/8	5,175	4,420	3,880	3,315	2,335 2,335	2,030	1,750 1,750	1,520		
#8	8	13 19¼	14% 12	13	9¾	10,350	8,990	7,760	6,745	2,985 4,125	4,060	2,240 3.095	3,045		
πο	12	17 28%	231/s 18	17	12%	15,525	13,485	11,640	10,115	2,780 4,125	5,695	2,085 3,095	4,270		
	20	25 48	40½ 30	25	17¾	25,870	22,480	19,405	16,860	2,630 4,125	9,015	1,975 3,095	6,760		
	5	11¼ 12	111/ <sub>4</sub> 111/ <sub>4</sub>	111/4	10½	7,730	6,175	5,800	4,635	_	_	_	_		
#10	10	16¼ 24	17% 15	161⁄4	131⁄4	15,465	14,490	11,595	10,870	_	_	_	_		
π10	15	21¼ 36	28% 22½	211/4	17%	23,195	21,735	17,395	16,300	_	_	_	_		
	25	31 ½ 60	49¾ 37½	311/4	241/2	38,655	36,225	28,990	27,170	_	_	_	_		

	Tension Design Strength of Rebar Steel (lb.)								
Rebar Size	ASTM A615 GR 60	ASTM A706 GR 60							
#3	6,435	5,720							
#4	11,700	10,400							
#5	18,135	16,120							
#6	25,740	22,880							
#7	35,100	31,200							
#8	46,215	41,080							
#10	74,100	66,040							

<sup>\*</sup> See page 12 for an explanation of the load table icons.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

- 1. Tension design strength must be the lesser of the concrete, bond or rebar steel design strength.
- Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 180°F and long-term temperature of 110°F.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 6. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 7. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 8. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

### **AT-XP®** Design Information — Concrete



AT-XP® Allowable Tension Loads for Rebar in Normal-Weight Concrete (f'  $_{\rm C}=2,\!500$  psi) — Static Load









					Allowable Tension Load Based on Concrete or		rete or Bond (lb.)		
Rebar Size	Nominal Embed. Depth (in.)		mensions for ked (in.)		imensions for ed (in.)	Edge Distance sid	es = c <sub>ac</sub> on all les		es = $1\frac{\%}{0}$ on one side on three sides
		h <sub>a</sub>	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked
	2%	41⁄4 53⁄4	41/ <sub>4</sub> 35/ <sub>8</sub>	_	_	1,110	_	605 700	_
	3	47/8 71/4	5% 4½	47/8	35/8	1,405	470	570 785	295
#3	41/2	6% 10%	9 6¾	6%	35/8	2,105	705	530 785	445
	6	7% 14½	12½ 9	77/8	3%	2,805	945	510 785	595
	7½	9% 18	15% 11¼	9%	35/8	3,505	1,180	505 785	745
	2¾	51/4 65/8	43/4	_	_	1,680	_	930 930	_
	3	5½ 7¼	51/8 43/4	5½	43/4	1,830	1,425	945 1,020	790
#4	6	8½ 14½	11%	8½	55/8	3,665	2,850	815 1,205	1,490
	8	10½ 19¼	16½ 12	10½	67/8	4,885	3,800	785 1,205	1,885
	10	12½ 24	21 15	12½	8	6,110	4,750	770 1,205	2,270
	31/8	61/4 71/2	57/8 57/8	61/4	57/8	2,340	1,880	1,195 1,195	965
#5	5	81/8 12	91/4	81/8	57/8	3,745	3,005	1,230 1,705	1,545
	71/2	10% 18	143/4	10%	7%	5,610	4,515	1,145 1,705	2,140
	12½	15% 30	26 18¾	15%	10¾	9,355	7,520	1,085 1,705 1,500	3,295
	3½	7 1/4 8 1/2 9 3/4	7 7 11	71/4	7	3,095	2,560	1,500 1,500 1,650	1,240
#6	6	141/2	9	9¾	71/2	5,305	4,390	2.280	2,095
	9	12¾ 21⅓ 10¾	17% 13½ 31	12¾	9%	7,955	6,580	1,535 2,280 1,455	2,955
	15	18¾ 36 8⅓	22½ 8½	18¾	13%	13,260	10,970	2,280 1,765	4,610
	3¾	9 11%	81/8 125/8	81/8	73/4	3,785	2,865	1,765 2,105	1,395
#7	7	167/8 147/8	10½ 20%	113/8	91/4	7,070	6,010	2,103 2,910 1,960	2,720
	101/2	25½ 21%	15 <sup>3</sup> / <sub>4</sub> 35 <sup>3</sup> / <sub>4</sub>	147/8	121/8	10,605	9,015	2,910 1,855	3,855
	17½	42	261/4 91/8	217/8	17	17,670	15,025	2,910 1,670	6,070
	4	9% 13	91/8 143/8	9	91/8	3,695	3,155	1,670 2,130	1,450
#8	8	19¼ 17	12 231/8	13	9¾	7,395	6,420	2,130 2,945 1,985	2,900
	12	28% 25	18 40½	17	12%	11,090	9,630	2,945 1,880	4,070
	20	48 111/4	30 111/4	25	17¾	18,480	16,055	2,945	6,440
	5	12	111/4	111/4	10½	5,520	4,410	_	_
#10	10	16¼ 24	17% 15	161/4	131/4	11,045	10,350	_	_
	15	21 1/4 36	28% 22½	21 1/4	17%	16,570	15,525	_	_
	25	31 ½ 60	49¾ 37½	31 1/4	241/2	27,610	25,875	_	_

	Allowable Tension Load of Rebar Steel (lb.)						
Rebar Size	ASTM A615 GR 60	ASTM A706 GR 60					
#3	4,595	4,085	]				
#4	8,355	7,430					
#5	12,955	11,515					
#6	18,385	16,345					
#7	25,070	22,285					
#8	33,010	29,345	1				
#10	52.930	47.170	1				

Allowable tension load must be the lesser of the concrete, bond or rebar steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 180°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



AT-XP® Allowable Tension Loads for Rebar in Normal-Weight Concrete  $(f'_C = 2.500 \text{ psi})$  — Wind Load









' <sub>C</sub> = 2,500 psi) — Wind			monoion <del>e for</del>	Minimum Di	imanajan <del>a far</del>	Allowable Tension Load Based on Concrete or Bond (lb.)					
Rebar Size	Nominal Embed. Depth (in.)		mensions for ked (in.)		imensions for ed (in.)	Edge Distan	ces = c <sub>ac</sub> on ides	Edge Distances side and c <sub>ac</sub> o	= 1¾" on one n three sides		
	(,	ha	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked		
	23/8	4 1/4 5 3/4	41/ <sub>4</sub> 35/ <sub>8</sub>	_	_	935	_	505 590	_		
	3	4 <sup>7</sup> / <sub>8</sub> 7 <sup>1</sup> / <sub>4</sub>	55/8 41/2	47/8	35/8	1,180	395	475 660	250		
#3	41/2	6%	9	63/8	35%	1,765	595	445	375		
	6	10% 7%	6¾ 12½	77/8	35/8	2,355	790	660 430	500		
	71/2	14½ 9%	9 15%	93/8	35/8	2,945	990	660 425	625		
	23/4	18 5¼	11 ½ 4¾			1,410	_	660 785			
		6% 5½	4¾ 5⅓		42/			785 790			
	3	7 ½ 8 ½	4 <sup>3</sup> / <sub>4</sub> 11 <sup>7</sup> / <sub>8</sub>	5½	43/4	1,540	1,195	855 685	665		
#4	6	141/2	9	8½	5%	3,080	2,395	1,015 660	1,250		
	8	10½ 19¼	16½ 12	10½	67/8	4,105	3,190	1,015	1,585		
	10	12½ 24	21 15	12½	8	5,135	3,990	650 1,015	1,905		
#5	31/8	6 1/4 7 1/2	57/8 57/8	61/4	57/8	1,965	1,580	1,005 1,005	810		
	5	81/8 12	9½ 7½	81/8	57/8	3,145	2,525	1,035 1,430	1,295		
	7½	10% 18	14¾ 11¼	10%	7%	4,715	3,790	965 1,430	1,795		
	121/2	15% 30	26 18¾	15%	10¾	7,855	6,320	910 1,430	2,770		
	3½	7½ 8½	7	71/4	7	2,600	2,150	1,260 1,260	1,040		
	6	9¾ 14½	11 9	93/4	71/2	4,455	3,685	1,385 1,915	1,760		
#6	9	12¾	17%	123/4	97/8	6,685	5,530	1,290	2,480		
	15	21% 18¾	13½ 31	18¾	137/8	11,140	9,215	1,915 1,220	3,875		
	3¾	36 8½	22½ 81/8	81/8	73/4	3,180	2,405	1,915 1,480	1,170		
	7	9 11%	81/8 125/8	11%	91/4	5,935	5,050	1,480 1,770	2,285		
#7	10½	167/8 147/8	10½ 20%	147/8	121/8	8,905	7,570	2,445 1,645	3,240		
		25½ 21%	15¾ 35¾					2,445 1,560			
	17½	42 9	261/4 91/8	21%	17	14,845	12,620	2,445 1,400	5,095		
	4	9% 13	91/8 143/8	9	91/8	3,105	2,650	1,400 1,790	1,220		
#8	8	19¼ 17	12 231/8	13	9¾	6,210	5,395	2,475 1,670	2,435		
	12	287/8	18	17	12%	9,315	8,090	2,475	3,415		
	20	25 48	40½ 30	25	17¾	15,520	13,490	1,580 2,475	5,410		
	5	11¼ 12	11 ½ 11 ½	111/4	101/2	4,640	3,705	_	_		
#10	10	16¼ 24	17% 15	161⁄4	131/4	9,280	8,695	_	_		
#10	15	21 ¼ 36	28% 22½	211/4	17%	13,915	13,040	_	_		
	25	31 ½ 60	49¾ 37½	311/4	241/2	23,195	21,735	_	_		

	Allowable Tension Lo	ad of Rebar Steel (lb.)
Rebar Size	ASTM A615 GR 60	ASTM A706 GR 60
#3	3,860	3,430
#4	7,020	6,240
#5	10,880	9,670
#6	15,445	13,730
#7	21,060	18,720
#8	27,730	24,650
#10	44,460	39,625

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or rebar steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 180°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

#### **AT-XP®** Design Information — Concrete



AT-XP® Allowable Tension Loads for Rebar in Normal-Weight Concrete ( $f'_{\rm C}=2,500~{\rm psi}$ ) — Seismic Load

ĺ	IDC	
	IRC	







	No series al	Minimum Dim	oncione for	Minimum		Allowable Tension Load Based on Concrete or Bond (lb.)  Edge Distances = 134" on one side and c <sub>ac</sub> on							
Rebar Size	Nominal Embed.	Uncracked (in.)		Dimensions for Cracked		Edge Distances = c <sub>ac</sub> on all sides			Edge Distand	es = 1¾" o three s		nd c <sub>ac</sub> on	
	Depth (in.)			(in.	:	SDC			C-F <sup>6,7</sup>	SDC A	-B⁵	SDC (	C-F <sup>6,7</sup>
	(,	h <sub>a</sub>	c <sub>ac</sub>	ha	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	23/8	4 ½ 5¾	41/ <sub>4</sub> 35/ <sub>8</sub>		_	1,090	_	815	_	590 685	_	445 515	_
	3	4 <sup>7</sup> / <sub>8</sub> 7 <sup>1</sup> / <sub>4</sub>	55/8 41/2	47/8	35/8	1,375	460	1,030	345	555 770	290	420 580	215
#3	41/2	6% 10%	9 6¾	6%	35/8	2,060	695	1,545	520	520 770	440	390 580	330
	6	77/8 141/2	12½ 9	77/8	3%	2,750	925	2,060	695	500 770	580	380 580	440
	71/2	9% 18	157/8 111/4	9%	35/8	3,435	1,155	2,575	870	495 770	730	370 580	545
	2¾	5 1/4 65/8	43/ <sub>4</sub> 43/ <sub>4</sub>	_	_	1,645	_	1,235	_	915 915	_	685 685	_
	3	5½ 7¼	5 1/8 4 3/4	5½	43/4	1,795	1,395	1,350	1,045	925 1,000	775	695 750	580
#4	6	8½ 14½	11%	8½	5%	3,590	2,795	2,695	2,095	800 1,185	1,460	600 885	1,095
	8	10½ 19¼	16½ 12	10½	6%	4,790	3,725	3,590	2,795	770 1,185	1,850	580 885	1,385
	10	12½ 24	21 15	12½	8	5,990	4,655	4,490	3,495	755 1,185	2,225	565 885	1,665
	31/8	61/4 71/2	57/8 57/8	61/4	57/8	2,295	1,840	1,720	1,385	1,175 1,175	945	880 880	705
#5	5	81/8 12	91/4 71/2	81/8	5%	3,670	2,945	2,750	2,210	1,210 1,670	1,510	905 1,250	1,135
	71/2	10% 18	143/4	10%	75/8	5,500	4,425	4,125	3,320	1,125 1,670	2,095	845 1,250	1,570
	12½	15 <sup>5</sup> / <sub>8</sub>	26 18¾	15%	10¾	9,165	7,370	6,875	5,525	1,065 1,670	3,230	800 1,250	2,420
	3½	71/4 81/2	7	71/4	7	3,030	2,510	2,275	1,880	1,470 1,470	1,215	1,105 1,105	910
#6	6	9¾ 14½	11 9	9¾	7½	5,200	4,300	3,900	3,225	1,615 2,235	2,055	1,210 1,675	1,540
	9	12¾ 21⅙	17% 13½	12¾	97/8	7,800	6,450	5,850	4,835	1,505 2,235 1,425	2,895	1,125 1,675	2,175
	15	18¾ 36	31 22½	18¾	13%	12,995	10,750	9,750	8,060	2,235	4,520	1,070 1,675	3,390
	3¾	81/8 9	81/8 81/8	81/8	73/4	3,710	2,805	2,785	2,105	1,730 1,730	1,365	1,295 1,295	1,025
#7	7	113/8 167/8	12% 10½	11%	91/4	6,925	5,890	5,195	4,415	2,065 2,855	2,665	1,545 2,140	2,000
	10½	147/8 251/4	20% 15%	14%	121/8	10,390	8,835	7,790	6,625	1,920 2,855	3,780	1,440 2,140	2,835
	17½	217/8 42	35¾ 26¼	21%	17	17,320	14,725	12,990	11,045	1,820 2,855	5,945	1,365 2,140	4,460
	4	9 95%	91/8 91/8	9	91/8	3,625	3,095	2,715	2,320	1,635 1,635	1,420	1,225 1,225	1,065
#8	8	13 191⁄4	14% 12	13	9¾	7,245	6,295	5,430	4,720	2,090 2,890	2,840	1,570 2,165	2,130
0	12	17 28%	231/8	17	12%	10,870	9,440	8,150	7,080	1,945 2,890	3,985	1,460 2,165	2,990
	20	25 48	40½ 30	25	17¾	18,110	15,735	13,585	11,800	1,840 2,890	6,310	1,385 2,165	4,730
	5	111/ <sub>4</sub> 12	111/4	111/4	10½	5,410	4,325	4,060	3,245	_	_	_	_
#10	10	161/4 24	17% 15	161⁄4	131⁄4	10,825	10,145	8,115	7,610	_	_	_	
,,,,,	15	21 1/4 36	28% 22½	211/4	17%	16,235	15,215	12,175	11,410		_	_	_
	25	31 ½ 60	49¾ 37½	311/4	241/2	27,060	25,360	20,295	19,020	_	_	_	_

	Allowable Tension Lo	ad of Rebar Steel (lb.)
Rebar Size	ASTM A615 GR 60	ASTM A706 GR 60
#3	4,505	4,005
#4	8,190	7,280
#5	12,695	11,285
#6	18,020	16,015
#7	24,570	21,840
#8	32,350	28,755
#10	51,870	46,230

<sup>\*</sup> See page 12 for an explanation of the load table icons.

- 1. Allowable tension load must be the lesser of the concrete, bond or rebar steel load.
- 2. Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 180°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha=\%.7=1.43$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- Allowable tension loads in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

## AT-XP® Design Information — Masonry



**Adhesive** Anchors

AT-XP® Allowable Tension and Shear Loads for Threaded Rod and Rebar in the Face of Fully Grouted CMU Wall Construction 1, 3, 4, 5, 6, 8, 9, 10, 11

BC	<b>1</b>	<b>*</b>		7

Diameter (in.) or Rebar	Drill Bit Diameter	Minimum Embedment <sup>2</sup>	Allowable Load Based on Bond Strength <sup>7</sup> (lb.)			
Size No.	(in.)	(in.)	Tension Load	Shear Load		
		Threaded Rod Installed in the Face of CMU Wal	I			
3/8	1/2	3%	1,265	1,135		
1/2	5%	4½	1,910	1,660		
5/8	3/4	5%	2,215	1,810		
3/4	7/8	6½	2,260	1,810		
		Rebar Installed in the Face of CMU Wall				
#3	1/2	3%	1,180	1,315		
#4	5⁄8	4½	1,720	1,565		
#5	3/4	5%	1,835	1,565		

- Allowable load shall be the lesser of the bond values shown in this table and steel values, shown on page 37.
- 2. Embedment depth shall be measured from the outside face of masonry wall.
- Critical and minimum edge distance and spacing shall comply with the information on page 36. Figure 2 on page 36 illustrates critical and minimum edge and end distances.
- 4. Minimum allowable nominal width of CMU wall shall be 8 inches. No more than one anchor shall be permitted per masonry cell.
- Anchors shall be permitted to be installed at any location in the face of the fully grouted masonry wall construction (cell, web, bed joint), except anchors shall not be installed within 1½ inches of the head joint, as show in Figure 2 on page 36.
- Tabulated allowable load values are for anchors installed in fully grouted masonry walls.
- 7. Tabulated allowable loads are based on a safety factor of 5.0.
- Tabulated allowable load values shall be adjusted for increased base material temperatures in accordance with Figure 1 below, as applicable.
- Threaded rod and rebar installed in fully grouted masonry walls are permitted to resist dead, live, seismic and wind loads.
- Threaded rod shall meet or exceed the tensile strength of ASTM F1554, Grade 36 steel, which is 58,000 psi.
- 11. For installations exposed to severe, moderate or negligible exterior weathering conditions, as defined in Figure 1 of ASTM C62, allowable tension loads shall be multiplied by 0.80.

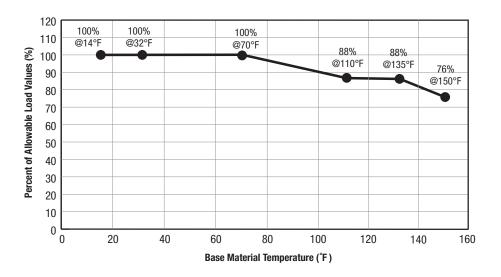


Figure 1. Load capacity based on in-service temperature for AT-XP® adhesive in the face of fully grouted CMU wall construction

<sup>\*</sup> See page 12 for an explanation of the load table icons.

### **AT-XP®** Design Information — Masonry



AT-XP® Edge Distance and Spacing Requirements and Allowable Load Reduction Factors — Threaded Rod and Rebar in the Face of Fully Grouted CMU Wall Construction<sup>7</sup>

IBC			• <b>1</b>	
[ ]	100,000,000	Sales Sales		

			Edge or Edge Distance <sup>1,8</sup>						Spacing <sup>2,9</sup>				
		Critical (Fi Capa		Minim	Minimum (Reduced Anchor Capacity) <sup>4</sup>				Critical (Full Anchor Capacity) <sup>5</sup> Minimum (Reduced Anchor Capac			or Capacity) <sup>6</sup>	
Rod Dia. (in.) or Rebar Size No.	Minimum Embed. Depth (in.)	Critical Edge or End Distance, C <sub>cr</sub> (in.)	Allowable Load Reduction Factor	Minimum Edge or End Distance, C <sub>min</sub> (in.)	Allowable	Load Reduct	ion Factor	Critical Spacing, S <sub>cr</sub> (in.)	Allowable Load Reduction Factor	Minimum Spacing, S <sub>min</sub> (in.)	Allowab Reductio		
		Load Di	rection		Load Di	Load Direction			irection	Load Direction		ı	
		Tension or	Tension or	Tension or	Tension	She	ar <sup>10</sup>	Tension or	Tension or	Tension or	Tension	Shear	
		Shear	Shear	Shear	ICHSIOH	Perp.	Para.	Shear	Shear	Shear	101191011	Sileai	
3/8	3%	12	1.00	4	1.00	0.76	0.94	8	1.00	4	1.00	1.00	
1/2	41/2	12	1.00	4	0.90	0.57	0.94	8	1.00	4	1.00	1.00	
5/8	5%	12	1.00	4	0.72	0.47	0.94	8	1.00	4	1.00	1.00	
3/4	61/2	12	1.00	4	0.72	0.47	0.94	8	1.00	4	1.00	1.00	
#3	3%	12	1.00	4	1.00	0.62	0.95	8	1.00	4	1.00	1.00	
#4	41/2	12	1.00	4	1.00	0.37	0.82	8	1.00	4	1.00	0.89	
#5	5%	12	1.00	4	1.00	0.37	0.82	8	1.00	4	1.00	0.89	

- Edge distance (C<sub>cr</sub> or C<sub>min</sub>) is the distance measured from anchor centerline to edge or end of CMU masonry wall. Refer to Figure 2 below for an illustration showing critical and minimum edge and end distances.
- Anchor spacing (S<sub>cr</sub> or S<sub>min</sub>) is the distance measured from centerline to centerline of two anchors.
- 3. Critical edge distance,  $C_{cr}$ , is the least edge distance at which tabulated allowable load of an anchor is achieved where a load reduction factor equals 1.0 (no load reduction).
- 4. Minimum edge distance,  $C_{min}$ , is the least edge distance where an anchor has an allowable load capacity which shall be determined by multiplying the allowable loads assigned to anchors installed at critical edge distance,  $C_{cn}$  by the load reduction factors shown above.
- Critical spacing, S<sub>cr</sub>, is the least anchor spacing at which tabulated allowable load of an anchor is achieved such that anchor performance is not influenced by adjacent anchors.
- 6. Minimum spacing,  $S_{min}$ , is the least spacing where an anchors has an allowable load capacity , which shall be determined by multiplying the allowable loads assigned to anchors installed at critical spacing distance,  $S_{cr}$ , by the load reduction factors shown above.
- Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.
- Load reduction factor for anchors loaded in tension with spacing between critical and minimum shall be obtained by linear interpolation.
- 10. Perpendicular shear loads act towards the edge or end. Parallel shear loads act parallel to the edge or end (see Figure 3 below). Perpendicular and parallel shear load reduction factors are cumulative when the anchor is located between the critical minimum edge and end distance.

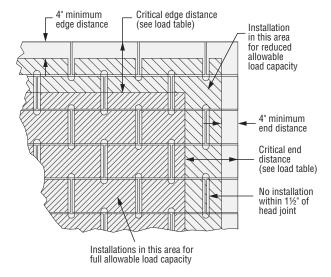
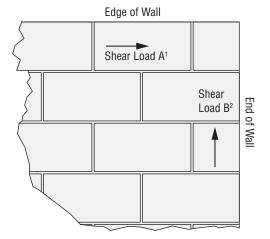


Figure 2. Allowable Anchor Locations for Full and Reduced Load Capacity When Installation Is in the Face of Fully Grouted CMU Masonry Wall Construction



**Figure 3.** Direction of Shear Load in Relation to Edge and End of Wall

- 1. Direction of Shear Load A is parallel to edge of wall and perpendicular to end of wall.
- Direction of Shear Load B is parallel to end of wall and perpendicular to edge of wall.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

SIMPSON StrongTie

AT-XP® Allowable Tension and Shear Loads — Threaded Rod Based on Steel Strength<sup>1</sup>

IBC 1	<b>→</b>	
-------	----------	--

		Tension	Load Based o	n Steel Stren	gth² (lb.)	Shear Load Based on Steel Strength <sup>3</sup> (lb.)						
Threaded Rod	Tensile			Stainle	ss Steel	ASTM		Stainless Steel				
Diameter (in.)	Stress Area (in.²)	ASTM F1554 Grade 36 <sup>4</sup>	ASTM A193 Grade B7 <sup>6</sup>	ASTM A193 Grade B6 <sup>5</sup>			ASTM A193 Grade B7 <sup>6</sup>		ASTM A193 Grades B8 and B8M <sup>7</sup>			
3/8	0.078	1,495	3,220	2,830	1,930	770	1,660	1,460	995			
1/2	0.142	2,720	5,860	5,155	3,515	1,400	3,020	2,655	1,810			
5/8	0.226	4,325	9,325	8,205	5,595	2,230	4,805	4,225	2,880			
3/4	0.334	6,395	13,780	12,125	8,265	3,295	7,100	6,245	4,260			

- 1. Allowable load shall be the lesser of bond values given on page 35 and steel values in the table above.
- 2. Allowable Tension Steel Strength is based on the following equation:  $F_V = 0.33 \times F_U x$  Tensile Stress Area.
- 3. Allowable Shear Steel Strength is based on the following equation:  $F_V = 0.17 \times F_U \times Tensile Stress Area$ .
- 4. Minimum specified tensile strength ( $F_U$  = 58,000 psi) of ASTM F1554, Grade 36 used to calculate allowable steel strength.
- 5. Minimum specified tensile strength ( $F_u$  = 110,000 psi) of ASTM A193, Grade B6 used to calculate allowable steel strength.
- 6. Minimum specified tensile strength ( $F_u$  = 125,000 psi) of ASTM A193, Grade B7 used to calculate allowable steel strength.
- 7. Minimum specified tensile strength ( $F_u$  = 75,000 psi) of ASTM A193, Grades B8 and B8M used to calculate allowable steel strength.

# AT-XP® Allowable Tension and Shear Loads — Deformed Reinforcing Bar Based on Steel Strength¹



	Doloittioa i toittioio	ing bai bacca	or otoor otronge		_				
	Drill Bit Diameter (in.)		Tension I	Load (lb.)	Shear Load (lb.)				
		Minimum Embedment <sup>2</sup>	Based on St	eel Strength	Based on Steel Strength				
		(in.)	ASTM A615 Grade 40 <sup>2</sup>	ASTM A615 Grade 60 <sup>3</sup>	ASTM A615 Grade 40 <sup>4,5</sup>	ASTM A615 Grade 60 <sup>4,6</sup>			
	#3	0.11	2,200	2,640	1,310	1,685			
	#4	0.20	4,000	4,800	2,380	3,060			
	#5	0.31	6,200	7,400	3,690	4,745			

- 1. Allowable load shall be the lesser of bond values given on page 35 and steel values in the table above.
- 2. Allowable Tension Steel Strength is based on AC58 Section 3.3.3 (20,000 psi x tensile stress area) for Grade 40 rebar.
- 3. Allowable Tension Steel Strength is based on AC58 Section 3.3.3 (24,000 psi x tensile stress area) for Grade 60 rebar.

- 4. Allowable Shear Steel Strength is based on AC58 Section 3.3.3 ( $F_{\rm V}=0.17$  x  $F_{\rm U}$  x Tensile Stress Area).
- 5.  $F_{\rm u} = 70,000$  psi for Grade 40 rebar.
- $6. F_{\text{u}} = 90,000 \text{ psi for Grade } 60 \text{ rebar}$

<sup>\*</sup> See page 12 for an explanation of the load table icons.

### SET-XP® High-Strength Epoxy Adhesive

SIMPSON
Strong-Tie

Cracked

Concrete

SET-XP® epoxy anchoring adhesive is a high-strength formula for anchoring and doweling in cracked and uncracked concrete and masonry applications. It is a two-part system with the resin and hardener being simultaneously dispensed and mixed through the mixing nozzle. When properly mixed, adhesive will be a uniform teal color for easy post-installation identification.

### **Features**

- 1:1 two-component, high-solids, epoxy-based anchoring adhesive formula
- Passed the demanding ICC-ES AC308 adverse-condition tests pertaining to elevated temperatures and long-term sustained loads
- Code listed under the IBC/IRC for cracked and uncracked concrete per ICC-ES ESR-2508
- Code listed under the IBC/IRC for masonry per IAPMO UES ER-265
- Suitable for use under static and seismic loading conditions in cracked and uncracked concrete and masonry
- Cure times: 24 hours at 70°F, 72 hours at 50°F
- Easy hole-cleaning no power-brushing required
- Suitable for use in dry or water-saturated concrete
- For best results, store between 45°F and 90°F
- Available in 8.5 oz., 22 oz. and 56 oz. cartridges for application versatility
- · Manufactured in the USA using global materials

### **Applications**

- Threaded rod anchoring and rebar doweling into concrete and masonry
- · Suitable for horizontal, vertical and overhead applications
- Multiple DOT listings refer to www.strongtie.com/DOT for current approvals

Codes: ICC-ES ESR-2508 (concrete); IAPMO UES ER-265 (masonry); City of L.A. RR25744 (concrete), RR25965 (masonry); Florida FL-17449.2 (concrete), FL-16230.3 (masonry); AASHTO M-235 and ASTM C881 (Type I and IV, Grade 3, Class C); NSF/ANSI Standard 61 (216 in.²/1,000 gal.)

### **Chemical Resistance**

See pages 320-321.

### Installation and Application Instructions

(See also pages 124-127.)

- Surfaces to receive epoxy must be clean.
- Base material temperature must be 50°F or above at the time of installation. For best results, material should be between 70°F and 80°F at time of application.
- To warm cold material, store cartridges in a warm, uniformly heated area or storage container. Do not immerse cartridges in water to facilitate warming.
- Mixed material in nozzle can harden in 30 minutes at temperatures of 70°F and above.





### **Design Example**

See page 328.

### Suggested Specifications

See www.strongtie.com for more information.



### SET-XP® High-Strength Epoxy Adhesive



### Test Criteria

Anchors installed with SET-XP® adhesive have been tested in accordance with ICC-ES Acceptance Criteria for Post-Installed Adhesive Anchors in Masonry Elements (AC58) and Adhesive Anchors in Concrete Elements (AC308).

Property	Test Method	Result*
Consistency	ASTM C881	Passed, non-sag
Glass transition temperature	ASTM E1356	155°F
Bond strength (moist cure)	ASTM C882	3,742 psi at 2 days
Water absorption	ASTM D570	0.10%
Compressive yield strength	ASTM D695	14,830 psi
Compressive modulus	ASTM D695	644,000 psi
Shore D Durometer	ASTM D2240	84
Gel time	ASTM C881	49 minutes
Volatile Organic Compound (VOC)	_	3 g/L

<sup>\*</sup>Material and curing conditions: 73 ± 2°F, unless otherwise noted.

### SET-XP® Cartridge System

Model No.	Capacity (ounces)	Cartridge Type	Carton Quantity	Dispensing Tool(s)	Mixing Nozzle
SET-XP10 <sup>4</sup>	8.5	Single	12	CDT10S	
SET-XP22-N⁵	22	Side-by-Side	10	EDT22S, EDTA22P, EDTA22CKT	EMN22i
SET-XP56	56	Side-by-Side	6	EDTA56P	

- 1. Cartridge estimation guidelines are available at www.strongtie.com/apps.
- Detailed information on dispensing tools, mixing nozzles and other adhesive accessories is available on pages 128 through 135, or at www.strongtie.com.
- 3. Use only Simpson Strong-Tie® mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair SET-XP adhesive performance.
- 4. Two EMN22i mixing nozzles and two nozzle extensions are supplied with each cartridge.
- 5. One EMN22i mixing nozzle and one nozzle extension are provided with each cartridge.

### Cure Schedule

	laterial erature	Cure Time (hrs.)				
°F	°C	(1115.)				
50	10	72				
60	16	48				
70	21	24				
90	32	24				
110	43	24				

For water-saturated concrete, the cure times must be doubled.



SET-XP® Installation Information and Additional Data for Threaded Rod and Rebar in Normal-Weight Concrete<sup>1</sup>









Characteristic		Symbol	Units	Nominal Anchor Diameter (in.) / Rebar Size							
Glidiacteristic	Glialacterisuc			% / #3	1/2 / #4	<b>5% / #5</b>	3/4 / #6	7/8 / # <b>7</b>	1 / #8	11/4 / #10	
			Instal	lation Inform	ation						
Drill Bit Diameter		d <sub>hole</sub>	in.	1/2	5/8	3/4	7/8	1	11/8	1%	
Maximum Tightening Torque		T <sub>inst</sub>	ftlb.	10	20	30	45	60	80	125	
Parmitted Embadment Depth Pance	Minimum	h <sub>ef</sub>	in.	23/8	2¾	31/8	31/2	3¾	4	5	
Permitted Embedment Depth Range	Maximum	h <sub>ef</sub>	in.	71/2	10	121/2	15	171/2	20	25	
Minimum Concrete Thickness	S	h <sub>min</sub>	in.				$h_{ef} + 5d_0$				
Critical Edge Distance <sup>2</sup>		Cac	in.				See footnote 2	2			
Minimum Edge Distance		C <sub>min</sub>	in.		1%						
Minimum Anchor Spacing		S <sub>min</sub>	in.			;	3			6	

<sup>1.</sup> The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.

 $[h/h_{ef}] \leq 2.4$ 

 $\tau_{\textit{k,uncr}} = \text{the characteristic bond strength in uncracked concrete, given in the tables that follow} \leq k_{\textit{uncr}} ((h_{\textit{ef}} \times f^{1}_{\textit{c}})^{0.5} / (/\textit{i} \times d_{\textit{a}}))$ 

h =the member thickness (inches)

hef = the embedment depth (inches)

<sup>2.</sup>  $c_{ac} = h_{ef} (\tau_{k,uncr}/1160)^{0.4} \times [3.1 - 0.7(h/_{hef})]$ , where:



### IBC





**Adhesive** Anchors

### SET-XP® Tension Strength Design Data for Threaded Rod in Normal-Weight Concrete<sup>1</sup>

JE 174 10	nsion Strength Design Data for Threa	adou i lou	11111011	TICK! V	Nominal Anchor Diameter (in.)						
	Characteristic		Symbol	Units	3/8	1/2	5%	3/4	7/8	1	11/4
		Steel Stre	enath in T	ension	/0	/2	/8	/4	/6	•	1 /4
	Minimum Tensile Stress Area	01001.011	$A_{se}$	in <sup>2</sup>	0.078	0.142	0.226	0.334	0.462	0.606	0.969
	Tension Resistance of Steel — ASTM F1554, Grade	e 36	00		4,525	8,235	13,110	19,370	26,795	35,150	56,200
	Tension Resistance of Steel — ASTM A193, Grade E	B7			9,750	17,750	28,250	41,750	57,750	75,750	121,12
Threaded Rod	Tension Resistance of Steel — Type 410 Stainless (A Grade B6)	(ASTM A193,	$N_{sa}$	lb.	8,580	15,620	24,860	36,740	50,820	66,660	106,590
	Tension Resistance of Steel — Type 304 and 316 S (ASTM A193, Grade B8 & B8M)	Stainless			4,445	8,095	12,880	19,040	26,335	34,540	55,235
	Strength Reduction Factor — Steel Failure		φ	_				$0.75^{7}$			
	Concrete Breako	out Strength in	Tension (	2,500 p	si ≤ f' <sub>C</sub> ≤	8,000 psi) <sup>1</sup>	2				
Effectiveness Factor — Uncracked Concrete			<i>k</i> <sub>uncr</sub>	_				24			
Effectiveness Fa	actor — Cracked Concrete		<i>k</i> <sub>cr</sub>	_				17			
Strength Reduct	tion Factor — Breakout Failure		φ	_	0.65 <sup>9</sup>						
	Bond Strei	ength in Tension	n (2,500 <sub> </sub>	osi ≤ f'c	≤ 8,000 μ	osi) <sup>12</sup>					
l la ava al ca d	Characteristic Bond Strength <sup>5,13</sup>		$ au_{k,uncr}$	psi	770	1,150	1,060	970	885	790	620
Uncracked Concrete 2,3,4	Permitted Embedment Depth Range	Minimum Maximum	h <sub>ef</sub>	in.	23/8 71/2	2¾ 10	31/8 121/2	3½ 15	3¾ 17½	4 20	5 25
Ougaliad	Characteristic Bond Strength <sup>5,10,11,13</sup>		$ au_{k,cr}$	psi	595	510	435	385	355	345	345
Cracked Concrete 2,3,4	Permitted Embedment Depth Range	Minimum Maximum	h <sub>ef</sub>	in.	3 7½	4 10	5 12½	6 15	7 17½	8 20	10 25
	Bond Strength in Tension — Bo	ond Strength R	eduction	Factors	for Cont	inuous Spo	ecial Inspe	ction			
Strength Reduct	tion Factor — Dry Concrete		φ <sub>dry, ci</sub>	_				0.658			
Strength Reduct	tion Factor — Water-saturated Concrete — h <sub>ef</sub> ≤ 12d <sub>ε</sub>	a	φ <sub>sat,ci</sub>	_	0.	55 <sup>8</sup>			0.458		
Additional Facto	or for Water-saturated Concrete — h <sub>ef</sub> ≤ 12d <sub>a</sub>		K <sub>sat,ci</sub> <sup>6</sup>	_	N	/A		1		0.	84
Strength Reduct	tion Factor — Water-saturated Concrete — h <sub>ef</sub> > 12d	la	φ <sub>sat,ci</sub>	_				0.458			
	or for Water-saturated Concrete — h <sub>ef</sub> > 12d <sub>a</sub>		k <sub>sat,ci</sub> 6	_				0.57			
	Bond Strength in Tension — E	Bond Strength	Reductio	n Facto	rs for Per	iodic Spec	ial Inspec	tion			
Strength Reduction Factor — Dry Concrete			$\phi_{dry,pi}$	_				0.558			
Strength Reduct	tion Factor — Water-saturated Concrete — $h_{ef} \le 12d_{\epsilon}$	a	φ <sub>sat,pi</sub>	_				0.458			
Additional Facto	or for Water-saturated Concrete — h <sub>ef</sub> ≤ 12d <sub>a</sub>		K <sub>sat,pi</sub> 6	_		1		0.93		0.	71
Strength Reduct	tion Factor — Water-saturated Concrete — h <sub>ef</sub> > 12d	la	φ <sub>sat,pi</sub>	_				0.458		1	
Additional Facto	or for Water-saturated Concrete — h <sub>ef</sub> > 12d <sub>a</sub>		K <sub>sat,pi</sub> 6					0.48			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- $2. \ \ \text{Temperature Range: Maximum short-term temperature of } 150^{\circ}\text{F. Maximum long-term temperature of } 110^{\circ}\text{F. } \\$
- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term concrete temperatures are constant temperatures over a significant time period.
- 5. For anchors that only resist wind or seismic loads, bond strengths may be increased b 72%.
- 6. In water-saturated concrete, multiply  $\tau_{k,uncr}$  and  $\tau_{k,cr}$  by  $K_{sat}$ .
- 7. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 8. The value of *φ* applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of *φ*.
- 9. The value of φ applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition A are met, refer to Section D.4.4 to determine the appropriate value of φ. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of φ.
- 10. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for  $\frac{7}{6}$  anchors must be multiplied by  $\alpha_{N,selis} = 0.80$ .
- 11. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for 1" anchors must be multiplied by  $\alpha_{N,sels} = 0.92$ .
- 12. The values of  $f_C'$  used for calculation purposes must not exceed 8,000 psi (55.1 MPa) for uncracked concrete. The value of  $f_C'$  used for calculation purposes must not exceed 2,500 psi (17.2 MPa) for tension resistance in cracked concrete.
- 13. For applications where maximum short-term temperature is 110°F (43°C) and the maximum long-term temperature is 75°F (24°C), bond strengths may be increased 93%. No additional increase is permitted for anchors that only resist wind or seismic loads.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



### SET-XP® Tension Strength Design Data for Rebar in Normal-Weight Concrete<sup>1</sup>



Oleanestanistia		Ob I	112				Rebar Size	;		
Characteristic		Symbol	Units	#3	#4	#5	#6	#7	#8	#10
	Ste	eel Strength in	Tension							
Minimum Tensile Stress Area		$A_{se}$	in <sup>2</sup>	0.11	0.2	0.31	0.44	0.6	0.79	1.23
Tension Resistance of Steel — R (ASTM A615 Grade 60)	ebar	$N_{sa}$	lb.	9,900	18,000	27,900	39,600	54,000	71,100	110,700
Strength Reduction Factor – Stee	l Failure	$\phi$	_				$0.65^{7}$			
Concrete Br	eakout Strer	ngth in Tension	ı (2,500 ps	$i \le f'_{C} \le 8$	000 psi) <sup>10</sup>					
acked Concrete		<i>k</i> <sub>uncr</sub>	_				24			
Effectiveness Factor — Cracked Concrete			_				17			
Strength Reduction Factor — Breakout Failure							0.65 <sup>9</sup>			
Bond	Strength in	Tension (2,50	$0 \text{ psi} \leq f_C^i \leq$	8,000 ps	i) <sup>10</sup>					
Characteristic Bond Strength <sup>5,11</sup>		$\tau_{k,uncr}$	psi	895	870	845	820	795	770	720
Permitted Embedment Depth	Minimum	h	in	2%	23/4	31/8	31/2	3¾	4	5
Range	Maximum	11 <sub>ef</sub>	111.	71/2	10	121/2	15	171/2	20	25
Characteristic Bond Strength <sup>5,11</sup>		$\tau_{k,cr}$	psi	365	735	660	590	515	440	275
Permitted Embedment Depth	Minimum	h	in	3	4	5	6	7	8	10
Range	Maximum	Hef	111.	71/2	10	12½	15	171/2	20	25
Bond Strength in Tension -	— Bond Stre	ength Reduction	n Factors	for Contin	uous Spec	cial Inspec	tion			
Ory Concrete		φ <sub>dry,ci</sub>	_				$0.65^{8}$			
Vater-saturated Concrete - h <sub>ef</sub> ≤ 12	2da	φ <sub>sat,ci</sub>	_	0.	55 <sup>8</sup>			0.458		
turated Concrete - h <sub>ef</sub> ≤ 12d <sub>a</sub>		K <sub>sat,ci</sub> 6	_	N	/A		1		0.	84
Vater-saturated Concrete - h <sub>ef</sub> > 12	2d <sub>a</sub>	φsat.ci	_				0.458			
turated Concrete - h <sub>ef</sub> > 12d <sub>a</sub>		K <sub>sat,ci</sub> 6	_				0.57			
Bond Strength in Tension	— Bond St	rength Reduct	ion Factor	s for Perio	dic Specia	al Inspecti	on			
Ory Concrete		φ <sub>drv.pi</sub>	_				0.558			
Strength Reduction Factor — Water-saturated Concrete - $h_{ef} \le 12d_a$					0.45 <sup>8</sup>					
turated Concrete - h <sub>ef</sub> ≤ 12d <sub>a</sub>		.,	_		1		0.93		0.	71
Vater-saturated Concrete - h <sub>ef</sub> > 12	2d <sub>a</sub>		_				0.458			
turated Concrete - h <sub>ef</sub> > 12d <sub>a</sub>			_				0.48			
	Tension Resistance of Steel — R (ASTM A615 Grade 60)  Strength Reduction Factor — Steet  Concrete Broked Concrete ed Concrete Breakout Failure  Bond Characteristic Bond Strength <sup>5,11</sup> Permitted Embedment Depth Range Characteristic Bond Strength <sup>5,11</sup> Permitted Embedment Depth Range  Bond Strength in Tension - Dry Concrete Vater-saturated Concrete - $h_{ef} \le 12d_a$ Vater-saturated Concrete - $h_{ef} > 12d_a$ Bond Strength in Tension Try Concrete Vater-saturated Concrete - $h_{ef} > 12d_a$ Vater-saturated Concrete - $h_{ef} > 12d_a$ Bond Strength in Tension Try Concrete Vater-saturated Concrete - $h_{ef} < 12d_a$	Minimum Tensile Stress Area  Tension Resistance of Steel — Rebar (ASTM A615 Grade 60)  Strength Reduction Factor — Steel Failure  Concrete Breakout Strench Strench Strench Strench Strench Strength in Characteristic Bond Strength $^{5,11}$ Permitted Embedment Depth Range $\frac{\text{Minimum}}{\text{Maximum}}$ Characteristic Bond Strength $^{5,11}$ Permitted Embedment Depth Range $\frac{\text{Minimum}}{\text{Maximum}}$ Bond Strength in Tension — Bond Strench Str	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Steel Strength in Tension         Minimum Tensile Stress Area $A_{Se}$ in²       0.11       0.2         Tension Resistance of Steel — Rebar (ASTM A615 Grade 60)       N <sub>Sa</sub> lb.       9,900       18,000         Strength Reduction Factor — Steel Failure $\phi$ —         Concrete Breakout Strength in Tension (2,500 psi ≤ f'c ≤ 8,000 psi)¹¹⁰         Cked Concrete $k_{uncr}$ —         Breakout Failure $\phi$ —         Bond Strength in Tension (2,500 psi ≤ f'c ≤ 8,000 psi)¹⁰         Characteristic Bond Strength in Tension (2,500 psi ≤ f'c ≤ 8,000 psi)¹⁰         Characteristic Bond Strength in Tension (2,500 psi ≤ f'c ≤ 8,000 psi)¹⁰         Characteristic Bond Strength in Tension (2,500 psi ≤ f'c ≤ 8,000 psi)¹⁰         Permitted Embedment Depth Maximum Maximum       h <sub>ef</sub> in.       2³%       2³¼         Permitted Embedment Depth Maximum Maximum       h <sub>ef</sub> in.       2³%       2³¼         Permitted Embedment Depth Maximum Maximum       h <sub>ef</sub> in.       3       4         Permitted Embedment Depth Maximum Maximum       h <sub>ef</sub> in.       7½       10         Bond Strength in Tension — Bond Strength Reduction Factors for C	Characteristic       Symbol       Units       #3       #4       #5         Steel Strength in Tension         Minimum Tensile Stress Area       A <sub>SS</sub> in²       0.11       0.2       0.31         Tension Resistance of Steel — Rebar (ASTM A615 Grade 60)       N <sub>Sa</sub> lb.       9,900       18,000       27,900         Strength Reduction Factor – Steel Failure         Concrete $k_{uncr}$ —         Concrete $k_{uncr}$ —         Breakout Failure $\phi$ —         Breakout Strength in Tension Tension (2,500 psi ≤ f'c ≤ 8,000 psi)** </td <td><math display="block"> \begin{array}{c c c c c c c c c c c c c c c c c c c </math></td> <td></td> <td>  Symbol   Symbol   Symbol   Steel Strength in Tension   Steel Strength in Tension Resistance of Steel — Rebar (ASTM A615 Grade 60)   Strength Reduction Factor – Steel Failure   φ   −</td>	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		Symbol   Symbol   Symbol   Steel Strength in Tension   Steel Strength in Tension Resistance of Steel — Rebar (ASTM A615 Grade 60)   Strength Reduction Factor – Steel Failure   φ   −

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- 2. Temperature Range: Maximum short-term temperature of 150°F. Maximum long-term temperature of 110°F.
- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term concrete temperatures are constant temperatures over a significant time period.
- 5. For anchors that only resist wind or seismic loads, bond strengths may be increased b 72%.
- 6. In water-saturated concrete, multiply  $au_{\textit{k,uncr}}$  and  $au_{\textit{k,cr}}$  by  $extit{K}_{\textit{sat}}$ .
- The value of φ applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of φ.
- 8. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of  $\phi$ .
- 9. The value of φ applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition A are met, refer to Section D.4.4 to determine the appropriate value of φ. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of φ.
- 10. The values of  $f'_c$  used for calculation purposes must not exceed 8,000 psi (55.1 MPa) for uncracked concrete. The value of  $f'_c$  used for calculation purposes must not exceed 2,500 psi (17.2 MPa) for tension resistance in cracked concrete.
- 11. For applications where maximum short-term temperature is 110°F (43°C) and the maximum long-term temperature is 75°F (24°C), bond strengths may be increased 93%. No additional increase is permitted for anchors that only resist wind or seismic loads.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **SET-XP®** Design Information — Concrete



### IBC





SET-XP® Shear Strength Design Data for Threaded Rod in Normal-Weight Concrete<sup>1</sup>

	Characteristic	Cumbal	Unito			Nominal A	Anchor Dia	meter (in.)			
	Characteristic	Буший	mbol Units	3/8	1/2	5/8	3/4	7/8	1	11/4	
	Stee	l Strengtl	n in Shea	r							
	Minimum Shear Stress Area	A <sub>se</sub>	in. <sup>2</sup>	0.078	0.142	0.226	0.334	0.462	0.606	0.969	
	Shear Resistance of Steel — ASTM F1554, Grade 36			2,260	4,940	7,865	11,625	16,080	21,090	33,720	
	Shear Resistance of Steel — ASTM A193, Grade B7			4,875	10,650	16,950	25,050	34,650	45,450	72,675	
	Shear Resistance of Steel — Type 410 Stainless (ASTM A193, Grade B6)	V <sub>sa</sub>	lb.	4,290	9,370	14,910	22,040	30,490	40,000	63,955	7
Threaded	Shear Resistance of Steel — Type 304 and 316 Stainless (ASTM A193, Grade B8 & B8M)			2,225	4,855	7,730	11,420	15,800	20,725	33,140	_ (
Rod	Reduction for Seismic Shear — ASTM F1554, Grade 36			0.87	0.78		0.	68		0.65	1
	Reduction for Seismic Shear — ASTM A193, Grade B7			0.87	0.78		0.	68		0.65	<
	Reduction for Seismic Shear — Stainless (ASTM A193, Grade B6)	$lpha_{V\!\!,seis}$ 5	_	0.69	0.82		0.75		0.83	0.72	
	Reduction for Seismic Shear — Stainless (ASTM A193, Grade B8 & B8M)			0.69	0.82		0.75		0.83	0.72	•
	Strength Reduction Factor — Steel Failure	φ	_	$0.65^{2}$							
	Concrete B	reakout S	trength	n Shear							
	Outside Diameter of Anchor	do	in.	0.375	0.5	0.625	0.75	0.875	1	1.25	
	Load Bearing Length of Anchor in Shear	$\ell_e$	in.				h <sub>ef</sub>				
Strength Reduction Factor — Breakout Failure		φ	_				$0.70^{3}$				1
	Concrete	Pryout St	rength ir	Shear							П
Coefficient for Pryout Strength			_		1.	0 for $h_{ef}$ < 1	2.50"; 2.0 1	for $h_{ef} \ge 2.5$	50"		
	Strength Reduction Factor — Pryout Failure	φ	_				0.704				

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 3. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition A are met, refer to Section D.4.3 to determine
- the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 4. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 5. The values of  $V_{\rm SS}$  are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F,  $V_{\rm SS}$  must be multiplied by  $\alpha_{V,\rm Seis}$  for the corresponding anchor steel type.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



SET-XP® Shear Strength Design Data for Rebar in Normal-Weight Concrete<sup>1</sup>



	Ohawadawiatia	Compleal	Heite	Rebar Size							
	Characteristic	Symbol	Units	#3	#4	#5	#6	#7	#8	#10	
		Steel Stren	gth in Shea	ar							
Minimum Shear Stress Area		A <sub>se</sub>	in <sup>2</sup>	0.11	0.2	0.31	0.44	0.6	0.79	1.23	
Rebar	Shear Resistance of Steel — Rebar (ASTM A615 Grade 60)	V <sub>sa</sub>	lb.	4,950	10,800	16,740	23,760	32,400	42,660	66,420	
neuai	Reduction for Seismic Shear — Rebar (ASTM A615 Grade 60)		_	0.85	0.85 0.88 0.84			0.	77	0.59	
	Strength Reduction Factor — Steel Failure		_				0.602				
	Concr	ete Breakou	t Strength	in Shear							
	Outside Diameter of Anchor	do	in.	0.375	0.5	0.625	0.75	0.875	1	1.25	
	Load-Bearing Length of Anchor in Shear	$\ell_e$	in.	h <sub>ef</sub>							
	Strength Reduction Factor — Breakout Failure	φ	_	0.70 <sup>3</sup>							
	Conc	rete Pryout	Strength in	Shear							
	Coefficient for Pryout Strength	<i>k<sub>cp</sub></i>	_		1.	of for $h_{ef} < 2$	2.50"; 2.0 f	for $h_{ef} \ge 2.5$	50"		
	Strength Reduction Factor — Pryout Failure	φ	_				0.704				

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 3. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition A are met, refer to Section
- D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 4. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 5. The values of  $V_{\rm sa}$  are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F,  $V_{\rm sa}$  must be multiplied by  $\alpha_{V_{\rm S}{\rm eis}}$ .



SET-XP® Development Length for Rebar Dowels in Normal-Weight Concrete<sup>1,2,3,4,5,6</sup>

IRC
IDU



			Deve	elopment Length, in. (	(mm)	
Rebar Size	Top Cover in. (mm)	f' <sub>c</sub> = 2,500 psi (17.2 MPa) Concrete	f' <sub>c</sub> = 3,000 psi (20.7 MPa) Concrete	f' <sub>c</sub> = 4,000 psi (27.6 MPa) Concrete	f' <sub>c</sub> = 6,000 psi (41.4 MPa) Concrete	f' <sub>c</sub> = 8,000 psi (55.2 MPa) Concrete
<b>#3</b> (9.5)	<b>1½</b> (38)	<b>12</b> (305)				
<b>#4</b> (12.7)	<b>1½</b> (38)	<b>15</b> (381)	<b>14</b> (356)	<b>12</b> (305)	<b>12</b> (305)	<b>12</b> (305)
<b>#5</b> (15.9)	<b>1½</b> (38)	<b>18</b> (457)	<b>17</b> (432)	<b>15</b> (381)	<b>12</b> (305)	<b>12</b> (305)
<b>#6</b> (19.1)	<b>1½</b> (38)	<b>22</b> (559)	<b>20</b> (508)	<b>18</b> (457)	<b>14</b> (356)	<b>13</b> (330)
<b>#7</b> (22.2)	<b>3</b> (76)	<b>32</b> (813)	<b>29</b> (737)	<b>25</b> (635)	<b>21</b> (533)	<b>18</b> (457)
<b>#8</b> (25.4)	<b>3</b> (76)	<b>36</b> (914)	<b>33</b> (838)	<b>29</b> (737)	<b>24</b> (610)	<b>21</b> (533)
<b>#9</b> (28.7)	<b>3</b> (76)	<b>41</b> (1041)	<b>38</b> (965)	<b>33</b> (838)	<b>27</b> (686)	<b>23</b> (584)
<b>#10</b> (32.3)	<b>3</b> (76)	<b>46</b> (1168)	<b>42</b> (1067)	<b>37</b> (940)	<b>30</b> (762)	<b>26</b> (660)
<b>#11</b> (35.8)	<b>3</b> (76)	<b>51</b> (1295)	<b>47</b> (1194)	<b>41</b> (1041)	<b>33</b> (838)	<b>29</b> (737)

<sup>1.</sup> Tabulated development lengths are for static, wind and seismic load cases in Seismic Design Category A and B.

<sup>2.</sup> Rebar is assumed to be ASTM A615 Grade 60 or A706 ( $f_y = 60,000$  psi). For rebar with a higher yield strength, multiply tabulated values by  $f_y / 60,000$  psi.

<sup>3.</sup> Concrete is assumed to be normal-weight concrete. For lightweight concrete, multiply tabulated values by 1.33.

<sup>4.</sup> Tabulated values assume bottom cover of less than 12 inches cast below rebars ( $\Psi_t$  = 1.0).

<sup>5.</sup> Uncoated rebar must be used.

<sup>6.</sup> The value of  $K_{tr}$  is assumed to be 0. Refer to ACI 318 Section 12.2.3.



SET-XP® Tension Design Strength for Threaded Rod Anchors in Normal-Weight Concrete (f'<sub>c</sub> = 2,500 psi)

IBC	1		*
l J	252	[ [ [ ] ]	37500

	Nominal	Minimum	Dimensions	Minimum I	Dimensions	Tension Design Strength Based on Concrete or Bond (lb.)							
Rod Dia.	Embed.	for Und	cracked	for Cr	acked			= c <sub>ac</sub> on all s	sides	Ĭ	and Cac on	= 1¾" on one three sides	
(in.)	Depth (in.)		n.)		n.)	SDC			C-F <sup>7,8</sup>	SDC	A-B <sup>6</sup>	SDC	
	(,	ha	Cac	ha	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	2%	4 ½ 5 ¾	33/ <sub>4</sub> 35/ <sub>8</sub>	_	_	1,185	_	890	_	675 800	_	505 600	_
	3	47/8 71/4	5 4½	47/8	31/4	1,500	1,150	1,125	865	635 880	775	475 660	585
3/8	41/2	63/8 107/8	8 1/8 6 3/4	6%	31/4	2,250	1,725	1,685	1,295	590 880 570	1,165	445 660	875
	6	7 1/8 1 4 1/2	111/8 9	77/8	43/8	2,995	2,300	2,250	1,725	880	1,555	430 660	1,165
	71/2	9% 18	141/4 111/4	9%	5%	3,745	2,875	2,810	2,160	560 880	1,945	420 660	1,455
	23/4	51/4 65/8	51/8 51/8	_	_	2,730	_	2,050	_	1,470 1,470	_	1,105 1,105	_
	4	6½ 9%	77/8 6	6½	51/8	3,975	1,755	2,980	1,315	1,400 1,935	945	1,050 1,450	710
1/2	6	8½ 14½	12% 9	81/2	51/8	5,960	2,635	4,470	1,975	1,300 1,935 1,260	1,420	975 1,450	1,065
	8	10½ 19¼	17½ 12 22¼	10½	51/4	7,950	3,510	5,960	2,635	1,260 1,935 1,235	1,890	945	1,420
	10	12½	15	12½	6%	9,935	4,390	7,450	3,290	1.935	2,365	925 1,450	1,775
	31/8	61/4 71/2	61/4 61/4 91/2	_		3,580		2,685	_	1,805 1,805	_	1,355 1,355	
5/8	5	8½ 12	71/2	81/8	61/4	5,730	2,335	4,295	1,750	1,875 2,590	1,175	1,405	885
78	71/2	10% 18	15% 11¼	10%	61/4	8,595	3,500	6,445	2,625	1,745 2,590	1,765	1,310 1,945	1,325
	12½	15% 30	26 <sup>7</sup> / <sub>8</sub> 18 <sup>3</sup> / <sub>4</sub>	15%	75/8	14,320	5,830	10,740	4,375	1,655 2,590	2,945	1,240 1,945	2,210
	31/2	7 ½ 8 ½	7 1/8 7 1/8	_	_	4,385	_	3,290	_	2 120	_	1,590 1,590 1,750	_
3/4	6	93/4	9	9¾	71/8	7,520	3,000	5,640	2,250	2,120 2,335 3,230	1,450	2.420	1,090
74	9	12¾ 21⅓	17¾ 13½	12¾	71/8	11,280	4,500	8,460	3,375	2,175 3.230	2,180	1,630 2,420	1,635
	15	18¾ 36	31 1/8 22 1/2	18¾	9	18,795	7,505	14,100	5,625	2,060 3,230	3,630	1,545 2,420	2,720
	3¾	8 1/8 9	77/8 77/8	_	_	5,020	_	3,010	_	2,355 2,355	_	1,410 1,410	_
7/8	7	11% 16%	12% 10½	11%	77/8	9,365	3,745	5,620	2,250	2,795 3,865	1,755	1,680 2,320	1,055
76	10½	147/8 251/4	197/8 153/4	147/8	71/8	14,050	5,620	8,430	3,370	2,605 3,865	2,635	1,560 2,320	1,580
	17½	21% 42	35 261/4 81/2	21 1/8	10	23,415	9,365	14,050	5,620	2,465 3,865	4,390	1,480 2,320	2,635
	4	9 95%	81/2	_	_	5,455	_	3,765	_	2,505 2,505	_	1,730 1,730	_
1	8	13 19¼ 17	13½ 12 21¾	13	81/2	10,905	4,755	7,525	3,280	3,155 4,360	2,185	2,175 3,010	1,510
'	12	287/8	18	17	81/2	16,360	7,135	11,290	4,920	2,935 4,360 2,785	3,280	2,025 3,010	2,265
	20	25 48	381/4	25	121/4	27,265	11,890	18,815	8,205	2,785 4,360	5,465	1,920 3,010	3,770
	5	11½ 12	9½ 9½	_	_	6,705	_	5,030	_	_	_	_	_
11/4	10	161/ <sub>4</sub> 24	15% 15	161⁄4	9½	13,415	7,430	10,060	5,570	_	_	_	_
1 74	15	21 ½ 36	24 <sup>3</sup> / <sub>4</sub> 22 <sup>1</sup> / <sub>2</sub>	21 1/4	111/8	20,120	11,145	15,090	8,360	_	_	_	
	25	31 ½ 60	43% 37½	31 1/4	15%	33,530	18,575	25,150	13,930	_	_	_	_

Threaded Rod		Tension E	Design Strength (	of Threaded Rod	Steel (lb)	
Dia. (in.)	ASTM F1554, GR 36	ASTM F1554, GR 55	ASTM F1554, GR 105	ASTM A193, B6	ASTM A193, B7	ASTM A193, B8/B8M
3/8	3,370	4,360	7,270	6,395	7,270	3,310
1/2	6,175	7,990	13,315	11,715	13,315	6,070
5/8	9,835	12,715	21,190	18,645	21,190	9,660
3/4	14,530	18,790	31,315	27,555	31,315	14,280
7/8	20,095	25,990	43,315	38,115	43,315	19,750
1	26,365	34,090	56,815	49,995	56,815	25,905
11/4	42,150	54,505	90,845	79,945	90,845	41,425

- Tension design strength must be the lesser of the concrete, bond or threaded rod steel design strength.
- 2. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.

- The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level
- also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.

  7. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3. Design strengths in Bold indicate that the anchor ductility requirements of D.3.3.4.3 (a)1 to 3 are satisfied when using ASTM F1554 Grade 36 threaded rod. Any other ductility requirements must be satisfied.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **SET-XP®** Design Information — Concrete

SET-XP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete  $(f'_{c} = 2,500 \text{ psi})$  — Static Load







<u>C</u> ,	Naminal Embad	Minimum Di	mensions for	Minimum Di	mensions for	Allowable 1	Tension Load Ba	ised on Concrete o	or Bond (lb.)
Rod Dia. (in.)	Nominal Embed. Depth (in.)	Uncr (i	acked n.)		cked n.)		nces = c <sub>ac</sub> sides	Edge Distances side and C <sub>ac</sub> (	s = 134" on one on three sides
	()	h <sub>a</sub>	C <sub>ac</sub>	ha	C <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked
	23/8	41/ <sub>4</sub> 53/ <sub>4</sub>	3 <sup>3</sup> / <sub>4</sub> 3 <sup>5</sup> / <sub>8</sub>	_	_	845	_	480 570	_
	3	47/8 71/4	5 4½	47/8	31/4	1,070	820	455 630	555
3/8	41/2	6% 10%	8 1/8 6 3/4	6%	31⁄4	1,605	1,230	420 630	830
	6	7% 14½	11 1/8 9	71/8	43/8	2,140	1,645	405 630	1,110
	71/2	9% 18	141⁄4 111⁄4	9%	5%	2,675	2,055	400 630	1,390
	23/4	51/4 65/8	51/8 51/8	_	_	1,950	_	1,050 1,050	_
	4	6½ 95/8	77/8 6	61/2	51/8	2,840	1,255	1,000	675
1/2	6	8½ 14½	12 <sup>5</sup> / <sub>8</sub>	81/2	51/8	4,255	1,880	930 1.380	1,015
	8	10½ 19¼	17½ 12	10½	51/4	5,680	2,505	900 1,380	1,350
	10	12½ 24	22½ 15	12½	6%	7,095	3,135	880 1.380	1,690
	31/8	6¼ 7½	6½ 6¼	_	_	2,555	_	1,290 1,290	_
F./	5	81/8 12	9½ 7½	81/8	61/4	4,095	1,670	1,340 1,850	840
5/8	71/2	105/8 18	15% 11¼	10%	61/4	6,140	2,500	1,245 1,850	1,260
	12½	15% 30	267/8 183/4	15%	7%	10,230	4,165	1,180 1,850	2,105
	3½	7½ 8½	71/8 71/8	_	_	3,130	_	1,515 1,515	_
3/	6	9¾ 14½	11 9	9¾	71/8	5,370	2,145	1,670 2,305	1,035
3/4	9	12¾ 21%	17¾ 13½	12¾	71/8	8,055	3,215	1,555 2,305	1,555
	15	18¾ 36	31 1/8 22 1/2	18¾	9	13,425	5,360	1,470 2,305	2,595
	3¾	81/8 9	7% 7%	_	_	3,585	_	1,680 1.680	_
7/8	7	11% 16%	12% 10½	11%	77/8	6,690	2,675	1,995 2,760	1,255
1/8	101/2	14% 25¼	197/8 153/4	14%	77/8	10,035	4,015	1,860 2,760	1,880
	17½	21% 42	35 261/4	21%	10	16,725	6,690	1,760 2,760	3,135
	4	9 9% 13	8½ 8½	_	_	3,895	_	1.790	_
1	8	13 19¼	13½ 12	13	81/2	7,790	3,395	1,790 2,255 3,115	1,560
1	12	17	21¾ 18	17	81/2	11,685	5,095	3,115 2,095 3,115	2,345
	20	287/8 25 48	38¼ 30	25	121/4	19,475	8,495	3,115 1,990 3,115	3,905
	5	11¼ 12	9½ 9½	_	_	4,790	_	_	_
41/	10	16¼ 24	15% 15	161⁄4	91/2	9,580	5,305	_	_
11⁄4	15	21 ½ 36	24 <sup>3</sup> / <sub>4</sub> 22 <sup>1</sup> / <sub>2</sub>	211/4	111/8	14,370	7,960	_	_
	25	31 ½ 60	43 % 37 ½	311/4	15%	23,950	13,270	_	_

Threaded		Allowable Tension Load of Threaded Rod Steel (lb.)										
Rod Dia. (in.)	ASTM F1554, GR 36	ASTM F1554, GR 55	ASTM F1554, GR 105	ASTM A193, B6	ASTM A193, B7	ASTM A193, B8/B8M						
3/8	2,405	3,115	5,195	4,570	5,195	2,365						
1/2	4,410	5,705	9,510	8,370	9,510	4,335						
5/8	7,025	9,080	15,135	13,320	15,135	6,900						
3/4	10,380	13,420	22,370	19,680	22,370	10,200						
7/8	14,355	18,565	30,940	27,225	30,940	14,105						
1	18,830	24,350	40,580	35,710	40,580	18,505						
1 1/4	30,105	38,930	64,890	57,105	64,890	29,590						

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or threaded rod steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of

<sup>\*</sup> See page 12 for an explanation of the load table icons.

<sup>110°</sup>F. Tension design strengths are converted to allowable tension loads using a conversion factor of a = 1.4. The conversion factor a is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.



SET-XP $^{\odot}$  Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete (f' $_{\rm C}$  = 2,500 psi) — Wind Load

$\overline{}$	 $\overline{}$	•
20		
ВU	ii	
	200 200	





$(I_C - 2,300)$	poi) vvii k	LUau				Allanoshia T			an Daniel (lla)	
Rod Dia. (in.)	Nominal Embed. Depth		mensions for ked (in.)	Minimum Di Crack	mensions for ed (in.)		tances =	ased on Concrete or Bond (lb.)  Edge Distances = 1¾" on one side and cac on three sides		
	(in.)	h <sub>a</sub>	Cac	h <sub>a</sub>	Cac	Uncracked	Cracked	Uncracked	Cracked	
	2%	4½ 5¾	3 <sup>3</sup> / <sub>4</sub> 3 <sup>5</sup> / <sub>8</sub>			710	_	405 480	_	
	3	47/8 71/4	5 4½	47/8	31/4	900	690	380 530	465	
3/8	41/2	6% 10%	8½ 6¾	63/8	31/4	1,350	1,035	355 530	700	
	6	71/8 141/2	11½ 9	77/8	43/8	1,795	1,380	340 530	935	
	7½	9% 18	141/4 111/4	9%	5%	2,245	1,725	335 530	1,165	
	23/4	51/4 65/8	51% 51%	_	_	1,640	_	880 880	_	
	4	6½ 95/8	77/8 6	61/2	51/8	2,385	1,055	840 1160	565	
1/2	6	8½ 14½	12% 9	81/2	51/8	3,575	1,580	780 1,160	850	
	8	10½ 19¼	17½ 12	10½	51/4	4,770	2,105	755 1,160	1,135	
	10	12½ 24	22¼ 15	12½	63/8	5,960	2,635	740 1,160	1,420	
	31/8	61/4 71/2	61/4 61/4	_	_	2,150	_	1,085 1.085	_	
5/	5	81⁄8 12	9½ 7½	81/8	61/4	3,440	1,400	1,125 1,555	705	
5/8	71/2	10% 18	15% 11¼	10%	61/4	5,155	2,100	1,045 1,555	1,060	
	12½	15% 30	26% 18%	15%	75/8	8,590	3,500	995 1,555	1,765	
	31/2	71/ <sub>4</sub> 81/ <sub>2</sub>	7 1/8 7 1/8	_	_	2,630	_	1,270 1,270	_	
3/4	6	9¾ 14½	11 9	9¾	71/8	4,510	1,800	1,400 1,940	870	
74	9	12¾ 21%	17¾ 13½	12¾	71/8	6,770	2,700	1,305 1,940	1,310	
	15	18¾ 36	31 1/8 22 1/2	18¾	9	11,275	4,505	1,235 1,940	2,180	
	3¾	81/8 9	77/8 77/8	_	_	3,010	_	1,415 1,415	_	
7/8	7	11% 16%	12% 10½	11%	77/8	5,620	2,245	1,675 2,320	1,055	
'/8	10½	14% 25¼	197/s 153/4	14%	77/8	8,430	3,370	1,565 2,320	1,580	
	17½	21 7/8 42	35 261/4	21%	10	14,050	5,620	1,480 2,320	2,635	
	4	9 9%	8½ 8½	_	_	3,275	_	1,505 1,505	_	
1	8	13 19¼	13½ 12	13	8½	6,545	2,855	1,895 2,615	1,310	
1	12	17 28%	21 <sup>3</sup> / <sub>4</sub> 18	17	81/2	9,815	4,280	1,760 2,615	1,970	
	20	25 48	38¼ 30	25	121/4	16,360	7,135	1,670 2,615	3,280	
	5	11¼ 12	9½ 9½		_	4,025	_	_	_	
1 1/4	10	16¼ 24	15% 15	161⁄4	9½	8,050	4,460	_	_	
1 74	15	21 ¼ 36	24¾ 22½	21 1/4	111/8	12,070	6,685	_	_	
	25	31 ¼ 60	43% 37½	311/4	15%	20,120	11,145	_	_	

Threaded Rod	Allowable Tension Load of Threaded Rod Steel (lb.)										
Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M					
3/8	2,020	2,615	4,360	3,835	4,360	1,985					
1/2	3,705	4,795	7,990	7,030	7,990	3,640					
5/8	5,900	7,630	12,715	11,185	12,715	5,795					
3/4	8,720	11,275	18,790	16,535	18,790	8,570					
7/8	12,055	15,595	25,990	22,870	25,990	11,850					
1	15,820	20,455	34,090	29,995	34,090	15,545					
1 1/4	25.290	32,705	54.505	47.965	54.505	24.855					

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or threaded rod steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = \%.6 = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



SET-XP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete  $(f'_{C} = 2,500 \text{ psi})$  — Seismic Load

٢	
П	DC
Ш	IDU





1	

Name	Freebook	Minimum I	Dimensions	Minimum I	Nimoneione	Allowable Tension Load Based on Concrete or Bond (lb.)							
Nom. Insert	Embed. Depth,	for Unc	cracked	for Cr	acked	Edge	Distances	= c <sub>ac</sub> on all s	sides	Edge		= 1¾" on on three sides	e side
Diam. (in.)	h <sub>ef</sub> (in.)	(ii	n.)		1.)	SDC	A-B <sup>5</sup>	SDC	C-F <sup>6,7</sup>	SDC	A-B <sup>5</sup>	SDC	C-F <sup>6,7</sup>
(111.)	(111.)	h <sub>a</sub>	Cac	ha	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	2%	4½ 5¾	3¾ 35/8	_	_	830		625		475 560		355 420	
	3	47/8 71/4	5 4½	47/8	31/4	1,050	805	790	605	445 615	545	335 460	410
3/8	41/2	63/8 107/8	8 1/8 6 3/4	6%	31/4	1,575	1,210	1,180	905	415 615	815	310 460	615
	6	77/8 141/2	11½ 9	77/8	43/8	2,095	1,610	1,575	1,210	400 615 390	1,090	300 460	815
	71/2	9% 18	141/4 111/4	9%	5%	2,620	2,015	1,965	1,510	615	1,360	295 460	1,020
	23/4	51/4 65/8	51/8 51/8	_	_	1,910	_	1,435		1,030 1,030		775 775	_
	4	6½ 95/8	77/8 6	61/2	51/8	2,785	1,230	2,085	920	980 1,355	660	735 1,015	495
1/2	6	8½ 14½	12% 9	81/2	51/8	4,170	1,845	3,130	1,385	910 1,355	995	685 1,015	745
	8	10½ 19¼	17½ 12	10½	51/4	5,565	2,455	4,170	1,845	880 1,355	1,325	660 1,015	995
	10	12½ 24	22½ 15	12½	6%	6,955	3,075	5,215	2,305	865 1,355	1,655	650 1,015	1,245
	31/8	61/4 71/2	6½ 6¼	_	_	2,505	_	1,880		1,265 1,265		950 950	
5/8	5	81/8 12	9½ 7½	81/8	61/4	4,010	1,635	3,005	1,225	1,315 1,815	825	985 1,360	620
/6	71/2	10% 18	15% 11¼	10%	61/4	6,015	2,450	4,510	1,840	1,220 1,815	1,235	915 1,360	930
	121/2	15% 30 71/4	267/8 183/4	15%	75/8	10,025	4,080	7,520	3,065	1,160 1,815	2,060	870 1,360	1,545
	31/2	81/2	7 1/8 7 1/8	_	_	3,070	_	2,305	_	1,485 1,485	_	1,115 1,115	_
3/4	6	9¾ 14½	11 9	9¾	71/8	5,265	2,100	3,950	1,575	1,635 2,260	1,015	1,225 1,695	765
/4	9	12¾ 21⅓	17¾ 13½	12¾	71/8	7,895	3,150	5,920	2,365	1,525 2,260	1,525	1,140 1,695	1,145
	15	18¾ 36	31 1/8 22 1/2	18¾	9	13,155	5,255	9,870	3,940	1,440 2,260	2,540	1,080 1,695	1,905
	3¾	81/8 9	77/8 77/8	_	_	3,515		2,105		1,650 1,650		985 985	_
7/8	7	11% 16%	12% 10½	11%	77/8	6,555	2,620	3,935	1,575	1,955 2,705 1,825 2,705	1,230	1,175 1,625	740
/8	10½	147/8 251/4	197/8 153/4	147/8	77/8	9,835	3,935	5,900	2,360	1,825 2,705	1,845	1,090 1,625	1,105
	171/2	217/8 42	35 26¼	217/8	10	16,390	6,555	9,835	3,935	1,725 2,705	3,075	1,035 1,625	1,845
	4	9 9% 13	8½ 8½	_	_	3,820	_	2,635	_	1,755 1,755 2,210	_	1,210 1,210 1,525	_
1	8	191/4	13½ 12 21¾	13	81/2	7,635	3,330	5,270	2,295	3.050	1,530	2.105	1,055
	12	17 28% 25	18	17	81/2	11,450	4,995	7,905	3,445	2,055 3,050	2,295	1,420 2,105 1,345	1,585
	20	48	38¼ 30	25	121/4	19,085	8,325	13,170	5,745	1,950 3,050	3,825	1,345 2,105	2,640
	5	11½ 12	9½ 9½	_	_	4,695	_	3,520	_	_	_	_	_
1 1/4	10	161/ <sub>4</sub> 24	15% 15	161/4	91/2	9,390	5,200	7,040	3,900	_	_	_	_
1 /4	15	21 1/4 36 31 1/4	24¾ 22½	211/4	111/8	14,085	7,800	10,565	5,850	_		_	_
	25	31 ½ 60	43% 37½	311/4	15%	23,470	13,005	17,605	9,750	_	_	_	_

Threaded	Allowable Tension Load of Threaded Rod Steel (lb.)										
Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M					
3/8	2,360	3,050	5,090	4,475	5,090	2,315					
1/2	4,325	5,595	9,320	8,200	9,320	4,250					
5/8	6,885	8,900	14,835	13,050	14,835	6,760					
3/4	10,170	13,155	21,920	19,290	21,920	9,995					
7/8	14,065	18,195	30,320	26,680	30,320	13,825					
1	18,455	23,865	39,770	34,995	39,770	18,135					
1 1/4	29.505	38.155	63.590	55.960	63,590	29.000					

- 1. Allowable tension load must be the lesser of the concrete, bond or threaded rod
- 2. Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = 1.43$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- \* See page 12 for an explanation of the load table icons.

- 5. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3. Design strengths in Bold indicate that the anchor ductility requirements of D.3.3.4.3 (a)1 to 3 are satisfied when using ASTM F1554 Grade 36 threaded rod. Any other ductility requirements must be satisfied.
- 7. Allowable tension loads in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# SET-XP® Design Information — Concrete



SET-XP® Tension Design Strength for Rebar in Normal-Weight Concrete (f'<sub>c</sub> = 2,500 psi)

IBC		

					Tension Design Strength Based on Concrete or Bond (lb.)						d (lb.)	.)	
Rebar	Nominal Embed.	for Und	Dimensions cracked	for Cr	Dimensions acked		Distances	= c <sub>ac</sub> on all s	sides		Distances =	= 1¾" on one three sides	e side
Size	Depth	(11)	n.)	(II)	n.)	SDC	A-B <sup>6</sup>	SDC	C-F <sup>7,8</sup>	SDC	A-B <sup>6</sup>	SDC (	C-F <sup>7,8</sup>
	(in.)	ha	c <sub>ac</sub>	ha	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	2%	4 1/4 5 3/4	4 35/8	_	_	1,380	_	1,035	_	765 895	_	575 670	_
	3	47/8 71/4	53/8 41/2	47/8	3½	1,740	700	1,305	525	720 995	455	540 745	340
#3	41/2	63/8 107/8	85/8 63/4	63/8	3½	2,615	1,055	1,960	790	670 995	685	505 745	510
	6	77/8 141/2	117/8	77/8	3½	3,485	1,405	2,615	1,055	650 995	910	485 745	685
	71/2	9% 18	151/8 111/4	9%	3½	4,355	1,755	3,265	1,315	635 995	1,140	475 745	855
	2¾	51/4 65/8	4½ 4½	_	_	2,065	_	1,550	_	1,180 1,180	_	885 885	_
	4	6½ 9%	7	6½	41/2	3,005	2,525	2,255	1,895	1,090 1.505	1,440	815 1,130	1,080
#4	6	8½ 14½	11% 9	8½	5½	4,510	3,790	3,380	2,840	1,015 1,505	2,035	760 1.130	1,525
	8	10½ 19¼	15% 12	10½	65/8	6,015	5,050	4,510	3,790	980	2,525	735 1,130	1,895
	10	12½ 24	19% 15	12½	75/8	7,515	6,315	5,635	4,735	960 1,505	2,995	720 1,130	2,245
	31/8	61/4 71/2	5½ 5½	_	_	2,860	-	2,145	_	1,500 1,500	_	1,125 1,125	_
#5	5	8 1/8 12	83/ <sub>4</sub> 71/ <sub>2</sub>	81/8	5½	4,575	3,560	3,430	2,670	1,520 2,105	1,865	1,140 1,575	1,400
110	7 1/2	10% 18	14 111/4	10%	67/8	6,860	5,340	5,145	4,005	1,415 2,105	2,640	1,060 1,575	1,980
	12½	15% 30	24% 18¾	15%	9%	11,435	8,895	8,575	6,670	1,340 2,105	4,005	1,005 1,575	3,005
	31/2	71/4 81/2	6½ 6½	_	_	3,725	_	2,795	_	1,845 1,845	_	1,385 1,385	
#6	6	93/4	10%	9¾	61/2	6,385	4,555	4,790	3,415	2,000 2,765	2,260	1,500 2,075	1,695
	9	12¾ 21¾	16% 13½	12¾	81/8	9,575	6,835	7,180	5,125	1,860 2,765	3,235	1,395 2,075	2,425
	15	18¾ 36	291/8 221/2	18¾	11%	15,960	11,390	11,970	8,545	1,765 2,765	4,965	1,325 2,075	3,725
	33/4	81/8 9	7½ 7½	_	_	4,505	_	3,380	_	2,145 2,145	_	1,610 1,610	_
#7	7	11% 16%	117/8 101/2	11%	71/2	8,415	5,430	6,310	4,070	2,145 2,525 3,485	2,585	1,890 2,615	1,940
	10½	147/8 251/4	191/8 153/4	147/8	91/8	12,620	8,145	9,465	6,110	2,350 3,485 2,225	3,740	1,760 2,615	2,805
	17½	21%	33½ 26¼	21%	12¾	21,035	13,575	15,775	10,180	3.485	5,770	1,670 2,615	4,330
	4	9 95%	83% 83%	_	_	5,330		3,995	_	2,455 2,455	_	1,845 1,845	
#8	8	13 19¼ 17	13% 12 21½	13	83/8	10,660	6,095	7,995	4,570	3,085 4,265	2,810	2,315 3,200	2,110
	12	28%	18 37%	17	9¾	15,985	9,145	11,990	6,860	2,870 4,265	4,070	2,155 3,200	3,055
	20	25 48 111/4	30 101/8	25	13¾	26,645	15,240	19,985	11,430	2,720 4,265	6,380	3,200	4,785
	5	12 161/4	101/8 101/8 161/4	_	_	7,765	_	5,825	_	_	_	_	
#10	10	24 211/4	15 261/8	161/4	101/8	15,530	5,940	11,645	4,455	_		_	_
	15	36 311/4	20 1/8 22 1/2 46	211/4	101/8	23,295	8,910	17,470	6,680	_		_	_
	25	60	371/2	311/4	131/2	38,825	14,850	29,115	11,135	_	_	_	_

Rebar	Tension Design Strength of Rebar Steel (lb.)						
Size	ASTM A615 GR 60	ASTM A706 GR 60	3				
#3	6,435	5,720	5				
#4	11,700	10,400	6				
#5	18,135	16,120					
#6	25,740	22,880	7				
#7	35,100	31,200	] '				
#8	46,215	41,080	8				
#10	74,100	66,040					

- 1. Tension design strength must be the lesser of the concrete, bond or rebar steel design strength.
- Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 6. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 7. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 8. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



SET-XP $^{\odot}$  Allowable Tension Loads for Rebar in Normal-Weight Concrete (f' $_{\rm C}$  = 2,500 psi) — Static Load

	ı
IDC	
IDU	





Rebar Size	Nominal Embed. Depth		mensions for ked (in.)		mensions for ed (in.)				
	(in.)	ha	c <sub>ac</sub>	ha	Cac	Uncracked	Cracked	Uncracked	Cracked
	23/8	41⁄4 53⁄4	4 35%	_	_	985	_	545 640	_
	3	4 1/8 7 1/4	5% 4½	47/8	3½	1,245	500	515 710	325
#3	41/2	6% 10%	85% 63/4	6%	31/2	1,870	755	480 710	490
	6	71/8 141/2	11% 9	77/8	31/2	2,490	1,005	465 710	650
	71/2	9% 18	151/8 111/4	9%	31/2	3,110	1,255	455 710	815
	23/4	51/4 65/8	4½ 4½	_	_	1,475	_	845 845	_
	4	6½ 9%	7 6	6½	41/2	2,145	1,805	780 1,075	1,030
#4	6	8½ 14½	11% 9	8½	5½	3,220	2,705	725 1,075	1,455
	8	10½ 19¼	15% 12	10½	65/8	4,295	3,605	700 1,075	1,805
	10	12½ 24	19% 15	12½	75/8	5,370	4,510	685 1,075	2,140
	31/8	61/4 71/2	5½ 5½	_	_	2,045	_	1,070 1,070	_
#5	5	81/8 12	83/4 71/2	81/8	5½	3,270	2,545	1,085 1,505	1,330
#3	71/2	10% 18	14 111⁄4	10%	67/8	4,900	3,815	1,010 1,505	1,885
	12½	15% 30	245/8 183/4	15%	95/8	8,170	6,355	955 1,505	2,860
	31/2	71/4 81/2	6½ 6½	_	_	2,660	_	1,320 1,320	_
#6	6	9¾ 14½	10% 9	93/4	6½	4,560	3,255	1,430 1,975	1,615
#0	9	12¾ 21%	16% 13½	12¾	81/8	6,840	4,880	1,330 1,975	2,310
	15	18¾ 36	291/8 221/2	18¾	11%	11,400	8,135	1,260 1,975	3,545
	3¾	81/8 9	7½ 7½	_	_	3,220	_	1,530 1,530	_
#7	7	11% 16%	11% 10½	11%	7½	6,010	3,880	1,805 2,490	1,845
""	10½	14% 25¼	191/8 153/4	14%	91/8	9,015	5,820	1,680 2,490	2,670
	17½	21% 42	33½ 26¼	21%	12¾	15,025	9,695	1,590 2,490	4,120
	4	9 95%	8% 8%	_	_	3,805	_	1,755 1,755	_
#8	8	13 19¼	13% 12	13	8%	7,615	4,355	2,205 3,045	2,005
110	12	17 28%	21½ 18	17	9¾	11,420	6,530	2,050 3,045	2,905
	20	25 48	37% 30	25	13¾	19,030	10,885	1,945 3,045	4,555
	5	11¼ 12	101/8 101/8	_	_	5,545	_	_	_
#10	10	16¼ 24	16¼ 15	161/4	101/8	11,095	4,245	_	_
,,,,,	15	21¼ 36	261/8 221/2	211/4	101/8	16,640	6,365	_	_
	25	31 ¼ 60	46 37½	31 1/4	13½	27,730	10,605	_	_

Rebar Size	Allowable Tension Load of Rebar Steel (lb.)					
neuai size	ASTM A615 GR 60	ASTM A706 GR 60				
#3	4,595	4,085				
#4	8,355	7,430				
#5	12,955	11,515				
#6	18,385	16,345				
#7	25,070	22,285				
#8	33,010	29,345				
#10	52,930	47,170				

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or rebar steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

SIMPSON Strong-Tie

SET-XP $^{\odot}$  Allowable Tension Loads for Rebar in Normal-Weight Concrete (f' $_{\rm C}$  = 2,500 psi) — Wind Load

$\overline{}$			_
l	ı	<b>•</b>	.01
IIRC	ш		6. 9
IDU	ı	V P 2 1 1 1 1 1 1	
		25 S 1 2 S 2	

Rebar   Nominal			mensions for	Minimum Dimensions for		Allowable Te Edge Distan		d Based on Concrete or Bond (lb.)  Edge Distances = 1¾" on on		
enai Size	Embed. Depth (in.)	Uncracl	ked (in.)	Crack	ed (in.)	all s	ides		on three sides	
	(111.)	ha	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked	
	23/8	41/ <sub>4</sub> 53/ <sub>4</sub>	4 35/8	_	_	830	_	460 535	_	
	3	47/8 71/4	5% 4½	47/8	31/2	1,045	420	430 595	275	
#3	41/2	6% 10%	85/8 63/4	6%	31/2	1,570	635	400 595	410	
	6	7% 14½	11% 9	77/8	31/2	2,090	845	390 595	545	
	71/2	9% 18	151/8 111/4	9%	31/2	2,615	1,055	380 595	685	
	2¾	51/4 65/8	4½ 4½	_	_	1,240	_	710 710	_	
	4	6½ 9%	7	61/2	41/2	1,805	1,515	655 905	865	
‡4	6	8½ 14½	11% 9	81/2	51/2	2,705	2,275	610 905	1,220	
	8	10½ 19¼	15% 12	10½	6%	3,610	3,030	590 905	1,515	
	10	12½ 24	19% 15	12½	75/8	4,510	3,790	575 905	1,795	
	31/8	61/4 71/2	5½ 5½	_	_	1,715	_	900	_	
ŧ5	5	81/8 12	83/ <sub>4</sub> 71/ <sub>2</sub>	81/8	5½	2,745	2,135	910 1,265	1,120	
· O	71/2	10% 18	14 111⁄4	10%	67/8	4,115	3,205	850 1,265	1,585	
	12½	15% 30	24% 18¾	15%	95/8	6,860	5,335	805 1,265	2,405	
	31/2	71/ <sub>4</sub> 81/ <sub>2</sub>	6½ 6½	_	_	2,235	_	1,105 1,105	_	
6	6	9¾ 14½	10% 9	9¾	61/2	3,830	2,735	1,200 1,660	1,355	
-0	9	12¾ 21%	16% 13½	12¾	81/8	5,745	4,100	1,115 1,660	1,940	
	15	18¾ 36	29 1/8 22 1/2	18¾	113/8	9,575	6,835	1,060 1,660	2,980	
	3¾	81/8 9	7½ 7½		_	2,705	_	1,285 1,285	_	
<del>!</del> 7	7	11% 16%	11% 10½	11%	71/2	5,050	3,260	1,515 2,090	1,550	
1	10½	14% 25¼	191/8 153/4	147/8	91/8	7,570	4,885	1,410 2,090	2,245	
	17½	21 1/8 42	33½ 26¼	21%	12¾	12,620	8,145	1,335 2,090	3,460	
	4	9 95%	83/8 83/8	_	_	3,200	_	1,475 1,475	_	
8	8	13 19¼	13% 12	13	83/8	6,395	3,655	1,850 2,560	1,685	
0	12	17 28%	21½ 18	17	9¾	9,590	5,485	1,720 2,560	2,440	
	20	25 48	37% 30	25	13¾	15,985	9,145	1,630 2,560	3,830	
	5	111⁄4 12	101/8 101/8	_	_	4,660	_	_	_	
10	10	161⁄4 24	16¼ 15	161⁄4	101/8	9,320	3,565	_	_	
IU	15	21 ¼ 36	261/8 221/2	211/4	101/8	13,975	5,345	_		
	25	31 1/4 60	46 37½	311/4	13½	23,295	8,910	_		

Rebar	Allowable Tension Load of Rebar Steel (lb.)							
Size	ASTM A615 GR 60	ASTM A706 GR 60						
#3	3,860	3,430						
#4	7,020	6,240						
#5	10,880	9,670						
#6	15,445	13,730						
#7	21,060	18,720						
#8	27,730	24,650						
#10	44,460	39,625						

- 1. Allowable tension load must be the lesser of the concrete, bond or rebar steel load.
- 2. Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using  $\alpha$  conversion factor of  $\alpha$  = 167. The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



SET-XP $^{\odot}$  Allowable Tension Loads for Rebar in Normal-Weight Concrete (f' $_{\rm C}$  = 2,500 psi) — Seismic Load







(1 C - Z	2,500 psi)		imum										
Rebar	Nominal Embed.	Dimens	sions for acked	Dimens	ions for cked	Edg	Edge Distances = $c_{ac}$ on all sides			Edge	Distances =	= 1¾" on one three sides	side
Size	Depth (in.)	(i	n.)	(iı	n.)		A-B⁵		C-F <sup>6,7</sup>	SDC	A-B <sup>5</sup>	SDC	C-F <sup>6,7</sup>
	()	ha	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	23/8	41/ <sub>4</sub> 53/ <sub>4</sub>	4 35/8		_	965	_	725	_	535 625	_	405 470	_
	3	47/8 71/4	5% 4½	47/8	3½	1,220	490	915	370	505 695	320	380 520	240
#3	41/2	6% 10%	85/8 63/4	6%	31/2	1,830	740	1,370	555	470 695	480	355 520	355
	6	71/8 141/2	11% 9	77/8	31/2	2,440	985	1,830	740	455 695	635	340 520 335 520 620	480
	71/2	9% 18	151/8 111/4	9%	31/2	3,050	1,230	2,285	920	445 695 825	800	335 520	600
	23/4	51/4 65/8	4½ 4½	_	_	1,445	_	1,085	_	825 825	_	620 620	_
	4	6½ 9%	7 6	6½	41/2	2,105	1,770	1,580	1,325	825 765 1,055	1,010	620 570 790	755
#4	6	8½ 14½	11% 9	81/2	5½	3,155	2,655	2,365	1,990	710 1.055	1,425	530 790	1,070
	8	10½ 19¼	15% 12	10½	6%	4,210	3,535	3,155	2,655	685 1 055	1,770	515 790 505 790	1,325
	10	12½ 24	19% 15	12½	7%	5,260	4,420	3,945	3,315	670 1,055 1,050	2,095	505 790	1,570
	31/8	61/4 71/2	5½ 5½	_	_	2,000	_	1,500	_	1,050 1,050	_	790	_
#5	5	81/8 12	83/ <sub>4</sub> 71/ <sub>2</sub>	81/8	5½	3,205	2,490	2,400	1,870	1,050 1,050 1,065 1,475 990	1,305	800 1,105	980
#10	71/2	10% 18	14 111⁄4	10%	6%	4,800	3,740	3,600	2,805		1,850	740 1,105	1,385
	12½	15% 30	24% 18¾	15%	9%	8,005	6,225	6,005	4,670	940 1,475 1,290 1,290 1,400 1,935	2,805	1,105 740 1,105 705 1,105	2,105
	31/2	71/ <sub>4</sub> 81/ <sub>2</sub>	6½ 6½	_	_	2,610	_	1,955	_	1,290 1,290	_	970	_
#6	6	9¾ 14½	10% 9	9¾	61/2	4,470	3,190	3,355	2,390	1,400 1,935	1,580	1,050 1,455	1,185
#0	9	12¾ 21¾	16% 13½	12¾	81/8	6,705	4,785	5,025	3,590	1,300 1,935	2,265	975 1,455	1,700
	15	18¾ 36	291/8 221/2	18¾	11%	11,170	7,975	8,380	5,980	1,300 1,935 1,235 1,935 1,500	3,475	930 1,455	2,610
	3¾	81/8 9	7½ 7½	_	_	3,155		2,365		1,500 1,500		975 1,455 930 1,455 1,125 1,125 1,325 1,830 1,230 1,830	_
#7	7	11% 16%	11% 10½	11%	71/2	5,890	3,800	4,415	2,850	1,500 1,500 1,770 2,440 1,645 2,440	1,810	1,325 1,830	1,360
111	10½	14% 25¼	191/8 153/4	147/8	91/8	8,835	5,700	6,625	4,275	1,645 2,440	2,620	1,230 1,830	1,965
	17½	21 1/8 42	33½ 26¼	21%	12¾	14,725	9,505	11,045	7,125	1,560	4,040	1,170 1,830	3,030
	4	9 9% 13	8% 8%	_	_	3,730	_	2,795	_	1,720 1,720	_	1,290 1,290	_
#8	8	191/4	13% 12	13	8%	7,460	4,265	5,595	3,200	2,160 2,985	1,965	1,620 2,240	1,475
110	12	17 28%	21½ 18	17	93/4	11,190	6,400	8,395	4,800	1,720 1,720 2,160 2,985 2,010 2,985	2,850	1,290 1,290 1,620 2,240 1,510 2,240 1,430 2,240	2,140
	20	25 48	37% 30	25	13¾	18,650	10,670	13,990	8,000	1,905 2,985	4,465	1,430 2,240	3,350
	5	11 1/4 12	101/8 101/8	_	_	5,435		4,080	_	_	_	_	_
#10	10	161/4 24 211/4	16¼ 15	161⁄4	101//8	10,870	4,160	8,150	3,120	_	_	_	_
"10	15	36	26 1/8 22 1/2	211/4	101//8	16,305	6,235	12,230	4,675	_	_	_	_
	25	31 ½ 60	46 37½	311/4	13½	27,180	10,395	20,380	7,795	_		_	

Rebar	Allowable Tension Load of Rebar Steel (lb.)							
Size	ASTM A615 GR 60	ASTM A706 GR 60						
#3	4,505	4,005						
#4	8,190	7,280						
#5	12,695	11,285						
#6	18,020	16,015						
#7	24,570	21,840						
#8	32,350	28,755						
#10	51,870	46,230						

- 1. Allowable tension load must be the lesser of the concrete, bond or rebar steel load.
- 2. Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using  $\alpha$  conversion factor of  $\alpha$  = %.7 = 1.43. The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Allowable tension loads in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



SET-XP® Allowable Tension and Shear Loads for Threaded Rod and Rebar in the Face of Fully Grouted CMU Wall Construction  $^{\rm 1,\,3,\,4,\,5,\,6,\,8,\,9,\,10,\,11}$ 

IBC	<b>1</b>	<b>→</b>			
-----	----------	----------	--	--	--

Diameter (in.) or	Drill Bit Diameter (in.)	Minimum Embedment <sup>2</sup> (in.)	Allowable Load Based on Bond Strength <sup>7</sup> (lb.)					
Rebar Size Ńo.	Dilli bit Diailletei (III.)	Willimum Embedinent (iii.)	Tension Load	Shear Load				
Threaded Rod Installed in the Face of CMU Wall								
3/8	1/2	3%	1,490	1,145				
1/2	5%	41/2	1,825	1,350				
5/8	3/4	5%	1,895	1,350				
3/4	7/8	61/2	1,895	1,350				
	Reba	r Installed in the Face of CMU	Wall					
#3	1/2	3%	1,395	1,460				
#4	5/8	41/2	1,835	1,505				
#5	3/4	5%	2,185	1,505				

- 1. Allowable load shall be the lesser of the bond values shown in this table and steel values, shown on page 61.
- Embedment depth shall be measured from the outside face of masonry wall.
- Critical and minimum edge distance and spacing shall comply with the information on page 55. Figure 2 on page 55 illustrates critical and minimum edge and end distances.
- Minimum allowable nominal width of CMU wall shall be 8 inches.
   No more than one anchor shall be permitted per masonry cell.
- 5. Anchors shall be permitted to be installed at any location in the face of the fully grouted masonry wall construction (cell, web, bed joint), except anchors shall not be installed within 1½ inches of the head joint, as show in Figure 2 on page 55.
- Tabulated allowable load values are for anchors installed in fully grouted masonry walls.
- 7. Tabulated allowable loads are based on a safety factor of 5.0.
- Tabulated allowable load values shall be adjusted for increased base material temperatures in accordance with Figure 1 below, as applicable.
- 9. Threaded rod and rebar installed in fully grouted masonry walls are permitted to resist dead, live, seismic and wind loads.
- 10. Threaded rod shall meet or exceed the tensile strength of ASTM F1554, Grade 36 steel, which is 58,000 psi.
- 11. For installations exposed to severe, moderate or negligible exterior weathering conditions, as defined in Figure 1 of ASTM C62, allowable tension loads shall be multiplied by 0.80.

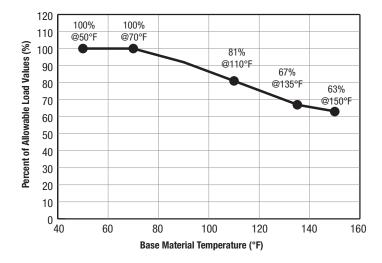


Figure 1. Load capacity based on in-service temperature for SET-XP® epoxy adhesive in the face of fully grouted CMU wall construction

<sup>\*</sup> See page 12 for an explanation of the load table icons.

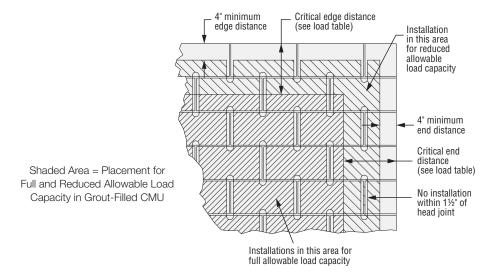


SET-XP® Edge Distance and Spacing Requirements and Allowable Load Reduction Factors – Threaded Rod and Rebar in the Face of Fully Grouted CMU Wall Construction7

		CARR O	
IBC	/ <del></del> \		

			Ed	ge or Edge Dis	tance <sup>1,8</sup>					Spacing <sup>2,9</sup>			
		Critical (F Capa	ull Anchor city) <sup>3</sup>	Minimum (	Reduced An	educed Anchor Capacity) <sup>4</sup>			Critical (Full Anchor Capacity) <sup>5</sup> Minimum (			Reduced Anchor Capacity) <sup>6</sup>	
Rod Dia. (in.) or Rebar Size No.	Minimum Embed. Depth (in.)	Critical Edge or End Distance, C <sub>cr</sub> (in.)	Allowable Load Reduction Factor	Minimum Edge or End Distance, C <sub>min</sub> (in.)	Allowable Load Reduction Factor		Critical Spacing, <i>S<sub>cr</sub></i> (in.)	Allowable Load Reduction Factor	Minimum Spacing, S <sub>min</sub> (in.)		ole Load on Factor		
110.	()	Load Di	irection		Load Direction		Load D	irection		Load Direction			
		Tension or	Tension or	Tension or	Shear <sup>10</sup>		Tension or	Tension or	Tension or	Tanaian	Chass		
		Shear	Shear	Shear	Tension	Perp.	Para.	Shear	Shear	Shear	Tension	Shear	
3/8	3%	12	1.00	4	0.91	0.72	0.94	8	1.00	4	1.00	1.00	
1/2	41/2	12	1.00	4	1.00	0.58	0.87	8	1.00	4	0.82	1.00	
5/8	5%	12	1.00	4	1.00	0.48	0.87	8	1.00	4	0.82	1.00	
3/4	61/2	12	1.00	4	1.00	0.44	0.85	8	1.00	4	0.82	1.00	
#3	3%	12	1.00	4	0.96	0.62	0.84	8	1.00	4	0.87	0.91	
#4	41/2	12	1.00	4	0.88	0.54	0.82	8	1.00	4	0.87	0.91	
#5	5%	12	1.00	4	0.88	0.43	0.82	8	1.00	4	0.87	1.00	

- Edge distance (C<sub>Cr</sub> or C<sub>min</sub>) is the distance measured from anchor centerline to edge or end of CMU masonry wall. Refer to Figure 2 below for an illustration showing critical and minimum edge and end distances.
- 2. Anchor spacing (S<sub>cr</sub> or S<sub>min</sub>) is the distance measured from centerline to centerline of two anchors.
- 3. Critical edge distance,  $C_{cr}$ , is the least edge distance at which tabulated allowable load of an anchor is achieved where a load reduction factor equals 1.0 (no load reduction).
- 4. Minimum edge distance, C<sub>min</sub>, is the least edge distance where an anchor has an allowable load capacity which shall be determined by multiplying the allowable loads assigned to anchors installed at critical edge distance, C<sub>cn</sub> by the load reduction factors shown above.
- Critical spacing, S<sub>cn</sub> is the least anchor spacing at which tabulated allowable load of an anchor is achieved such that anchor performance is not influenced by adjacent anchors.
- 6. Minimum spacing,  $S_{min}$ , is the least spacing where an anchors has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical spacing distance,  $S_{cr}$ , by the load reduction factors shown above.
- Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.
- Load reduction factor for anchors loaded in tension with spacing between critical and minimum shall be obtained by linear interpolation.
- 10. Perpendicular shear loads act towards the edge or end. Parallel shear loads act parallel to the edge or end (see Figure 5 on page 57). Perpendicular and parallel shear load reduction factors are cumulative when the anchor is located between the critical minimum edge and end distance.



**Figure 2.** Allowable anchor locations for full and reduced load capacity when installation is in the face of fully grouted CMU masonry wall construction

<sup>\*</sup> See page 12 for an explanation of the load table icons.



SET-XP® Allowable Tension and Shear Loads for Threaded Rod and Rebar in the Top of Fully Grouted CMU Wall Construction<sup>1, 2, 4, 5, 6, 7, 9, 10, 11, 12</sup>

IDO	<b>1</b>	<b></b>	்யீ	*
IBC	20 20	530 530		

Diameter (in.) or	Drill Bit Diameter	Minimum Embedment <sup>3</sup>	Allowable Load Based on Bond Strength <sup>7,8</sup> (lb.)					
Rebar Size Ńo.	(in.)	(in.)	Tension Load	Shear Perp.	Shear Parallel			
	Threaded Rod Installed in the Top of CMU Wall							
1/2	5/8	41/2	1,485	590	1,050			
72	78	12	2,440	665	1,625			
E/	3/4	5%	1,700	565	1,435			
5/8	74	15	2,960	660	1,785			
3/4	7/8	61/2	1,610	735	1,370			
74		21	4,760	670	1,375			
		Rebar Instal	led in the Top of CMU Wall					
#4	5/8	41/2	1,265	550	865			
#4	78	12	2,715	465	1,280			
#5	3/.	5%	1,345	590	1,140			
#3	3/4	15	3,090	590	1,285			

- 1. Allowable load shall be the lesser of the bond values shown in this table and steel values, shown on page 61.
- 2. Allowable loads are for installation in the grouted CMU core opening.
- 3. Embedment depth shall be measured from the horizontal surface of the grouted CMU core opening on top of the masonry wall.
- 4. Critical and minimum edge distance, end distance and spacing shall comply with the information on pages 57 and 58. Figures 3A and 3B on page 57 illustrate critical and minimum edge and end distances.
- 5. Minimum allowable nominal width of CMU wall shall be 8 inches (203 mm).
- 6. Anchors are permitted to be installed in the CMU core opening shown in Figures 3A and 3B on page 57. Anchors are limited to one installation per CMU core opening.
- 7. Tabulated allowable load values are for anchors installed in fully grouted masonry walls.
- 8. Tabulated allowable loads are based on a safety factor of 5.0 .
- 9. Tabulated allowable load values shall be adjusted for increased base material temperatures in accordance with Figure 1 on page 54, as applicable.
- 10. Threaded rod and rebar installed in fully grouted masonry walls with SET-XP® adhesive are permitted to resist dead, live, seismic and wind loads.
- 11. Threaded rod shall meet or exceed the tensile strength of ASTM F1554, Grade 36 steel, which is 58,000 psi.
- 12. For installations exposed to severe, moderate or negligible exterior weathering conditions, as defined in Figure 1 of ASTM C62, allowable tension loads shall be multiplied by 0.80.



SET-XP® Edge and End Distance Requirements and Allowable Load Reduction Factors — Threaded Rod and Rebar in the Top of Fully Grouted CMU Wall Construction<sup>1,4,5</sup>

	<b>□</b> E3	(See )	ď
<b>IBC</b>			l

Critical (Full A		Full Anchor C	apacity) <sup>2</sup>	Minimum End (Reduced Anchor Capacity) <sup>3</sup>			Minimum Edge (Reduced Anchor Capacity) <sup>6</sup>						
Rod Dia. (in.) or Rebar Size No.	Minimum Embed. Depth (in.)	Critical Edge, <i>C<sub>cr</sub></i> (in.)	Critical End Distance, <i>C<sub>cr</sub></i> (in.)	Allowable Load Reduction Factor	Minimum End Distance, <i>C<sub>min</sub></i> (in.)		End Allowable eduction Fac		Minimum Edge, <i>C<sub>min</sub></i> (in.)		llowable Loa eduction Fac		
			Load Direction	1		Load D	irection			Load D	irection		
		Tension or	Tension or	Tension or	Tension or	Tension	Sh	ear <sup>6</sup>	Tension or	Tension		ear <sup>6</sup>	
		Shear	Shear	Shear	Shear	Shear Shear	Shear	Perp.	Parallel	Shear	101131011	Perp.	Parallel
1/2	41/2	2¾	20	1.00	313/16	0.88	0.84	0.66	13/4	0.83	0.63	0.77	
/2	12	2¾	20	1.00	313/16	0.64	0.91	0.34	13/4	0.95	0.55	0.69	
5/8	5%	2¾	20	1.00	41/4	0.90	1.00	0.50	13/4	0.82	0.57	0.71	
78	15	23/4	20	1.00	41/4	0.38	0.85	0.29	13/4	0.91	0.72	0.73	
7/8	77/8	23/4	20	1.00	41/4	0.98	0.72	0.57	_	_	_	_	
'/8	21	23/4	20	1.00	41/4	0.63	0.96	0.64	_	_	_	_	
#4	41/2	23/4	20	1.00	41/4	0.96	0.90	0.76	_	_	_	_	
#4	12	23/4	20	1.00	41/4	0.58	1.00	0.46	_	_	_	_	
#5	5%	23/4	20	1.00	41/4	1.00	0.86	0.60	_	_	_	_	
#3	15	23/4	20	1.00	41/4	0.41	0.76	0.49	_		_	_	

- 1. Edge and end distances ( $C_{Cr}$  or  $C_{min}$ ) are the distances measured from anchor centerline to edge or end of CMU masonry wall. Refer to Figures 3A and 3B below for illustrations showing critical and minimum edge and end distances.
- Critical edge and end distances, C<sub>Cr,</sub> are the least edge distances at which tabulated allowable load of an anchor is achieved where a load reduction factor equals 1.0 (no load reduction).
- 3. Minimum edge and end distances,  $C_{min}$ , are the least edge distances where an anchor has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical edge distance,  $C_{Cr}$ , by the load reduction factors shown above.
- Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- 5. Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.
- 6. Perpendicular shear loads act towards the edge or end. Parallel shear loads act parallel to the edge or end (see Figure 5 below). Perpendicular and parallel shear load reduction factors are cumulative when the anchor is located between the critical minimum edge and end distance.

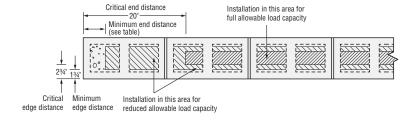


Figure 3A. Allowable anchor locations of ½"- and 5%"-diameter threaded rod for full and reduced load capacity when installation is in the top of fully grouted CMU masonry wall construction

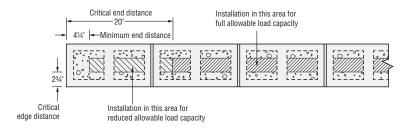
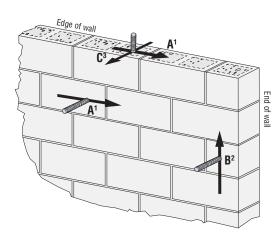


Figure 3B. Allowable anchor locations of %"-diameter threaded rod and #4 and #5 rebar for full and reduced load capacity when installation is in the top of fully grouted CMU masonry wall construction



- 1. Direction of shear load A is parallel to edge of wall and perpendicular to end of wall.
- 2. Direction of shear load B is parallel to end of wall and perpendicular to edge of wall.
- 3. Direction of shear load C is perpendicular to edge of wall.

**Figure 5.** Direction of shear load in relation to edge and end of wall

<sup>\*</sup> See page 12 for an explanation of the load table icons.



SET-XP® Spacing Distance Requirements and Allowable Load Reduction Factors — Threaded Rod and Rebar in the Top of Fully Grouted CMU Wall Construction<sup>1,4,5</sup>

1	$\overline{}$	1
	IDC	
	IDU	







		Critical ( (Full Ancho	Spacing r Capacity)²	Minimum Spacing (Reduced Anchor Capacity) <sup>3</sup>			
Rod Dia. (in.) or Rebar Size No.	Minimum Embed. Depth	Critical Spacing, $S_{cr}$ (in.)	Allowable Load Reduction Factor	Minimum Spacing, $S_{cr}$ (in.)	Allowable Load	Reduction Factor	
	(in.)	Load Di	rection		Load Direction		
		Tension or Shear	Tension or Shear	Tension or Shear	Tension	Shear	
1/2	41/2	18	1.00	8	0.80	0.92	
1/2	12	48	1.00	8	0.63	0.98	
5/8	5%	22.5	1.00	8	0.86	1.00	
78	15	60	1.00	8	0.56	1.00	
7/8	77/8	31.5	1.00	8	0.84	0.82	
1/8	21	84	1.00	8	0.51	0.98	
#4	41/2	18	1.00	8	0.97	0.93	
#4	12	48	1.00	8	0.75	1.00	
#5	5%	22.5	1.00	8	1.00	1.00	
#5	15	60	1.00	8	0.82	1.00	

<sup>1.</sup> Anchor spacing ( $S_{cr}$  or  $S_{min}$ ) is the distance measured from centerline to centerline of two anchors.

<sup>2.</sup> Critical spacing,  $S_{cr}$ , is the least anchor spacing at which tabulated allowable load of an anchor is achieved such that anchor perofrmance is not influenced by adiacent anchors.

<sup>3.</sup> Minimum spacing,  $S_{min}$ , is the least spacing where an anchor has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical spacing distance,  $S_{cr}$ , by the load reduction factors shown above.

<sup>4.</sup> Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.

<sup>5.</sup> Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.



SET-XP® Allowable Tension and Shear Loads – Threaded Rod in the Face of Hollow CMU Wall Construction  $^{1,3,4,5,6,8,9,10,11}$ 

IBC		<b>→</b>		
-----	--	----------	--	--

Diameter	Drill Bit Diameter	Minimum Embed <sup>2</sup>	Allowable Load Based	on Bond Strength <sup>7</sup> (lb.)		
(in.)	(in.)	(in.)	Tension	Shear		
3/8	9/16	11⁄4	245	415		
1/2	3/4	11⁄4	245	505		
5/8	7/8	11/4	290	530		

- 1. Allowable load shall be the lesser of bond values shown in this table and steel values shown on page 61.
- 2. Embedment depth is considered the minimum wall thickness of 8" x 8" x 16" ASTM C90 concrete masonry blocks, and is measured from the outside to the inside face of the block wall. The minimum length Opti-Mesh plastic screen tube for use in hollow CMU is 3½".
- 3. Critical and minimum edge distance and spacing shall comply with the information provided on page 60. Figure 4 on page 60 illustrates critical and minimum edge and end distances.
- 4. Anchors are permitted to be installed in the face shell of hollow masonry wall construction as shown in Figure 4.
- 5. Anchors are limited to one or two anchors per masonry cell and must comply with the spacing and edge distance requirements provided.
- 6. Tabulated load values are for anchors installed in hollow masonry walls.
- 7. Tabulated allowable loads are based on a safety factor of 5.0.
- 8. Tabulated allowable load values shall be adjusted for increased base material temperatures in accordance with Figure 1 on page 54, as applicable.
- 9. Threaded rods installed in hollow masonry walls with SET-XP® adhesive are permitted to resist dead, live load and wind load applications.
- 10. Threaded rods must meet or exceed the tensile strength of ASTM F1554, Grade 36, which is 58,000 psi.
- 11. For installations exposed to severe, moderate or negligible exterior weathering conditions, as defined in Figure 1 of ASTM C62, allowable tension loads must be multiplied by 0.80.



SET-XP® Edge, End and Spacing Distance Requirements and Allowable Load Reduction Factors — Threaded Rod in the Face of Hollow CMU Wall Construction<sup>7</sup>

BC	<b>○</b>	

		Edg	e or End Distan	ce <sup>1,8</sup>		Spacing <sup>2,9</sup>						
	Critical (Full An	chor Capacity) <sup>3</sup>	Minimum (F	Reduced Ancho	r Capacity)4	Crit (Full Ancho	ical r Capacity)⁵	Minimum (F	Minimum (Reduced Anchor Capacity) <sup>6</sup>			
Rod Diameter (in.)	Critical Edge or End Distance, <i>C<sub>cr</sub></i> (in.)	Allowable Load Reduction Factor	Minimum Edge or End Distance, <i>C<sub>min</sub></i> (in.)	Allowable Load Reduction Factor		Critical Spacing, <i>S<sub>cr</sub></i> (in.)	Allowable Load Reduction Factor	Minimum Spacing, S <sub>min</sub> (in.)	Allowable Load Reduction Factor			
	Load Di	irection		Load Direction		Load Direction		Load Direction				
	Tension or Shear	Tension or Shear	Tension or Shear	Tension	Shear <sup>10</sup>	Tension or Shear	Tension or Shear	Tension or Shear	Tension	Shear		
3/8	12	1.00	4	0.71	0.57	8	1.00	4	0.56	0.92		
1/2	12	1.00	4	0.73	0.51	8	1.00	4	0.61	0.85		
5/8	12	1.00	4	0.66	0.49	8	1.00	4	0.65	0.76		

- Edge and end distances (C<sub>cr</sub> or C<sub>min</sub>) are the distances measured from anchor centerline to edge or end of CMU masonry wall. Refer to Figure 4 below for an illustration showing critical and minimum edge and end distances.
- 2. Anchor spacing  $(S_{Cr} \circ S_{min})$  is the distance measured from centerline to centerline of two anchors.
- 3. Critical edge and end distances,  $C_{cr}$ , are the least edge distances at which tabulated allowable load of an anchor is achieved where a load reduction factor equals 1.0 (no load reduction).
- 4. Minimum edge and end distances, C<sub>min</sub>, are the least edge distances where an anchor has an allowable load capacity which shall be determined by multiplying the allowable loads assigned to anchors installed at critical edge distance, C<sub>Cr</sub>, by the load reduction factors shown above.
- Critical spacing, S<sub>Cr</sub>, is the least anchor spacing at which tabulated allowable load of an anchor is achieved such that anchor performance is not influenced by adjacent anchors.
- 6. Minimum spacing,  $S_{min}$ , is the least spacing where an anchors has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical spacing distance,  $S_{Cr}$ , by the load reduction factors shown above.
- 7. Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- 8. Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.
- 9. Load reduction factor for anchors loaded in tension with spacing between critical and minimum shall be obtained by linear interpolation.
- 10. Perpendicular shear loads act toward the edge or end. Parallel shear loads act parallel to the edge or end (see Figure 5 on page 57). Perpendicular and parallel shear load reduction factors are cumulative when the anchor is located between the critical minimum edge and end distance.

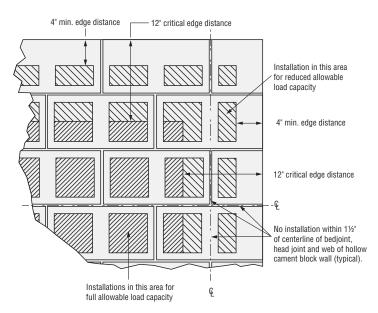


Figure 4. Allowable anchor locations for full and reduced load capacity when installation is in the face of hollow CMU masonry wall construction

<sup>\*</sup> See page 12 for an explanation of the load table icons



# SET-XP® Allowable Tension and Shear Loads — Threaded Rod Based on Steel Strength<sup>1</sup>

IBC		<b>→</b>	*
-----	--	----------	---

		Tension	Load Based o	n Steel Streng	jth² (lb.)	Shear I	Load Based on	Steel Strengt	h <sup>3</sup> (lb.)	
Threaded Rod Tensil	Tensile Stress			Stainless Steel				Stainless Steel		
Diameter (in.)		ASTM F1554 Grade 36 <sup>4</sup>	ASTM A193 Grade B7 <sup>6</sup>	ASTM A193 Grade B6 <sup>5</sup>	ASTM A193 Grades B8 and B8M <sup>7</sup>	ASTM F1554 Grade 36 <sup>4</sup>	ASTM A193 Grade B7 <sup>6</sup>	ASTM A193 Grade B6 <sup>5</sup>	ASTM A193 Grades B8 and B8M <sup>7</sup>	
3/8	0.078	1,495	3,220	2,830	1,930	770	1,660	1,460	995	
1/2	0.142	2,720	5,860	5,155	3,515	1,400	3,020	2,655	1,810	
5/8	0.226	4,325	9,325	8,205	5,595	2,230	4,805	4,225	2,880	
3/4	0.334	6,395	13,780	12,125	8,265	3,295	7,100	6,245	4,260	
7/8	0.462	8,845	19,055	16,770	11,435	4,555	9,815	8,640	5,890	

- 1. Allowable load shall be the lesser of bond values given on pages 54, 56 or 59 and steel values in the table above.
- 2. Allowable Tension Steel Strength is based on the following equation:  $F_{V} = 0.33 \times F_{U} \times Tensile$  Stress Area.
- 3. Allowable Shear Steel Strength is based on the following equation:  $F_V = 0.17 \times F_U \times Tensile$  Stress Area.
- 4. Minimum specified tensile strength ( $F_U$  = 58,000 psi) of ASTM F1554, Grade 36 used to calculate allowable steel strength.
- 5. Minimum specified tensile strength ( $F_U = 110,000$  psi) of ASTM A193, Grade B6 used to calculate allowable steel strength.
- 6. Minimum specified tensile strength ( $F_U$  = 125,000 psi) of ASTM A193, Grade B7 used to calculate allowable steel strength.
- 7. Minimum specified tensile strength ( $F_U = 75,000$  psi) of ASTM A193, Grades B8 and B8M used to calculate allowable steel strength.

# SET-XP® Allowable Tension and Shear Loads — Deformed Reinforcing Bar Based on Steel Strength¹



		Tension	Load (lb.)	Shear Load (lb.)  Based on Steel Strength			
Rebar Size	Tensile Stress Area	Based on S	teel Strength				
	(in.²)	ASTM A615 Grade 40 <sup>2</sup>	ASTM A615 Grade 60 <sup>3</sup>	ASTM A615 Grade 40 <sup>4,5</sup>	ASTM A615 Grade 60 <sup>4,6</sup>		
#3	0.11	2,200	2,640	1,310	1,685		
#4	0.20	4,000	4,800	2,380	3,060		
#5	0.31	6,200	7,400	3,690	4,745		

- 1. Allowable load shall be the lesser of bond values given on pages 54, 56 or 59 and steel values in the table above.
- 2. Allowable Tension Steel Strength is based on AC58 Section 3.3.3 (20,000 psi x tensile stress area) for Grade 40 rebar.
- 3. Allowable Tension Steel Strength is based on AC58 Section 3.3.3 (24,000 psi x tensile stress area) for Grade 60 rebar.
- 4. Allowable Shear Steel Strength is based on AC58 Section 3.3.3 ( $F_v = 0.17 \times F_u \times Tensile Stress Area.$ )
- $5. F_u = 70,000$  psi for Grade 40 rebar.
- 6.  $F_u$  = 90,000 psi for Grade 60 rebar.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

### ET-HP® Epoxy Adhesive

SIMPSON
Strong-Tie

ET-HP® is a two-component, high-solids, epoxy-based system for use as a high-strength, non-shrink anchor-grouting material. Resin and hardener are dispensed and mixed simultaneously through the mixing nozzle. ET-HP® is formulated for anchoring threaded rod and rebar into concrete (cracked/uncracked) and masonry.

### **Features**

- Passed the demanding ICC-ES AC308 adverse-condition tests pertaining to elevated temperatures and long-term sustained loads
- Code listed under the IBC/IRC for cracked and uncracked concrete per ICC-ES ESR-3372
- Code listed under the IBC/IRC for masonry per IAPMO UES ER-241
- Suitable for use under static and seismic loading conditions in cracked and uncracked concrete and masonry
- Cure times: 24 hours at 80°F, 72 hours at 50°F
- Easy hole-cleaning no power-brushing required
- Suitable for use in dry or water-saturated concrete
- · When properly mixed, adhesive will be a uniform gray color
- Available in 22 oz. and 56 oz. cartridges for application versatility
- Manufactured in the USA using global materials

### **Applications**

- Threaded rod anchoring and rebar doweling into concrete and unreinforced masonry
- · Suitable for horizontal, vertical and overhead applications
- Multiple DOT listings refer to www.strongtie.com/DOT for current approvals

**Codes:** ICC-ES ESR-3372 (concrete); ICC-ES ESR-3638 (unreinforced masonry); IAPMO UES ER-241 (masonry); City of L.A. RR25120 (unreinforced masonry); AASHTO M-235 and ASTM C881 (Type IV, Grade 3, Class C); multiple DOT listings; FL-17449.1; FL-16230.2.

### Chemical Resistance

See pages 320-321.

### Installation and Application Instructions

(See also pages 124-127.)

- Surfaces to receive epoxy must be clean.
- Base material temperature must be 50°F or above at the time of installation. For best results, material should be 70°–80°F at time of application.
- To warm cold material, store cartridges in a warm, uniformly heated area or storage container. Do not immerse cartridges in water to facilitate warming.
- Mixed material in nozzle can harden in 30 minutes at temperatures of 70°F and above.





### Design Example

See pages 324 and 328.

### Suggested Specifications

See www.strongtie.com for more information.



### ET-HP® Epoxy Adhesive



### **Test Criteria**

Anchors installed with ET-HP® adhesive have been tested in accordance with ICC-ES Acceptance Criteria for Post-Installed *Adhesive Anchors in Masonry Elements* (AC58) and *Adhesive Anchors in Concrete Elements* (AC308).

Property	Test Method	Result*
Consistency	ASTM C881	Non-sag/thixotropic paste
Heat deflection	ASTM D648	133°F (56°C)
Glass transition temperature	ASTM D648	168°F (76°C)
Bond strength (moist cure, 60°F)	ASTM C882	2,300 psi (2 days) 2,440 psi (14 days)
Water absorption	ASTM D570	0.34% (24 hours)
Compressive yield strength (cured 60°F)	ASTM D695	16,300 psi (7 days)
Compressive modulus	ASTM D695	595,500 psi (7 days)
Gel time	ASTM C881	10 minutes – 60 gram mass 30 minutes – thin film
Shore D Durometer	ASTM D2240	87
Volatile Organic Compound (VOC)	_	3 g/L

<sup>\*</sup>Material and curing conditions: 73  $\pm$  2°F unless otherwise noted.

### ET-HP® Cartridge Systems

Model No.	Capacity ounces	Cartridge Type	Carton Quantity	Dispensing Tools	Mixing Nozzle
ET-HP22-N <sup>4</sup>	22	Side-by-side	10	EDT22S EDTA22CKT	EMN22i
ET-HP22	22	Side-by-side	10	EDTA22CKT EDTA22P	EMN22i
ET-HP56	56	Side-by-side	6	EDTA56P	EMN22i or EMN50

- 1. Cartridge estimation guidelines are available at www.strongtie.com/apps.
- Detailed information on dispensing tools, mixing nozzles and other adhesive accessories is available on pages 128 through 135, or at www.strongtie.com.
- 3. Use only Simpson Strong-Tie® mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair ET-HP adhesive performance.
- 4. One EMN22i mixing nozzle and one nozzle extension are supplied with each cartridge.

### Cure Schedule

Base N Tempe	Cure Time	
°F	°C	111113
50	10	72 hrs.
60	16	24 hrs.
80	27	24 hrs.
100	38	24 hrs.

For water-saturated concrete, the cure times must be doubled.



ET-HP® Installation Information and Additional Data for Threaded Rod and Rebar in Normal-Weight Concrete<sup>1</sup>







Characteriatio	Characteristic		Symbol Units		Nom	inal Anchor	Diameter (	in.) / Rebar	Size	
Glididelelistic				% / #3	1/2 / #4	5% / #5	3/4 / #6	7⁄8 / # <b>7</b>	1 / #8	11/4 / #10
Installation Information										
Drill Bit Diameter		d <sub>hole</sub>	in.	1/2	5/8	3/4	7/8	1	11/8	13/8
Maximum Tightening Torque		T <sub>inst</sub>	ftlb.	10	20	30	45	60	80	125
Permitted Embedment Depth Range	Minimum	h <sub>ef</sub>	in.	23/8	23/4	31/8	31/2	3¾	4	5
remilled Embedment Depth hange	Maximum	h <sub>ef</sub>	in.	41/2	6	7 1/2	9	10½	12	15
Minimum Concrete Thicknes	S	h <sub>min</sub>	in.	h <sub>ef</sub> + 5d <sub>o</sub>						
Critical Edge Distance <sup>2</sup>	Cac	in.	See foonote 2							
Minimum Edge Distance		C <sub>min</sub>	in.	1¾					23/4	
Minimum Anchor Spacing		Smin	in.			;	3			6

<sup>1.</sup> The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.

 $[h/h_{ef}] \leq 2.4$ 

 $\tau_{k,uncr}$  = the characteristic bond strength in uncracked concrete, given in the tables that follow  $\leq k_{uncr} \left( \left( h_{ef} \times f_C' \right)^{0.5} / \left( T \times d_a \right) \right)$ 

h =the member thickness (inches)

 $h_{ef}$  = the embedment depth (inches)

<sup>2.</sup>  $c_{ac} = h_{ef}(\tau_{k,uncr}/1160)^{0.4} \times [3.1 - 0.7(h/h_{ef})]$ , where:



ET-HP®	HP® Tension Strength Design Data for Threaded Rod in Normal-Weight Concrete1										
	Characteristic		Symbol	Unite			Nominal	Anchor Dian	neter (in.)		
	Glididelelistic		Syllibul	UIIILS	3/8	1/2	5/8	3/4	7/5	1	1¼
			Steel	Streng	jth in Tensi	on					
	Minimum Tensile Stress Area		A <sub>se</sub>	in. <sup>2</sup>	0.078	0.142	0.226	0.334	0.462	0.606	0.969
	Tension Resistance of Steel — ASTM I	1554, Grade 36			4,525	8,235	13,110	19,370	26,795	35,150	56,200
	Tension Resistance of Steel — ASTM A	193, Grade B7			9,750	17,750	28,250	41,750	57,750	75,750	121,125
nou (	Tension Resistance of Steel — Type 4 (ASTM A193, Grade B6)	10 Stainless	N <sub>sa</sub>	lb.	8,580	15,620	24,860	36,740	50,820	66,660	106,590
	Tension Resistance of Steel — Type 304 and 316 Stainless (ASTM A193, Grade B8 & B8M)				4,445	8,095	12,880	19,040	26,335	34,540	55,235
	Strength Reduction Factor — Steel Fa	lure	φ	_	0.756						
	Co	ncrete Breakou	t Strengt	th in Te	nsion (2,50	$0 \text{ psi} \leq f'_{\text{C}} \leq$	8,000 psi)12				
Effectiveness Factor — Uncracked Concrete $k_{uncr}$ — 24											
Effectivene	ess Factor — Cracked Concrete		Kcr	_	<del>-</del> 17						
Strength R	Reduction Factor — Breakout Failure		φ	_	0.65 <sup>8</sup>						
		Bond Strer	gth in Te	nsion (	2,500 psi ≤	f' <sub>c</sub> ≤ 8,000	psi) <sup>12</sup>				
Uncracked	Characteristic Bond Strength <sup>5,13</sup>		$ au_{k,uncr}$	psi	390	380	370	360	350	335	315
Concrete	Dayne itted Fush advacut Double Days	Minimum	6	4.0	2%	23/4	31/8	3½	3¾	4	5
2,3,4	Permitted Embedment Depth Range	Maximum	h <sub>ef</sub>	in.	41/2	6	71/2	9	101/2	12	15
Crooked	Characteristic Bond Strength <sup>5,9,10,11,12,13</sup>		$ au_{k,cr}$	psi	160	200	160	205	190	165	140
Cracked Concrete	2 11 15 1 1 12 11 2	Minimum			23/8	23/4	31/8	3½	3¾	4	5
2,3,4 F	Permitted Embedment Depth Range	Maximum	h <sub>ef</sub>	in.	41/2	6	7½	9	10½	12	15
	Bond Strength	in Tension — B	ond Stre	ngth Re	eduction Fa	ctors for Pe	riodic Spec	al Inspectio	n		
Strength Reduction Factor — Dry Concrete		$\phi_{dry}$					0.657				

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- Temperature Range: Maximum short-term temperature of 150°F (66°C). Maximum long-term temperature of 110°F (43°C).

Strength Reduction Factor — Water-Saturated Concrete

- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term concrete temperatures are constant temperatures over a significant time period.
- 5. For anchors that only resist wind or seismic loads, bond strengths may be multiplied by 2.70.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

- 6. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of  $\phi$ .
- 7. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value
- The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition A are met, refer to Section D.4.4 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of  $\phi$ .

9. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for 3/8" and 11/4" anchors must be multiplied by

 $0.45^{7}$ 

- 10. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for ½", %" and ¾" anchors must be multiplied by  $\alpha_{N,seis} = 0.85$ .
- 11. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for %" anchors must be multiplied by  $\alpha_{N,seis} = 0.82.$
- 12. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for 1" anchors must be multiplied by  $\alpha_{N,seis} = 0.70.$
- 13. For applications where maximum short-term temperature is 110°F (43°C) and the maximum long-term temperature is 75°F (24°C), bond strengths may be multiplied by 3.50. No additional increase is permitted for anchors that only resist wind or seismic loads.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



### IBC







### ET-HP® Tension Strength Design Data for Rebar in Normal-Weight Concrete<sup>1</sup>

	Characteristic		Symbol	Units		Rebar Size					
	Gildracteristic		Symbol	UIIILS	#3	#4	#5	#6	#7	#8	#10
Steel Strength in Tension											
Minimum Tensile Stress Area			A <sub>se</sub>	in <sup>2</sup>	0.11	0.2	0.31	0.44	0.6	0.79	1.23
Rebar	Tension Resistance of Steel — Rebar (AST	N <sub>sa</sub>	lb.	9,900	18,000	27,900	39,600	54,000	71,100	110,700	
	Strength Reduction Factor – Steel Failure			_				$0.65^{6}$			
	Concret	e Breakout Streng	th in Tensio	n (2,500 ps	$i \le f'_{c} \le 8$	,000 psi)					
Effectiveness Factor — Uncracked Concrete			<i>k</i> <sub>uncr</sub>	_				24			
Effectiveness Factor — Cracked Concrete				_	17						
Strength Reduction Factor — Breakout Failure				_				0.658			
	E	Bond Strength in Te	ension (2,50	0 psi ≤ f' <sub>c</sub> ≤	8,000 ps	si)					
	Characteristic Bond Strengt	$ au_{k,uncr}$	psi	370	360	350	335	325	315	295	
Uncracked Concrete 2,3,4	0 11 15 1 1 10 11 0	Minimum		1	2%	2¾	31/8	3½	3¾	4	5
	Permitted Embedment Depth Range	Maximum	h <sub>ef</sub>	in.	41/2	6	71/2	9	10½	12	15
	Characteristic Bond Strengt	h <sup>5,9</sup>	$ au_{k,cr}$	psi	130	140	155	165	180	190	215
Cracked Concrete 2,3,4	Dayso: tto d Fash adas ant Danth Days	Minimum	<u></u>	in	2%	2¾	31/8	3½	3¾	4	5
	Permitted Embedment Depth Range	Maximum	h <sub>ef</sub>	in.	41/2	6	71/2	9	10½	12	15
	Bond Strength in Tension - B	ond Strength Red	uction Facto	rs for Perio	dic and C	ontinuous	Special I	nspection			
	Strength Reduction Factor — Dry Concrete		$\phi_{dry}$	_	0.65 <sup>7</sup>						
Strer	ngth Reduction Factor — Water-saturated Co	ncrete	$\phi_{sat}$	_				0.457			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- 2. Temperature Range: Maximum short-term temperature of 150°F (66°C). Maximum long-term temperature of 110°F (43°C).
- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term concrete temperatures are constant temperatures over a significant time period.
- 5. For anchors that only resist wind or seismic loads, bond strengths may be multiplied by 2.70.
- 6. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of  $\phi$ .
- 7. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of  $\phi$ .
- 8. The value of *φ* applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.4 (c) for Condition A are met, refer to Section D.4.4 to determine the appropriate value of *φ*. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.5 to determine the appropriate value of *φ*.
- 9. For applications where maximum short-term temperature is 110°F (43°C) and the maximum long-term temperature is 75°F (24°C), bond strengths may be multiplied by 3.50. No additional increase is permitted for anchors that only resist wind or seismic loads.



**Adhesive** Anchors

### ET-HP® Shear Strength Design Data for Threaded Rod in Normal-Weight Concrete<sup>1</sup>

IBC	<b>→</b>		
-----	----------	--	--

	Charactaristia	Cumbal	Unito	Nominal Anchor Diameter (in.)						
	Characteristic	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	11/4
	Steel Strengt	h in Shea	ır							
	Minimum Shear Stress Area	Ase	in. <sup>2</sup>	0.078	0.142	0.226	0.334	0.462	0.606	0.969
	Shear Resistance of Steel — ASTM F1554, Grade 36			2,260	4,940	7,865	11,625	16,080	21,090	33,720
	Shear Resistance of Steel — ASTM A193, Grade B7	V <sub>sa</sub>		4,875	10,650	16,950	25,050	34,650	45,450	72,675
	Shear Resistance of Steel — Type 410 Stainless (ASTM A193, Grade B6)		lb.	4,290	9,370	14,910	22,040	30,490	40,000	63,955
Threaded Rod	Shear Resistance of Steel — Type 304 and 316 Stainless (ASTM A193, Grade B8 & B8M)			2,225	4,855	7,730	11,420	15,800	20,725	33,140
Hou	Reduction for Seismic Shear — ASTM F1554, Grade 36			0.	63		0.85		0.	75
	Reduction for Seismic Shear — ASTM A193, Grade B7			0.63		0.85			0.	75
	Reduction for Seismic Shear — Stainless (ASTM A193, Grade B6)	$lpha_{V\!,seis}^{ 5}$	_	0.60			0.85		0.	75
	Reduction for Seismic Shear — Stainless (ASTM A193, Grade B8 & B8M)			0.	60	0.85			0.75	
	Strength Reduction Factor — Steel Failure	φ	_	0.65 <sup>2</sup>						
	Concrete Breakout S	Strength i	in Shear	•						
	Outside Diameter of Anchor	d <sub>o</sub>	in.	0.375	0.5	0.625	0.75	0.875	1	1.25
	Load Bearing Length of Anchor in Shear	$\ell_e$	in.				h <sub>ef</sub>			
	Strength Reduction Factor — Breakout Failure	φ	_				$0.70^{3}$			
	Concrete Pryout St	trength in	Shear							
	Coefficient for Pryout Strength	K <sub>CP</sub>	_	1.0 for $h_{ef}$ < 2.50"; 2.0 for $h_{ef} \ge 2.50$ "						
	Strength Reduction Factor — Pryout Failure	φ	_				0.704			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 3. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 4. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- The values of V<sub>sa</sub> are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, V<sub>sa</sub> must be multiplied by αV,<sub>seis</sub> for the corresponding anchor steel type.



### ET-HP® Shear Strength Design Data for Rebar in Normal-Weight Concrete<sup>1</sup>







	Charactaristic	Cumbal	Units				Rebar Size	е		
	Characteristic	Symbol	UIIILS	#3	#4	#5	#6	#7	#8	#10
	Ste	in Shear								
	Minimum Shear Stress Area	Ase	in. <sup>2</sup>	0.11	0.2	0.31	0.44	0.6	0.79	1.23
Dobor	Shear Resistance of Steel — Rebar (ASTM A615 Grade 60)	V <sub>sa</sub>	lb.	4,950	10,800	16,740	23,760	32,400	42,660	66,420
Rebar	Reduction for Seismic Shear — Rebar (ASTM A615 Grade 60)	$\alpha_{V,seis}^{5}$	-	0.6 0.8 0.7				75		
	Strength Reduction Factor — Steel Failure	φ					$0.60^{2}$			
	Concrete E	Breakout St	rength in	Shear						
	Outside Diameter of Anchor	$\mathcal{O}_{0}$	in.	0.375	0.5	0.625	0.75	0.875	1	1.25
	Load-Bearing Length of Anchor in Shear	$\ell_e$	in.				h <sub>ef</sub>			
	Strength Reduction Factor — Breakout Failure	φ	_				$0.70^{3}$			
	Concrete	Pryout Stre	ength in S	near						
	Coefficient for Pryout Strength	K <sub>CP</sub>	_	1.0 for $h_{ef} < 2.50$ "; 2.0 for $h_{ef} \ge 2.50$ "						
	Strength Reduction Factor — Pryout Failure	φ	_				0.704			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-11.
- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 3. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of φ. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of φ.
- 4. The value of φ applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 5. The values of V<sub>Sa</sub> are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F,  $V_{sa}$  must be multiplied by  $\alpha_{V,seis}$ .



ET-HP® Tension Design Strengths for Threaded Rod Anchors in Normal-Weight Concrete (f'<sub>c</sub> = 2,500 psi)

	_	
IBC	1	<b>I</b>





						Tension Design Strength Based on Concrete or Bond (lb.)										
Rod Dia.	Nominal Embed.			Minimum Dimensions for Cracked (in.)		Edge Distances = c <sub>ac</sub> on all sides				Edge Distances = 1¾" on one side and c <sub>ac</sub> on three sides						
(in.)	Depth (in.)	(	,	(,		SDC A-B <sup>6</sup>		SDC C-F <sup>7,8</sup>		SDC A-B <sup>6</sup>		SDC C-F <sup>7,8</sup>				
		ha	c <sub>ac</sub>	ha	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked			
	2%	41/4	3%	_	_	710	_	415	_	465	_	270	_			
3/8	3	47/8	41/2	47/8	21/4	895	365	525	215	440	305	255	180			
	41/2	6%	6¾	6%	21/4	1,345	550	785	320	410	455	240	265			
23/4	23/4	51/4	41/8	_	_	1,065	_	680	_	705	_	450	_			
1/2	4	61/2	6	61/2	3	1,550	810	985	515	635	565	405	360			
	6	81/2	9	81/2	3	2,320	1,215	1,480	775	590	850	375	540			
	31/8	61/4	43/4	61/4	35/8	1,475	635	940	405	925	395	590	255			
5/8	5	81/8	71/2	81/8	35/8	2,360	1,015	1,505	645	865	635	550	405			
	71/2	10%	111/4	10%	35/8	3,540	1,520	2,260	970	805	955	510	610			
	31/2	71/4	51/4	71/4	43/8	1,925	1,110	1,225	705	1,115	645	710	410			
3/4	6	93/4	9	9¾	43/8	3,300	1,900	2,105	1,215	1,110	1,100	710	700			
	9	12¾	131/2	12¾	45/8	4,950	2,855	3,155	1,820	1,035	1,655	660	1,055			
	3¾	81/8	5%	81/8	5	2,330	1,285	1,435	790	1,275	705	785	435			
7/8	7	11%	101/2	11%	5	4,355	2,400	2,675	1,475	1,380	1,315	850	805			
	10½	147/8	15¾	141/8	5%	6,530	3,600	4,015	2,215	1,285	1,970	790	1,210			
	4	9	6	9	5%	2,755	1,350	1,445	710	1,440	705	755	370			
1	8	13	12	13	5%	5,505	2,695	2,890	1,415	1,665	1,410	875	740			
	12	17	18	17	5¾	8,260	4,045	4,335	2,125	1,550	2,115	815	1,110			
	5	111/4	71/2	111/4	6¾	4,020	1,775	2,350	1,040	_	_	_	_			
1 1/4	10	161/4	15	161/4	6¾	8,040	3,550	4,705	2,075	_	_	_	_			
	15	211/4	221/2	211/4	67/8	12,060	5,320	7,055	3,115	_	_	_	_			

Threaded	Tension Design Strength of Threaded Rod Steel (lb.)										
Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M					
3/8	3,370	4,360	7,270	6,395	7,270	3,310					
1/2	6,175	7,990	13,315	11,715	13,315	6,070					
5/8	9,835	12,715	21,190	18,645	21,190	9,660					
3/4	14,530	18,790	31,315	27,555	31,315	14,280					
7/8	20,095	25,990	43,315	38,115	43,315	19,750					
1	26,365	34,090	56,815	49,995	56,815	25,905					
11/4	42,150	54,505	90,845	79,945	90,845	41,425					

- 1. Tension design strength must be the lesser of the concrete, bond or threaded rod steel design strength.
- 2. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.

- 5. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 6. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 7. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3. Design strengths in Bold indicate that the anchor ductility requirements of D.3.3.4.3 (a)1 to 3 are satisfied when using ASTM F1554 Grade 36 threaded rod. Any other ductility requirements
- 8. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



ET-HP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete ( $f'_c = 2,500~psi$ ) — Static Load

$\overline{}$			1
h	D	c	М
ш	D	u	,







	No. and and	Minimum Dimensions for Minimum Dimensions for				Allowable Tension Load Based on Concrete or Bond (Ib.)					
Rod Dia. (in.)	Nominal Embed. Depth (in.)	Uncracked (in.)			Cracked (in.)		tances = all sides	Edge Distances = $1\frac{3}{4}$ " on one side and $c_{ac}$ on three sides			
	(111.)	ha	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked		
	2%	41/4	35/8	_	_	505	_	330	_		
3/8	3	47/8	41/2	47/8	21/4	640	260	315	220		
	41/2	6%	6¾	6%	21/4	960	395	295	325		
	23/4	51/4	41/8	_	_	760	_	505	_		
1/2	4	61/2	6	61/2	3	1,105	580	455	405		
	6	81/2	9	81/2	3	1,655	870	420	605		
31/8	31/8	61/4	43/4	61/4	3%	1,055	455	660	280		
5/8	5	81/8	7 1/2	81/8	3%	1,685	725	620	455		
	71/2	10%	111/4	10%	3%	2,530	1,085	575	680		
	31/2	71/4	51/4	7 1/4	43/8	1,375	795	795	460		
3/4	6	9¾	9	93/4	43/8	2,355	1,355	795	785		
	9	12¾	13½	12¾	45%	3,535	2,040	740	1,180		
	3¾	81/8	5%	81/8	5	1,665	920	910	505		
7/8	7	11%	101/2	11%	5	3,110	1,715	985	940		
	10½	14%	15¾	147/8	5%	4,665	2,570	920	1,405		
	4	9	6	9	5%	1,970	965	1,030	505		
1	8	13	12	13	5%	3,930	1,925	1,190	1,005		
	12	17	18	17	5¾	5,900	2,890	1,105	1,510		
	5	111/4	71/2	111/4	6¾	2,870	1,270	_	_		
1 1/4	10	161⁄4	15	161/4	6¾	5,745	2,535	_	_		
	15	211/4	221/2	211/4	67/8	8,615	3,800	_	_		

Threaded	Allowable Tension Load of Threaded Rod Steel (lb.)										
Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M					
3/8	2,405	3,115	5,195	4,570	5,195	2,365					
1/2	4,410	5,705	9,510	8,370	9,510	4,335					
5/8	7,025	9,080	15,135	13,320	15,135	6,900					
3/4	10,380	13,420	22,370	19,680	22,370	10,200					
7/8	14,355	18,565	30,940	27,225	30,940	14,105					
1	18,830	24,350	40,580	35,710	40,580	18,505					
1 1/4	30,105	38,930	64,890	57,105	64,890	29,590					

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or threaded rod steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.



ET-HP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete ( $f'_c = 2,500~psi$ ) — Wind Load





1		4
ı	( Common	
ı		

		Minimum Di	mensions for	Minimum Di	manajana far	Allowable Te	ension Load Ba	Based on Concrete or Bond (lb.)			
Rod Dia. (in.)	Nominal Embed. Depth (in.)				Minimum Dimensions for Cracked (in.)		tances = all sides	Edge Distances = $1\frac{3}{4}$ " on one side and $c_{ac}$ on three sides			
	(,	ha	Cac	h <sub>a</sub>	Cac	Uncracked	Cracked	Uncracked	Cracked		
	2%	41/4	3%	_	_	425	_	280	_		
3/8	3	47/8	41/2	47/8	21/4	535	220	265	185		
	41/2	6%	6¾	6%	21/4	805	330	245	275		
	23/4	51/4	41/8	_	_	640	_	425	_		
1/2	4	61/2	6	6½	3	930	485	380	340		
	6	81/2	9	81/2	3	1,390	730	355	510		
	31/8	61/4	43/4	61/4	35/8	885	380	555	235		
5/8	5	81/8	71/2	81/8	35/8	1,415	610	520	380		
	71/2	10%	111/4	10%	35%	2,125	910	485	575		
	3½	71/4	51/4	71/4	43/8	1,155	665	670	385		
3/4	6	93/4	9	93/4	43/8	1,980	1,140	665	660		
	9	12¾	131/2	12¾	45/8	2,970	1,715	620	995		
	3¾	81/8	5%	81/8	5	1,400	770	765	425		
7/8	7	11%	101/2	11%	5	2,615	1,440	830	790		
	10½	147/8	15¾	147/8	5%	3,920	2,160	770	1,180		
	4	9	6	9	5%	1,655	810	865	425		
1	8	13	12	13	5%	3,305	1,615	1,000	845		
	12	17	18	17	5¾	4,955	2,425	930	1,270		
	5	111/4	71/2	111/4	63/4	2,410	1,065	_	_		
1 1/4	10	161/4	15	161/4	63/4	4,825	2,130	_	_		
	15	211/4	221/2	211/4	67/8	7.235	3.190	_	_		

Threaded	Allowable Tension Load of Threaded Rod Steel (lb.)											
Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M						
3/8	2,020	2,615	4,360	3,835	4,360	1,985						
1/2	3,705	4,795	7,990	7,030	7,990	3,640						
5/8	5,900	7,630	12,715	11,185	12,715	5,795						
3/4	8,720	11,275	18,790	16,535	18,790	8,570						
7/8	12,055	15,595	25,990	22,870	25,990	11,850						
1	15,820	20,455	34,090	29,995	34,090	15,545						
1 1/4	25,290	32,705	54,505	47,965	54,505	24,855						

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or threaded rod steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = \frac{1}{6.6} = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.



ET-HP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete (f'  $_{\rm c}$  = 2,500 psi) — Seismic Load









Rod Dia. (in.)	Nominal Embed. Depth (in.)	Minimum Dimensions for Uncracked (in.)		Minimum Dimensions for Cracked (in.)		Allowable Tension Load Based on Concrete or Bond (lb.)							
						Edge Distances = c <sub>ac</sub> on all sides				Edge Distances = $1\%$ " on one side and $c_{ac}$ on three sides			
						SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>		SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>	
		ha	c <sub>ac</sub>	ha	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
3/8	23/8	41/4	35/8	_	_	495	_	290	_	325	_	190	_
	3	47/8	41/2	47/8	21/4	625	255	370	150	310	215	180	125
	41/2	6%	6¾	6%	21/4	940	385	550	225	285	320	170	185
1/2	23/4	51/4	41/8	_	_	745	_	475	_	495	_	315	_
	4	61/2	6	61/2	3	1,085	565	690	360	445	395	285	250
	6	81/2	9	81/2	3	1,625	850	1,035	545	415	595	265	380
5/8	31/8	61/4	43/4	61/4	35/8	1,035	445	660	285	650	275	415	180
	5	81/8	71/2	81/8	3%	1,650	710	1,055	450	605	445	385	285
	71/2	10%	111/4	10%	35/8	2,480	1,065	1,580	680	565	670	355	425
3/4	31/2	71/4	51/4	71/4	43/8	1,350	775	860	495	780	450	495	285
	6	93/4	9	93/4	43/8	2,310	1,330	1,475	850	775	770	495	490
	9	12¾	131/2	12¾	45/8	3,465	2,000	2,210	1,275	725	1,160	460	740
7/8	3¾	81/8	5%	81/8	5	1,630	900	1,005	555	895	495	550	305
	7	11%	10½	11%	5	3,050	1,680	1,875	1,035	965	920	595	565
	101/2	14%	15¾	141/8	5%	4,570	2,520	2,810	1,550	900	1,380	555	845
1	4	9	6	9	5%	1,930	945	1,010	495	1,010	495	530	260
	8	13	12	13	5%	3,855	1,885	2,025	990	1,165	985	615	520
	12	17	18	17	53/4	5,780	2,830	3,035	1,490	1,085	1,480	570	775
1 1/4	5	111/4	71/2	111/4	6¾	2,815	1,245	1,645	730	_	_	_	_
	10	161/4	15	161/4	6¾	5,630	2,485	3,295	1,455	_	_	_	_
	15	211/4	221/2	211/4	67/8	8,440	3,725	4,940	2,180	_	_	_	_

Threaded	Allowable Tension Load of Threaded Rod Steel (lb.)										
Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M					
3/8	2,360	3,050	5,090	4,475	5,090	2,315					
1/2	4,325	5,595	9,320	8,200	9,320	4,250					
5/8	6,885	8,900	14,835	13,050	14,835	6,760					
3/4	10,170	13,155	21,920	19,290	21,920	9,995					
7/8	14,065	18,195	30,320	26,680	30,320	13,825					
1	18,455	23,865	39,770	34,995	39,770	18,135					
11/4	29,505	38,155	63,590	55,960	63,590	29,000					

- 1. Allowable tension load must be the lesser of the concrete, bond or threaded rod steel load.
- 2. Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = \frac{1}{4}$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Design strengths in **Bold** indicate that the anchor ductility requirements of D.3.3.4.3 (a)1 to 3 are satisfied when using ASTM F1554 Grade 36 threaded rod. Any other ductility requirements must be satisfied.
- 8. Allowable tension loads in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.



ET-HP® Tension Design Strengths for Rebar in Normal-Weight Concrete (f'<sub>c</sub> = 2,500 psi)

IBC		

		Embed. Uncracked (in.)				Tension Design Strength Based on Concrete or Bond (lb.)								
Rebar Size	Nominal Embed.			ions for Dimensions for		Edge	Edge Distances = c <sub>ac</sub> on all sides				Edge Distances = $1\frac{3}{4}$ " on one side and $c_{ac}$ on three sides			
SIZE	Depth (in.)					SDC A-B <sup>6</sup>		SDC C-F <sup>7,8</sup>		SDC A-B <sup>6</sup>		SDC C-F <sup>7,8</sup>		
		ha	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	
	2%	41/4	3%	_	_	670	_	500	_	445	_	335	_	
#3	3	47/8	41/2	47/8	21/4	845	295	635	220	420	250	315	190	
	41/2	6%	6¾	6%	21/4	1,270	440	950	330	390	375	295	280	
	23/4	51/4	41/8	_	_	1,010	_	755	_	675	_	505	_	
#4	4	61/2	6	61/2	3	1,465	575	1,100	430	610	410	455	310	
	6	81/2	9	81/2	3	2,200	865	1,650	650	565	615	425	460	
	31/8	61/4	43/4	61/4	35/8	1,390	615	1,040	460	885	390	660	295	
#5	5	81/8	71/2	81/8	35/8	2,220	985	1,665	735	820	625	615	470	
	71/2	10%	111/4	10%	35/8	3,330	1,475	2,500	1,105	760	940	570	705	
	31/2	71/4	51/4	71/4	41/4	1,805	895	1,355	670	1,060	525	795	395	
#6	6	9¾	9	9¾	41/4	3,095	1,535	2,325	1,150	1,050	900	790	675	
	9	12¾	13½	12¾	41/4	4,645	2,300	3,485	1,725	980	1,350	735	1,015	
	3¾	81/8	5%	81/8	47/8	2,190	1,195	1,645	895	1,215	660	910	495	
#7	7	11%	10½	113/8	47/8	4,090	2,225	3,065	1,670	1,305	1,230	980	925	
	101/2	141/8	15¾	14%	51/8	6,135	3,340	4,600	2,505	1,215	1,850	910	1,385	
	4	9	6	9	5%	2,580	1,560	1,935	1,170	1,365	825	1,025	620	
#8	8	13	12	13	5%	5,160	3,120	3,870	2,340	1,570	1,650	1,175	1,240	
	12	17	18	17	65%	7,745	4,680	5,810	3,510	1,460	2,475	1,095	1,860	
	5	111⁄4	71/2	111/4	61/2	3,780	2,745	2,835	2,060	_	_	_	_	
#10	10	161/4	15	161/4	7	7,555	5,490	5,665	4,115	_	_	_	_	
	15	211/4	221/2	21 1/4	91/8	11,335	8,230	8,500	6,175	_	_	_	_	

Rebar Size	Tension Design Strength of Rebar Steel (lb.)					
neudi Size	ASTM A615 GR 60	ASTM A706 GR 60				
#3	6,435	5,720				
#4	11,700	10,400				
#5	18,135	16,120				
#6	25,740	22,880				
#7	35,100	31,200				
#8	46,215	41,080				
#10	74,100	66,040				

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

- 1. Tension design strength must be the lesser of the concrete, bond or rebar steel design strength.
- Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D
  assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature
  of 110°F.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 6. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 7. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 8. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



ET-HP $^{\odot}$  Allowable Tension Loads for Rebar in Normal-Weight Concrete (f' $_{\rm C}$  = 2,500 psi) — Static Load









	Minimum Di		Minimum Di		Allowable Tension Load Based on Concrete or Bond (lb.)				
Rebar Size	Nominal Embed. Depth (in.)	Uncrac	mensions for ked (in.)		mensions for ed (in.)	Edge Dis c <sub>ac</sub> on a	tances = III sides	Edge Distances = $1\frac{3}{4}$ " on one side and $c_{ac}$ on three sides	
	(,	ha	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked
	23/8	41/4	35/8	_	_	480	_	320	_
#3	3	47/8	41/2	47/8	21/4	605	210	300	180
	41/2	6%	6¾	6%	21/4	905	315	280	270
	23/4	51/4	41/8	_	_	720	_	480	_
#4	4	61/2	6	61/2	3	1,045	410	435	295
	6	81/2	9	81/2	3	1,570	620	405	440
	31/8	61/4	43/4	61/4	35/8	995	440	630	280
#5	5	81/8	71/2	81/8	35/8	1,585	705	585	445
	71/2	10%	111/4	10%	35/8	2,380	1,055	545	670
	31/2	71/4	51/4	71/4	41/4	1,290	640	755	375
#6	6	93/4	9	9¾	41/4	2,210	1,095	750	645
	9	12¾	13½	12¾	41/4	3,320	1,645	700	965
	3¾	81/8	5%	81/8	47/8	1,565	855	870	470
#7	7	11%	10½	11%	47/8	2,920	1,590	930	880
	101/2	147/8	15¾	147/8	51/8	4,380	2,385	870	1,320
	4	9	6	9	5%	1,845	1,115	975	590
#8	8	13	12	13	5%	3,685	2,230	1,120	1,180
	12	17	18	17	65/8	5,530	3,345	1,045	1,770
	5	111/4	71/2	111/4	61/2	2,700	1,960	_	_
#10	10	161/4	15	161/4	7	5,395	3,920	_	_
	15	211/4	221/2	211/4	91/8	8,095	5,880	_	_

Rebar Size	Allowable Tension Load of Rebar Steel (lb.)					
nebai Size	ASTM A615 GR 60	ASTM A706 GR 60				
#3	4,595	4,085				
#4	8,355	7,430				
#5	12,955	11,515				
#6	18,385	16,345				
#7	25,070	22,285				
#8	33,010	29,345				
#10	52,930	47,170				

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or rebar steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



ET-HP $^{\odot}$  Allowable Tension Loads for Rebar in Normal-Weight Concrete (f' $_{\rm C}$  = 2,500 psi) — Wind Load

$\overline{}$	
IDO	ш
IIBG	ш
	l F





		Minimum Di	mensions for	Minimum Di	mensions for	Allowable Tension Load Based on Concrete or Bond (lb.)				
Rebar Size	Nominal Embed. Depth (in.)	Uncracked (in.)			ed (in.)		tances = III sides	Edge Distances side and c <sub>ac</sub> o	Edge Distances = 1¾" on one side and c <sub>ac</sub> on three sides	
	(,	h <sub>a</sub>	Cac	ha	Cac	Uncracked	Cracked	Uncracked	Cracked	
	2%	41/4	35/8	_	_	400	_	265	_	
#3	3	47/8	41/2	47/8	21/4	505	175	250	150	
	41/2	6%	6¾	6%	21/4	760	265	235	225	
	23/4	51/4	41/8	_	_	605	_	405	_	
#4	4	61/2	6	61/2	3	880	345	365	245	
	6	81/2	9	81/2	3	1,320	520	340	370	
	31/8	61/4	43/4	61/4	3%	835	370	530	235	
#5	5	81//8	71/2	81/8	35%	1,330	590	490	375	
	71/2	10%	111/4	10%	3%	2,000	885	455	565	
	31/2	71/4	51/4	71/4	41/4	1,085	535	635	315	
#6	6	9¾	9	9¾	41/4	1,855	920	630	540	
	9	12¾	13½	12¾	41/4	2,785	1,380	590	810	
	33/4	81/8	5%	81/8	47/8	1,315	715	730	395	
#7	7	11%	10½	11%	47/8	2,455	1,335	785	740	
	101/2	147/8	15¾	147/8	51/8	3,680	2,005	730	1,110	
	4	9	6	9	5%	1,550	935	820	495	
#8	8	13	12	13	5%	3,095	1,870	940	990	
	12	17	18	17	6%	4,645	2,810	875	1,485	
	5	111⁄4	71/2	111/4	61/2	2,270	1,645	_	_	
#10	10	161/4	15	161/4	7	4,535	3,295	_	_	
	15	211/4	221/2	211/4	91/8	6,800	4,940	_	_	

Rebar Size	Allowable Tension Load of Rebar Steel (lb.)					
neuai Size	ASTM A615 GR 60	ASTM A706 GR 60				
#3	3,860	3,430				
#4	7,020	6,240				
#5	10,880	9,670				
#6	15,445	13,730				
#7	21,060	18,720				
#8	27,730	24,650				
#10	44,460	39,625				

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>1.</sup> Allowable tension load must be the lesser of the concrete, bond or rebar steel load.

<sup>2.</sup> Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of  $150^{\circ}$ F and long-term temperature of  $110^{\circ}$ F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = \%.6 = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.

<sup>3.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>4.</sup> Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



ET-HP $^{\odot}$  Allowable Tension Loads for Rebar in Normal-Weight Concrete (f' $_{\rm C}$  = 2,500 psi) — Seismic Load









						Allowable Tension Load Based on Concrete or Bond (lb.)							
Rebar Size	Nominal Embed.	Minimum Dimensions for Uncracked (in.)		Dimens	imum sions for ed (in.)	Edg	e Distances	= c <sub>ac</sub> on all si	des	Edge		= 1¾" on one three sides	side
Size	Depth (in.)				ou (III.)	SDC A-B <sup>5</sup>		SDC	C-F <sup>6,7</sup>	SDC	A-B⁵	SDC C-F <sup>6,7</sup>	
		ha	c <sub>ac</sub>	ha	c <sub>ac</sub>	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	2%	41/4	3%	_		470	_	350	_	310	_	235	_
#3	3	47/8	41/2	47/8	21/4	590	205	445	155	295	175	220	135
	41/2	6%	6¾	6%	21/4	890	310	665	230	275	265	205	195
	23/4	51/4	41/8	_	_	705	_	530	_	475	_	355	_
#4	4	61/2	6	61/2	3	1,025	405	770	300	425	285	320	215
	6	81/2	9	81/2	3	1,540	605	1,155	455	395	430	300	320
	31/8	61/4	43/4	61/4	35/8	975	430	730	320	620	275	460	205
#5	5	81/8	71/2	81/8	35/8	1,555	690	1,165	515	575	440	430	330
	71/2	10%	111/4	10%	35/8	2,330	1,035	1,750	775	530	660	400	495
	31/2	71/4	51/4	71/4	41/4	1,265	625	950	470	740	370	555	275
#6	6	9¾	9	9¾	41/4	2,165	1,075	1,630	805	735	630	555	475
	9	123/4	13½	12¾	41/4	3,250	1,610	2,440	1,210	685	945	515	710
	3¾	81/8	5%	81/8	47/8	1,535	835	1,150	625	850	460	635	345
#7	7	11%	10½	11%	47/8	2,865	1,560	2,145	1,170	915	860	685	650
	101/2	147/8	15¾	14%	51/8	4,295	2,340	3,220	1,755	850	1,295	635	970
	4	9	6	9	5%	1,805	1,090	1,355	820	955	580	720	435
#8	8	13	12	13	5%	3,610	2,185	2,710	1,640	1,100	1,155	825	870
	12	17	18	17	65%	5,420	3,275	4,065	2,455	1,020	1,735	765	1,300
	5	111/4	71/2	111/4	61/2	2,645	1,920	1,985	1,440	_	_	_	_
#10	10	161/4	15	161/4	7	5,290	3,845	3,965	2,880	_	_	_	_
	15	211/4	221/2	211/4	91/8	7,935	5,760	5,950	4,325	_	_	_	_
	4 8 12 5 10	9 13 17 111/4 161/4	6 12 18 7½ 15	9 13 17 11¼ 16¼	5% 5% 6% 6½ 7	1,805 3,610 5,420 2,645 5,290	1,090 2,185 3,275 1,920 3,845	1,355 2,710 4,065 1,985 3,965	820 1,640 2,455 1,440 2,880	955 1,100 1,020 —	580 1,155 1,735 —		720 825 765 —

Rebar Size	Allowable Tension Load of Rebar Steel (lb.)					
neudi Size	ASTM A615 GR 60	ASTM A706 GR 60				
#3	4,505	4,005				
#4	8,190	7,280				
#5	12,695	11,285				
#6	18,020	16,015				
#7	24,570	21,840				
#8	32,350	28,755				
#10	51,870	46,230				

- 1. Allowable tension load must be the lesser of the concrete, bond or rebar steel load.
- 2. Allowable tension loads are calculated based on the strength design provisions of ACI 318-11 Appendix D assuming dry concrete, periodic inspection, short-term temperature of 150°F and long-term temperature of 110°F. Tension design strengths are converted to allowable tension loads using a conversion factor of  $\alpha = \%.7 = 1.43$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Interpolation between embedment depths is not permitted.
- 5. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the Designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Allowable tension loads in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.



**Adhesive** Anchors

ET-H	⊃® Allo\	vable Te	nsion Lo	ads for	
Threa	aded Ro	od Ancho	ors in No	rmal-We	eight Concrete

Rod	Drill	Embed.	Critical	Critical	Base	Tension Load ed on Bond Stre	ength	Tension Load Based on Steel Strength			
Dia. in.	Bit Dia.	Depth in.	Depth in.	oth Eage Sp		(13	f' <sub>c</sub> ≥ 2,000 psi 3.8 MPa) Concr		F1554 Grade 36	A193 GR B7	F593 304SS
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	
<b>3/8</b> (9.5)	1/2	<b>3½</b> (89)	<b>5</b> 1/4 (133)	<b>14</b> (356)	<b>8,777</b> (39.0)	<b>324</b> (1.4)	<b>2,195</b> (9.8)	<b>2,105</b> (9.4)	<b>4,535</b> (20.2)	<b>3,630</b> (16.1)	
<b>½</b> (12.7)	5/8	<b>4 ½</b> (108)	<b>6</b> % (162)	<b>17</b> (432)	<b>15,368</b> (68.4)	<b>605</b> (2.7)	<b>3,840</b> (17.1)	<b>3,750</b> (16.7)	<b>8,080</b> (35.9)	<b>6,470</b> (28.8)	
<b>5%</b> (15.9)	3/4	<b>5</b> (127)	<b>7½</b> (191)	<b>20</b> (508)	<b>22,877</b> (101.8)	<b>718</b> (3.2)	<b>5,720</b> (25.4)	<b>5,875</b> (26.1)	<b>12,660</b> (56.3)	<b>10,120</b> (45.0)	
<b>3/4</b> (19.1)	7/8	<b>6</b> 3/4 (171)	<b>10</b>	<b>27</b> (686)	<b>35,459</b> (157.7)	<b>4,940</b> (22.0)	<b>8,865</b> (39.4)	<b>8,460</b> (37.6)	<b>18,230</b> (81.1)	<b>12,400</b> (55.2)	
7/8 (22.2)	1	<b>7</b> 3/4 (197)	<b>11 %</b> (295)	<b>31</b> (787)	<b>43,596</b> (193.9)	<b>1,130</b> (5.0)	<b>10,900</b> (48.5)	<b>11,500</b> (51.2)	<b>24,785</b> (110.2)	<b>16,860</b> (75.0)	
<b>1</b> (25.4)	1 1/8	<b>9</b> (229)	<b>13½</b> (343)	<b>36</b> (914)	<b>47,333</b> (210.5)	<b>1,243</b> (5.5)	<b>11,835</b> (52.6)	<b>15,025</b> (66.8)	<b>32,380</b> (144.0)	<b>22,020</b> (97.9)	
<b>1 1/8</b> (28.6)	1 1/4	<b>10</b>	<b>15</b> 1/4 (387)	<b>40 ½</b> (1029)	<b>61,840</b> (275.1)	_	<b>15,460</b> (68.8)	<b>19,025</b> (84.6)	<b>41,000</b> (182.4)	<b>27,880</b> (124.0)	
<b>1 1/4</b> (31.8)	1 3/8	<b>11 ½</b> (286)	<b>16</b> % (429)	<b>45</b> (1143)	<b>78,748</b> (350.3)	<b>4,738</b> (21.1)	<b>19,685</b> (87.6)	<b>23,490</b> (104.5)	<b>50,620</b> (225.2)	<b>34,420</b> (153.1)	

- 1. Allowable load must the lesser of the bond or steel strength.
- 2. The allowable loads listed under allowable bond are based on a safety factor of 4.0.  $\,$
- 3. Refer to allowable load-adjustment factors for spacing and edge distance on pages 84 and 85.
- 4. Refer to in-service temperature sensitivity chart below for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.
- Anchors are not permitted to resist tension forces in overhead or wall installations unless proper consideration is given to fireexposure and elevated-temperature conditions.

### In-Service Temperature Sensitivity

	•	-
Base M Temp	Percent Allowable	
°F	°C	Load
40	4	100%
70	21	100%
110	43	100%
135	57	85%
150	66	69%

- Refer to temperature-sensitivity chart for allowable bond strength reduction for temperature. See page 319 for more information.
- Percent allowable load may be linearly interpolated for intermediate base material temperatures.
- 3. °C = (°F-32) / 1.8

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC

# **ET-HP®** Design Information — Concrete

ET-HP® Allowable Shear Loads for Threaded Rod Anchors in Normal-Weight Concrete



Rod	Drill	Embed.	Critical	Critical				on		
Dia. in.	Bit Dia.	Depth in.	Edge Dist. in.	Spacing Dist. in.		f' <sub>c</sub> ≥ 2,000 ps .8 MPa) Conc		F1554 Grade 36	A193 GR B7	F593 304SS
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)			Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
3/8 (9.5)	1/2	<b>3½</b> (89)	<b>5</b> 1/4 (133)	<b>5</b> ½ (133)	<b>7,615</b> (33.9)	<b>591</b> (2.6)	<b>1,905</b> (8.5)	<b>1,085</b> (4.8)	<b>2,340</b> (10.4)	<b>1,870</b> (8.3)
1/2 (12.7)	5/8	<b>4 ½</b> (108)	<b>6</b> % (162)	<b>6</b> % (162)	<b>11,273</b> (50.1)	<b>1,502</b> (6.7)	<b>2,820</b> (12.5)	<b>1,930</b> (8.6)	<b>4,160</b> (18.5)	<b>3,330</b> (14.8)
<b>5/8</b> (15.9)	3/4	<b>5</b> (127)	<b>7½</b> (191)	<b>7½</b> (191)	<b>19,559</b> (87.0)	<b>1,289</b> (5.7)	<b>4,890</b> (21.8)	<b>3,025</b> (13.5)	<b>6,520</b> (29.0)	<b>5,220</b> (23.2)
<b>3/4</b> (19.1)	7/8	<b>6¾</b> (171)	<b>10</b>	<b>10</b>	<b>27,696</b> (123.2)	<b>2,263</b> (10.1)	<b>6,925</b> (30.8)	<b>4,360</b> (19.4)	<b>9,390</b> (41.8)	<b>6,385</b> (28.4)
7/ <sub>8</sub> (22.2)	1	<b>7</b> 3/4 (197)	<b>11 %</b> (295)	<b>11 %</b> (295)	_	_	<b>6,925</b> (30.8)	<b>5,925</b> (26.4)	<b>12,770</b> (56.8)	<b>8,685</b> (38.6)
<b>1</b> (25.4)	1 1/8	<b>9</b> (229)	<b>13½</b> (343)	<b>13 ½</b> (343)	<b>53,960</b> (240.0)	<b>3,821</b> (17.0)	<b>13,490</b> (60.0)	<b>7,740</b> (34.4)	<b>16,680</b> (74.2)	<b>11,345</b> (50.5)
<b>1 1/8</b> (28.6)	1 1/4	<b>10 1/8</b> (257)	<b>15 1/4</b> (387)	<b>15 1/4</b> (387)	<b>59,280</b> (263.7)	_	<b>14,820</b> (65.9)	<b>9,800</b> (43.6)	<b>21,125</b> (94.0)	<b>14,365</b> (63.9)
<b>1 ½</b> (31.8)	1 3/8	<b>11 ½</b> (286)	<b>16</b> % (429)	<b>16</b> % (429)	<b>64,572</b> (287.2)	<b>3,503</b> (15.6)	<b>16,145</b> (71.8)	<b>12,100</b> (53.8)	<b>26,075</b> (116.0)	<b>17,730</b> (78.9)

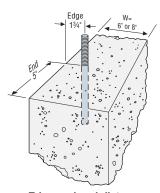
- 1. Allowable load must be the lesser of the load based on concrete edge distance or steel strength.
- 2. The allowable loads based on concrete edge distance are based on a safety factor of 4.0.
- 3. Refer to allowable load-adjustment factors for spacing and edge distance on pages 84 and 85.
- 4. Refer to in-service temperature sensitivity chart on page 77 for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

### ET-HP® Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete Stemwall



Dad Dia	D.:II Dia	Embed.	Stemwall	Min.	Min.	Tension Load Based on Bond Strength			Tension Load Based on Steel Strength
Rod Dia. in. (mm)	Drill Bit Dia. in.	Depth in.	Width in.	Edge Dist. in.	End Dist. in.		' <sub>c</sub> ≥ 2,000 p 8 MPa) Con		F1554 Grade 36
()		(mm)	(mm)	(mm)	(mm)			Allowable lb. (kN)	Allowable lb. (kN)
<b>5%</b> (15.9)	3/4	<b>9 ½</b> (241.3)	<b>6</b> (152.4)	<b>1 3/4</b> (44.5)	<b>5</b> (127.0)	<b>10,720</b> (47.7)	<b>1,559</b> (6.9)	<b>2,680</b> (11.9)	<b>5,875</b> (26.1)
<b>5%</b> (15.9)	3/4	<b>12</b> (304.8)	<b>6</b> (152.4)	<b>1 3/4</b> (44.5)	<b>5</b> (127.0)	<b>16,150</b> (71.8)	<b>260</b> (1.2)	<b>4,040</b> (18.0)	<b>5,875</b> (26.1)
<b>7/8</b> (22.2)	1	<b>12½</b> (317.5)	<b>8</b> (203.2)	<b>1 3/4</b> (44.5)	<b>5</b> (127.0)	<b>17,000</b> (75.6)	<b>303</b> (1.3)	<b>4,250</b> (18.9)	<b>11,500</b> (51.2)
<b>7/8</b> (22.2)	1	<b>15½</b> (393.7)	<b>8</b> (203.2)	<b>1 3/4</b> (44.5)	<b>5</b> (127.0)	<b>23,340</b> (103.8)	<b>762</b> (3.4)	<b>5,835</b> (26.0)	<b>11,500</b> (51.2)

- 1. Allowable load must be the lesser of the bond or steel strength.
- 2. The allowable loads listed under allowable bond are based on a safety factor of 4.0.
- 3. Refer to in-service temperature sensitivity chart on page 77 for allowable load adjustment for temperature.
- 4. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.



Edge and end distances for threaded rod in concrete foundation stemwall corner installation

<sup>\*</sup> See page 12 for an explanation of the load table icons.



### ET-HP® Allowable Tension Loads for Rebar Dowels in Normal-Weight Concrete

IBC	1	
		L B

L 1-1 II	7 (110 )	able lei	IOIOIT LO	100 101 1							
Rebar	Drill	Embed.	Critical Edge	Critical Spacing			on Load Base				Tension Load Based on Steel Strength
Size No.	Bit Dia.	Depth in.	Dist. in.	Dist. in.	$f'_{\it C} \ge 2,000 \; \text{psi}$ $f'_{\it C} \ge 4,000 \; \text{psi}$ (13.8 MPa) Concrete (27.6 MPa) Concrete					si crete	ASTM A615 Grade 60 Rebar
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
#4		<b>4 ½</b> (108)	<b>6</b> % (162)	<b>17</b> (432)	<b>17,596</b> (78.3)	<b>533</b> (2.4)	<b>4,400</b> (19.6)	_	_	<b>4,400</b> (19.6)	4,800
(12.7)	5/8	<b>6</b> (152)	<b>9</b> (229)	<b>24</b> (610)	_	_	_	<b>20,250</b> (90.1)	<b>263</b> (1.2)	<b>5,060</b> (22.5)	(21.4)
#5	3/4	<b>5</b> (127)	<b>7½</b> (191)	<b>20</b> (508)	<b>25,427</b> (113.1)	<b>1,899</b> (8.4)	<b>6,355</b> (28.3)	_	_	<b>6,355</b> (28.3)	7,440
(15.9)	9/4	<b>9</b> % (238)	<b>14</b>	<b>37 ½</b> (953)	_	_	_	<b>29,510</b> (131.3)	<b>2,270</b> (10.1)	<b>7,375</b> (32.8)	(33.1)
#6	7/8	<b>6</b> 3⁄4 (171)	<b>10 1/8</b> (257)	<b>27</b> (686)	<b>41,812</b> (186.0)	<b>595</b> (2.6)	<b>10,455</b> (46.5)	_	_	<b>10,455</b> (46.5)	10,560
(19.1)	/8	<b>11 1/4</b> (286)	<b>16</b> % (429)	<b>45</b> (1,143)	_	_	_	<b>44,210</b> (196.7)	<b>1,227</b> (5.5)	<b>11,050</b> (49.2)	(47.0)
#7	1	<b>7</b> 3⁄4 (197)	<b>11 %</b> (295)	<b>31</b> (787)	<b>50,241</b> (223.5)	<b>2,995</b> (13.3)	<b>12,560</b> (55.9)	_	_	<b>12,560</b> (55.9)	14,400
(22.2)	,	<b>13</b> % (333)	<b>19¾</b> (502)	<b>52½</b> (1,334)	_	_	_	<b>59,325</b> (263.9)	<b>3,444</b> (15.3)	<b>14,830</b> (66.0)	(64.1)
		<b>9</b> (229)	<b>13 ½</b> (343)	<b>36</b> (914)	<b>60,145</b> (267.5)	<b>5,493</b> (24.4)	<b>15,035</b> (66.9)	_	_	<b>15,035</b> (66.9)	
<b>#8</b> (25.4)	1 1/8	<b>12</b> (305)	<b>18</b> (457)	<b>48</b> (1,219)	_	_	_	_	_	<b>18,260</b> (81.2)	<b>18,960</b> (84.3)
		<b>15</b> (381)	<b>22 ½</b> (572)	<b>60</b> (1,524)	_	_	_	<b>85,970</b> (382.4)	<b>17,965</b> (79.9)	<b>21,490</b> (95.6)	
		<b>9</b> (229)	<b>13 ½</b> (343)	<b>36</b> (914)	_	_	<b>15,035</b> (66.9)	_	_	<b>15,035</b> (66.9)	
<b>#9</b> (28.6)	1 1/4	<b>13</b> (330)	<b>19 ½</b> (495)	<b>52</b> (1,321)	_	_	_	_	_	<b>21,310</b> (94.8)	<b>24,000</b> (106.8)
		<b>16</b> % (429)	<b>25</b> % (645)	<b>67 ½</b> (1,715)	_	_	_	<b>110,370</b> (491.0)	<b>4,768</b> (21.2)	<b>27,590</b> (122.7)	
		<b>11 ½</b> (286)	<b>16</b> % (429)	<b>45</b> (1,143)	<b>70,685</b> (314.4)	<b>1,112</b> (4.9)	<b>17,670</b> (78.6)	_	_	<b>17,670</b> (78.6)	
<b>#10</b> (31.8)	1 ½	<b>15</b> (381)	<b>22 ½</b> (572)	<b>60</b> (1,524)	_	_	_	_	_	<b>23,960</b> (106.6)	<b>30,480</b> (135.6)
		<b>18¾</b> (476)	<b>28 ½</b> (714)	<b>75</b> (1,905)	_	_	_	<b>120,976</b> (538.1)	<b>6,706</b> (29.8)	<b>30,245</b> (134.5)	
		<b>12</b> % (314)	<b>18</b> % (473)	<b>49 ½</b> (1,257)	<b>78,422</b> (348.8)	<b>4,603</b> (20.5)	<b>19,605</b> (87.2)	_	_	<b>19,605</b> (87.2)	
<b>#11</b> (34.9)	1 5/8	<b>16½</b> (419)	<b>24 %</b> (629)	<b>66</b> (1,676)	_	_	_	_	_	<b>28,605</b> (127.2)	<b>37,440</b> (166.5)
		<b>20</b> % (524)	<b>31</b> (787)	<b>82 ½</b> (2,096)	_	_	_	<b>150,415</b> (669.1)	<b>8,287</b> (36.9)	<b>37,605</b> (167.3)	
<b>#14</b> (44.5)	2	<b>15</b> % (400)	<b>23</b> % (600)	<b>63</b> (1,600)	<b>91,518</b> (407.1)	<b>3,797</b> (16.9)	<b>22,880</b> (101.8)	_	_	<b>22,880</b> (101.8)	<b>54,000</b> (240.2)

<sup>1.</sup> Allowable load must be the lesser of the bond or steel strength.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>2.</sup> The allowable loads listed under allowable bond are based on a safety factor of 4.0.

 $<sup>3.\,{\</sup>sf Refer}\ {\sf to}\ {\sf allowable}\ {\sf load-adjustment}\ {\sf factors}\ {\sf for}\ {\sf spacing}\ {\sf and}\ {\sf edge}\ {\sf distance}\ {\sf on}\ {\sf pages}\ {\sf 84}\ {\sf and}\ {\sf 85}.$ 

<sup>4.</sup> Refer to in-service temperature sensitivity chart on page 77 for allowable load adjustment for temperature.

<sup>5.</sup> Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

<sup>6.</sup> Anchors are not permitted to resist tension forces in overhead or wall installations unless proper consideration is given to fire-exposure and elevated-temperature conditions.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



IBC 🔁 🖫

ET-HP® Allowable Shear Loads for Rebar Dowels in Normal-Weight Concrete

EI-HP° All	owable Sh	ear Loads	ior Rebar L	Jowels III I	ionnai-vve	igni Concre	ele 🛌	
Rebar	Drill Bit	Embed.	Critical	Critical Spacing Dist. in.		ear Load Based crete Edge Dist		Shear Load Based on Steel Strength
Size No.	Dia. in.	Depth in.	Edge Dist. in.			f' <sub>c</sub> ≥ 2,500 psi '.2 MPa) Concre		ASTM A615 Grade 60 Rebar
(mm)		(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
<b>#4</b> (12.7)	5/8	<b>4 ½</b> (108)	<b>8</b> (203)	<b>6</b> % (162)	<b>13,564</b> (60.3)	<b>971</b> (4.3)	<b>3,390</b> (15.1)	<b>3,060</b> (13.6)
<b>#5</b> (15.9)	3/4	<b>5</b> (127)	<b>10</b> (254)	<b>7½</b> (191)	<b>20,914</b> (93.0)	<b>3,034</b> (13.5)	<b>5,230</b> (23.3)	<b>4,740</b> (21.1)
<b>#6</b> (19.1)	7/8	<b>6¾</b> (171)	<b>12</b> (305)	<b>10 1/8</b> (257)	<b>30,148</b> (134.1)	<b>1,322</b> (5.9)	<b>7,535</b> (33.5)	<b>6,730</b> (29.9)
<b>#7</b> (22.2)	1	<b>7</b> 3/4 (197)	<b>14</b> (356)	<b>11 </b> % (295)	<b>39,838</b> (177.2)	<b>1,854</b> (8.2)	<b>9,960</b> (44.3)	<b>9,180</b> (40.8)
<b>#8</b> (25.4)	1 1/8	<b>9</b> (229)	<b>16</b> (406)	<b>13 ½</b> (343)	<b>53,090</b> (236.2)	<b>3,562</b> (15.8)	<b>13,270</b> (59.0)	<b>12,085</b> (53.8)
<b>#9</b> (28.7)	1 1/4	<b>10 </b> 1/8 (257)	<b>18</b> (457)	<b>15 1/4</b> (387)	<b>63,818</b> (148.7)	<b>3,671</b> (16.3)	<b>15,955</b> (71.0)	<b>15,300</b> (68.1)
<b>#10</b> (32.3)	1 ½	<b>11 1/4</b> (286)	<b>20</b> (508)	<b>16</b>	<b>82,782</b> (368.2)	<b>2,245</b> (10.0)	<b>20,695</b> (92.1)	<b>19,430</b> (86.4)
<b>#11</b> (35.8)	1 %	<b>12</b> % (314)	<b>22</b> (559)	<b>18</b> % (473)	<b>96,056</b> (427.3)	<b>3,671</b> (16.3)	<b>24,015</b> (106.8)	<b>23,865</b> (106.2)
<b>#14</b> (43.0)	2	<b>12</b> % (314)	<b>22</b> (559)	<b>18</b> % (473)	_	_	<b>24,015</b> (106.8)	<b>34,425</b> (153.1)

- 1. Allowable load must be the lesser of the load based on concrete edge distance or steel strength.
- 2. The allowable loads based on concrete edge distance are based on a safety factor of 4.0.
- 3. Refer to allowable load-adjustment factors for spacing and edge distance on pages 84 and 85.
- 4. Refer to in-service temperature sensitivity chart on page 77 for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

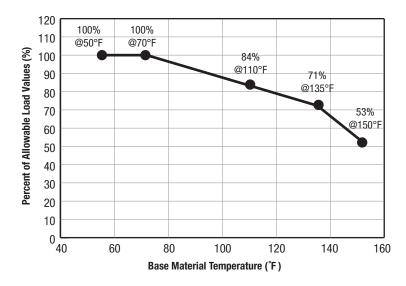


ET-HP® Allowable Tension and Shear Loads for Threaded Rod and Rebar in the Face of Fully Grouted CMU Wall Construction<sup>1, 3, 4, 5, 6, 8, 9, 10, 11, 12</sup>

IBC	1	<b>→</b>		
l J	200	200	[ [ ]	

Diameter (in.) or	Drill Bit Diameter	Minimum Embedment <sup>2</sup>	Allowable Load Based on Bond Strength <sup>7</sup> (lb.)			
Rebar Size Ńo.	(in.)	(in.)	Tension Load	Shear Load		
	Threade	MU Wall				
3/8	1/2	3%	1,425	845		
1/2	5/8	41/2	1,425	1,470		
5/8	3/4	5%	1,560	1,835		
3/4	7/8	6½	1,560	2,050		
	Reb	ar Installed in the Face of CMU	Wall			
#3	1/2	3%	1,275	1,335		
#4	5/8	41/2	1,435	1,355		
#5	3/4	5%	1,550	1,355		

- 1. Allowable load shall be the lesser of the bond values shown in this table and steel values, shown on page 83.
- 2. Embedment depth shall be measured from the outside face of masonry wall.
- 3. Critical and minimum edge distance and spacing shall comply with the information on page 82. Figure 2 on page 82 illustrates critical and minimum edge and end distances.
- 4. Minimum allowable nominal width of CMU wall shall be 8 inches. The minimum allowable member thickness shall be no less than 1½ times the actual anchor embedment.
- 5. No more than one anchor shall be permitted per masonry cell.
- 6. Anchors shall be permitted to be installed at any location in the face of the fully grouted masonry wall construction (cell, web, bed joint), except anchors shall not be installed within 1½ inches of the head joint, as show in Figure 2 on page 82.
- 7. Tabulated allowable load values are for anchors installed in fully grouted masonry walls.
- 8. Tabulated allowable loads are based on a safety factor of 5.0.
- 9. Tabulated allowable load values shall be adjusted for increased base material temperatures in accordance with Figure 1 below, as applicable.
- 10. Threaded rod and rebar installed in fully grouted masonry walls with ET-HP® are permitted to resist dead, live, seismic and wind loads.
- 11. Threaded rod shall meet or exceed the tensile strength of ASTM F1554, Grade 36 steel, which is 58,000 psi.
- 12. For installations exposed to severe, moderate or negligible exterior weathering conditions, as defined in Figure 1 of ASTM C62, allowable tension loads shall be multiplied by 0.80.



**Figure 1.** Load capacity based on in-service temperature for ET-HP® epoxy adhesive in the face of fully grouted CMU wall construction

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# ET-HP® Design Information — Masonry



ET-HP® Edge Distance and Spacing Requirements and Allowable Load Reduction Factors — Threaded Rod and Rebar in the Face of Fully Grouted CMU Wall Construction<sup>2,7</sup>

IDC			Territor.	· • • • • • • • • • • • • • • • • • • •	(== =
IDU	<del>/ →</del> i	Ĭ <b>4</b> →Ň			

				Edge or End D	Distance <sup>1,8</sup>	Spacing <sup>2,9</sup>						
		Crit (Full Ancho	ical r Capacity)³	Minimum (Reduced Anchor Capacity) <sup>4</sup>					ical r Capacity)⁵	Minimum (Reduced Anchor Capacity) <sup>6</sup>		
Rod Dia. (in.) or Rebar Size No.	Minimum Embed. Depth (in.)	Critical Edge or End Distance, <i>C<sub>cr</sub></i> (in.)	Allowable Load Reduction Factor	Minimum Edge or End Distance, <i>C<sub>min</sub></i> (in.)		Allowable Load Reduction Factor			Allowable Load Reduction Factor	Minimum Spacing, S <sub>min</sub> (in.)	Allowab Reductio	
110.		Load Di	rection		Load Direction		Load D	irection	Load Direction			
			Tension or	Tension or	Tension	Shear <sup>10</sup>		Tension or	Tension or	Tension or	Tension Shear	Choor
		Shear	Shear	Shear	IEHSIOH	Perp.	Parallel	Shear	Shear	Shear	IGUSIOU	Sileai
3/8	3%	12	1.00	4	0.76	1.00	1.00	8	1.00	4	0.47	0.94
1/2	41/2	12	1.00	4	1.00	0.92	0.9	8	1.00	4	0.60	0.96
5/8	5%	12	1.00	4	1.00	0.55	0.86	8	1.00	4	0.72	0.98
3/4	61/2	12	1.00	4	1.00	0.55	0.86	8	1.00	4	0.85	1.00
#3	3%	12	1.00	4	0.96	0.86	1.00	8	1.00	4	0.37	0.92
#4	41/2	12	1.00	4	1.00	0.71	1.00	8	1.00	4	0.69	0.96
#5	5%	12	1.00	4	1.00	0.71	1.00	8	1.00	4	1.00	1.00

- 1. Edge distance (C<sub>Cr</sub> or C<sub>min</sub>) is the distance measured from anchor centerline to edge or end of CMU masonry wall. Refer to Figure 2 below for an illustration showing critical and minimum edge and end distances.
- 2. Anchor spacing ( $S_{cr}$  or  $S_{min}$ ) is the distance measured from centerline to centerline of two anchors.
- Critical edge distance, C<sub>cr</sub>, is the least edge distance at which tabulated allowable load of an anchor is achieved where a load reduction factor equals 1.0 (no load reduction).
- 4. Minimum edge distance,  $C_{min}$ , is the least edge distance where an anchor has an allowable load capacity which shall be determined by multiplying the allowable loads assigned to anchors installed at critical edge distance,  $C_{cr}$ , by the load reduction factors shown above.
- Critical spacing, S<sub>cn</sub> is the least anchor spacing at which tabulated allowable load of an anchor is achieved such that anchor performance is not influenced by adiacent anchors.
- Minimum spacing, S<sub>min</sub>, is the least spacing where an anchors has an allowable load capacity, which shall be determined by multiplying the allowable loads assigned to anchors installed at critical spacing distance, S<sub>cr</sub>, by the load reduction factors shown above.
- 7. Reduction factors are cumulative. Multiple reduction factors for more than one spacing or edge or end distance shall be calculated separately and multiplied.
- 8. Load reduction factor for anchors loaded in tension or shear with edge distances between critical and minimum shall be obtained by linear interpolation.
- 9. Load reduction factor for anchors loaded in tension with spacing between critical and minimum shall be obtained by linear interpolation.
- 10. Perpendicular shear loads act towards the edge or end. Parallel shear loads act parallel to the edge or end (see Figure 3 below). Perpendicular and parallel shear load reduction factors are cumulative when the anchor is located between the critical minimum edge and end distance.

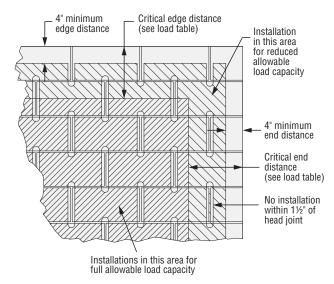


Figure 2. Allowable anchor placement in grouted CMU face shell

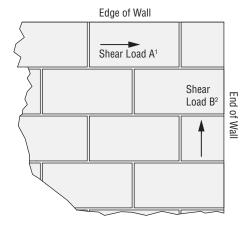


Figure 3. Anchor placement in grouted CMU mortar "T" joint

- 1. Direction of Shear Load A is parallel to edge of wall and perpendicular to end of wall.
- 2. Direction of Shear Load B is parallel to end of wall and perpendicular to edge of wall.

<sup>\*</sup> See page 12 for an explanation of the load table icons

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **ET-HP®** Design Information — Masonry



### ET-HP® Allowable Tension and Shear Loads — Threaded Rod Based on Steel Strength<sup>1</sup>

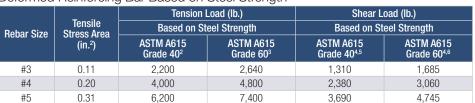
IBC	<b>→</b>	*

		Tension	Load Based o	n Steel Stren	Shear L	Shear Load Based on Steel Strength <sup>3</sup> (lb.)			
Threaded Tensile Rod Stress Diameter Area (in.) (in.²)	ASTM F1554 Grade 36 <sup>4</sup>	ASTM A193 Grade B7 <sup>6</sup>	Stainle	ss Steel	ASTM	ASTMA	Stainl	ess Steel	
			ASTM A193 Grade B6 <sup>5</sup>	ASTM A193 Grades B8 and B8M <sup>7</sup>	F1554	193 Grade B76	ASTM A193 Grade B6 <sup>5</sup>	ASTM A193 Grades B8 and B8M <sup>7</sup>	
3/8	0.078	1,495	3,220	2,830	1,930	770	1,660	1,460	995
1/2	0.142	2,720	5,860	5,155	3,515	1,400	3,020	2,655	1,810
5/8	0.226	4,325	9,325	8,205	5,595	2,230	4,805	4,225	2,880
3/4	0.334	6,395	13,780	12,125	8,265	3,295	7,100	6,245	4,260

- 1. Allowable load shall be the lesser of bond values given on page 81 and steel values in the table above.
- 2. Allowable Tension Steel Strength is based on the following equation:  $F_v = 0.33 \times F_u \times Tensile Stress Area.$
- 3. Allowable Shear Steel Strength is based on the following equation:  $F_V = 0.17 \times F_U \times \text{Tensile Stress Area.}$
- F1554, Grade 36 used to calculate allowable steel strength.
- 5. Minimum specified tensile strength ( $F_u = 110,000 \text{ psi}$ ) of ASTM A193, Grade B6 used to calculate allowable steel strength.
- 6. Minimum specified tensile strength ( $F_u = 125,000 \text{ psi}$ ) of ASTM A193, Grade B7 used to calculate allowable steel
- 4. Minimum specified tensile strength ( $F_u$  = 58,000 psi) of ASTM 7. Minimum specified tensile strength ( $F_u$  = 75,000 psi) of ASTM A193 Grades B8 and B8M used to calculate allowable steel

IBC

### ET-HP® Allowable Tension and Shear Loads — Deformed Reinforcing Bar Based on Steel Strength<sup>1</sup>



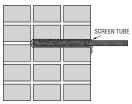
- 1. Allowable load shall be the lesser of bond values given on page 81 and steel values in the table above.
- 2. Allowable Tension Steel Strength is based on AC58 Section 3.3.3 (20,000 psi x tensile stress area) for Grade
- 3. Allowable Tension Steel Strength is based on AC58
- Section 3.3.3 (24,000 psi x tensile stress area) for Grade 60 rebar
- 4. Allowable Shear Steel Strength is based on AC58 Section 3.3.3 ( $F_V = 0.17 \times F_U \times \text{Tensile Stress Area}$ ).
- 5.  $F_u = 70,000$  psi for Grade 40 rebar.
- 6. F<sub>u</sub> = 90,000 psi for Grade 60 rebar.

### ET-HP® Allowable Tension and Shear Loads for Installations in Unreinforced Brick Masonry Walls — Minimum URM Wall Thickness is 13" (3 wythes thick)

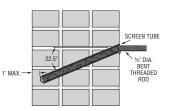
					-	· · · · · · · · · · · · · · · · · · ·							
Rod	Rod Drill Dia. Bit in. Dia. (mm) in.		Min. Edge/End Dist. in.	Min. Vertical	Min. Horiz.	Tension Load Based on URM Strength	Shear Load Based on URM Strength						
in.				Spacing Dist. in.	Spacing Dist. in.	Minimum Net Mortar Strength = 50 psi	Minimum Net Mortar Strength = 50 psi						
		(mm)	(mm)	(mm)	(mm)	Allowable lb. (kN)	Allowable lb. (kN)						
	Configuration A (Simpson Strong-Tie® ETS or ETSP Screen Tube Required)												
<b>3/4</b> (19.1)	1	<b>8</b> (203)	<b>24</b> (610)	<b>18</b> (457)	<b>18</b> (457)	_	<b>1,000</b> (4.4)						
		Configurati	ion B (Simp	son Strong	-Tie® ETS o	r ETSP Screen Tube Requi	red)						
3/ <sub>4</sub> (19.1)	1	13 (330)	<b>16</b> (406)	<b>18</b> (457)	<b>24</b> (610)	<b>1,200</b> (5.3)	<b>1,000</b> (4.4)						
	Config	uration C (S	Simpson Str	ong-Tie® E	TS Screen 1	Tube and AST Steel Sleeve	Required)						
5 <b>%</b> (15.9)	1	**	<b>24</b> (610)	<b>18</b> (457)	<b>18</b> (457)	<b>1,200</b> (5.3)	<b>750</b> (3.3)						

- Threaded rods must comply with ASTM F1554 Grade
- 2. All holes are drilled with a 1"-diameter carbide-tipped drill bit with the drill set in the rotation-only mode.
- The unreinforced brick walls must have a minimum thickness of 13 inches (three wythes of brick).
- The allowable load is applicable only where in-place shear tests indicate minimum net mortar strength of 50 psi.
- 5. The allowable load for Configuration B and C anchors subjected to a combined tension and shear load is determined by assuming a straight-line relationship between allowable tension and shear.
- The anchors installed in unreinforced brick walls are limited to resisting seismic or wind forces only.
- Configuration A has a straight threaded rod or rebar embedded 8 inches into the wall with a 31/32"-diameter by 8-inch-long screen tube (part # ETS758 or ETS758P) This configuration is designed to resist shear loads only.
- \* See page 12 for an explanation of the load table icons

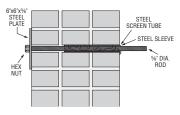
- 8. Configuration B has a 3/4" threaded rod bent and installed at a 22.5-degree angle and installed 13 inches into the wall, to within 1-inch (maximum) of the exterior wall surface. This configuration is designed to resist tension and shear loads. The pre-bent threaded rod is installed with a 31/32" diameter by 13-inch-long screen tube (part # ETS7513 or ETS7513P).
- Configuration C is designed to resist tension and shear forces. It consists of a %"-diameter, ASTM F1554 Grade 36 threaded rod and an 8"-long sleeve (part # AST800) and a 31/32"-diameter by 8-inch-long screen tube (part # ETS758). The steel sleeve has a plastic plug in one end. A 6" by 6" by %" thick ASTM A 36 steel plate is located on the back face of the wall.
- 10. Special inspection requirements are determined by local jurisdiction and must be confirmed by the local building official.
- Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.



**Configuration A** (Shear)



Configuration B (Tension & Shear)



**Configuration C** (Tension & Shear)

### Installation Instructions for Configuration C

- 1. Drill hole perpendicular to the wall to a depth of 8" with a 1"-diameter carbide-tipped drill bit (rotation-only mode).
- 2. Clean hole with oil-free compressed air and a nylon brush.
- 3. Fill 8" steel screen tube with mixed adhesive and insert into hole
- 4. Insert steel sleeve slowly into screen tube (adhesive will displace).
- 5. Allow adhesive to cure (see cure schedule).
- 6. Drill through plastic plug in (inside) end of steel sleeve with 5/8" bit.
- Drill completely through the wall with %" carbide-tipped concrete drill bit (rotation-only mode).
- 7. Insert %" rod through hole and attach metal plate and nut.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC

# ET-HP® Design Information — Concrete



ET-HP® Allowable Load-Adjustment Factors in Normal-Weight Concrete: Edge Distance, Tension and Shear Loads

### How to use these charts

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance ( $c_{act}$ ) at which the anchor is to be installed.
- 5. The load-adjustment factor ( $f_c$ ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple edges are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- Adjustment factors are to be applied to allowable tension load based on bond strength values or allowable Shear Load Based on Concrete Edge Distance values only.

### Edge Distance Tension (f<sub>c</sub>)

age Disi	IIICE I	16118		.lc/															
Dia.	3/8	1/2		5/8		3/4		7/8		1				1 1/8	1 1/4				
lge Reba		#	4	#	5	#	6	#	7	#	8	#	9		#1	10	#1	1	#14
st. E	3½ 4	4 1/4	6	5	9%	63/4	111/4	73/4	131/8	9	15	9	16 1/8	101/8	111/4	18¾	12%	20 %	15¾
act C <sub>C</sub> r	51/4 6	6%	9	7 1/2	14 1/8	101/8	16%	11%	19¾	131/2	22 1/2	131/2	25%	151/4	16%	28 1/8	18%	31	23%
n.) <sub>Cmin</sub>	13/4 1	13/4	1¾	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	23/4	2¾	2¾	2¾	23/4	2¾	23/4	23/4
f <sub>cmin</sub>	0.50 0	0.50	0.59	0.50	0.64	0.50	0.57	0.50	0.52	0.50	0.47	0.50	0.47	0.58	0.58	0.51	0.58	0.51	0.58
3/4	0.50 0	0.50	0.59	0.50	0.64	0.50	0.57	0.50	0.52	0.50	0.47								
3/4	0.64 0	0.61	0.65	0.59	0.67	0.56	0.60	0.55	0.55	0.54	0.50	0.50	0.47	0.58	0.58	0.51	0.58	0.51	0.58
3	0.68 0	0.64	0.66	0.61	0.68	0.57	0.61	0.56	0.55	0.55	0.50	0.51	0.48	0.59	0.59	0.51	0.59	0.51	0.59
4	0.82 0	0.74	0.72	0.70	0.71	0.63	0.63	0.61	0.58	0.60	0.53	0.56	0.50	0.62	0.62	0.53	0.61	0.53	0.61
5	0.96 0	0.85	0.77	0.78	0.73	0.69	0.66	0.66	0.61	0.64	0.55	0.60	0.52	0.66	0.65	0.55	0.64	0.55	0.63
6	1.00 0	0.96	0.83	0.87	0.76	0.75	0.69	0.72	0.63	0.68	0.58	0.65	0.55	0.69	0.68	0.57	0.67	0.57	0.65
7	1	1.00	0.89	0.96	0.79	0.81	0.72	0.77	0.66	0.72	0.60	0.70	0.57	0.72	0.71	0.59	0.69	0.58	0.67
8			0.94	1.00	0.82	0.87	0.75	0.82	0.69	0.77	0.63	0.74	0.59	0.76	0.74	0.61	0.72	0.60	0.69
9			1.00		0.85	0.93	0.78	0.87	0.71	0.81	0.66	0.79	0.62	0.79	0.77	0.63	0.75	0.62	0.71
0					0.88	0.99	0.80	0.92	0.74	0.85	0.68	0.84	0.64	0.82	0.80	0.65	0.77	0.64	0.73
2					0.94	1.00	0.86	1.00	0.79	0.94	0.73	0.93	0.69	0.89	0.86	0.69	0.82	0.67	0.77
4					1.00		0.92		0.85	1.00	0.78	1.00	0.73	0.96	0.91	0.73	0.88	0.71	0.81
6							0.98		0.90		0.83		0.78	1.00	0.97	0.77	0.93	0.74	0.85
8							1.00		0.95		0.89		0.83		1.00	0.80	0.98	0.77	0.89
20									1.00		0.94		0.87			0.84	1.00	0.81	0.93
22											0.99		0.92			0.88		0.84	0.97
24											1.00		0.97			0.92		0.88	1.00
26													1.00			0.96		0.91	
28																1.00		0.95	
30																		0.98	
32																		1.00	
24 26 28 30													0.97			0.92 0.96			0.88 0.91 0.95 0.98



### Edge Distance Shear (f<sub>c</sub>)

	Dia.	3/8	1/2	. 07	5/8		3/4		7/8		1			1 1/8	1 1/4			
Edao	Rebar	76	/2	#4	70	#5	/4	#6	76	#7		#8	#9	1 /0	1 /4	#10	#11	#14
Edge Dist.	E	31/2	4 1/4	4 1/4	5	5	63/4	63/4	73/4	73/4	9	9	101/8	101/8	11 1/4	111/4	12%	12%
Cact	C <sub>Cr</sub>	51/4	6%	8	71/2	10	101/8	12	11%	14	131/2	16	18	151/4	16%	20	22	22
(in.)	C <sub>min</sub>	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	23/4	23/4	23/4	23/4	23/4	23/4
	f <sub>cmin</sub>	0.29	0.20	0.16	0.13	0.10	0.13	0.10	0.13	0.09	0.08	0.08	0.08	0.14	0.14	0.14	0.14	0.14
1 3/4	0,,,,,,	0.29	0.20	0.16	0.13	0.10	0.13	0.10	0.13	0.09	0.08	0.08						
23/4		0.49	0.37	0.29	0.28	0.21	0.23	0.19	0.22	0.16	0.16	0.14	0.08	0.14	0.14	0.14	0.14	0.14
3		0.54	0.42	0.33	0.32	0.24	0.26	0.21	0.24	0.18	0.18	0.16	0.10	0.16	0.16	0.15	0.15	0.15
4		0.75	0.59	0.46	0.47	0.35	0.36	0.30	0.33	0.26	0.26	0.23	0.16	0.23	0.22	0.20	0.20	0.20
5		0.95	0.76	0.60	0.62	0.45	0.47	0.39	0.42	0.33	0.33	0.29	0.22	0.29	0.28	0.25	0.24	0.24
6		1.00	0.94	0.73	0.77	0.56	0.57	0.47	0.50	0.41	0.41	0.35	0.28	0.36	0.34	0.30	0.29	0.29
7			1.00	0.87	0.92	0.67	0.68	0.56	0.59	0.48	0.49	0.42	0.34	0.43	0.40	0.35	0.33	0.33
8				1.00	1.00	0.78	0.78	0.65	0.68	0.55	0.57	0.48	0.40	0.50	0.46	0.40	0.37	0.37
9						0.89	0.88	0.74	0.77	0.63	0.65	0.55	0.46	0.57	0.52	0.45	0.42	0.42
10						1.00	0.99	0.82	0.86	0.70	0.73	0.61	0.52	0.64	0.58	0.50	0.46	0.46
11							1.00	0.91	0.94	0.78	0.80	0.68	0.58	0.71	0.64	0.55	0.51	0.51
12								1.00	1.00	0.85	0.88	0.74	0.64	0.78	0.70	0.60	0.55	0.55
13										0.93	0.96	0.81	0.70	0.85	0.76	0.65	0.60	0.60
14										1.00	1.00	0.87	0.76	0.91	0.82	0.70	0.64	0.64
15												0.94	0.82	0.98	0.89	0.75	0.69	0.69
16												1.00	0.88	1.00	0.95	0.80	0.73	0.73
18													1.00		1.00	0.90	0.82	0.82
20																1.00	0.91	0.91
22																	1.00	1.00



- $2.\,c_{act}$  = actual edge distance at which anchor is installed (inches).
- $3.c_{CT}$  = critical edge distance for 100% load (inches).
- $4. c_{min} = minimum edge distance for reduced load (inches).$

- 5.  $f_c$  = adjustment factor for allowable load at actual edge distance.
- $6.f_{\rm ccr}$  = adjustment factor for allowable load at critical edge distance. fccr is always = 1.00.
- 7. f<sub>cmin</sub> = adjustment factor for allowable load at minimum edge distance.
- 8.  $f_c = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min}) / (c_{cr} c_{min})].$



<sup>\*</sup> See page 12 for an explanation of the load table icons.



ET-HP® Allowable Load-Adjustment Factors in Normal-Weight Concrete: Spacing, Tension and Shear Loads

#### How to use these charts

- 1. The following tables are for reduced spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the spacing ( $s_{\it act}$ ) at which the anchor is to be installed.
- 5. The load-adjustment factor ( $f_s$ ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple spacings are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- Adjustment factors are to be applied to allowable Tension Load Based on Bond Strength values or allowable Shear Load Based on Concrete Edge Distance values only.

Spac	ing I	ensio	n (t <sub>s</sub> )
	D:-	0.4	4/

ρασ	, ii ig ic		. 0.																	<u>Contractors</u>
	Dia.	3/8	1/2	_	5/8	_	3/4		7/8	_	1			^	1 1/8	11/4				114.4
	Rebar		#		#	-		6		7	#		#			#1		#1		#14
Sact	E	3 1/2	4 1/4	6	5	9%	6¾	111/4	73/4	13 1/8	9	15	9	16%	10 1/8	111/4		12%		15¾
(in.)	S <sub>cr</sub>	14	17	24	20	37 1/2	27	45	31	52 ½	36	60	36	67 1/2		45	75			63
	Smin	13/4	21/8	3	2 1/2	43/4	3%	5%	3 1/8	6%	4 1/2	7 1/2	4 1/2	8 1/2	5 1/8	5%	9%	61/4	10%	7 1/8
	f <sub>smin</sub>	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89
13/4		0.89																		
2		0.89																		
4		0.91	0.90	0.90	0.90		0.89		0.89											
6		0.93	0.92	0.91	0.91	0.89	0.90	0.89	0.90		0.90		0.90		0.89	0.89				
8		0.95	0.93	0.92	0.92	0.90	0.91	0.90	0.91	0.89	0.90	0.89	0.90		0.90	0.90		0.89		0.89
10		0.96	0.95	0.93	0.94	0.91	0.92	0.90	0.91	0.90	0.91	0.90	0.91	0.89	0.91	0.90	0.89	0.90		0.89
12		0.98	0.96	0.94	0.95	0.91	0.93	0.91	0.92	0.90	0.92	0.90	0.92	0.90	0.91	0.91	0.89	0.90	0.89	0.90
14		1.00	0.98	0.95	0.96	0.92	0.94	0.91	0.93	0.91	0.92	0.90	0.92	0.90	0.92	0.91	0.90	0.91	0.90	0.90
16			0.99	0.96	0.97	0.93	0.95	0.92	0.94	0.91	0.93	0.91	0.93	0.90	0.92	0.92	0.90	0.91	0.90	0.91
18			1.00	0.97	0.99	0.93	0.96	0.92	0.95	0.92	0.94	0.91	0.94	0.91	0.93	0.92	0.90	0.92	0.90	0.91
20				0.98	1.00	0.94	0.97	0.93	0.96	0.92	0.94	0.92	0.94	0.91	0.94	0.93	0.91	0.92	0.90	0.91
24				1.00		0.95	0.99	0.94	0.97	0.93	0.96	0.92	0.96	0.92	0.95	0.94	0.91	0.94	0.91	0.92
28						0.97	1.00	0.95	0.99	0.94	0.97	0.93	0.97	0.93	0.96	0.95	0.92	0.95	0.92	0.93
32						0.98		0.96	1.00	0.95	0.99	0.94	0.99	0.93	0.97	0.96	0.93	0.96	0.92	0.94
36						0.99		0.97		0.96	1.00	0.95	1.00	0.94	0.99	0.97	0.93	0.97	0.93	0.95
40						1.00		0.99		0.97		0.96		0.95	1.00	0.99	0.94	0.98	0.94	0.95
45								1.00		0.98		0.97		0.96		1.00	0.95	0.99	0.94	0.96
50										0.99		0.98		0.97			0.96	1.00	0.95	0.97
55										1.00		0.99		0.98			0.97		0.96	0.98
60												1.00		0.99			0.97		0.97	0.99
65														1.00			0.98		0.97	1.00
70																	0.99		0.98	
75																	1.00		0.99	
32 1/2																			1.00	

See Notes Below.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

#### Spacing Shear (f<sub>o</sub>)

											) <del>(describ</del> )
	Dia.	3/8	1/2	5/8	3/4	7/8	1	11/8	11/4		
	Rebar		#4	#5	#6	#7	#8	#9	#10	#11	#14
Sact	E	3 1/2	4 1/4	5	63/4	7¾	9	101/8	111/4	12%	12%
(in.)	s <sub>cr</sub>	5 1/4	6%	7 1/2	101/8	11%	13 1/2	151/4	161/8	18%	18%
	Smin	1 3/4	21/8	21/2	3%	31/8	4 1/2	51/8	5%	6 1/4	6 1/4
	f <sub>smin</sub>	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83	0.83
1 3/4		0.83									
2		0.84									
3		0.89	0.87	0.85							
4		0.94	0.91	0.88	0.85	0.83					
5		0.99	0.95	0.92	0.87	0.85	0.84				
6		1.00	0.99	0.95	0.90	0.88	0.86	0.84	0.84		
7			1.00	0.98	0.92	0.90	0.88	0.86	0.85	0.84	0.84
8				1.00	0.95	0.92	0.90	0.88	0.87	0.85	0.85
9					0.97	0.94	0.92	0.90	0.88	0.87	0.87
10					1.00	0.96	0.93	0.91	0.90	0.88	0.88
12						1.00	0.97	0.95	0.93	0.91	0.91
14							1.00	0.98	0.96	0.94	0.94
16								1.00	0.99	0.96	0.96
18									1.00	0.99	0.99
20										1.00	1.00

<sup>1.</sup> E = Embedment depth (inches).

<sup>2.</sup>  $S_{act}$  = actual spacing distance at which anchors are installed (inches).

<sup>3.</sup>  $S_{cr}$  = critical spacing distance for 100% load (inches).

<sup>4.</sup>  $S_{min}$  = minimum spacing distance for reduced load (inches).

 $<sup>5.</sup>f_{\rm S}=$  adjustment factor for allowable load at actual spacing distance.

<sup>6.</sup> f<sub>scr</sub> = adjustment factor for allowable load at critical spacing distance, fscr is always = 1.00.

<sup>7.</sup> f<sub>smin</sub> = adjustment factor for allowable load at minimum spacing distance.

<sup>8.</sup>  $f_s = f_{smin} + [(1 - f_{smin}) (s_{act} - s_{min}) / (s_{cr} - s_{min})].$ 

<sup>\*</sup> See page 12 for an explanation of the load table icons.

### **AT** Acrylic Adhesive



AT is a high-strength, acrylic-based adhesive anchoring system, formulated for use as a high-strength anchor-grouting material in a wide range of temperature conditions. It is a two-part system, with the resin and initiator being simultaneously dispensed and mixed through the mixing nozzle.

### **Features**

- Code listed under the IBC/IRC for URM per ICC-ES ESR-1958
- Cure times 24 hours at 0°F, 1 hour at 60°F
- Non-sag gel formulation ideal for horizontal, vertical and overhead applications
- Easy hole-cleaning procedure no power-brushing required
- Suitable for use in damp or wet anchor sites
- · When properly mixed, adhesive will be a uniform gray color
- Available in 9.6 oz., 12.5 oz. and 30 oz. cartridges for application versatility
- Manufactured in the USA using global materials

### **Applications**

- Threaded rod anchoring and rebar doweling into concrete, masonry and URM (red brick)
- Multiple DOT listings refer to www.strongtie.com/DOT for current approvals

**Codes:** ICC-ES ESR-1958 (URM); AASHTO M-235 and ASTM C881 (Type I and IV, Grade 3, Class A, B and C – except AT adhesive is a non-epoxy formulated for fast cure time); multiple DOT listings (refer to strongtie.com/DOT).

### **Chemical Resistance**

See pages 320-321.

### Installation and Application Instructions

(See also pages 124-127.)

- Surfaces to receive adhesive must be clean.
- Base material temperature must be 0°F or above at the time of installation.
- For information on installations below 0°F, contact Simpson Strong-Tie.
- Mixed material in nozzle can harden in 5–7 minutes at temperatures of 70°F and above.

### **Design Example**

See page 324.

### Suggested Specifications

See www.strongtie.com for more information.



AT Adhesive

### **AT** Acrylic Adhesive

# SIMPSON Strong-Tie

### **Test Criteria**

Anchors installed with AT adhesive have been tested in accordance with ICC-ES Acceptance Criteria for Anchors in Unreinforced Masonry Elements (AC60).

Property	Test Method	Result*
Consistency	ASTM C881	Non-sag/thixotropic paste
Heat deflection	ASTM D648	142°F (61°C)
Bond strength (moist cure, 60°F)	ASTM C882	2,960 psi (2 days) 3,567 psi (14 days)
Water absorption	ASTM D570	0.25% (24 hours)
Compressive yield strength (cured 60°F)	ASTM D695	10,930 psi (7 days)
Compressive modulus (cured 60°F)	ASTM D695	502,330 psi (7 days)
Shore D hardness	ASTM D2240	91
Gel time	ASTM C881	5 minutes
VOC	ASTM D2369	25 g/L
Shrinkage coefficient	ASTM D2566	0.004 in./in.

<sup>\*</sup>Material and curing conditions: 73 ± 2°F, unless otherwise noted.

### AT Adhesive Cartridge Systems

Model No.	Capacity (ounces)	Cartridge Type	Carton Quantity	Dispensing Tools	Mixing Nozzle
AT10	9.6	Single	12	CDT10S	
AT13	12.5	Side-by-side	10	ADT813S	
AT30	30	Side-by-side	5	ADT30S ADTA30CKT ADTA30P	AMN19Q

- 1. Cartridge estimation guidelines are available at www.strongtie.com/apps.
- Detailed information on dispensing tools, mixing nozzles and other adhesive accessories is available on pages 128 through 135, or at www.strongtie.com.
- 3. Use only Simpson Strong-Tie® mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair AT adhesive performance.

### In-Service Temperature Sensitivity

	laterial erature	Percent Allowable Load for	Percent Allowable Load for
°F	°C	$T_{inst} = 0$ °F	$T_{inst} \ge 70^{\circ} F$
0	-18	100%	100%
32	0	100%	100%
70	21	100%	100%
110	43	82%	82%
135	57	74%	82%
150	66	38%	65%
180	82	22%	28%

- Refer to in-service temperature sensitivity chart for allowable bond strength reduction for in-service temperature. See page 319.
- 2.  $T_{\textit{inst}}$  is the base material temperature during installation and curing of the adhesive.
- 3. Percent allowable load for  $T_{inst}$  = 0°F (-18°C) is to be used for  $T_{inst}$  between 0°F (-18°C) and 70°F (21°C).
- Percent allowable load may be linearly interpolated for intermediate base material in-service temperatures.
- $5. \, ^{\circ}\text{C} = (^{\circ}\text{F-32}) \, / \, 1.8$

### Cure Schedule

	laterial erature	Cure Time (hrs.)
°F	°C	(1110.)
0	-18	24
25	-4	8
40	4	4
60	16	1
70	21	30 min.
100	38	20 min.



AT Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete (continued on next page)

	<b>1</b>	<b>*</b>
IRC	20 20	

Rod Drill Embed.			Critical	Critical	Base	Tension Load d on Bond Str		Base	Tension Load d on Steel Stren	gth
Dia. in.	Bit Dia.	Depth in.	Edge Dist. in.	Spacing Dist. in.		f' <sub>c</sub> ≥ 2,000 ps .8 MPa) Conc		F1554 Grade 36	A193 GR B7	F593 304SS
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
		<b>1</b> 3/4 (44)	<b>2</b> 5/8 (67)	<b>7</b> (178)	<b>3,362</b> (15.0)	<b>99</b> (0.4)	<b>840</b> (3.7)			
3/8 (9.5)	7/16	<b>3½</b> (89)	<b>5</b> ½ (133)	<b>6</b> 1/8 (156)	<b>8,937</b> (39.8)	<b>314</b> (1.4)	<b>2,235</b> (9.9)	<b>2,105</b> (9.4)	<b>4,535</b> (20.2)	<b>3,630</b> (16.1)
		<b>4½</b> (114)	<b>6¾</b> (171)	<b>18</b> (457)	<b>10,411</b> (46.3)	<b>525</b> (2.3)	<b>2,605</b> (11.6)			
		<b>2</b> 1/8 (54)	<b>3¾</b> 6 (81)	<b>8½</b> (216)	<b>5,252</b> (23.4)	<b>501</b> (2.2)	<b>1,315</b> (5.8)			
<b>½</b> (12.7)	9/16	<b>4½</b> (108)	<b>6</b> % (162)	<b>7½</b> (191)	<b>16,668</b> (74.1)	<b>822</b> (3.7)	<b>4,165</b> (18.5)	<b>3,750</b> (16.7)	<b>8,080</b> (35.9)	<b>6,470</b> (28.8)
		<b>6</b> (152)	<b>9</b> (229)	<b>24</b> (610)	<b>19,182</b> (85.3)	<b>331</b> (1.5)	<b>4,795</b> (21.3)			
		<b>2½</b> (64)	<b>3¾</b> (95)	<b>10</b> (254)	<b>8,495</b> (37.8)	<b>561</b> (2.5)	<b>2,125</b> (9.5)			
		<b>4</b> (102)	<b>5</b> % (143)	<b>16</b> (406)	_	_	<b>4,315</b> (19.2)			
<b>5%</b> (15.9)	11/16	<b>5½</b> (140)	<b>7½</b> (191)	<b>9</b> 5/8 (244)	<b>26,025</b> (115.8)	<b>1,866</b> (8.3)	<b>6,505</b> (28.9)	<b>5,875</b> (26.1)	<b>12,660</b> (56.3)	<b>10,120</b> (45.0)
		<b>7</b> ½6 (189)	<b>10</b> % (276)	<b>29¾</b> (756)	_	_	<b>7,215</b> (32.1)			
		<b>9</b> % (238)	<b>14</b> 1/8 (359)	<b>37½</b> (953)	<b>31,683</b> (140.9)	<b>1,571</b> (7.0)	<b>7,920</b> (35.2)			

See notes on next page.

3/4" - 11/4" diameters on next page



SIMPSON
Strong-Tie

AT Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete (continued from previous page)

IBC			
-----	--	--	--

Rod Drill		Embed.	Critical	Critical		Tension Load d on Bond St	rength	Base	Tension Load ed on Steel Strer	igth
Dia. in.	Bit Dia.	Depth in.	Edge Dist. in.	Spacing Dist. in.	(13	f' <sub>c</sub> ≥ 2,000 ps .8 MPa) Cond	si crete	F1554 Grade 36	A193 GR B7	F593 304SS
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
		<b>3</b> % (86)	<b>5½</b> 6 (129)	<b>13½</b> (343)	<b>12,991</b> (57.8)	<b>725</b> (3.2)	<b>3,250</b> (14.5)			
		<b>5½</b> 6 (129)	<b>7</b> 5/8 (194)	<b>20</b> 1/4 (514)	_	_	<b>6,330</b> (28.2)			
<b>3/4</b> (19.1)	13/16	<b>6¾</b> (171)	<b>10</b> 1/8 (257)	<b>11</b> % (302)	<b>37,616</b> (167.3)	<b>1,817</b> (8.1)	<b>9,405</b> (41.8)	<b>8,460</b> (37.6)	<b>18,230</b> (81.1)	<b>12,400</b> (55.2)
		<b>9</b> (229)	<b>13½</b> (343)	<b>36</b> (914)	_	_	<b>10,000</b> (44.5)			
		<b>111/4</b> (286)	<b>16</b> % (429)	<b>45</b> (1143)	<b>42,381</b> (188.5)	<b>683</b> (3.0)	<b>10,595</b> (47.1)			
		<b>37/8</b> (98)	<b>5</b> <sup>13</sup> / <sub>16</sub> (148)	<b>15½</b> (394)	<b>14,206</b> (63.2)	<b>457</b> (2.0)	<b>3,550</b> (15.8)			
		<b>5</b> <sup>13</sup> / <sub>16</sub> (148)	<b>8³/4</b> (222)	<b>231/4</b> (591)	_	_	<b>7,130</b> (31.7)			<b>16,860</b> (75.0)
7/ <sub>8</sub> (22.2)	1	<b>7</b> 3/4 (197)	<b>11</b> % (295)	13% (346)	<b>42,848</b> (190.6)	<b>3,155</b> (14.0)	<b>10,710</b> (47.6)	<b>11,500</b> (51.2)	<b>24,785</b> (110.2)	
, ,		<b>10</b> 7/ <sub>16</sub> (265)	<b>15</b> % (397)	<b>41</b> <sup>3</sup> ⁄ <sub>4</sub> (1060)	_	_	<b>12,250</b> (54.5)		(1.0.2)	
		<b>13</b> 1/8 (333)	<b>19</b> 5/8 (498)	<b>52½</b> (1334)	<b>55,148</b> (245.3)	<b>5,673</b> (25.2)	<b>13,785</b> (61.3)			
		<b>4½</b> (114)	<b>6¾</b> (171)	<b>18</b> (457)	<b>20,797</b> (92.5)	<b>1,763</b> (7.8)	<b>5,200</b> (23.1)			<b>22,020</b> (97.9)
		<b>6</b> 3⁄4 (171)	<b>10</b> 1/8 (257)	<b>27</b> (686)	_	_	<b>10,165</b> (45.2)		<b>32,380</b> (144.0)	
<b>1</b> (25.4)	1 1/16	<b>9</b> (229)	13½ (343)	<b>15¾</b> (400)	<b>60,504</b> (269.1)	<b>2,065</b> (9.2)	<b>15,125</b> (67.3)	<b>15,025</b> (66.8)		
		<b>12</b> (305)	<b>18</b> (457)	<b>48</b> (1219)	_	_	<b>17,880</b> (79.5)			
		<b>15</b> (381)	<b>22½</b> (572)	<b>60</b> (1524)	<b>82,529</b> (367.1)	<b>5,146</b> (22.9)	<b>20,630</b> (91.8)			
		<b>5</b> 1/8 (130)	<b>7¾</b> (197)	<b>20½</b> (521)	<b>26,600</b> (118.3)	_	<b>6,650</b> (29.6)			
		<b>7</b> 5/8 (194)	<b>11½</b> (292)	<b>30½</b> (775)	_	_	<b>11,780</b> (52.4)			
<b>1</b>	13/16	<b>10</b> 1/8 (257)	<b>15</b> 1/4 (387)	<b>17¾</b> (451)	<b>67,600</b> (300.7)	_	<b>16,900</b> (75.2)	<b>19,025</b> (84.6)	<b>41,000</b> (182.4)	<b>27,880</b> (124.0)
		<b>13½</b> (343)	<b>20</b> 1/4 (514)	<b>54</b> (1372)	_	_	<b>21,385</b> (95.1)			
		<b>16</b> % (429)	<b>25</b> % (645)	<b>67½</b> (1715)	<b>103,460</b> (460.2)	_	<b>25,865</b> (115.1)			
		<b>5</b> % (143)	<b>87/16</b> (214)	<b>22½</b> (572)	<b>32,368</b> (144.0)	<b>2,054</b> (9.1)	<b>8,090</b> (36.0)			
		<b>87/</b> 16 (214)	<b>12¾</b> (324)	<b>33¾</b> (857)	_	_	<b>13,090</b> (58.2)			
<b>1</b> 1/4 (31.8)	1 5/16	<b>111/4</b> (286)	<b>16</b> % (429)	<b>19¾</b> (502)	<b>72,363</b> (321.9)	<b>7,457</b> (33.2)	<b>18,090</b> (80.5)	<b>23,490</b> (104.5)	<b>50,620</b> (225.2)	<b>34,420</b> (153.1)
		<b>15</b> (381)	<b>22½</b> (572)	<b>60</b> (1524)	_	_	<b>24,860</b> (110.6)	(101.0) (210.1)	(1.551.)	
		<b>18¾</b> (476)	<b>28</b> 1/8 (714)	<b>75</b> (1905)	<b>126,500</b> (562.7)	<b>15,813</b> (70.3)	<b>31,625</b> (140.7)			

1. Reference page 318 for oversize holes.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

- 2. Allowable load must be the lesser of the bond or steel strength.
- 3. The allowable loads listed under allowable bond are based on a safety factor of 4.0.
- 4. Refer to allowable load-adjustment factors for spacing and edge distance on pages 97, 99 and 100.
- $5. \, \text{Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.} \\$
- 6. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.
- Anchors are not permitted to resist tension forces in overhead or wall installations unless proper consideration is given to fire-exposure and elevated-temperature conditions.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

SIMPSON Strong-Tie

AT Allowable Shear Loads for Threaded Rod Anchors in Normal-Weight Concrete

IBC	





		Embed.	Critical	Critical		ar Load Base rete Edge Dis		Shear Load Based on Steel Strength		
Dia. in.	Bit Dia.	Depth in.	Edge Dist. in.	Spacing Dist. in.	(13	f' <sub>c</sub> ≥ 2,000 ps .8 MPa) Conc	i rete	F1554 Grade 36	A193 GR B7	F593 304SS
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
		<b>13/4</b> (44)		<b>25/8</b> (67)	<b>4,869</b> (21.7)	<b>369</b> (1.6)	<b>1,215</b> (5.4)			
<b>3/8</b> (9.5)	7/16	<b>3½</b> (89)	<b>5</b> 1⁄4 (133)	<b>5</b> ½ (133)	<b>5,540</b> (24.6)	<b>620</b> (2.8)	<b>1,385</b> (6.2)	<b>1,085</b> (4.8)	<b>2,340</b> (10.4)	<b>1,870</b> (8.3)
		<b>4½</b> (114)		<b>51/4</b> (133)	_	_	<b>1,385</b> (6.2)			
		<b>2</b> 1/8 (54)		<b>31/4</b> (83)	<b>8,318</b> (37.0)	<b>643</b> (2.9)	<b>2,080</b> (9.3)			<b>3,330</b> (14.8)
<b>½</b> (12.7)	9/16	<b>4½</b> (108)	<b>6</b> % (162)	<b>6</b> % (162)	<b>9,998</b> (44.5)	<b>522</b> (2.3)	<b>2,500</b> (11.1)	<b>1,930</b> (8.6)	<b>4,160</b> (18.5)	
		<b>6</b> (152)		<b>6</b> % (162)	_	_	<b>2,500</b> (11.1)			
		<b>2½</b> (64)		<b>3¾</b> (95)	<b>14,806</b> (65.9)	<b>728</b> (3.2)	<b>3,700</b> (16.5)			
<b>5%</b> (15.9)	11/16	<b>5½</b> (140)	<b>7½</b> (191)	<b>81/4</b> (210)	<b>15,692</b> (69.8)	<b>305</b> (1.4)	<b>3,925</b> (17.5)	<b>3,025</b> (13.5)	<b>6,520</b> (29.0)	<b>5,220</b> (23.2)
		<b>9</b> % (238)		<b>81/4</b> (210)	_	_	<b>3,925</b> (17.5)			
		<b>3</b> % (86)		<b>5</b> 1/8 (130)	<b>20,350</b> (90.5)	_	<b>5,090</b> (22.6)	<b>4,360</b> (19.4)		
<b>3/4</b> (19.1)	13/16	<b>6¾</b> (171)	<b>10</b> 1/8 (257)	<b>10</b> 1/8 (257)	<b>20,350</b> (90.5)	<b>1,521</b> (6.8)	<b>5,090</b> (22.6)		<b>9,390</b> (41.8)	<b>6,385</b> (28.4)
		<b>11</b> ½ (286)		<b>10</b> 1/8 (257)	_	_	<b>5,090</b> (22.6)			
		<b>3</b> % (98)		<b>5</b> % (149)	<b>27,475</b> (122.2)	<b>1,655</b> (7.4)	<b>6,870</b> (30.6)		<b>12,770</b> (56.8)	<b>8,685</b> (38.6)
<b>7/8</b> (22.2)	1	<b>7</b> 3/4 (197)	<b>11%</b> (295)	<b>11%</b> (295)	<b>30,876</b> (137.3)	<b>1,714</b> (7.6)	<b>7,720</b> (34.3)	<b>5,925</b> (26.4)		
		<b>13</b> 1/8 (333)		<b>11%</b> (295)	_	_	<b>7,720</b> (34.3)			
		<b>4½</b> (114)		<b>6¾</b> (171)	<b>32,687</b> (145.4)	<b>2,287</b> (10.2)	<b>8,170</b> (36.3)			
<b>1</b> (25.4)	1 ½16	<b>9</b> (229)	<b>13½</b> (343)	<b>13½</b> (343)	<b>33,858</b> (150.6)	<b>2,035</b> (9.1)	<b>8,465</b> (37.7)	<b>7,740</b> (34.4)	<b>16,680</b> (74.2)	<b>11,345</b> (50.5)
		<b>15</b> (381)		<b>13½</b> (343)	_	_	<b>8,465</b> (37.7)			
		<b>5</b> 1/8 (130)		<b>7</b> 3/4 (197)	<b>41,536</b> (184.8)	_	<b>10,385</b> (46.2)			
<b>1 </b> 1/8 (28.6)	13/16	<b>10</b> 1/8 (257)	<b>15</b> 1/4 (387)	<b>15</b> ½ (387)	<b>49,812</b> (221.6)	_	<b>12,455</b> (55.4)	<b>9,800</b> (43.6)	<b>21,125</b> (94.0)	<b>14,365</b> (63.9)
		<b>16</b> % (429)		<b>15</b> 1⁄ <sub>4</sub> (387)	_	_	<b>12,455</b> (55.4)			
		<b>5</b> % (143)		<b>8½</b> (216)	<b>50,385</b> (224.1)	<b>1,090</b> (4.8)	<b>12,595</b> (56.0)			
<b>1 1/4</b> (31.8)		<b>11</b> ½ (286)	<b>16</b> % (429)	<b>16</b> % (429)	<b>65,765</b> (292.5)	<b>4,636</b> (20.6)	<b>16,440</b> (73.1)	<b>12,100</b> (53.8)	<b>26,075</b> (116.0)	<b>17,730</b> (78.9)
		<b>18¾</b> (476)		<b>16</b> % (429)	_	_	<b>16,440</b> (73.1)			

<sup>1.</sup> Allowable load must be the lesser of the load based on concrete edge distance or steel strength.

<sup>2.</sup> The allowable loads based on concrete edge distance are based on a safety factor of 4.0.

<sup>3.</sup> Refer to allowable load-adjustment factors for spacing and edge distance on pages 98 and 100.

<sup>4.</sup> Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.

<sup>5.</sup> Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only.
For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **AT** Design Information — Concrete



### AT Allowable Tension Loads for Rebar Dowels in Normal-Weight Concrete

7 (1 7 (1)	JVVUD	10 10110	JOH LOC	200 101	Hobai D	0000111	MOITHAI-V	voigint O	31101010		
Rebar	Drill	Embed.	Critical Edge	Critical			n Load Base	d on Bond S	trength		Tension Load Based on Steel Strength
Size No.	Bit Dia.	Depth in.	Dist. in.	Spacing Dist. in.	f (13.	' <sub>c</sub> ≥ 2,000 ps 8 MPa) Cond	si crete	f (27.	' <sub>c</sub> ≥ 4,000 ps 6 MPa) Cond	si erete	ASTM A615 Grade 60 Rebar
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
#3	1/2	<b>3½</b> (89)	<b>5</b> 1/4 (133)	<b>6</b> 1/8 (156)	<b>8,245</b> (36.7)	<b>849</b> (3.8)	<b>2,060</b> (9.2)	_	_	<b>2,060</b> (9.2)	2,640
(9.5)	/2	<b>4½</b> (114)	<b>5</b> 1/4 (133)	<b>6</b> 1/8 (156)	_	_	<b>2,060</b> (9.2)	_	_	<b>2,060</b> (9.2)	(11.7)
		<b>4½</b> (108)	<b>6</b> % (162)	<b>7½</b> (191)	<b>12,743</b> (56.7)	<b>1,760</b> (7.8)	<b>3,185</b> (14.2)	_	_	<b>3,185</b> (14.2)	
<b>#4</b> (12.7)	9/16	<b>5</b> % (149)	<b>8</b> 7/8 (225)	<b>23½</b> (597)	_	_	<b>3,185</b> (14.2)	_	_	<b>3,985</b> (17.7)	<b>4,800</b> (21.4)
		<b>7½</b> (191)	<b>11</b>	<b>30</b> (762)	_	_	<b>3,185</b> (14.2)	<b>19,124</b> (85.1)	<b>854</b> (3.8)	<b>4,780</b> (21.3)	
		<b>5½</b> (140)	<b>7½</b> (191)	<b>9</b> 5⁄8 (244)	<b>20,396</b> (90.7)	<b>1,412</b> (6.3)	<b>5,100</b> (22.7)	_	_	<b>5,100</b> (22.7)	
<b>#5</b> (15.9)	3/4	<b>7½</b> (184)	<b>10</b> % (276)	<b>29</b> (737)	_	_	<b>5,100</b> (22.7)	_	_	<b>6,095</b> (27.1)	<b>7,440</b> (33.1)
		<b>9</b> % (191)	<b>14</b> 1/8 (359)	<b>37½</b> (953)	_	_	<b>5,100</b> (22.7)	<b>28,115</b> (125.1)	<b>1,496</b> (6.7)	<b>7,030</b> (31.3)	
		<b>6¾</b> (171)	<b>10</b> 1/8 (257)	<b>11</b> % (302)	<b>31,839</b> (141.6)	<b>1,454</b> (6.5)	<b>7,960</b> (35.4)	_	_	<b>7,960</b> (35.4)	
<b>#6</b> (19.1)	7/8	<b>9</b> (229)	<b>13½</b> (343)	<b>36</b> (914)	_	_	<b>7,960</b> (35.4)	_	_	<b>8,730</b> (38.8)	<b>10,560</b> (47.0)
		<b>11</b> 1/4 (286)	<b>16</b> % (429)	<b>45</b> (1143)	_	_	<b>7,960</b> (35.4)	<b>37,992</b> (169.0)	<b>1,999</b> (8.9)	<b>9,500</b> (42.3)	
		<b>7¾</b> (197)	<b>11</b> % (295)	<b>13</b> % (346)	<b>35,250</b> (156.8)	<b>2,693</b> (12.0)	<b>8,815</b> (39.2)	_	_	<b>8,815</b> (39.2)	
<b>#7</b> (22.2)	1	<b>10½</b> (267)	<b>15</b> % (400)	<b>42</b> (1067)	_	_	<b>8,815</b> (39.2)	_	_	<b>10,815</b> (48.1)	<b>14,400</b> (64.1)
		<b>13</b> 1/8 (333)	<b>19</b> % (498)	<b>52½</b> (1334)	_	_	<b>8,815</b> (39.2)	<b>50,889</b> (226.4)	<b>3,717</b> (16.5)	<b>12,720</b> (56.6)	
		<b>9</b> (229)	<b>13½</b> (343)	<b>15¾</b> (400)	<b>49,973</b> (222.3)	<b>5,023</b> (22.3)	<b>12,495</b> (55.6)	_	_	<b>12,495</b> (55.6)	
<b>#8</b> (25.4)	11/8	<b>12</b> (305)	<b>18</b> (457)	<b>48</b> (1219)	_	_	<b>12,495</b> (55.6)	_	_	<b>16,325</b> (72.6)	<b>18,960</b> (84.3)
		<b>15</b> (381)	<b>22½</b> (572)	<b>60</b> (1524)	_	_	<b>12,495</b> (55.6)	<b>80,598</b> (358.5)	<b>2,195</b> (9.8)	<b>20,150</b> (89.6)	
<b>#9</b> (28.6)	1 1/4	<b>16</b> % (429)	<b>25</b> % (645)	<b>67½</b> (1715)	_	_	_	<b>96,096</b> (427.5)	<b>489</b> (2.2)	<b>24,025</b> (106.9)	<b>24,000</b> (106.8)
<b>#10</b> (31.8)	1%	<b>18</b> 3/4 (476)	<b>28</b> 1/8 (714)	<b>75</b> (1905)	_	_	_	<b>124,031</b> (551.7)	<b>2,447</b> (10.9)	<b>31,010</b> (137.9)	<b>30,480</b> (135.6)
<b>#11</b> (34.9)	1%	<b>20</b> % (524)	<b>31</b> (787)	<b>82½</b> (2096)	_	_	_	<b>166,059</b> (738.7)	<b>4,222</b> (18.8)	<b>41,515</b> (184.7)	<b>37,440</b> (166.5)

- 1. Allowable load must be the lesser of the bond or steel strength.
- 2. The allowable loads listed under allowable bond are based on a safety factor of 4.0.
- 3. Refer to allowable load-adjustment factors for spacing and edge distance on pages 97, 99 and 100.
- 4. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.
- Anchors are not permitted to resist tension forces in overhead or wall installations unless proper consideration is given to fire-exposure and elevated-temperature conditions.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



# AT Allowable Shear Loads for Rebar Dowels in Normal-Weight Concrete



Rebar	D D	Embed.	Critical	Critical		ar Load Base rete Edge Dis		Shear Load Based on Steel Strength
Size No.	Drill Bit Dia. in.	Depth in.	Edge Dist. in.	Spacing Dist. in.	f' <sub>c</sub> ≥ 2,000	psi (13.8 MP	a) Concrete	ASTM A615 Grade 60 Rebar
(mm)		(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
#3	1/2	<b>3½</b> (89)	6	51/4	<b>8,294</b> (36.9)	<b>515</b> (2.3)	<b>2,075</b> (9.2)	1,680
(9.5)	72	<b>4½</b> (114)	(152)	(133)	_	_	<b>2,075</b> (9.2)	(7.5)
#4	9/16	<b>4½</b> (108)	8	6%	<b>11,012</b> (49.0)	<b>383</b> (1.7)	<b>2,755</b> (12.3)	3,060
(12.7)	716	<b>7½</b> (191)	(203)	(162)	_	_	<b>2,755</b> (12.3)	(13.6)
#5	3/4	<b>5½</b> (140)	10	81/4	<b>15,758</b> (70.1)	<b>1,154</b> (5.1)	<b>3,940</b> (17.5)	4,740
(15.9)	94	<b>9</b> % (238)	(254)	(210)	_	_	<b>3,940</b> (17.5)	(21.1)
#6	7/	<b>6¾</b> (171)	12	101/8	<b>23,314</b> (103.7)	<b>1,494</b> (6.6)	<b>5,830</b> (25.9)	6,730
(19.1)	7/8	<b>111/4</b> (286)	(305)	(257)	_	_	<b>5,830</b> (25.9)	(29.9)
#7	1	<b>7¾</b> (197)	14	11%	<b>32,662</b> (145.3)	<b>5,588</b> (24.9)	<b>8,165</b> (36.3)	9,180
(22.2)		<b>13</b> 1/8 (333)	(356)	(295)		_	<b>8,165</b> (36.3)	(40.8)
<b>#8</b> (25.4)	11/8	<b>9</b> (229)	16	13½	<b>33,428</b> (148.7)	<b>2,319</b> (10.3)	<b>8,360</b> (37.2)	12,085
	1 78	<b>15</b> (381)	(406)	13½ (343)	_	_	<b>8,360</b> (37.2)	(53.8)

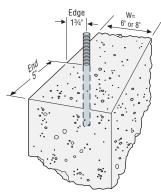
- 1. Allowable load must be the lesser of the load based on concrete edge distance or steel strength.
- 2. The allowable loads based on concrete edge distance are based on a safety factor of 4.0.
- 3. Refer to allowable load-adjustment factors for spacing and edge distance on pages 98 and 100.
- 4. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

# AT Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete Stemwall



De d Die	Duitt Dit	Embed.	Stemwall	Min.	Min.		ad Based on Strength	Tension Load Based on Steel Strength
Rod Dia. in. (mm)	in. Dia. Depth Width Dist. Dist. fin. in. in. in. in. in. in. in. in. in.			,500 psi a) Concrete	F1554 Grade 36			
		(mm) 	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lbs. (kN)	Allowable lbs. (kN)
<b>5%</b> (15.9)	11/16	<b>10</b> (254.0)	<b>6</b> (152.4)	<b>13/4</b> (44.5)	<b>5</b> (127.0)	<b>12,913</b> (57.4)	<b>3,230</b> (14.4)	<b>5,875</b> (26.1)
<b>7/8</b> (22.2)	1	<b>15</b> (381.0)	<b>8</b> (203.2)	<b>13/4</b> (44.5)	<b>5</b> (127.0)	<b>21,838</b> (97.1)	<b>5,460</b> (24.3)	<b>11,500</b> (51.2)

- 1. Allowable load must be the lesser of the bond or steel strength.
- 2. The allowable loads listed under allowable bond are based on a safety factor of 4.0.
- 3. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 4. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.



Edge and end distances for threaded rod in concrete foundation stemwall corner installation

<sup>\*</sup> See page 12 for an explanation of the load table icons.



### AT Allowable Tension Loads for Threaded Rod Anchors in Sand-Lightweight Concrete

ii i Oai i	u Ligi	twoignit	00110101	0													
Rod	Drill	in. Dist.	Critical		ion Load Baso Bond Strengtl		Tension Load Based on Steel Strength										
Dia. in.	Bit Dia.		in.	in.	in.	Depth in.	Depth in.	Depth in.	Depth in.	Depth	Dist.	Spacing Dist. in.	Dist. T <sub>c</sub> ≥ 3,000 psi (20.7 MPa)			F1554 Grade 36	A193 GR B7
(mm)	ın.	in. (mm) (mm)		(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)							
3/8	7/	<b>13/4</b> (44)	<b>2</b> % (67)	<b>3½</b> (89)	<b>2,842</b> (12.6)	<b>226</b> (1.0)	<b>710</b> (3.2)	2,105	<b>4,535</b> (20.2)	3,630							
(9.5)	7/16	<b>3½</b> (89)	<b>5</b> 1/4 (133)	<b>7</b> (178)	<b>5,132</b> (22.8)	<b>762</b> (3.4)	<b>1,280</b> (5.7)	(9.4)		(16.1)							
1/2	0/	<b>2</b> 1/8 (54)	<b>3</b> 1/8 (79)	<b>4½</b> (108)	<b>4,415</b> (19.6)	<b>454</b> (2.0)	<b>1,100</b> (4.9)	3,750	8,080	6,470							
(12.7)	9/16	<b>4½</b> (108)	<b>6</b> % (162)	<b>8½</b> (216)	<b>6,709</b> (29.8)	<b>1,002</b> (4.5)	<b>1,675</b> (7.5)	(16.7)	(35.9)	(28.8)							
5/8	11/	<b>2½</b> (64)	<b>3¾</b> (95)	<b>5</b> (127)	<b>5,568</b> (24.8)	<b>498</b> (2.2)	<b>1,390</b> (6.2)	5,875	12,660	10,120							

1,155

1,575

(7.0)

(191)1. Allowable load must be the lesser of the bond or steel strength.

(127)

71/2

11/16

(15.9)

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

2.100% of the allowable load is permitted at critical spacing. No reduction in spacing is allowed.

10

(254)

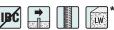
- 3. Refer to allowable load-adjustment factors for edge distance on page 101.
- 4. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.
- 6. Anchors are not permitted to resist tension forces in overhead or wall installations unless proper consideration is given to fire-exposure and elevated-temperature conditions.

6,298

(28.0)

7. The allowable loads listed under allowable bond are based on a safety factor of 4.0.

### AT Allowable Shear Loads for Threaded Rod Anchors in Sand-Lightweight Concrete



(26.1)

(56.3)

(45.0)

Rod	Drill	Embed. Depth in.	Denth   Eage				ar Load Base rete Edge Dis		Shear Load Based on Steel Strength			
Dia. in.	Bit Dia.		Dist. in.	Dist.	hist. 1'c ≥ 3,000 psi (20.7 MPa)			F1554 Grade 36	A193 GR B7	F593 304SS		
(mm) in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)			
3/8	7/16	<b>1</b> 3/4 (44)	<b>2</b> 5/8 (67)	<b>3½</b> (89)	<b>3,042</b> (13.5)	<b>249</b> (1.1)	<b>760</b> (3.4)	1,085	2,340	1,870		
(9.5)	'/16	<b>3½</b> (89)	<b>5</b> ½ (133)	<b>7</b> (178)	<b>5,320</b> (23.7)	<b>187</b> (0.8)	<b>1,330</b> (5.9)	(4.8)	(10.4)	(8.3)		
1/2	9/16	<b>2</b> 1/8 (54)	<b>3</b> 1/8 (79)	<b>4½</b> (108)	<b>4,076</b> (18.1)	<b>458</b> (2.0)	<b>1,020</b> (4.5)	1,930	<b>4,160</b> (18.5)	3,330		
(12.7)	%16	<b>4½</b> (108)	<b>6</b> % (162)	<b>8½</b> (216)	<b>9,838</b> (43.8)	<b>625</b> (2.8)	<b>2,460</b> (10.9)	(8.6)		(14.8)		
5/8	11/	<b>2½</b> (64)	<b>3¾</b> (95)	<b>5</b> (127)	<b>5,360</b> (23.8)	<b>351</b> (1.6)	<b>1,340</b> (6.0)	3,025	6,520	5,220		
(15.9)	<b>5</b> (127)	<b>7½</b> (191)	<b>10</b> (254)	<b>12,430</b> (55.3)	<b>518</b> (2.3)	<b>3,105</b> (13.8)	(13.5)	(29.0)	(23.2)			

- 1. Allowable load must be the lesser of the load based on concrete edge distance or steel strength.
- 2. The allowable loads based on concrete edge distance are based on a safety factor of 4.0.
- 3. Refer to allowable load-adjustment factors for edge distance on page 101.
- 4. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.
- 6.100% of the allowable load is permitted at critical spacing. No reduction in spacing is allowed.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **AT** Design Information — Masonry



AT Allowable Tension and Shear Loads for Threaded Rod Anchors in 6- and 8-Inch Normal-Weight Grout-Filled CMI I

Ancho	nchors in 6- and 8-inch Normal-Weight Grout-Filled Civio												
Rod Dia.	a. Bit Depth Edge End Spacing		Spacing	Allowable L	t-Filled CMU oads Based Strength	8-Inch Grout-Filled CMU Allowable Loads Based on CMU Strength							
in.	Dia.	iń.	Dist. in.	Dist. in.	Dist. in.	Tension	Shear	Tension	Shear				
(mm)	in.	(mm)	(mm)	(mm)	(mm)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)				
Anchor Installed in Face Shell (See Figure 1)													
1/2 (12.7)	9/16	<b>4½</b> (108)	<b>12</b> (305)	<b>12</b> (305)	<b>17</b> (432)	<b>770</b> (3.4)	<b>1,325</b> (5.9)	<b>770</b> (3.4)	<b>1,325</b> (5.9)				
3/4	13/16	63/4	12	<b>4</b> (102)	<b>27</b> (686)	_	_	<b>1,375</b> (6.1)	_				
(19.1)	19/16	(171)	(305)	<b>12</b> (305)	<b>27</b> (686)	_	_	_	<b>2,670</b> (11.9)				
	Anchor Installed in Mortar "T" Joint (See Figure 2)												
<b>3/4</b> (19.1)	13/16	<b>6¾</b> (171)	<b>16</b> (406)	<b>8</b> (203)	<b>27</b> (686)	_	_	_	<b>1,030</b> (4.6)				

See notes 1-7 below

(19.1)

AT Allowable Tension and Shear Loads for Threaded Rod

(406)

(203)

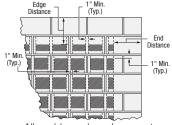
(686)

ncnor	s in 6-	and 8-in	cn Norm	ıaı-vveigr	it Grout-F	-Illea CIVIU	634 634 634 63		
Dia.	Drill	Embed.	Min.	Min. End Dist. in. (mm)	Min. Spacing - Dist. in. (mm)	6- and 8-Inch Grout-Filled CMU Allowable Loads Based on CMU Strength			
	Bit Dia.	Depth in. (mm)	Edge Dist.			Tension	Shear Perpendicular <sup>8</sup>	Shear Parallel <sup>9</sup>	
	in.		in. (mm)			Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	

Dia. in.	Bit Dia.	Depth in.	Dist. in.	Dist. in.	Dist. in.	Tension	Shear Perpendicular <sup>8</sup>	Shear Parallel <sup>9</sup>
(mm)	in.	(mm)	(mm)	(mm)	(mm)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
		And	chor Installe	ed in Cell O <sub>l</sub>	pening (Top-	of-Wall) (See Fi	gure 3)	
<b>½</b> (12.7)	9/16	<b>4½</b> (108)	13/4 (44)	<b>11</b> (279)	<b>17</b> (432)	<b>650</b> (2.9)	<b>285</b> (1.3)	<b>705</b> (3.1)
5/8	11/16	<b>5</b> (127)	<b>1</b> 3/4 (44)	<b>11</b> (279)	<b>20</b> (508)	<b>815</b> 3.6	<b>330</b> (1.5)	<b>755</b> (3.4)
(15.9)	. 716	<b>12</b> (305)	13/4 (44)	<b>11</b> (279)	<b>48</b> (1219)	<b>1,120</b> (5.0)	<b>410</b> (1.8)	<b>815</b> (3.6)
7/8 (22.2)	1	<b>12</b> (305)	<b>1</b> 3/4 (44)	<b>11</b> (279)	<b>48</b> (1219)	<b>1,385</b> (6.2)	<b>290</b> (1.3)	<b>1,030</b> (4.6)

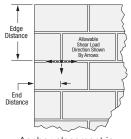
- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- 2. Values for 6- and 8-inch wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry, f'<sub>m</sub>, at 28 days is 1500 psi.
- 3. Embedment depth is measured from the outside face of the concrete masonry unit for installations through a face shell.
- 4. Allowable loads may be increased 331/3% for shortterm loading due to wind or seismic forces where permitted by code.
- 5. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 6. The tabulated allowable loads are based on a safety factor of 5.0.
- 7. Anchors must be spaced a minimum distance of four times the anchor embedment.
- 8. Shear load applied perpendicular to edge of
- 9. Shear load applied parallel to edge of CMU wall.

Figure 1



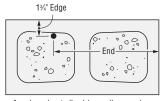
Allowable anchor placement in grouted CMU face shell

Figure 2



Anchor placement in grouted CMU mortar "T" joint

Figure 3



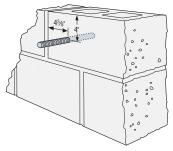
Anchor installed in cell opening (top of wall)

### AT Allowable Tension and Shear Loads for Threaded Rod Anchors in Lightweight, Medium-Weight and Normal-Weight Hollow CMU

1 VOITTICA	vvoigin	. I IOIIOVV C	71410					
Rod	Drill	Embed.	Min. Edge	Min. End	6- and	8-Inch Hollow Based on Cl	CMU Allowabl MU Strength	e Loads
Dia. in.	Bit Dia.	Depth in.	Dist.	Dist.	Tens	sion	Sh	ear
(mm)	in.	(mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
An	chor Insta	lled in Face S	Shell with Sir	npson Stong	-Tie® Stainless	s-Steel Screen	Tube (See Fig	jure 4)
<b>3/8</b> (9.5)	9/16	<b>3½</b> (88.9)	<b>4</b> (101.6)	<b>4</b> % (117.5)	<b>1,400</b> (6.2)	<b>280</b> (1.2)	<b>1,326</b> (5.9)	<b>265</b> (1.2)
1/2 (12.7)	11/16	3½ (88.9)	<b>4</b> (101.6)	<b>4</b> 5/8 (117.5)	_	<b>280</b> (1.2)	_	<b>265</b> (1.2)
<b>5/8</b> (15.9)	7/8	<b>3</b> (76.2)	<b>4</b> (101.6)	<b>45%</b> (117.5)		<b>280</b> (1.2)	_	<b>265</b> (1.2)

- 1. See notes 1, 2, 3, 5, 6, 7 above.
- 2. Set drill to rotation-only mode when drilling into hollow CMU.

### Figure 4



Anchor installed in face shell with screen tube in hollow cell

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **AT** Design Information — Masonry

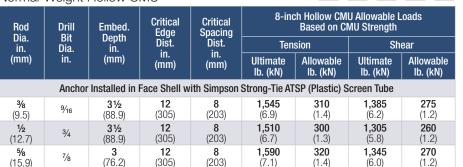


AT Allowable Tension and Shear Loads for Installations in Unreinforced Brick Masonry Walls—Minimum URM Wall Thickness is 13" (3 wythes thick)

						,	
Rod/Rebar	Drill	Embed.	Min. Edge/End	Min. Vertical	Min. Horiz.	Tension Load Based on URM Strength	Shear Load Based on URM Strength
Dia./Size in. (mm)	Bit Dia. in.	Depth in. (mm)	Ďist. in.	Spacing Dist. in.	Spacing Dist. in.	Minimum Net Mortar Strength = 50 psi	Minimum Net Mortar Strength = 50 psi
` ′			(mm)	(mm)	(mm)	Allowable lb. (kN)	Allowable lb. (kN)
	С	onfigurati	on A (Simpso	on Strong-1	Tie® ATS or	ATSP Screen Tube Requ	ired)
<b>3/4</b> (19.1)	1	<b>8</b> (203)	<b>24</b> (610)	<b>18</b> (457)	<b>18</b> (457)	_	<b>1,000</b> (4.4)
<b>#5</b> (15.9)	1	<b>8</b> (203)	<b>24</b> (610)	<b>18</b> (457)	<b>18</b> (457)	_	<b>750</b> (3.3)
<b>#6</b> (19.1)	1	<b>8</b> (203)	<b>24</b> (610)	<b>18</b> (457)	<b>18</b> (457)	_	<b>1,000</b> (4.4)
	(	Configurati	ion B (Simps	on Strong-	Tie ATS or	ATSP Screen Tube Requi	red)
<b>3/4</b> (19.1)	1	<b>13</b> (330)	<b>16</b> (406)	<b>18</b> (457)	<b>24</b> (610)	<b>1,200</b> (5.3)	<b>1,000</b> (4.4)
	Configu	ration C (S	Simpson Stro	ng-Tie ATS	Screen Tu	be and AST Steel Sleeve	Required)
<b>5%</b> (15.9)	1	**	<b>24</b> (610)	<b>18</b> (457)	<b>18</b> (457)	<b>1,200</b> (5.3)	<b>750</b> (3.3)

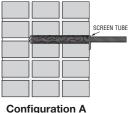
- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- 2. All holes are drilled with a 1" diameter carbide-tipped drill bit with the drill set in the rotation-only mode.
- 3. The unreinforced brick walls must have a minimum thickness of 13 inches (three wythes of brick).
- 4. The allowable load is applicable only where in-place shear tests indicate minimum net mortar strength of 50 psi.
- 5. The allowable load for Configuration B and C anchors subjected to a combined tension and shear load is determined by assuming a straight-line relationship between allowable tension and shear.
- 6. The anchors installed in unreinforced brick walls are limited to resisting seismic or wind forces only.
- Configuration A has a straight threaded rod or rebar embedded 8 inches into the wall with a <sup>3</sup>½" diameter by 8-inch long screen tube (part # ATS758 or ATS758P). This configuration is designed to resist shear loads only.
- 8. Configuration B has a ¾" threaded rod bent and installed at a 22.5-degree angle and installed 13 inches into the wall, to within 1-inch (maximum) of the exterior wall surface. This configuration is designed to resist tension and shear loads. The pre-bent threaded rod is installed with a <sup>3</sup>½" diameter by 13-inch long screen tube (part # ATS7513 or ATS7513P).
- 9. Configuration C is designed to resist tension and shear forces. It consists of a %" diameter, ASTM F1554 Grade 36 threaded rod and an 8" long steel sleeve (part # AST800) and a <sup>3</sup>/½" diameter by 8-inch long screen tube (part # ATS758). The steel sleeve has a plastic plug in one end. A 6" by 6" by %" thick ASTM A 36 steel plate is located on the back face of the wall.
- Special inspection requirements are determined by local jurisdiction and must be confirmed by the local building official.
- 11. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.

### AT Allowable Tension and Shear Loads for Threaded Rod Anchors in Lightweight, Medium-Weight and Normal-Weight Hollow CMU

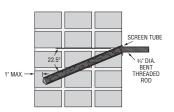


**IBC** 

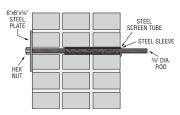
- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- 2. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.
- Edge distances may be reduced to 4" with a corresponding 37% reduction in tension capacity. Shear capacity is unaffected.
- 4. Values for 8-inch wide, lightweight, medium-weight and normal-weight concrete masonry units with min. compressive strength of 1,900 psi and 11/4" thick face shell.
- 5. Embedment depth is measured from the outside face of the concrete masonry unit.
- 6. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 7. Set drill to rotation-only mode when drilling into hollow CMU.



Configuration A (Shear)



Configuration B (Tension & Shear)



Configuration C (Tension & Shear)

# Installation Instructions for Configuration C

- Drill hole perpendicular to the wall to a depth of 8" with a 1" diameter carbide-tipped drill bit (rotation only mode).
- 2. Clean hole with oil-free compressed air and a nylon brush.
- 3. Fill 8" steel screen tube with mixed adhesive and insert into hole.
- 4. Insert steel sleeve slowly into screen tube (adhesive will displace).
- 5. Allow adhesive to cure (see cure schedule).
- 6. Drill through plastic plug in (inside) end of steel sleeve with \( \frac{\pi}{n} \) bit.
- 7. Drill completely through the wall with %" carbide tipped concrete drill bit (rotation mode only).
- 8. Insert %" rod through hole and attach metal plate and nut.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **AT** Design Information — Masonry

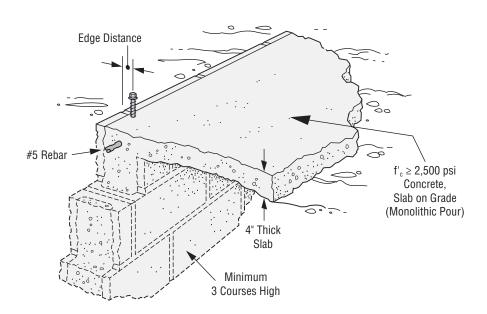


AT Allowable Tension Loads for Threaded Rod Anchors in 8-inch Lightweight, Medium-Weight and Normal-Weight CMU Chair Blocks Filled with Normal-Weight Concrete

IBC		*
-----	--	---

		Min.	Min.	Critical -	8-inch Con CMU Cha	crete-Filled air Block
Rod Dia. in. (mm)	Drill Bit Dia. in.	Embed. Depth in.	Edge Dist. in.	Spacing Dist. in.	Allowable Te Based on Cl	nsion Loads MU Strength
()	""	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)
		<b>4½</b> (114)	<b>13/4</b> (44.5)	<b>18</b> (457)	<b>3,540</b> (15.7)	<b>710</b> (3.2)
<b>½</b> (12.7)	9/16	<b>7</b> (178)	<b>13/4</b> (44.5)	<b>28</b> (711)	<b>6,285</b> (28.0)	<b>1,255</b> (5.6)
		<b>12</b> (305)	<b>13/4</b> (44.5)	<b>48</b> (1,220)	<b>18,950</b> (84.3)	<b>3,750</b> (16.7)
		<b>4½</b> (114)	<b>1¾</b> (44.5)	<b>18</b> (457)	<b>4,775</b> (21.2)	<b>955</b> (4.2)
5/8	11/	<b>7</b> (178)	<b>1¾</b> (44.5)	<b>28</b> (711)	<b>7,960</b> (35.4)	<b>1,590</b> (7.1)
(15.9)	) 11/16	<b>12</b> (305)	<b>13/4</b> (44.5)	<b>48</b> (1,219)	_	<b>3,400</b> (15.1)
		<b>15</b> (381)	<b>13/4</b> (44.5)	<b>60</b> (1,524)	<b>22,425</b> (99.8)	<b>4,485</b> (20.0)

- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- 2. Values are for 8-inch wide concrete masonry units CMU filled with concrete with minimum compressive strength of 2,500 psi and poured monolithically with the floor slab.
- 3. Center #5 rebar in CMU cell and concrete slab as shown.
- 4. The tabulated allowable loads are based on a safety factor of 5.0.



<sup>\*</sup> See page 12 for an explanation of the load table icons.



AT Allowable Load Adjustment Factors in Normal-Weight Concrete: Edge Distance, Tension Load

### How to use these charts

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance ( $c_{act}$ ) at which the anchor is to be installed.
- 5. The load-adjustment factor (f<sub>c</sub>) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple edges are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- 9. Adjustment factors are to be applied to allowable tension load based on bond strength values only.

### Edgo Dictanco Toncion (f.)

	Dia.		3/8			1/2				5/8			3/4	
Edge	Rebar		#	3		#4		#4		#	5		#	6
Dist.	E	13/4	31/2	41/2	21/8	41/4	6	71/2	21/2	51/2	9%	3%	63/4	111/4
cact	Ccr	2%	51/4	6¾	33/16	6%	9	111/4	3¾	71/2	141/8	51/16	101/8	16%
(in.)	C <sub>min</sub>	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13⁄4
	f <sub>cmin</sub>	0.59	0.59	0.65	0.50	0.50	0.65	0.65	0.50	0.50	0.61	0.50	0.50	0.56
13/4		0.59	0.59	0.65	0.50	0.50	0.65	0.65	0.50	0.50	0.61	0.50	0.50	0.56
2		0.71	0.62	0.67	0.59	0.53	0.66	0.66	0.56	0.52	0.62	0.54	0.51	0.57
3		1.00	0.74	0.74	0.93	0.64	0.71	0.70	0.81	0.61	0.65	0.69	0.57	0.60
4			0.85	0.81	1.00	0.74	0.76	0.73	1.00	0.70	0.68	0.84	0.63	0.63
5			0.97	0.88		0.85	0.81	0.77		0.78	0.71	0.99	0.69	0.65
6			1.00	0.95		0.96	0.86	0.81		0.87	0.74	1.00	0.75	0.68
7				1.00		1.00	0.90	0.84		0.96	0.78		0.81	0.71
8							0.95	0.88		1.00	0.81		0.87	0.74
9							1.00	0.92			0.84		0.93	0.77
10								0.95			0.87		0.99	0.80
11								0.99			0.90		1.00	0.83
12								1.00			0.93			0.86
13											0.96			0.89
14											1.00			0.92
15														0.95
16														0.97
17														1.00









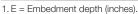


See notes below.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

### Edge Distance Tension (f<sub>c</sub>) (continued)

	Dia.		7/8			1			11/8			1 1/4		
Edge	Rebar		#	7		#	8			#9			#10	#11
Dist.	E	31/8	73/4	131/8	41/2	9	15	51/8	101/8	161/8	5%	111/4	18¾	20%
cact	Ccr	5 <sup>13</sup> / <sub>16</sub>	11%	19%	63/4	131/2	221/2	73/4	151/4	25%	87/16	16%	281/8	31
(in.)	Cmin	13/4	13/4	13/4	13/4	13/4	13/4	2¾	23/4	23/4	23/4	23/4	23/4	23/4
	f <sub>cmin</sub>	0.49	0.49	0.52	0.44	0.44	0.39	0.47	0.47	0.43	0.47	0.47	0.43	0.43
13/4		0.49	0.49	0.52	0.44	0.44	0.39							
23/4		0.62	0.54	0.55	0.55	0.49	0.42	0.47	0.47	0.43	0.47	0.47	0.43	0.43
4		0.77	0.61	0.58	0.69	0.55	0.46	0.60	0.52	0.46	0.59	0.52	0.46	0.46
6		1.00	0.71	0.63	0.92	0.64	0.51	0.81	0.61	0.51	0.77	0.59	0.50	0.50
8			0.81	0.69	1.00	0.74	0.57	1.00	0.69	0.56	0.96	0.67	0.55	0.54
10			0.92	0.74		0.83	0.63		0.78	0.61	1.00	0.74	0.59	0.58
12			1.00	0.80		0.93	0.69		0.86	0.66		0.82	0.64	0.62
14				0.85		1.00	0.75		0.95	0.71		0.89	0.68	0.66
16				0.90			0.81		1.00	0.76		0.97	0.73	0.70
18				0.96			0.87			0.81		1.00	0.77	0.74
20				1.00			0.93			0.86			0.82	0.78
22							0.99			0.91			0.86	0.82
24							1.00			0.97			0.91	0.86
26										1.00			0.95	0.90
28													1.00	0.94
30														0.98
32														1.00



<sup>2.</sup> cact = actual edge distance at which anchor is installed (inches).



<sup>3.</sup>  $c_{cr}$  = critical edge distance for 100% load (inches).

<sup>4.</sup>  $c_{min}$  = minimum edge distance for reduced load (inches).

<sup>5.</sup>  $f_c$  = adjustment factor for allowable load at actual edge distance.

<sup>6.</sup>  $f_{ccr}$  = adjustment factor for allowable load at critical edge distance.  $f_{ccr}$  is always = 1.00.

<sup>7.</sup>  $f_{cmin}$  = adjustment factor for allowable load at minimum edge distance.

<sup>8.</sup>  $f_c = f_{cmin} + [(1 - f_{cmin}) (c_{act} - c_{min}) / (c_{cr} - c_{min})].$ 

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC

### **AT** Design Information — Concrete



### AT Allowable Load Adjustment Factors in Normal-Weight Concrete: Edge Distance, Shear Load

#### How to use these charts

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or shear
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance (c<sub>act</sub>) at which the anchor is to be installed.
- 5. The load-adjustment factor ( $f_c$ ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple edges are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- 9. Adjustment factors are to be applied to allowable shear load based on concrete edge distance values only.

### Edge Distance Shear (f.)

Euge	DISTA	nce	SHE	ar (I <sub>C</sub> )	!																
	Dia.		3/8					1/2					5/8					3/4			
Edge	Rebar				#	3				#	4				#	5				#	6
Dist.	E	13/4	31/2	41/2	31/2	41/2	21/8	41/4	6	41/4	71/2	21/2	51/2	9%	51/2	9%	3%	63/4	111/4	63/4	111/4
Cact	C <sub>cr</sub>	51/4	51/4	51/4	6	6	6%	6%	6%	8	8	71/2	71/2	71/2	10	10	101/8	101/8	101/8	12	12
(in.)	C <sub>min</sub>	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4
	f <sub>cmin</sub>	0.40	0.35	0.39	0.19	0.39	0.18	0.15	0.25	0.16	0.25	0.12	0.11	0.14	0.10	0.14	0.10	0.11	0.14	0.10	0.14
13/4		0.40	0.35	0.39	0.19	0.39	0.18	0.15	0.25	0.16	0.25	0.12	0.11	0.14	0.10	0.14	0.10	0.11	0.14	0.10	0.14
23/4		0.57	0.54	0.56	0.38	0.53	0.36	0.33	0.41	0.29	0.37	0.27	0.26	0.29	0.21	0.24	0.21	0.22	0.24	0.19	0.22
3		0.61	0.58	0.61	0.43	0.57	0.40	0.38	0.45	0.33	0.40	0.31	0.30	0.33	0.24	0.27	0.23	0.24	0.27	0.21	0.24
31/2		0.70	0.68	0.70	0.52	0.64	0.49	0.47	0.53	0.40	0.46	0.39	0.38	0.40	0.29	0.32	0.29	0.30	0.32	0.25	0.29
4		0.79	0.77	0.78	0.62	0.71	0.58	0.56	0.61	0.46	0.52	0.46	0.46	0.48	0.35	0.37	0.34	0.35	0.37	0.30	0.33
41/2		0.87	0.86	0.87	0.71	0.78	0.67	0.66	0.70	0.53	0.58	0.54	0.54	0.55	0.40	0.43	0.40	0.40	0.42	0.34	0.37
5		0.96	0.95	0.96	0.81	0.86	0.76	0.75	0.78	0.60	0.64	0.62	0.61	0.63	0.45	0.48	0.45	0.46	0.47	0.39	0.41
51/2		1.00	1.00	1.00	0.90	0.93	0.84	0.84	0.86	0.66	0.70	0.69	0.69	0.70	0.51	0.53	0.50	0.51	0.53	0.43	0.45
6					1.00	1.00	0.93	0.93	0.94	0.73	0.76	0.77	0.77	0.78	0.56	0.58	0.56	0.56	0.58	0.47	0.50
61/2							1.00	1.00	1.00	0.80	0.82	0.85	0.85	0.85	0.62	0.64	0.61	0.61	0.63	0.52	0.54
7										0.87	0.88	0.92	0.92	0.93	0.67	0.69	0.66	0.67	0.68	0.56	0.58
71/2										0.93	0.94	1.00	1.00	1.00	0.73	0.74	0.72	0.72	0.73	0.60	0.62
8										1.00	1.00				0.78	0.79	0.77	0.77	0.78	0.65	0.66
81/2															0.84	0.84	0.83	0.83	0.83	0.69	0.71
9															0.89	0.90	0.88	0.88	0.88	0.74	0.75
91/2															0.95	0.95	0.93	0.93	0.94	0.78	0.79
10															1.00	1.00	0.99	0.99	0.99	0.82	0.83
101/2																	1.00	1.00	1.00	0.87	0.87
11																				0.91	0.92
111/2																				0.96	0.96
12																				1.00	1.00



### Edge Distance Shear (f<sub>a</sub>) (continued)

	Dia.		7/8					1					11/8			1 1/4	
Edge	Rebar				#	7				#	8						
Dist.	E	31//8	73/4	131/8	73/4	131/8	41/2	9	15	9	15	51/8	101/8	16%	5%	111/4	18¾
c <sub>act</sub> (in.)	C <sub>cr</sub>	11%	11%	11%	14	14	131/2	131/2	131/2	16	16	151/4	151/4	151/4	161/8	16%	16%
(in.)	C <sub>min</sub>	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	23/4	23/4	23/4	23/4	23/4	23/4
	f <sub>cmin</sub>	0.09	0.08	0.09	0.09	0.09	0.08	0.08	0.09	0.08	0.09	0.14	0.12	0.12	0.14	0.12	0.12
13/4		0.09	0.08	0.09	0.09	0.09	0.08	0.08	0.09	0.08	0.09						
2¾		0.18	0.17	0.18	0.16	0.16	0.16	0.16	0.17	0.14	0.15	0.14	0.12	0.12	0.14	0.12	0.12
3		0.21	0.20	0.21	0.18	0.18	0.18	0.18	0.19	0.16	0.17	0.16	0.14	0.14	0.16	0.14	0.14
4		0.30	0.29	0.30	0.26	0.26	0.26	0.26	0.26	0.23	0.23	0.23	0.21	0.21	0.22	0.20	0.20
5		0.39	0.38	0.39	0.33	0.33	0.33	0.33	0.34	0.29	0.30	0.29	0.28	0.28	0.28	0.26	0.26
6		0.48	0.48	0.48	0.41	0.41	0.41	0.41	0.42	0.35	0.36	0.36	0.35	0.35	0.34	0.32	0.32
7		0.57	0.57	0.57	0.48	0.48	0.49	0.49	0.50	0.42	0.43	0.43	0.42	0.42	0.40	0.38	0.38
8		0.67	0.66	0.67	0.55	0.55	0.57	0.57	0.57	0.48	0.49	0.50	0.49	0.49	0.46	0.45	0.45
9		0.76	0.76	0.76	0.63	0.63	0.65	0.65	0.65	0.55	0.55	0.57	0.56	0.56	0.52	0.51	0.51
10		0.85	0.85	0.85	0.70	0.70	0.73	0.73	0.73	0.61	0.62	0.64	0.63	0.63	0.58	0.57	0.57
11		0.94	0.94	0.94	0.78	0.78	0.80	0.80	0.81	0.68	0.68	0.71	0.70	0.70	0.64	0.63	0.63
12		1.00	1.00	1.00	0.85	0.85	0.88	0.88	0.88	0.74	0.74	0.78	0.77	0.77	0.70	0.70	0.70
13					0.93	0.93	0.96	0.96	0.96	0.81	0.81	0.85	0.84	0.84	0.76	0.76	0.76
14					1.00	1.00	1.00	1.00	1.00	0.87	0.87	0.91	0.91	0.91	0.82	0.82	0.82
15										0.94	0.94	0.98	0.98	0.98	0.89	0.88	0.88
16										1.00	1.00	1.00	1.00	1.00	0.95	0.95	0.95
17															1.00	1.00	1.00



 $2.c_{act}$  = actual edge distance at which anchor is installed (inches).  $3.c_{cr}$  = critical edge distance for 100% load (inches).

 $4.c_{min}$  = minimum edge distance for reduced load (inches).



<sup>\*</sup> See page 12 for an explanation of the load table icons.

<sup>5.</sup>  $f_C$  = adjustment factor for allowable load at actual edge distance.  $f_{\it ccr}$  = adjustment factor for allowable load at critical edge distance.  $f_{ccr}$  is always = 1.00.

<sup>6.</sup>  $f_{cmin}$  = adjustment factor for allowable load at minimum edge

<sup>7.</sup>  $f_c = f_{cmin} + [(1 - f_{cmin}) (c_{act} - c_{min}) / (c_{cr} - c_{min})].$ 



AT Allowable Load Adjustment Factors in Normal-Weight Concrete: Spacing, Tension Load

#### How to use these charts

- 1. The following tables are for reduced spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the spacing  $(s_{act})$  at which the anchor is to be installed.
- 5. The load-adjustment factor  $(f_s)$  is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple spacings are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values
- 9. Adjustment factors are to be applied to allowable tension load based on bond strength values only.

### Spacing Tension (f<sub>a</sub>)

	Dia.		3/8			1/2				5/8			3/4	
	Rebar		#	3		#4		#4		#	5		#	6
Sact	E	13/4	31/2	41/2	21/8	41/4	6	71/2	21/2	51/2	9%	3%	6¾	111/
(in.)	Scr	7	61/8	18	81/2	71/2	24	30	10	9%	371/2	131/2	11%	45
	Smin	7/8	13/4	21/4	11/8	21/8	3	3¾	11/4	23/4	43/4	13/4	3%	5%
	f <sub>smin</sub>	0.57	0.58	0.80	0.57	0.58	0.80	0.80	0.57	0.58	0.80	0.57	0.58	0.80
7/8		0.57												
1		0.58												
1 1/2		0.61			0.59				0.58					
2		0.65	0.60		0.62				0.61			0.58		
21/2		0.68	0.64	0.80	0.65	0.61			0.63			0.60		
3		0.72	0.68	0.81	0.67	0.64	0.80		0.66	0.59		0.61		
31/2		0.75	0.72	0.82	0.70	0.68	0.80		0.68	0.62		0.63	0.59	
4		0.79	0.76	0.82	0.73	0.71	0.81	0.80	0.71	0.65		0.65	0.61	
5		0.86	0.84	0.83	0.78	0.79	0.82	0.81	0.75	0.71	0.80	0.68	0.66	
6		0.93	0.92	0.85	0.84	0.86	0.83	0.82	0.80	0.77	0.81	0.72	0.71	0.80
7		1.00	1.00	0.86	0.89	0.93	0.84	0.82	0.85	0.83	0.81	0.75	0.76	0.81
8				0.87	0.95	1.00	0.85	0.83	0.90	0.88	0.82	0.79	0.81	0.81
9				0.89	1.00		0.86	0.84	0.95	0.94	0.82	0.82	0.85	0.82
10				0.90			0.87	0.84	1.00	1.00	0.83	0.86	0.90	0.82
12				0.92			0.89	0.86			0.84	0.93	1.00	0.83
14				0.95			0.90	0.87			0.85	1.00		0.84
16				0.97			0.92	0.89			0.86			0.85
18				1.00			0.94	0.90			0.88			0.86
20							0.96	0.92			0.89			0.87
24							1.00	0.94			0.91			0.89
28								0.97			0.93			0.91
32								1.00			0.95			0.93
36											0.98			0.95
40											1.00			0.97
45														1.00





C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

- $2.S_{act}$  = actual spacing distance at which anchors are installed (inches).
- 3.  $S_{cr}$  = critical spacing distance for 100% load (inches).
- $4. S_{min}$  = minimum spacing distance for reduced load (inches).
- $5. f_s = adjustment factor for allowable load at actual spacing distance.$
- $6.\,f_{SCT}$  = adjustment factor for allowable load at critical spacing distance.  $f_{SCT}$  is always = 1.00.
- $7.f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.
- 8.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$



Spacing Tension (f<sub>a</sub>) (continued)

	Dia.		7/8			1			11/8			11/4		
	Rebar		#	7		#	8			#9			#10	#11
Sact	E	31//8	73/4	131/8	41/2	9	15	51/8	101/8	161/8	5%	111/4	18¾	20%
(in.)	Scr	151/2	13%	521/2	18	15¾	60	201/2	17¾	671/2	221/2	19¾	75	821/2
	Smin	2	37/8	65/8	21/4	41/2	71/2	25/8	51/8	81/2	27/8	5%	9%	10%
	f <sub>smin</sub>	0.57	0.58	0.80	0.57	0.58	0.80	0.57	0.58	0.80	0.57	0.58	0.80	0.80
2		0.57												
3		0.60			0.59			0.58			0.57			
4		0.63	0.59		0.62			0.60			0.59			
5		0.67	0.63		0.65	0.60		0.63			0.62			
6		0.70	0.67		0.67	0.64		0.65	0.61		0.64	0.59		
8		0.76	0.76	0.81	0.73	0.71	0.80	0.70	0.68		0.68	0.65		
10		0.82	0.84	0.81	0.78	0.79	0.81	0.75	0.74	0.81	0.73	0.71	0.80	
12		0.89	0.93	0.82	0.84	0.86	0.82	0.80	0.81	0.81	0.77	0.77	0.81	0.80
14		0.95	1.00	0.83	0.89	0.93	0.82	0.84	0.88	0.82	0.81	0.83	0.81	0.81
16		1.00		0.84	0.95	1.00	0.83	0.89	0.94	0.83	0.86	0.89	0.82	0.82
20				0.86	1.00		0.85	0.99	1.00	0.84	0.95	1.00	0.83	0.83
24				0.88			0.86	1.00		0.85	1.00		0.84	0.84
28				0.89			0.88			0.87			0.86	0.85
32				0.91			0.89			0.88			0.87	0.86
36				0.93			0.91			0.89			0.88	0.87
40				0.95			0.92			0.91			0.89	0.88
50				0.99			0.96			0.94			0.92	0.91
60				1.00			1.00			0.97			0.95	0.94
70										1.00			0.98	0.97
80													1.00	0.99
83														1.00

See notes on previous page.

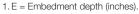
AT Allowable Load Adjustment Factors in Normal-Weight Concrete: Spacing, Shear Load

### How to use these charts

- 1. The following tables are for reduced spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the spacing  $(s_{act})$  at which the anchor is to be installed.
- 5. The load-adjustment factor (f<sub>s</sub>) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple spacings are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- 9. Adjustment factors are to be applied to allowable shear load based on concrete edge distance values only.

### Spacing Shear (f<sub>s</sub>)

	Dia.	3,	/8	1	/2	5	/8	3	4	7,	/8		1	1	1/8	1	1/4
	Rebar		#3		#4		#5		#6		#7		#8				
Sact	E	13/4	31/2	21/8	41/4	21/2	51/2	3%	6¾	31//8	73/4	41/2	9	51/8	101/8	5%	111/4
(in.)	Scr	25/8	51/4	31/4	6%	3¾	81/4	51/8	101//8	51//8	11%	63/4	131/2	73/4	151/4	81/2	16%
	Smin	7/8	13/4	11/8	21/8	11/4	23/4	13/4	3%	2	31//8	21/4	41/2	25/8	51/8	21/8	5%
	f <sub>smin</sub>	0.90	0.83	0.90	0.83	0.90	0.83	0.90	0.83	0.90	0.83	0.90	0.83	0.90	0.83	0.90	0.83
7/8		0.90															
1		0.91															
1½		0.94		0.92		0.91											
2		0.96	0.84	0.94		0.93		0.91		0.90							
21/2		0.99	0.87	0.96	0.85	0.95		0.92		0.91		0.91					
3		1.00	0.89	0.99	0.87	0.97	0.84	0.94		0.93		0.92		0.91		0.90	
3½			0.92	1.00	0.89	0.99	0.85	0.95	0.83	0.94		0.93		0.92		0.91	
4			0.94		0.91	1.00	0.87	0.97	0.85	0.95	0.83	0.94		0.93		0.92	
5			0.99		0.95		0.90	1.00	0.87	0.98	0.85	0.96	0.84	0.95		0.94	
6			1.00		0.99		0.93		0.90	1.00	0.88	0.98	0.86	0.97	0.84	0.96	0.84
7					1.00		0.96		0.92		0.90	1.00	0.88	0.99	0.86	0.97	0.85
8							0.99		0.95		0.92		0.90	1.00	0.88	0.99	0.87
9							1.00		0.97		0.94		0.92		0.90	1.00	0.88
10									1.00		0.96		0.93		0.91		0.90
12											1.00		0.97		0.95		0.93
14													1.00		0.98		0.96
16															1.00		0.99
17																	1.00



 $<sup>2.</sup> s_{act}$  = actual spacing distance at which anchors are installed (inches).

 $<sup>3.</sup> s_{cr}$  = critical spacing distance for 100% load (inches).

 $<sup>4.</sup> s_{min}$  = minimum spacing distance for reduced load (inches).

<sup>\*</sup> See page 12 for an explanation of the load table icons.

 $<sup>5.\,</sup>f_{\rm S}$  = adjustment factor for allowable load at actual spacing distance.

<sup>6.</sup>  $f_{SCT}$  = adjustment factor for allowable load at critical spacing distance.  $f_{scr}$  is always = 1.00.

<sup>7.</sup>  $f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.

<sup>8.</sup>  $f_s = f_{smin} + [(1 - f_{smin}) (s_{act} - s_{min}) / (s_{cr} - s_{min})].$ 



**Adhesive** Anchors

AT Allowable Load Adjustment Factors in Sand-Lightweight Concrete: Edge Distance, Tension and Shear Loads

### How to use these charts

- 1. The following tables are for reduced edge distance only.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance (c<sub>act</sub>) at which the anchor is to be installed.
- 5. The load-adjustment factor  $(f_c)$  is the intersection of the row
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple edges are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- 9. Adjustment factors are to be applied to allowable tension load based on bond strength values or allowable shear load based on concrete edge distance values only.

	Dia.	3,	/8	1,	/2	5	/8
Edge	E	13/4	31/2	21/8	41/4	21/2	5
Dist. Cact	c <sub>cr</sub>	25/8	51/4	31/8	6%	3¾	71/2
(in.)	C <sub>min</sub>	13/4	13/4	13/4	13/4	13/4	13/4
	f <sub>cmin</sub>	0.59	0.59	0.50	0.50	0.50	0.50
1¾		0.59	0.59	0.50	0.50	0.50	0.50
2		0.71	0.62	0.59	0.53	0.56	0.52
21/4		0.82	0.65	0.68	0.55	0.63	0.54
21/2		0.94	0.68	0.77	0.58	0.69	0.57
23/4		1.00	0.71	0.86	0.61	0.75	0.59
3			0.74	0.95	0.64	0.81	0.61
31/4			0.77	1.00	0.66	0.88	0.63
31/2			0.80		0.69	0.94	0.65
3¾			0.82		0.72	1.00	0.67
4			0.85		0.74		0.70
41/4			0.88		0.77		0.72
41/2			0.91		0.80		0.74
43/4			0.94		0.82		0.76
5			0.97		0.85		0.78
51/4			1.00		0.88		0.80
5½					0.91		0.83
5¾					0.93		0.85
6					0.96		0.87
61/4					0.99		0.89
6½					1.00		0.91
6¾							0.93
7							0.96
71/4							0.98
71/2							1.00



 $2.c_{act}$  = actual edge distance at which anchor is installed (inches).

 $3.c_{cr}$  = critical edge distance for 100% load (inches).

4.  $c_{min}$  = minimum edge distance for reduced load (inches).

 $5.f_{c}$  = adjustment factor for allowable load at actual edge distance.

6. f<sub>ccr</sub> = adjustment factor for allowable load at critical edge distance. fccr is always = 1.00.

 $7.f_{cmin}$  = adjustment factor for allowable load at minimum edge distance.

8.  $f_c = f_{cmin} + [(1 - f_{cmin}) (c_{act} - c_{min}) / (c_{cr} - c_{min})].$ 

### Edge Distance Shear (f<sub>c</sub>)

	Dia.	3,	<b>%</b>	1,	/2	5	/8
Edge	E	13/4	31/2	21/8	41/4	21/2	5
Dist. Cact	c <sub>cr</sub>	25/8	51/4	31/8	6%	3¾	71/2
(in.)	C <sub>min</sub>	13/4	13/4	13/4	13/4	13/4	13/4
	f <sub>cmin</sub>	0.40	0.35	0.18	0.15	0.12	0.11
13/4		0.40	0.35	0.18	0.15	0.12	0.11
2		0.57	0.40	0.33	0.20	0.23	0.15
21/4		0.74	0.44	0.48	0.24	0.34	0.19
21/2		0.91	0.49	0.63	0.29	0.45	0.23
2¾		1.00	0.54	0.78	0.33	0.56	0.26
3			0.58	0.93	0.38	0.67	0.30
31/4			0.63	1.00	0.43	0.78	0.34
31/2			0.68		0.47	0.89	0.38
3¾			0.72		0.52	1.00	0.42
4			0.77		0.56		0.46
41/4			0.81		0.61		0.50
41/2			0.86		0.66		0.54
43/4			0.91		0.70		0.57
5			0.95		0.75		0.61
51/4			1.00		0.79		0.65
51/2					0.84		0.69
5¾					0.89		0.73
6					0.93		0.77
61/4					0.98		0.81
61/2					1.00		0.85
6¾							0.88
7							0.92
71/4							0.96
71/2							1.00



### **SET** Epoxy Adhesive



SET is a high-strength, non-shrink, epoxy-based adhesive formulated for anchoring and doweling threaded rod and rebar. Resin and hardener are dispensed and mixed simultaneously through the mixing nozzle.

#### **Features**

- Code listed under the IBC/IRC for URM per ICC-ES ESR-1772
- Meets or exceeds the requirements of ASTM C881 specification for Type I and IV, Grade 3, Class C
- Cure times 24 hours at 65°F, 72 hours at 40°F
- Easy hole-cleaning procedure no power-brushing required
- Suitable for use in damp or wet anchor sites
- When properly mixed, adhesive will be a uniform gray color
- Available in 22 oz. and 56 oz. cartridges for application versatility
- Manufactured in the USA using global materials

### Applications

- Threaded rod anchoring and rebar doweling into concrete, masonry and URM (red brick)
- · Pick-proof sealant around doors, windows and fixtures
- Paste-over for crack injection preparation
- Bonding hardened concrete to hardened concrete
- CalTrans and multiple DOT listings; refer to www.strongtie.com/DOT

**Codes:** ICC-ES ESR-1772 (unreinforced masonry); Florida FL15730.5; AASHTO M-235 and ASTM C881 (Type I and IV, Grade 3, Class C); CalTrans Approved; Multiple DOT listings; NSF/ANSI Standard 61 (216 in.²/1,000 gal.)

### **Chemical Resistance**

See pages 320-321.

### Installation and Application Instructions

(See also pages 124-127.)

- Surfaces to receive epoxy must be clean.
- Base material temperature must be 40°F or above at the time of installation.
   For best results, material should be 70°-80°F at time of application.
- To warm cold material, store cartridges in a warm, uniformly heated area or storage container. Do not immerse cartridges in water to facilitate warming.
- Mixed material in nozzle can harden in 30 minutes at temperatures of 70°F and above.

### **Design Example**

See page 324.

### Suggested Specifications

See www.strongtie.com for more information.



**SET Adhesive** 

# **SET** Epoxy Adhesive



### Test Criteria

Anchors installed with SET adhesive have been tested in accordance with ICC-ES Acceptance Criteria for Anchors in Unreinforced Masonry Elements (AC60).

Property	Test Method	Result*
Consistency	ASTM C881	Non-sag/thixotropic paste
Heat deflection temperature	ASTM D648	136°F (58°C)
Bond strength (moist cure)	ASTM C882	3,218 psi (2 days) 3,366 psi (14 days)
Water absorption	ASTM D570	0.11% (24 hours)
Compressive yield strength	ASTM D695	5,065 psi (24 hours) 12,650 psi (7 days)
Compressive modulus	ASTM D695	439,000 psi (7 days)
Shore D Durometer	ASTM D2240	81
Gel time (75°F)	ASTM C881	30 minutes – 60 gram mass 60 minutes – thin film
VOC	ASTM D2369	6 g/L

<sup>\*</sup>Material and curing conditions: 73  $\pm$  2°F, unless otherwise noted.

### SET Cartridge System

Model No.	Tarring IVNE		Carton Quantity	Dispensing Tools	Mixing Nozzle
SET22	22	Side-by-side	10	EDT22S, EDTA22CKT	EMN22i
SET22-N <sup>4</sup>	22	Side-by-side	10	EDTA22P	EMN22i
SET56	56	Side-by-side	6	EDTA56P	EMN50

 $<sup>{\</sup>it 1. Cartridge estimation guidelines are available at www.strongtie.com/apps.}\\$ 

### Cure Schedule

Base N Tempe	Cure Time (hrs.)	
°F	°C	(1110.)
40	4	72
65	18	24
85	29	20
90	32	16

For water-saturated concrete (including damp and water-filled holes), the cure times must be doubled.

### In-Service Temperature Sensitivity

Base N Tempe	Percent Allowable	
°F	°C	Load
40	4	100%
70	21	100%
110	43	100%
135	57	75%
150	66	44%
180	82	20%

<sup>1.</sup> Refer to temperature sensitivity chart for allowable bond strength reduction for temperature. See page 319 for more information.

Detailed information on dispensing tools, mixing nozzles and other adhesive accessories is available on pages 128 through 135, or at www.strongtie.com.

<sup>3.</sup> Use only Simpson Strong-Tie® mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair SET adhesive performance.

<sup>4.</sup> One EMN22i mixing nozzle and one nozzle extension are supplied with each cartridge.

<sup>2.</sup> Percent allowable load may be linearly interpolated for intermediate base material temperatures.

 $<sup>3. \,^{\</sup>circ}\text{C} = (^{\circ}\text{F-}32) / 1.8$ 

# Strong-Tie

# **SET** Design Information — Concrete

SET Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete (continued on next page)

$\overline{}$		
ш	D	CI.
ш	155	



	[2]	*
250 250	翻	

Rod	Drill	Embed.	Critical	Critical		Tension	Load Base	d on Bond S	trength			Tension Load d on Steel Strer	ngth
Dia. in.	Bit Dia.	Depth in.	" Edge Dist. in.	Spacing Dist. in.	f' <sub>c</sub> ≥ 2,000 psi (13.8 MPa) Concrete		f' <sub>c</sub> ≥ 4,000 psi (27.6 MPa) Concrete			F1554 Grade 36	A193 GR B7	F593 304SS	
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Allow. lb. (kN)	Allow. lb. (kN)	Allow. lb. (kN)
		<b>1</b> 3/4 (44)	<b>25/8</b> (67)	<b>7</b> (178)	<b>1,900</b> (8.5)	<b>485</b> (2.2)	<b>475</b> (2.1)	<b>1,900</b> (8.5)	_	<b>475</b> (2.1)			
<b>3/8</b> (9.5)	1/2	<b>3½</b> (89)	<b>5</b> ½ (133)	<b>14</b> (356)	<b>10,200</b> (45.4)	<b>119</b> (0.5)	<b>2,550</b> (11.3)	<b>10,280</b> (45.7)	<b>97</b> (0.4)	<b>2,570</b> (11.4)	<b>2,105</b> (9.4)	<b>4,535</b> (20.2)	<b>3,630</b> (16.1)
		<b>4½</b> (114)	<b>6¾</b> (171)	<b>18</b> (457)	<b>10,613</b> (47.2)	<b>84</b> (0.4)	<b>2,655</b> (11.8)	<b>10,613</b> (47.2)	_	<b>2,655</b> (11.8)			
		<b>21/8</b> (54)	<b>3³/16</b> (81)	<b>8½</b> (216)	<b>7,216</b> (32.1)	<b>1,163</b> (5.2)	<b>1,805</b> (8.0)	<b>7,216</b> (32.1)	_	<b>1,805</b> (8.0)		<b>8,080</b> (35.9)	
<b>½</b> (12.7)	5/8	<b>4½</b> (108)	<b>6</b> % (162)	<b>17</b> (432)	<b>17,700</b> (78.7)	<b>629</b> (2.8)	<b>4,425</b> (19.7)	<b>18,400</b> (81.8)	<b>788</b> (3.5)	<b>4,600</b> (20.5)	<b>3,750</b> (16.7)		<b>6,470</b> (28.8)
		<b>6</b> (152)	<b>9</b> (229)	<b>24</b> (610)	<b>18,556</b> (82.5)	<b>853</b> (3.8)	<b>4,640</b> (20.6)	<b>18,556</b> (82.5)	_	<b>4,640</b> (20.6)			
		<b>2½</b> (64)	<b>3¾</b> (95)	<b>10</b> (254)	<b>6,780</b> (30.2)	<b>315</b> (1.4)	<b>1,695</b> (7.5)	<b>6,780</b> (30.2)	_	<b>1,695</b> (7.5)		<b>12,660</b> (56.3)	<b>10,120</b> (45.0)
		<b>3¾</b> (95)	<b>5</b> % (143)	<b>15</b> (381)	_	_	<b>4,190</b> (18.6)	_	_	<b>4,875</b> (21.7)			
<b>5</b> /8 (15.9)	3/4	<b>5</b> (127)	<b>7½</b> (191)	<b>20</b> (508)	<b>26,700</b> (118.8)	<b>1,121</b> (5.0)	<b>6,680</b> (29.7)	<b>32,200</b> (143.2)	<b>964</b> (4.3)	<b>8,050</b> (35.8)	<b>5,875</b> (26.1)		
		<b>73/16</b> (183)	<b>10</b> % (276)	<b>28¾</b> (730)	_		<b>7,515</b> (33.4)	_	_	<b>8,200</b> (36.5)			
		<b>9</b> % (238)	<b>14</b> 1/8 (359)	<b>37½</b> (953)	<b>33,402</b> (148.6)	<b>1,198</b> (5.3)	<b>8,350</b> (37.1)	<b>33,402</b> (148.6)	_	<b>8,350</b> (37.1)			
		<b>3</b> % (86)	<b>5</b> ½ <b>16</b> (129)	<b>13½</b> (343)	<b>15,456</b> (68.8)	<b>2,621</b> (11.7)	<b>3,865</b> (17.2)	<b>15,456</b> (68.8)	_	<b>3,865</b> (17.2)			
		<b>5½</b> <sub>16</sub> (129)	<b>7</b> 5/8 (194)	<b>20</b> 1/ <sub>4</sub> (514)	_	_	<b>7,195</b> (32.0)	_	_	<b>7,245</b> (32.2)			<b>12,400</b> (55.2)
<b>3/4</b> (19.1)	7/8	<b>6¾</b> (171)	<b>10</b> 1/8 (257)	<b>27</b> (686)	<b>42,100</b> (187.3)	<b>1,945</b> (8.7)	<b>10,525</b> (46.8)	<b>42,480</b> (189.0)	<b>1,575</b> (7.0)	<b>10,620</b> (47.2)	<b>8,460</b> (37.6)	<b>18,230</b> (81.1)	
		<b>9</b> (229)	<b>13½</b> (343)	<b>36</b> (914)	_	_	<b>11,220</b> (49.9)	_	_	<b>11,265</b> (50.1)			
		<b>11</b> 1/4 (286)	<b>16</b> % (429)	<b>45</b> (1143)	<b>47,634</b> (211.9)	<b>608</b> (2.7)	<b>11,910</b> (53.0)	<b>47,634</b> (211.9)	_	<b>11,910</b> (53.0)			

See notes on next page.





SET Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete (continued from previous page)

1	
- 1	ID6
- 1	186
- 1	-







**Adhesive** Anchors

Rod	Drill			Critical		Tensior	ı Load Base	d on Bond S	trength		Base	Tension Load d on Steel Strer	ngth
Dia. in.	Bit Dia.	Depth in.	Edge Dist. in.	Spacing Dist. in.	f (13.	' <sub>c</sub> ≥ 2,000 ps 8 MPa) Conc	si rete	f (27.	c ≥ 4,000 ps 6 MPa) Cond	i rete	F1554 Grade 36	A193 GR B7	F593 304SS
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Allow. lb. (kN)	Allow. lb. (kN)	Allow. lb. (kN)
		<b>3</b> 7/8 (98)	<b>5<sup>13</sup>/<sub>16</sub></b> (148)	<b>15½</b> (394)	<b>19,120</b> (85.1)	<b>1,239</b> (5.5)	<b>4,780</b> (21.3)	<b>19,120</b> (85.1)	_	<b>4,780</b> (21.3)			
		<b>5</b> <sup>13</sup> / <sub>16</sub> (148)	<b>8¾</b> (222)	<b>231/4</b> (591)	_	_	<b>8,535</b> (38.0)	_	_	<b>9,250</b> (41.1)			
<b>7/8</b> (22.2)	1	<b>73/4</b> (197)	<b>11</b> 5/8 (295)	<b>31</b> (787)	<b>49,160</b> (218.7)	<b>2,149</b> (9.6)	<b>12,290</b> (54.7)	<b>54,880</b> (244.1)	<b>1,050</b> (4.7)	<b>13,720</b> (61.0)	<b>11,500</b> (51.2)	<b>24,785</b> (110.2)	<b>16,860</b> (75.0)
		<b>107/16</b> (265)	<b>15</b> % (397)	<b>41</b> % (1060)	_	_	<b>14,480</b> (64.4)	_	_	<b>15,195</b> (67.6)			
		<b>13</b> 1/8 (333)	<b>19</b> 5/8 (498)	<b>52½</b> (1334)	<b>66,679</b> (296.6)	<b>506</b> (2.3)	<b>16,670</b> (74.2)	<b>66,679</b> (296.6)	_	<b>16,670</b> (74.2)			
		<b>4½</b> (114)	<b>6</b> 3/4 (171)	<b>18</b> (457)	<b>20,076</b> (89.3)	<b>2,388</b> (10.6)	<b>5,020</b> (22.3)	<b>20,076</b> (89.3)	_	<b>5,020</b> (22.3)			
		<b>6¾</b> (171)	<b>10</b> 1/8 (257)	<b>27</b> (686)	_	_	<b>10,020</b> (44.6)	_	_	<b>10,640</b> (47.3)		<b>32,380</b> (144.0)	<b>22,020</b> (97.9)
<b>1</b> (25.4)	11/8	<b>9</b> (229)	<b>13½</b> (343)	<b>36</b> (914)	<b>60,060</b> (267.2)	<b>5,472</b> (24.3)	<b>15,015</b> (66.8)	<b>65,020</b> (289.2)	<b>2,924</b> (13.0)	<b>16,255</b> (72.3)	<b>15,025</b> (66.8)		
		<b>12</b> (305)	<b>18</b> (457)	<b>48</b> (1219)	_	_	<b>17,810</b> (79.2)	_	_	<b>18,430</b> (82.0)			
		<b>15</b> (381)	<b>22½</b> (572)	<b>60</b> (1524)	<b>82,401</b> (366.5)	<b>6,432</b> (28.6)	<b>20,600</b> (91.6)	<b>82,401</b> (366.5)	_	<b>20,600</b> (91.6)			
		<b>5</b> 1/8 (130)	<b>73/4</b> (197)	<b>20½</b> (521)	<b>27,560</b> (122.6)	_	<b>6,890</b> (30.6)	<b>27,560</b> (122.6)	_	<b>6,890</b> (30.6)			
		<b>7</b> % (194)	<b>11½</b> (292)	<b>30½</b> (775)	_	_	<b>12,105</b> (53.8)	_	_	<b>12,500</b> (55.6)			<b>27,880</b> (124.0)
<b>1 ½</b> (28.6)	11/4	<b>10</b>	<b>151/4</b> (387)	<b>40½</b> (1029)	<b>69,200</b> (307.8)	_	<b>17,300</b> (77.0)	<b>72,340</b> (321.8)	_	<b>18,085</b> (80.4)	<b>19,025</b> (84.6)	<b>41,000</b> (182.4)	
		<b>13½</b> (343)	<b>201/4</b> (514)	<b>54</b> (1372)	_	_	<b>21,380</b> (95.1)	_	_	<b>21,770</b> (96.8)			
		<b>16</b> % (429)	<b>25</b> % (645)	<b>67½</b> (1715)	<b>101,820</b> (452.9)	_	<b>25,455</b> (113.2)	<b>101,820</b> (452.9)	_	<b>25,455</b> (113.2)			
		<b>5</b> 5/8 (143)	<b>87/16</b> (214)	<b>22½</b> (572)	<b>35,858</b> (159.5)	<b>2,389</b> (10.6)	<b>8,965</b> (39.9)	<b>35,858</b> (159.5)	_	<b>8,965</b> (39.9)			
		<b>87/16</b> (214)	<b>12³/4</b> (324)	<b>33¾</b> (857)	_	_	<b>14,115</b> (62.8)	_	_	<b>14,115</b> (62.8)			
<b>1 1/4</b> (31.8)	1%	<b>11</b> 1/4 (286)	<b>16</b> % (429)	<b>45</b> (1143)	<b>77,045</b> (342.7)	<b>7,024</b> (31.2)	<b>19,260</b> (85.7)	<b>77,045</b> (342.7)	_	<b>19,260</b> (85.7)	<b>23,490</b> (104.5)	<b>50,620</b> (225.2)	<b>34,425</b> (153.1)
		<b>15</b> (381)	<b>22½</b> (572)	<b>60</b> (1524)	_	_	<b>24,965</b> (111.0)	_	_	<b>24,965</b> (111.0)			
		<b>18¾</b> (476)	<b>28</b> 1/8 (714)	<b>75</b> (1905)	<b>122,681</b> (545.7)	<b>10,940</b> (48.7)	<b>30,670</b> (136.4)	<b>122,681</b> (545.7)	_	<b>30,670</b> (136.4)			

- 1. Allowable load must be the lesser of the bond or steel strength.
- 2. The allowable loads listed under allowable bond are based on a safety factor of 4.0.
- 3. Refer to allowable load-adjustment factors for spacing and edge distance on pages 116 and 118.
- 4. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.
- 6. Anchors are not permitted to resist tension forces in overhead or wall installations unless proper consideration is given to fire-exposure and elevated-temperature conditions.
- 7. Allowable load based on bond strength may be interpolated for concrete compressive strengths between 2,000 psi and 4,000 psi.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

SIMPSON
Strong-Tie

SET Allowable Shear Loads for Threaded Rod Anchors in Normal-Weight Concrete

ᆫ
- 6
100





Rod Dutil Bit		Embed	Embed. Critical		Shear Load Based on Concrete Edge Distance				ear Load Based Steel Strength	
Dia. in.	Drill Bit Dia. in.	Depth in.	Edge Dist. in.	Spacing Dist. in.		" <sub>c</sub> ≥ 2,000 ps 8 MPa) Cond		F1554 Grade 36	A193 GR B7	F593 304SS
(mm)	""	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
		<b>1</b> 3/4 (44)		<b>25/8</b> (67)	<b>4,573</b> (20.3)	<b>317</b> (1.4)	<b>1,145</b> (5.1)			
<b>3/8</b> (9.5)	1/2	<b>3½</b> (89)	<b>5</b> ½ (133)	<b>5</b> 1⁄4 (133)	<b>6,935</b> (30.8)	<b>965</b> (4.3)	<b>1,735</b> (7.7)	<b>1,085</b> (4.8)	<b>2,340</b> (10.4)	<b>1,870</b> (8.3)
		<b>4½</b> (114)		<b>5</b> 1/4 (133)	_	_	<b>1,735</b> (7.7)			
		<b>2</b> 1/8 (54)		<b>31/4</b> (83)	<b>7,001</b> (31.1)	<b>437</b> (1.9)	<b>1,750</b> (7.8)			
<b>½</b> (12.7)	5/8	<b>4½</b> (108)	<b>6</b> % (162)	<b>6</b> % (162)	<b>11,116</b> (49.4)	<b>1,696</b> (7.5)	<b>2,780</b> (12.4)	<b>1,930</b> (8.6)	<b>4,160</b> (18.5)	<b>3,330</b> (14.8)
		<b>6</b> (152)		<b>6</b> % (162)	_	_	<b>2,780</b> (12.4)			
		<b>2½</b> (64)		<b>3¾</b> (95)	<b>14,427</b> (64.2)	<b>826</b> (3.7)	<b>3,605</b> (16.0)			
<b>5%</b> (15.9)	3/4	<b>5</b> (127)	<b>7½</b> (191)	<b>7½</b> (191)	<b>19,501</b> (86.7)	<b>1,027</b> (4.6)	<b>4,875</b> (21.7)	<b>3,025</b> (13.5)	<b>6,520</b> (29.0)	<b>5,220</b> (23.2)
		<b>9</b> % (238)		<b>7½</b> (191)	_	_	<b>4,875</b> (21.7)			
		<b>3</b> % (86)	<b>10</b> 1/ <sub>8</sub> (257)	<b>5</b> 1/8 (130)	<b>21,180</b> (94.2)	<b>942</b> (4.2)	<b>5,295</b> (23.6)	<b>4,360</b> (19.4)		
<b>3/4</b> (19.1)	7/8	<b>6¾</b> (171)		<b>10</b> 1/8 (257)	<b>25,244</b> (112.3)	<b>2,538</b> (11.3)	<b>6,310</b> (28.1)		<b>9,390</b> (41.8)	<b>6,385</b> (28.4)
		<b>11</b> 1/4 (286)		<b>10</b> 1/8 (257)	_	_	<b>6,310</b> (28.1)			
		<b>3</b> % (98)		<b>5</b> % (149)	<b>28,333</b> (126.0)	<b>2,406</b> (10.7)	<b>7,085</b> (31.5)		<b>12,770</b> (56.8)	
7/8 (22.2)	1	<b>7¾</b> (197)	<b>11</b> 5/8 (295)	<b>11</b> % (295)	<b>33,533</b> (149.2)	<b>2,793</b> (12.4)	<b>8,385</b> (37.3)	<b>5,925</b> (26.4)		<b>8,685</b> (38.6)
		<b>13</b> 1/8 (333)		<b>11</b> % (295)	_	_	<b>8,385</b> (37.3)			
		<b>4½</b> (114)		<b>6¾</b> (171)	<b>30,520</b> (135.8)	<b>2,166</b> (9.6)	<b>7,630</b> (33.9)			
<b>1</b> (25.4)	1 1/8	<b>9</b> (229)	<b>13½</b> (343)	<b>13½</b> (343)	<b>50,187</b> (223.2)	<b>2,176</b> (9.7)	<b>12,545</b> (55.8)	<b>7,740</b> (34.4)	<b>16,680</b> (74.2)	<b>11,345</b> (50.5)
		<b>15</b> (381)		<b>13½</b> (343)	_	_	<b>12,545</b> (55.8)			
		<b>5</b> 1/8 (130)		<b>7¾</b> (197)	<b>41,325</b> (183.8)	_	<b>10,330</b> (46.0)			
<b>1 1/8</b> (28.6)	1 1/4	<b>10</b> 1/8 (257)	<b>15</b> 1/4 (387)	<b>151/4</b> (387)	<b>58,285</b> (259.3)	_	<b>14,570</b> (64.8)	<b>9,800</b> (43.6)	<b>21,125</b> (94.0)	<b>14,365</b> (63.9)
		<b>16</b> % (429)		<b>15</b> 1/4 (387)	_	_	<b>14,570</b> (64.8)			
		<b>5</b> 5/8 (143)		<b>8½</b> (216)	<b>52,130</b> (231.9)	<b>3,969</b> (17.7)	<b>13,035</b> (58.0)			
<b>1 ½</b> (31.8)	1%	<b>11</b> 1/4 (286)	<b>16</b> % (429)	<b>16</b> % (429)	<b>66,383</b> (295.3)	<b>3,948</b> (17.6)	<b>16,595</b> (73.8)	<b>12,100</b> (53.8)	<b>26,075</b> (116.0)	<b>17,730</b> (78.9)
		<b>18¾</b> (476)		<b>16</b> % (429)	_	_	<b>16,595</b> (73.8)			

<sup>1.</sup> Allowable load must be the lesser of the load based on concrete edge distance or steel strength.

<sup>2.</sup> The allowable loads based on concrete edge distance are based on a safety factor of 4.0.

<sup>3.</sup> Refer to allowable load-adjustment factors for spacing and edge distance on pages 117 and 119.

 $<sup>{\</sup>it 4.\,Refer\ to\ in-service\ temperature\ sensitivity\ chart\ for\ allowable\ load\ adjustment\ for\ temperature.}$ 

<sup>5.</sup> Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

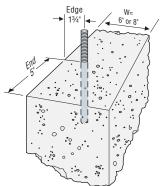


# SET Allowable Tension Loads for Threaded Rod Anchors in Normal-Weight Concrete Stemwall

IBC	1		*
-----	---	--	---

Rod Dia. Drill Bit in. Dia. (mm) in.	DIII Dit	Embed.	Stemwall Width in. (mm)	Min. Edge Dist. in. (mm)	Min. End Dist. in. (mm)	Tension Loa Bond S	Tension Load Based on Steel Strength	
	Dia.	Depth in.				f′ <sub>c</sub> ≥ 2,500 psi (17.2 MPa) Concrete		F1554 Grade 36
		(mm)				Ultimate lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
<b>5⁄8</b> (15.9)	3/4	<b>10</b> (254.0)	<b>6</b> (152.4)	<b>1¾</b> (44.5)	<b>5</b> (127.0)	<b>13,634</b> (60.6)	<b>3,410</b> (15.2)	<b>5,875</b> (26.1)
<b>7/8</b> (22.2)	1	<b>15</b> (381.0)	<b>8</b> (203.2)	<b>1</b> 3/ <sub>4</sub> (44.5)	<b>5</b> (127.0)	<b>22,664</b> (100.8)	<b>5,665</b> (25.2)	<b>11,500</b> (51.2)

- 1. Allowable load must be the lesser of the bond or steel strength.
- 2. The allowable loads listed under allowable bond are based on a safety factor of 4.0.
- 3. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 4. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.



Edge and end distances for threaded rod in concrete foundation stemwall corner installation

# SET Allowable Shear Loads for Threaded Rod Anchors in Normal-Weight Concrete, Load Applied Parallel to Concrete Edge



Rod Dia. Drill Bit in. Dia. (mm) in.	Dell Dit	Embed.	h Eage Dist.	Min. End Dist. in. (mm)		ear Load Based crete Edge Dista	Shear Load Based on Steel Strength	
	Dia.	Depth in. (mm)			(13	f' <sub>c</sub> ≥ 2,000 psi 3.8 MPa) Concre	F1554 Grade 36	
					Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
<b>½</b> (12.7)	5/8	<b>4</b> 1/4 (108.0)	<b>1</b> 3/4 (44.5)	<b>8½</b> (219.9)	<b>8,496</b> (37.8)	<b>654</b> (2.9)	<b>2,125</b> (9.5)	<b>1,930</b> (8.6)
<b>5%</b> (15.9)	3/4	<b>5</b> (127.0)	<b>1</b> 3/4 (44.5)	<b>10</b> (254.0)	<b>8,857</b> (39.4)	<b>225</b> (1.0)	<b>2,215</b> (9.9)	<b>3,025</b> (13.5)

- 1. Allowable load must be the lesser of the load based on concrete edge distance, steel strength or wood bearing capacity.
- 2. The allowable loads based on concrete edge distance are based on a safety factor of 4.0.
- 3. Refer to allowable load-adjustment factors for spacing on page 119.
- 4. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 5. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **SET** Design Information — Concrete



SET Allowable Tension Loads for Rebar Dowels in Normal-Weight Concrete

	lowable	Embed.		Critical Critical Edge Spacing Dist. in. in. (mm)	bai Bo	Tension	Tension Load Based on Steel Strength				
Size	Drill Bit Dia. in.	Depth in. (mm)	Edge Dist. in.		f' <sub>c</sub> ≥ 2,000 psi (13.8 MPa) Concrete			f¹ <sub>c</sub> ≥ 4,000 psi (27.6 MPa) Concrete			ASTM A615 Grade 60 Rebar
					Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Allowable lb. (kN)
#4	5/8	<b>41/</b> <sub>4</sub> (108)	<b>6</b> % (162)	<b>17</b> (432)	<b>16,480</b> (73.3)	<b>245</b> (1.1)	<b>4,120</b> (18.3)	<b>18,320</b> (81.5)	<b>560</b> (2.5)	<b>4,580</b> (20.4)	<b>4,800</b> (21.4)
(12.7)	78	<b>6</b> (152)	<b>9</b> (229)	<b>24</b> (610)	<b>19,360</b> (86.1)	<b>678</b> (3.0)	<b>4,840</b> (21.5)	<b>19,360</b> (86.1)	_	<b>4,840</b> (21.5)	
#5	3/4	<b>5</b> (127)	<b>7½</b> (191)	<b>20</b> (508)	<b>24,600</b> (109.4)	<b>2,598</b> (11.6)	<b>6,150</b> (27.4)	<b>26,040</b> (115.8)	<b>1,740</b> (7.7)	<b>6,510</b> (29.0)	<b>7,440</b> (33.1)
(15.9)	94	<b>9</b> % (238)	<b>14</b>	<b>37½</b> (953)	<b>48,380</b> (215.2)	<b>2,841</b> (12.6)	<b>12,095</b> (53.8)	<b>48,380</b> (215.2)	_	<b>12,095</b> (53.8)	
<b>#6</b> (19.1) 7/8	7/	<b>6¾</b> (171)	<b>10</b>	<b>27</b> (686)	<b>38,380</b> (170.7)	<b>4,044</b> (18.0)	<b>9,595</b> (42.7)	<b>40,500</b> (180.2)	<b>1,533</b> (6.8)	<b>10,125</b> (45.0)	<b>10,560</b> (47.0)
	'/8	<b>11</b> 1/4 (286)	<b>16</b> % (429)	<b>45</b> (1,143)	<b>65,020</b> (289.2)	<b>3,152</b> (14.0)	<b>16,255</b> (72.3)	<b>65,020</b> (289.2)	_	<b>16,255</b> (72.3)	
#7	4	<b>7¾</b> (197)	<b>11%</b> (295)	<b>31</b> (787)	<b>47,760</b> (212.4)	<b>1,266</b> (5.6)	<b>11,940</b> (53.1)	<b>47,760</b> (212.4)	_	<b>11,940</b> (53.1)	14,400
(22.2)		<b>13</b> 1/8 (333)	<b>19</b> % (498)	<b>52½</b> (1,334)	<b>81,560</b> (362.8)	<b>3,575</b> (15.9)	<b>20,390</b> (90.7)	<b>81,560</b> (362.8)	_	<b>20,390</b> (90.7)	(64.1)
#8	11/	<b>9</b> (229)	<b>13½</b> (343)	<b>36</b> (914)	<b>53,680</b> (238.8)	_	<b>13,420</b> (59.7)	<b>53,680</b> (238.8)	_	<b>13,420</b> (59.7)	<b>18,960</b> (84.3)
(25.4)	11/8	<b>15</b> (381)	<b>22½</b> (572)	<b>60</b> (1,524)	<b>94,240</b> (419.2)	<b>7,520</b> (33.5)	<b>23,560</b> (104.8)	<b>94,240</b> (419.2)	_	<b>23,560</b> (104.8)	
<b>#9</b> (28.6) 11/4	11/	<b>10</b> 1/8 (257)	<b>15</b> 1/4 (387)	<b>40½</b> (1,029)	<b>53,680</b> (238.8)	<b>7,977</b> (35.5)	<b>13,420</b> (59.7)	<b>53,680</b> (238.8)	_	<b>13,420</b> (59.7)	<b>24,000</b> (106.8)
	1 74	<b>16</b> % (429)	<b>25</b> % (645)	<b>67½</b> (1,715)	<b>111,460</b> (495.8)	<b>5,753</b> (25.6)	<b>27,865</b> (123.9)	<b>111,460</b> (495.8)	_	<b>27,865</b> (123.9)	
<b>#10</b> (31.8)	11/	<b>11</b> 1/4 (286)	<b>16</b> % (429)	<b>45</b> (1,143)	<b>76,000</b> (338.1)	<b>1,408</b> (6.3)	<b>19,000</b> (84.5)	<b>76,000</b> (338.1)	_	<b>19,000</b> (84.5)	<b>30,480</b> (135.6)
	1½	<b>18¾</b> (476)	<b>28</b> (711)	<b>75</b> (1,905)	<b>125,840</b> (559.8)	<b>9,551</b> (42.5)	<b>31,460</b> (139.9)	<b>125,840</b> (559.8)	_	<b>31,460</b> (139.9)	
<b>#11</b> (34.9)	15/	<b>12</b> % (314)	<b>18</b> % (473)	<b>49½</b> (1,257)	<b>87,500</b> (389.2)	<b>3,498</b> (15.6)	<b>21,875</b> (97.3)	<b>87,500</b> (389.2)	_	<b>21,875</b> (97.3)	37,440
	15/8	<b>20</b> 5/8 (524)	<b>28</b> (711)	<b>82½</b> (2,096)	<b>132,080</b> (587.5)	<b>11,297</b> (50.3)	<b>33,020</b> (146.9)	<b>132,080</b> (587.5)	_	<b>33,020</b> (146.9)	(166.5)

<sup>1.</sup> Allowable load must be the lesser of the bond or steel strength.

<sup>2.</sup> The allowable loads listed under allowable bond are based on a safety factor of 4.0.

<sup>3.</sup> Refer to allowable load-adjustment factors for spacing and edge distance on pages 116 and 118.

<sup>4.</sup> Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.

<sup>5.</sup> Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

<sup>6.</sup> Anchors are not permitted to resist tension forces in overhead or wall installations unless proper consideration is given to fire exposure and elevated-temperature conditions.

<sup>7.</sup> Allowable load based on bond strength may be interpolated for concrete compressive strengths between 2,000 psi and 4,000 psi.

# **SET** Design Information — Concrete



SET Allowable Shear Loads for Rebar Dowels in Normal-Weight Concrete

SET All	lowable	Shear	Loads 1	for Reba	ar Dowels in	Normal-Wei	ght Concrete	
Rebar	No. Dia. in.		Critical	Critical		hear Load Based ncrete Edge Dista		Shear Load Based on Steel Strength
Size No.		Depth in.	Edge Dist. in.	Spacing Dist. in.	f' <sub>c</sub> ≥ 2,0	00 psi (13.8 MPa)	) Concrete	ASTM A615 Grade 60 Rebar
(mm)		(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Allowable lb. (kN)
#4		<b>4½</b> (108)	6%	6%	<b>15,156</b> (67.4)	<b>542</b> (2.4)	<b>3,790</b> (16.9)	3,060
(12.7)	5/8	<b>6</b> (152)	(162)	(162)	<b>15,156</b> (67.4)	_	<b>3,790</b> (16.9)	(13.6)
#5	3/4	<b>5</b> (127)	7½	7½	<b>24,245</b> (107.8)	<b>1,121</b> (5.0)	<b>6,060</b> (27.0)	4,740
(15.9)	94	<b>9</b> % (238)	(191)	(191)	<b>24,245</b> (107.8)	_	<b>6,060</b> (27.0)	(21.1)
#6	7/8	<b>6¾</b> (171)	101/8	101/8	<b>33,195</b> (147.7)	<b>2,314</b> (10.3)	<b>8,300</b> (36.9)	6,730
(19.1)	78	<b>11</b> 1/4 (286)	(257)	(257)	<b>33,195</b> (147.7)	_	<b>8,300</b> (36.9)	(29.9)
#7		<b>7</b> 3⁄4 (197)	11%	<b>11</b> 5/8 (295)	<b>47,017</b> (209.1)	<b>2,227</b> (9.9)	<b>11,755</b> (52.3)	9,180
(22.2)	1	<b>13</b> 1/8 (333)	(295)		<b>47,017</b> (209.1)	_	<b>11,755</b> (52.3)	(40.8)
#8	11/8	<b>9</b> (229)	13½	13½	<b>58,880</b> (261.9)	_	<b>14,720</b> (65.5)	12,085
(25.4)	1 78	<b>15</b> (381)	(343)	(343)	<b>58,880</b> (261.9)	_	<b>14,720</b> (65.5)	(53.8)
#9	11/4	<b>10</b>	151/4	151⁄4	<b>58,880</b> (261.9)	<b>1,487</b> (6.6)	<b>14,720</b> (65.5)	15,300
(28.6)	1 74	<b>16</b> % (429)	(387)	(387)	<b>58,880</b> (261.9)	_	<b>14,720</b> (65.5)	(68.1)
#10	11/	<b>11</b> 1/4 (286)	167/8	167/8	<b>65,840</b> (292.9)	<b>7,120</b> (31.7)	<b>16,460</b> (73.2)	19,430
(31.8)	1½	<b>18¾</b> (476)	(429)	(429)	<b>65,840</b> (292.9)	_	<b>16,460</b> (73.2)	(86.4)
#11	15/	<b>12</b> % (314)	18%	18%	<b>81,400</b> (362.1)	<b>9,596</b> (42.7)	<b>20,350</b> (90.5)	23,870
(34.9)	1 5/8	20%	(473)	(473)	81,400	_	20,350	(106.2)

<sup>1.</sup> Allowable load must be the lesser of the load based on concrete edge distance or steel strength.

(90.5)

(362.1)

(524)

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>2.</sup> The allowable loads based on concrete edge distance are based on a safety factor of 4.0.

<sup>3.</sup> Refer to allowable load-adjustment factors for spacing and edge distance on pages 117 and 119.

<sup>4.</sup> Refer to in-service temperature Sensitivity chart for allowable load adjustment for temperature.

<sup>5.</sup> Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 © 2015 SIMPSON STRONG-TIE COMPANY INC.

# **SET** Design Information — Concrete



#### SET Allowable Tension Loads for Threaded Rod Anchors in Sand-Lightweight Concrete









Rod Drill Bi Dia. Dia. in. in.	D : 11 D : 1	ia. Depth in.	Critical	Critical	Ten	sion Load Base Bond Strengtl		Ter	nsion Load Based Steel Strength	on
	Dia.		Edge Dist. in.	st. Dist.	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Lightweight Concrete			F1554 Grade 36	A193 GR B7	F593 304SS
		(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
3/8	3/8 1/ (44)		<b>2</b> % (67)	<b>3½</b> (89)	<b>2,400</b> (10.7)	<b>540</b> (2.4)	<b>600</b> (2.7)	2,105	4,535	3,630
(9.5)	1/2	<b>3½</b> (89)	<b>5</b> ½ (133)	<b>7</b> (178)	<b>6,220</b> (27.7)	<b>422</b> (1.9)	<b>1,555</b> (6.9)	(9.4)	(20.2)	(16.1)
1/2	5/	<b>2</b> 1/8 (54)	<b>3</b> 1⁄8 (79)	<b>4½</b> (108)	<b>2,900</b> (12.9)	<b>550</b> (2.4)	<b>725</b> (3.2)	3,750	8,080	<b>6,470</b> (28.8)
(12.7)	5/8	<b>4½</b> (108)	<b>6</b> % (162)	<b>8½</b> (216)	<b>6,720</b> (29.9)	<b>1,087</b> (4.8)	<b>1,680</b> (7.5)	(16.7)	(35.9)	
5/8		<b>2½</b> (64)	<b>3¾</b> (95)	<b>5</b> (127)	<b>4,820</b> (21.4)	<b>327</b> (1.5)	<b>1,205</b> (5.4)	5,875	12,660	10,120
(15.9) 3/4	9/4	<b>5</b> (127)	<b>7½</b> (191)	<b>10</b> (254)	<b>9,160</b> (40.7)	<b>1,677</b> (7.5)	<b>2,290</b> (10.2)	(26.1)	(56.3)	(45.0)

- 1. Allowable load must be the lesser of the bond or steel strength.
- The allowable loads listed under allowable bond are based on a safety factor of 4.0.
- 3.100% of the allowable load is permitted at critical spacing. No reduction in spacing is allowed.
- 4. Refer to allowable load-adjustment factors for edge distance on page 120.
- 5. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 6. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.
- Anchors are not permitted to resist tension forces in overhead or wall installations unless proper consideration is given to fire-exposure and elevated-temperature conditions.

#### SET Allowable Shear Loads for Threaded Rod Anchors in Sand-Lightweight Concrete



Rod	Duitt Dia	Embed.	Critical	Critical		ear Load Base crete Edge Dis		Shear Load Based on Steel Strength			
Dia. in.	Drill Bit Dia. in.	Depth in. (mm)	Edge Dist. in.	st. Dist. 1.	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Lightweight Concrete			F1554 Grade 36	A193 GR B7	F593 304SS	
(mm) ''''			(mm)		Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	
3/8	1/	<b>13/4</b> (44)	<b>2</b> 5/8 (67)	<b>3½</b> (89)	<b>2,364</b> (10.5)	<b>129</b> (0.6)	<b>590</b> (2.6)	1,085	<b>2,340</b> (10.4)	<b>1,870</b> (8.3)	
(9.5)	1/2	<b>3½</b> (89)	<b>5</b> ½ (133)	<b>7</b> (178)	<b>5,784</b> (25.7)	<b>547</b> (2.4)	<b>1,445</b> (6.4)	(4.8)			
1/2	5/8	<b>2</b> 1/8 (54)	<b>3</b> 1/8 (79)	<b>4½</b> (108)	<b>2,948</b> (13.1)	<b>224</b> (1.0)	<b>735</b> (3.3)	1,930	<b>4,160</b> (18.5)	<b>3,330</b> (14.8)	
(12.7)	78	<b>4½</b> (108)	<b>6</b> % (162)	<b>8½</b> (216)	<b>8,436</b> (37.5)	<b>891</b> (4.0)	<b>2,110</b> (9.4)	(8.6)			
5/8	3/4	<b>2½</b> (64)	<b>3¾</b> (95)	<b>5</b> (127)	<b>3,584</b> (15.9)	<b>1,072</b> (4.8)	<b>895</b> (4.0)	3,025	6,520	5,220	
(15.9)	94	<b>5</b> (127)	<b>7½</b> (191)	<b>10</b> (254)	<b>11,784</b> (52.4)	<b>650</b> (2.9)	<b>2,945</b> (13.1)	(13.5)	(29.0)	(23.2)	

- 1. Allowable load must be the lesser of the load based on concrete edge distance or steel strength.
- The allowable loads based on concrete edge distance are based on a safety factor of 4.0.
- 3.100% of the allowable load is permitted at critical spacing. No reduction in spacing is allowed.
- 4. Refer to allowable load-adjustment factors for edge distance on page 120.
- Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 6. Anchors are permitted to be used within fire-resistive construction, provided the anchors resist wind or seismic loads only. For use in fire-resistive construction, the anchors can also be permitted to be used to resist gravity loads, provided special consideration has been given to fire-exposure conditions.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



SET Allowable Tension and Shear Loads for Threaded Rod Anchors in 8-inch Lightweight, Medium-Weight and Normal-Weight Grout-Filled CMU.

There agree and two many very transfer and the m											
Rod	Drill	Min. Embed.	nbed. Edge epth Dist.	Critical End		8-inch Grout-Filled CMU Allowable Loads Based on CMU Strength					
Dia. in.	Bit Dia.	Depth		Dist. C	Dist.	Ten	sion	Shear			
(mm)	in.	in. (mm)	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)		
Anchor Installed Anywhere on the Face of the CMU Wall (See Figure 1)											
<b>½</b> (12.7)	5/8	<b>4½</b> (108)	<b>17</b> (432)	<b>17</b> (432)	<b>17</b> (432)	<b>6,496</b> (28.9)	<b>1,300</b> (5.8)	<b>6,766</b> (30.1)	<b>1,355</b> (6.0)		
<b>5/8</b> (15.9)	3/4	<b>5</b> (127)	<b>20</b> (508)	<b>20</b> (508)	<b>20</b> (508)	<b>8,232</b> (36.6)	<b>1,645</b> (7.3)	<b>13,676</b> (60.8)	<b>2,735</b> (12.2)		
<b>3/4</b> (19.1)	7/8	<b>6¾</b> (171)	<b>27</b> (686)	<b>27</b> (686)	<b>27</b> (686)	<b>15,656</b> (69.6)	<b>3,130</b> (13.9)	<b>17,578</b> (78.2)	<b>3,515</b> (15.6)		

IBC

- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- Values for 8-inch wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry, f'm, at 28 days is 1500 psi.
- 3. Embedment depth is measured from the outside face of the concrete masonry unit.
- 4. Allowable loads may be increased 331/% for short-term loading due to wind forces or seismic forces where permitted by code.
- 5. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 6. The tabulated allowable loads are based on a safety factor of 5.0.
- 7. Refer to allowable load-adjustment factors for end distance, edge distance and spacing on page 121.

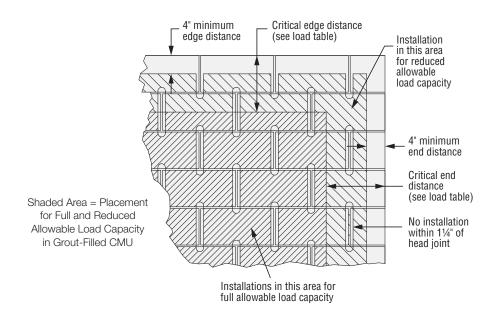


Figure 1

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Strong-Tie

# **SET** Design Information — Masonry

SET Allowable Tension and Shear Loads for Threaded Rod Anchors in 6- and 8-inch Lightweight, Medium-Weight and Normal-Weight Grout-Filled CMU — Anchor Installed in Cell Opening (Top of Wall)

IBC	1	<b>→</b>		*
	289 239	257	[ [ ]	

Rod Dia. in.	Drill Embed. Bit Depth Dia. in.		Min. Edge Dist. in.	dge End Spacing ist. Dist. Dist.		6- and 8-inch Grout-Filled CMU Allowable Loads Based on CMU Strength Tension Shear					
(mm)	ın.	(mm)	(mm)	(mm)	(mm)	Ultimate Ib. (kN)	Allowable lb. (kN)	Ultimate Ib. (kN)	Allowable lb. (kN)		
Allowable Tension and Shear Values EXCLUDING Earthquake Loads <sup>1</sup>											
<b>5%</b> (15.9)	3/4	<b>5</b> (127)	<b>3</b> (76)	<b>3½</b> (89)	<b>20</b> (508)	<b>12,573</b> (55.9)	<b>2,515</b> (11.2)	<b>9,530</b> (42.4)	<b>1,905</b> (8.5)		
<b>3/4</b> (19.1)	7/8	<b>5</b> (127)	<b>3</b> (76)	<b>3½</b> (89)	<b>20</b> (508)	_	<b>2,515</b> (11.2)	_	<b>1,905</b> (8.5)		
7/8 (22.2)	1	<b>12</b> (305)	<b>2</b> (51)	<b>3</b> 7/8 (98)	<b>48</b> (1219)	<b>8,908</b> (39.6)	<b>1,780</b> (7.9)	_	_		
			All	owable Ten	sion and Sh	ear Values INCLUDII	NG Earthquake Load	S <sup>2</sup>			
<b>5%</b> (15.9)	3/4	<b>5</b> (127)	<b>3</b> (76)	<b>3½</b> (89)	<b>20</b> (508)	<b>6,500</b> (28.9)	<b>1,300</b> (5.8)	<b>6,780</b> (30.2)	<b>1,355</b> (6.0)		
<b>3/4</b> (19.1)	7/8	<b>5</b> (127)	<b>3</b> (76)	<b>3½</b> (89)	<b>20</b> (508)	_	<b>1,300</b> (5.8)	_	<b>1,355</b> (6.0)		

- 1. Allowable tension and shear values EXCLUDING earthquake loads may not be increased for wind forces.
- 2. Allowable tension and shear values INCLUDING earthquake loads may be increased 331/3% for wind forces or seismic forces where permitted by code.
- 3. Also see notes 1-3 and 5-7 on next page.

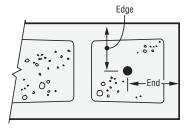


Figure 2
Anchor installed in cell opening (top of wall)



SET Allowable Tension and Shear Loads for Threaded Rod Anchors in Lightweight, Medium-Weight and Normal-Weight Hollow CMU

S	IBC	1	<b>→</b>	*

Rod Dia.	Drill Bit	Embed.	Min.	Min.	6- and 8-inch Hollow CMU Allowable Loads Based on CMU Strength				
in.	Dia.	Depth in.	Edge Dist. in.	End Dist. in.	Tension		Shear		
(mm)	in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	
	And	chor Installe	d in Face Shel	l with Simpso	n Strong-Tie® Ep	oxy Carbon-Stee	l Screen Tube		
<b>5%</b> (15.9)	7/8	<b>3½</b> (88.9)	<b>4</b> (101.6)	<b>4</b> % (117.5)	<b>881</b> (3.9)	<b>175</b> (0.8)	<b>1,440</b> (6.4)	<b>290</b> (1.3)	
<b>3/4</b> (19.1)	1	<b>3½</b> (88.9)	<b>4</b> (101.6)	<b>45%</b> (117.5)	_	<b>175</b> (0.8)	_	<b>290</b> (1.3)	

- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- Values for 8-inch wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry, f'm, at 28 days is 1500 psi.
- 3. Embedment depth is measured from the outside face of the concrete masonry unit for installations through a face shell.
- 4. Allowable loads may not be increased for short-term loading due to wind forces or seismic forces.
- 5. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 6. The tabulated allowable loads are based on a safety factor of 5.0.
- 7. Anchors must be spaced a minimum distance of four times the anchor embedment.
- 8. Screen tubes not for use with SET1.7KTA.
- 9. Set drill to rotation-only mode when drilling into hollow CMU.

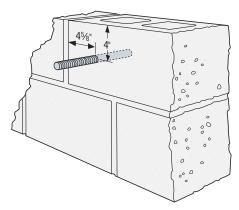


Figure 3
Anchor installed in face shell with screen tube in hollow cell

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **SET** Design Information — Masonry



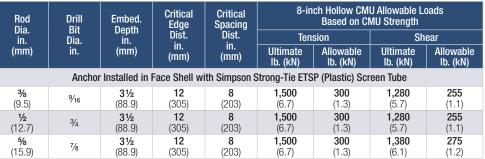
SET Allowable Tension and Shear Loads for Installations in Unreinforced Brick Masonry Walls — Minimum URM Wall Thickness is 13" (3 wythes thick)

•				
	<b>IBC</b>	<b>→</b>		*

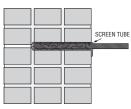
Rod/Rebar Dia./Size in. (mm)	Drill Bit Dia. in.	Embed. Depth in. (mm)	Min. Edge/End Dist. in. (mm)	Min. Vertical Spacing Dist. in. (mm)	Min. Horiz. Spacing Dist. in. (mm)	Tension Load Based on URM Strength Allowable lb. (kN)	Shear Load Based on URM Strength Allowable lb. (kN)				
	Configuration A (Simpson Strong-Tie® ETS or ETSP Screen Tube Required)										
<b>3/4</b> (19.1)	1	<b>8</b> (203)	<b>16</b> (406)	<b>16</b> (406)	<b>16</b> (406)	_	<b>1,000</b> (4.4)				
<b>#5</b> (15.9)	1	<b>8</b> (203)	<b>16</b> (406)	<b>16</b> (406)	<b>16</b> (406)	_	<b>750</b> (3.3)				
<b>#6</b> (19.1)	1	<b>8</b> (203)	<b>16</b> (406)	<b>16</b> (406)	<b>16</b> (406)	_	<b>1,000</b> (4.4)				
		Configur	ation B (Sin	npson Strong-Ti	e ETS or ETSP S	Screen Tube Required)					
<b>3/4</b> (19.1)	1	<b>13</b> (330)	<b>16</b> (406)	<b>16</b> (406)	<b>16</b> (406)	<b>1,200</b> (5.3)	<b>1,000</b> (4.4)				
	Conf	iguration C	(Simpson	Strong-Tie ETS	Screen Tube and	d AST Steel Sleeve Req	uired)				
<b>5%</b> (15.9)	1	**	<b>16</b> (406)	<b>16</b> (406)	<b>16</b> (406)	<b>1,200</b> (5.3)	<b>750</b> (3.3)				

- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- 2. All holes are drilled with a 1" diameter carbide-tipped drill bit with the drill set in the rotation-only mode.
- 3. The unreinforced brick walls must have a minimum thickness of 13 inches (three wythes of brick).
- 4. The allowable load is applicable only where in-place shear tests indicate minimum net mortar strength of 50 psi. For installations using a wet diamond core-drill bit, the allowable load is applicable only where in-place shear tests indicate minimum net mortar strength of 325 psi.
- The allowable load for Configuration B and C anchors subjected to a combined tension and shear load is determined by assuming a straight-line relationship between allowable tension and shear.
- 6. The anchors installed in unreinforced brick walls are limited to resisting seismic or wind forces only.
- 7. Configuration A has a straight threaded rod or rebar embedded 8 inches into the wall with a 31/32" diameter by 8-inch long screen tube (part # ETS758 or ETS758P). This configuration is designed to resist shear loads only.
- Configuration B has a ¾" threaded rod bent and installed at a 22.5-degree angle and installed 13 inches into the wall, to within 1-inch (maximum) of the exterior wall surface. This configuration is designed to resist tension and shear loads. The pre-bent threaded rod is installed with a <sup>3</sup>½" diameter by 13-inch long screen tube (part # ETS7513 or ETS7513P).
- 9. Configuration C is designed to resist tension and shear forces. It consists of a %" diameter, ASTM F1554 Grade 36 threaded rod and an 8" long sleeve (part # AST800) and a 31/2" diameter by 8-inch long screen tube (part # ETS758). The steel sleeve has a plastic plug in one end. A 6" by 6" by %" thick ASTM A 36 steel plate is located on the back face of the wall
- 10. Special inspection requirements are determined by local jurisdiction and must be confirmed by the local building official.
- 11. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 12. Screen tubes not for use with SET1.7KTA.

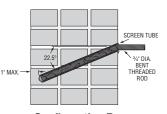
#### SET Allowable Tension and Shear Loads for Threaded Rod Anchors in Lightweight, Medium-Weight and Normal-Weight Hollow CMU



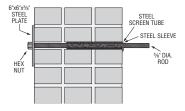
- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- 2. The tabulated allowable loads are based on a safety factor of 5.0
- 3. Edge distances may be reduced to 4" with a corresponding 32% reduction in tension capacity. Shear capacity is unaffected
- 4. Values for 8-inch wide, lightweight, medium-weight and normal-weight concrete masonry units with min. compressive strength of 1,900 psi and 11/4" thick face shell.
- 5. Embedment depth is measured from the outside face of the concrete masonry unit.
- 6. Refer to in-service temperature sensitivity chart for allowable load adjustment for temperature.
- 7. Allowable loads may not be increased for short-term loading due to wind or seismic forces. Wall design must satisfy applicable design standards and be capable of withstanding applied loads.
- 8. Screen tubes not for use with SET1.7KTA.
- 9. Set drill to rotation-only mode when drilling into hollow CMU.



Configuration A (Shear)



Configuration B (Tension & Shear)



Configuration C (Tension & Shear)

#### Installation Instructions for Configuration C

- Drill hole perpendicular to the wall to a depth of 8" with a 1" diameter carbidetipped drill bit (rotation only mode).
- 2. Clean hole with oil-free compressed air and a nylon brush.
- 3. Fill 8" steel screen tube with mixed adhesive and insert into hole.
- 4. Insert steel sleeve slowly into screen tube (adhesive will displace).
- 5. Allow adhesive to cure (see cure schedule).
- Drill through plastic plug in (inside) end of steel sleeve with 5%" bit.
- 7. Drill completely through the wall with %" carbide tipped concrete drill bit (rotation mode only)
- 8. Insert %" rod through hole and attach metal plate and nut.

**Adhesive** Anchors

<sup>\*</sup> See page 12 for an explanation of the load table icons

# **SET** Design Information — Masonry

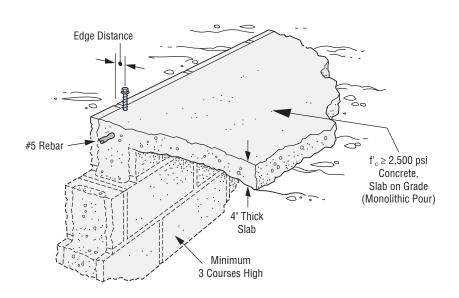


SET Allowable Tension Loads for Threaded Rod Anchors in 8" Lightweight, Medium-Weight and Normal-Weight CMU Chair Blocks Filled with Normal-Weight Concrete

		<i></i>
N ( 1 )		
	1	<b>1</b>

Rod Dia. in. (mm)	Drill Bit Dia. in.	Min. Embed. Depth in. (mm)	Min. Edge Dist. in. (mm)	Critical Spacing Dist. in. (mm)	8-inch Con CMU Cha Allowable Te Based ( Strei Ultimate Ib. (kN)	air Block ension Loads on CMU
1/2	5/8	<b>4½</b> (114)	<b>13/4</b> (44.5)	<b>18</b> (457)	<b>4,810</b> (21.4)	<b>960</b> (4.3)
(12.7)	78	<b>7</b> (178)	<b>13/4</b> (44.5)	<b>28</b> (711)	<b>7,715</b> (34.3)	<b>1,545</b> (6.9)
		<b>4½</b> (114)	<b>1¾</b> (44.5)	<b>18</b> (457)	<b>4,955</b> (22.0)	<b>990</b> (4.4)
<b>5</b> /8 (15.9)	3/4	<b>7</b> (178)	<b>1¾</b> (44.5)	<b>28</b> (711)	<b>7,600</b> (33.8)	<b>1,520</b> (6.8)
		<b>12</b> (305)	<b>13/4</b> (44.5)	<b>48</b> (1,219)	<b>12,200</b> (54.4)	<b>2,440</b> (10.9)

- 1. Threaded rods must comply with ASTM F1554 Grade 36 minimum.
- 2. Values are for 8-inch-wide concrete masonry units CMU filled with concrete with minimum compressive strength of 2,500 psi and poured monolithically with the floor slab.
- 3. Center #5 rebar in CMU cell and concrete slab as shown.
- 4. The tabulated allowable loads are based on a safety factor of 5.0.



C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC

# **SET** Design Information — Concrete



SET Allowable Load-Adjustment Factors in Normal-Weight Concrete: Edge Distance, Tension Load

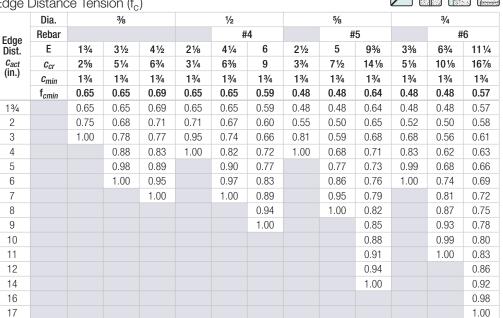
#### How to use these charts

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or shear
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance ( $c_{\it act}$ ) at which the anchor is to be installed.
- 5. The load-adjustment factor ( $f_c$ ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple edges are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.

BC 1 ( )

9. Adjustment factors are to be applied to allowable tension load based on bond strength values only.

#### Edge Distance Tension (f<sub>c</sub>)



See notes below.

#### Edge Distance Tension (f.) (continued)

Edge Distance for islant (16) (contained)															
	Dia.		7/8			1			11/8			11/4			
Edge	Rebar		#	7		#	8		#	9		#-	10	#-	1
Dist.	E	37/8	73/4	131/8	41/2	9	15	51/8	101/8	16%	5%	111/4	18¾	12%	20%
Cact	C <sub>cr</sub>	57/8	11%	19%	63/4	131/2	221/2	73/4	151/4	25%	81/2	16%	281/8	281/8	281/8
(in.)	C <sub>min</sub>	13/4	13/4	13/4	13/4	13/4	13/4	23/4	23/4	23/4	23/4	23/4	23/4	23/4	23/4
	f <sub>cmin</sub>	0.48	0.48	0.52	0.48	0.48	0.47	0.58	0.58	0.51	0.58	0.58	0.51	0.58	0.51
13/4		0.48	0.48	0.52	0.48	0.48	0.47								
23/4		0.61	0.53	0.55	0.58	0.52	0.50	0.58	0.58	0.51	0.58	0.58	0.51	0.58	0.51
4		0.77	0.60	0.58	0.71	0.58	0.53	0.69	0.62	0.54	0.67	0.62	0.53	0.61	0.53
6		1.00	0.70	0.63	0.92	0.67	0.58	0.85	0.69	0.58	0.82	0.68	0.57	0.67	0.57
8			0.81	0.69	1.00	0.76	0.63	1.00	0.76	0.62	0.97	0.74	0.61	0.72	0.61
10			0.91	0.74		0.85	0.68		0.82	0.67	1.00	0.80	0.65	0.77	0.65
12			1.00	0.80		0.93	0.73		0.89	0.71		0.86	0.69	0.82	0.69
14				0.85		1.00	0.78		0.96	0.75		0.91	0.73	0.88	0.73
16				0.90			0.83		1.00	0.80		0.97	0.77	0.93	0.77
18				0.96			0.89			0.84		1.00	0.80	0.98	0.81
20				1.00			0.94			0.88			0.84	1.00	0.84
24							1.00			0.97			0.92		0.92
28										1.00			1.00		1.00

<sup>\*</sup> See page 12 for an explanation of the load table icons

# **SET** Design Information — Concrete



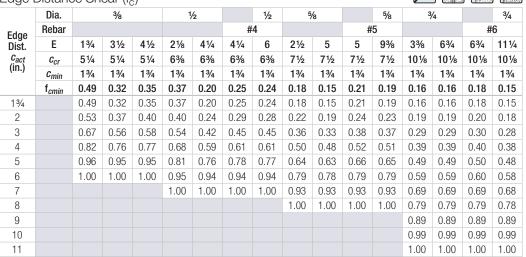
SET Allowable Load-Adjustment Factors in Normal-Weight Concrete: Edge Distance, Shear Load

#### How to use these charts

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance ( $c_{act}$ ) at which the anchor is to be installed.
- 5. The load-adjustment factor ( $f_c$ ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple edges are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- Adjustment factors are to be applied to allowable shear load based on concrete edge distance values only.

**IRC** → ← ← \*

#### Edge Distance Shear (f<sub>c</sub>)



See notes below.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

#### Edge Distance Shear (f<sub>c</sub>) (continued)

Edge I	Edge Distance Shear (f <sub>c</sub> ) (continued)																
	Dia.	7,	/8		7/8	1			1		11/8			11/4			
Edge	Rebar			#	7			#	8		#	9		#1	10	#1	11
Dist.	E	3%	73/4	73/4	131/8	41/2	9	9	15	51/8	101/8	16%	5%	111/4	18¾	12%	20%
c <sub>act</sub> (in.)	C <sub>cr</sub>	11%	11%	11%	11%	13½	13½	13½	13½	151/4	151/4	151/4	16%	16%	16%	18%	18%
(111.)	C <sub>min</sub>	13/4	1¾	13/4	13/4	13/4	13/4	13/4	13/4	2¾	23/4	23/4	23/4	23/4	23/4	23/4	23/4
	f <sub>cmin</sub>	0.14	0.13	0.14	0.10	0.14	0.10	0.12	0.10	0.17	0.16	0.12	0.17	0.16	0.12	0.16	0.12
13⁄4		0.14	0.13	0.14	0.10	0.14	0.10	0.12	0.10								
23/4		0.23	0.22	0.23	0.19	0.21	0.18	0.19	0.18	0.17	0.16	0.12	0.17	0.16	0.12	0.16	0.12
3		0.25	0.24	0.25	0.21	0.23	0.20	0.21	0.20	0.19	0.18	0.14	0.18	0.17	0.14	0.17	0.13
4		0.34	0.33	0.34	0.31	0.30	0.27	0.29	0.27	0.25	0.24	0.21	0.24	0.23	0.20	0.23	0.19
5		0.42	0.42	0.42	0.40	0.38	0.35	0.36	0.35	0.32	0.31	0.28	0.30	0.29	0.26	0.28	0.24
6		0.51	0.50	0.51	0.49	0.45	0.43	0.44	0.43	0.39	0.38	0.35	0.36	0.35	0.32	0.33	0.30
7		0.60	0.59	0.60	0.58	0.52	0.50	0.51	0.50	0.45	0.45	0.42	0.42	0.41	0.38	0.38	0.36
8		0.68	0.68	0.68	0.67	0.60	0.58	0.59	0.58	0.52	0.51	0.49	0.48	0.47	0.45	0.44	0.41
9		0.77	0.77	0.77	0.76	0.67	0.66	0.66	0.66	0.59	0.58	0.56	0.54	0.53	0.51	0.49	0.47
10		0.86	0.86	0.86	0.85	0.74	0.73	0.74	0.73	0.65	0.65	0.63	0.60	0.59	0.57	0.54	0.52
11		0.95	0.94	0.95	0.94	0.82	0.81	0.81	0.81	0.72	0.71	0.70	0.65	0.65	0.63	0.60	0.58
12		1.00	1.00	1.00	1.00	0.89	0.89	0.89	0.89	0.78	0.78	0.77	0.71	0.71	0.70	0.65	0.63
13						0.96	0.96	0.96	0.96	0.85	0.85	0.84	0.77	0.77	0.76	0.70	0.69
14						1.00	1.00	1.00	1.00	0.92	0.92	0.91	0.83	0.83	0.82	0.76	0.74
15										0.98	0.98	0.98	0.89	0.89	0.88	0.81	0.80
16										1.00	1.00	1.00	0.95	0.95	0.95	0.86	0.85
17													1.00	1.00	1.00	0.91	0.91
18%																1.00	1.00

- 1. E = Embedment depth (inches).
- 2. c<sub>act</sub> = actual edge distance at which anchor is installed (inches).
- 3.  $c_{cr}$  = critical edge distance for 100% load (inches).
- $4. c_{min} = minimum edge distance for reduced load (inches).$
- $5.f_{c}$  = adjustment factor for allowable load at actual edge distance.

<sup>6.</sup>  $f_{CCT}$  = adjustment factor for allowable load at critical edge distance.  $f_{CCT}$  is always = 1.00.

f<sub>cmin</sub> = adjustment factor for allowable load at minimum edge distance.

<sup>8.</sup>  $f_c = f_{cmin} + [(1 - f_{cmin}) (c_{act} - c_{min}) / (c_{cr} - c_{min})].$ 

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC

# **SET** Design Information — Concrete

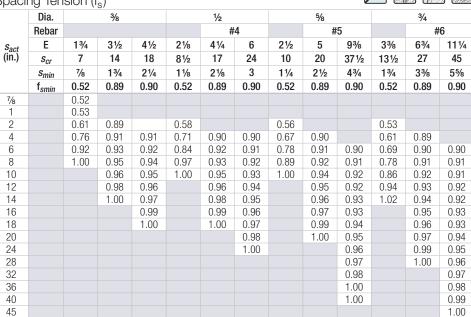


SET Allowable Load-Adjustment Factors in Normal-Weight Concrete: Spacing, Tension Load

#### How to use these charts

- 1. The following tables are for reduced spacing.
- Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the spacing  $(\mathbf{s}_{\mathit{act}})$  at which the anchor is to be installed.
- 5. The load-adjustment factor ( $\mathbf{f}_{_{\!S}}$  ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple spacings are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- Adjustment factors are to be applied to allowable tension load based on bond strength values only.

#### Spacing Tension (f<sub>s</sub>)



- 1. E = Embedment depth (inches).
- 2.  $s_{act}$  = actual spacing distance at which anchors are installed (inches).
- 3.  $s_{CT}$  = critical spacing distance for 100% load (inches).
- 4.  $s_{min}$  = minimum spacing distance for reduced load (inches).
- 5.  $f_s$  = adjustment factor for allowable load at actual spacing distance.
- f<sub>scr</sub> = adjustment factor for allowable load at critical spacing distance. f<sub>scr</sub> is always = 1.00.
- f<sub>smin</sub> = adjustment factor for allowable load at minimum spacing distance.
- 8.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})]$

#### Spacing Tension (f<sub>s</sub>) (continued)

	Dia.		7/8			1			11/8			1 1/4			
	Rebar		#	7		#	8		#	9		#-	10	#-	11
Sact	Е	31/8	73/4	131/8	41/2	9	15	51/8	101/8	161/8	5%	111/4	18¾	12%	20%
(in.)	S <sub>cr</sub>	15½	31	521/2	18	36	60	201/2	401/2	671/2	221/2	45	75	491/2	821/2
	Smin	2	31/8	65/8	21/4	41/2	71/2	25/8	51/8	81/2	21/8	5%	9%	61/4	10%
	f <sub>smin</sub>	0.52	0.89	0.90	0.52	0.89	0.90	0.52	0.89	0.90	0.52	0.89	0.90	0.89	0.90
2		0.52													
3		0.56			0.54			0.53			0.52				
4		0.59	0.89		0.57			0.56			0.55				
5		0.63	0.89		0.60	0.89		0.58			0.57				
6		0.66	0.90		0.63	0.90		0.61	0.89		0.60	0.89			
8		0.73	0.91	0.90	0.70	0.90	0.90	0.66	0.90		0.65	0.90		0.89	
10		0.80	0.91	0.91	0.76	0.91	0.90	0.72	0.91	0.90	0.69	0.90	0.90	0.90	
12		0.88	0.92	0.91	0.82	0.92	0.91	0.77	0.91	0.91	0.74	0.91	0.90	0.90	0.90
14		0.95	0.93	0.92	0.88	0.92	0.91	0.83	0.92	0.91	0.79	0.91	0.91	0.91	0.91
16		1.00	0.94	0.92	0.94	0.93	0.92	0.88	0.92	0.91	0.84	0.92	0.91	0.91	0.91
20			0.96	0.93	1.00	0.94	0.92	0.99	0.94	0.92	0.94	0.93	0.92	0.92	0.91
24			0.97	0.94		0.96	0.93	1.00	0.95	0.93	1.00	0.94	0.92	0.94	0.92
28			0.99	0.95		0.97	0.94		0.96	0.93		0.95	0.93	0.95	0.92
32			1.00	0.96		0.99	0.95		0.97	0.94		0.96	0.93	0.96	0.93
36				0.96		1.00	0.95		0.99	0.95		0.97	0.94	0.97	0.94
40				0.97			0.96		1.00	0.95		0.99	0.95	0.98	0.94
50				0.99			0.98			0.97		1.00	0.96	1.00	0.95
60				1.00			1.00			0.99			0.98		0.97
70										1.00			0.99		0.98
75													1.00		0.99
821/2															1.00

See notes above.

<sup>\*</sup> See page 12 for an explanation of the load table icons

# **SET** Design Information — Concrete

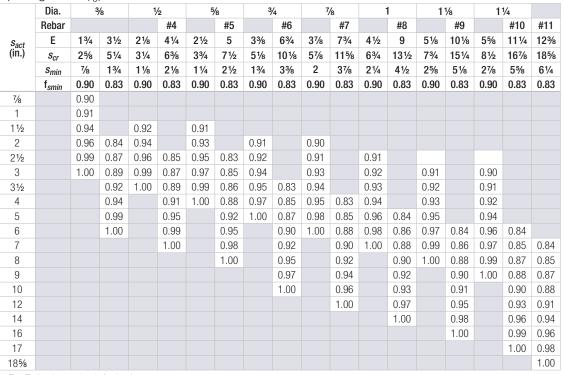


SET Allowable Load-Adjustment Factors in Normal-Weight Concrete: Spacing, Shear Load

#### How to use these charts

- 1. The following tables are for reduced spacing.
- Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the spacing (s<sub>act</sub>) at which the anchor is to be installed.
- 5. The load-adjustment factor ( $f_{\rm s}$ ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple spacings are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- Adjustment factors are to be applied to allowable shear load based on concrete edge distance values only.

#### Spacing Shear (f<sub>s</sub>)



<sup>1.</sup> E = Embedment depth (inches).

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

 $<sup>2.</sup> s_{act} = actual spacing distance at which anchors are installed (inches).$ 

<sup>3.</sup>  $s_{cr}$  = critical spacing distance for 100% load (inches).

<sup>4.</sup> s<sub>min</sub> = minimum spacing distance for reduced load (inches).

 $<sup>5.\,</sup>f_{\text{S}}$  = adjustment factor for allowable load at actual spacing distance.

<sup>6.</sup>  $f_{scr}$  = adjustment factor for allowable load at critical spacing distance. fscr is always = 1.00.

 $<sup>7.\,</sup>f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.

<sup>8.</sup>  $f_s = f_{smin} + [(1 - f_{smin}) (s_{act} - s_{min}) / (s_{cr} - s_{min})].$ 

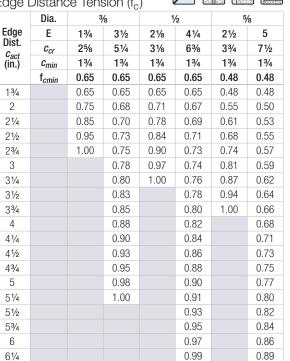
<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **SET** Design Information — Concrete

SET Allowable Load-Adjustment Factors in Sand-Lightweight Concrete: Edge Distance, Tension and Shear Loads How to use these charts

- 1. The following tables are for reduced edge distance only.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance ( $\mathbf{c}_{act}$ ) at which the anchor is to be installed.
- 5. The load-adjustment factor ( $\mathbf{f}_{_{\mathrm{C}}}$ ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple edges are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- 9. Adjustment factors are to be applied to allowable tension load based on bond strength values or allowable shear load based on concrete edge distance values only.

#### Edge Distance Tension (f<sub>c</sub>)



#### 71/2 1. E = Embedment depth (inches).

61/2 63/4

7

71/4

1.00

0.91

0.93

0.95

0.98

1.00

Edge	Distanc	e Shear	$(f_C)$

	Dia.	3	<b>/</b> 8	1,	/2	5	/8
Edge	E	13/4	31/2	21/8	41/4	21/2	5
Dist. c <sub>act</sub>	C <sub>cr</sub>	25/8	51/4	31/8	6%	3¾	71/2
(in.)	Cmin	13/4	13/4	13/4	13/4	13/4	13/4
	f <sub>cmin</sub>	0.25	0.25	0.20	0.20	0.15	0.15
13/4		0.25	0.25	0.20	0.20	0.15	0.15
2		0.46	0.30	0.35	0.24	0.26	0.19
21/4		0.68	0.36	0.49	0.29	0.36	0.22
21/2		0.89	0.41	0.64	0.33	0.47	0.26
2¾		1.00	0.46	0.78	0.37	0.58	0.30
3			0.52	0.93	0.42	0.68	0.33
31/4			0.57	1.00	0.46	0.79	0.37
31/2			0.63		0.50	0.89	0.41
3¾			0.68		0.55	1.00	0.45
4			0.73		0.59		0.48
41/4			0.79		0.63		0.52
41/2			0.84		0.68		0.56
43/4			0.89		0.72		0.59
5			0.95		0.76		0.63
51/4			1.00		0.81		0.67
51/2					0.85		0.70
5¾					0.89		0.74
6					0.94		0.78
61/4					0.98		0.82
61/2					1.00		0.85
6¾							0.89
7							0.93
71/4							0.96
71/2							1.00

<sup>2.</sup> Cact = actual edge distance at which anchor is installed (inches).

<sup>3.</sup>  $c_{cr}$  = critical edge distance for 100% load (inches).

 $<sup>4.</sup> c_{min}$  = minimum edge distance for reduced load (inches).

<sup>5.</sup>  $f_c$  = adjustment factor for allowable load at actual edge distance.

<sup>6.</sup>  $f_{ccr}$  = adjustment factor for allowable load at critical edge distance.  $f_{ccr}$  is always = 1.00.

<sup>7.</sup> f<sub>cmin</sub> = adjustment factor for allowable load at minimum edge distance.

<sup>8.</sup>  $f_c = f_{cmin} + [(1 - f_{cmin}) (c_{act} - c_{min}) / (c_{cr} - c_{min})].$ 

<sup>\*</sup> See page 12 for an explanation of the load table icons

**Adhesive** Anchors

# **SET** Design Information — Masonry



SET Allowable Load-Adjustment Factors in Face of Wall Installation in 8" Grout-Filled CMU: End/Edge Distance and Spacing, Tension and Shear Loads

#### How to use these charts

- 1. The following tables are for reduced end and edge distance and spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the end or edge distance ( $c_{act}$ ) or spacing ( $s_{act}$ ) at which the anchor is to be installed.
- 5. The load-adjustment factor (f<sub>c</sub> or f<sub>s</sub>) is the intersection of the row and
- 6. Multiply the allowable load by the applicable load-adjustment factor.
- 7. Reduction factors for multiple edges or spacing are multiplied together.
- 8. Adjustment factors do not apply to allowable steel strength values.
- based on CMU strength values only.

#### End Distance Tension (f<sub>c</sub>)

	Dia.	1/2	5/8	3/4	IBC
	E	41/4	5	6¾	150
c <sub>act</sub> (in.)	C <sub>cr</sub>	17	20	27	1
(111.)	C <sub>min</sub>	4	4	4	X1 53:
	f <sub>cmin</sub>	1.00	0.84	0.54**	(##/#
4		1.00	0.84	0.54	
8		1.00	0.88	0.62	<b></b>
12		1.00	0.92	0.70	<b>←</b> → I
16		1.00	0.96	0.78	
17		1.00	0.97	0.80	
20			1.00	0.86	
24				0.94	
27				1.00	

See notes below.

#### Edge Distance Tension (f<sub>c</sub>)

	Dia.	1/2	5/8	3/4	
c <sub>act</sub> (in.)	E	41/4	5	63/4	
	c <sub>cr</sub>	17	20	27	
(111.)	C <sub>min</sub>	4	4	4	
	f <sub>cmin</sub>	1.00	0.84	0.54**	
4		1.00	0.84	0.54	
8		1.00	0.88	0.62	
12		1.00	0.92	0.70	
16		1.00	0.96	0.78	
17		1.00	0.97	0.80	
20			1.00	0.86	
24				0.94	
27				1.00	

See notes below.

**IBC** 

- 9. Adjustment factors are to be applied to allowable tension or shear load

#### End and Edge Distance Shear (f<sub>c</sub>) Shear Load Perpendicular to

#### End or Edge

	Dia.	1/2	5/8	3/4
	E	41/4	5	63/4
c <sub>act</sub> (in.)	Ccr	17	20	27
(111.)	Cmin	4	4	4
	f <sub>cmin</sub>	0.43	0.25	0.25
4		0.43	0.25	0.25
8		0.61	0.44	0.38
12		0.78	0.63	0.51
16		0.96	0.81	0.64
17		1.00	0.86	0.67
20			1.00	0.77
24				0.90
27				1.00

#### End and Edge Distance Shear (f<sub>c</sub>) Shear Load Parallel to End or Edge

	Dia.	1/2	5/8	3/4
_	E	41/4	5	6¾
c <sub>act</sub> (in.)	c <sub>cr</sub>	17	20	27
	C <sub>min</sub>	4	4	4
	f <sub>cmin</sub>	0.95	0.51	0.45
4		0.95	0.51	0.45
8		0.97	0.63	0.55
12		0.98	0.76	0.64
16		1.00	0.88	0.74
17		1.00	0.91	0.76
20			1.00	0.83
24				0.93
27				1.00

# **IBC**





intersecting at a building corner).



\*\* The allowable tension load reduction factor is permitted to equal 1.0 provided both of the following conditions are met: (a) The anchor is installed with a minimum end distance,  $C_{min}$ , between 4 inches and 8 inches; and (b) a masonry return wall of identical construction is



- 1. E = Embedment depth (inches).
- $2. c_{act} = actual end or edge distance at which$ anchor is installed (inches).
- 3.  $c_{cr}$  = critical end or edge distance for 100% load (inches).
- 4. c<sub>min</sub> = minimum end or edge distance for reduced load (inches).
- 5.  $f_c$  = adjustment factor for allowable load at actual end or edge distance.
- 6.  $f_{ccr}$  = adjustment factor for allowable load at critical end or edge distance. f<sub>ccr</sub> is always = 1.00.
- 7. f<sub>cmin</sub> = adjustment factor for allowable load at minimum end or edge distance.
- 8.  $f_c = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min}) / (c_{cr} c_{min})].$

#### Spacing Tension (f.)

Opaciii	g iciisi	Off (IS)			
	Dia.	1/2	5/8	3/4	IBC
	E	41/4	5	6¾	
s <sub>act</sub> (in.)	Scr	17	20	27	1
(111.)	Smin	8	8	8	87 89
	f <sub>smin</sub>	0.89	0.81	0.59	(== =
8		0.89	0.81	0.59	
12		0.94	0.87	0.68	<u>n n</u>
16		0.99	0.94	0.76	Ĭ <b>← →</b> Ĭ
17		1.00	0.95	0.78	
20			1.00	0.85	
24				0.94	
27				1.00	

#### Spacing Shear (f<sub>s</sub>)

	0	( 0)		
	Dia.	1/2	5/8	3/4
_	E	41/4	5	63/4
s <sub>act</sub> (in.)	Scr	17	20	27
(111.)	Smin	8	8	8
	f <sub>smin</sub>	1.00	1.00	1.00
8				
12				
16				
17		1.00 fo	r all spacin	ıg ≥ 8 in.
20				
24				
27				









- 1. E = Embedment depth (inches).
- $2. s_{act} = actual spacing distance at which$ anchors are installed (inches).
- 3.  $s_{cr}$  = critical spacing distance for 100% load (inches).
- 4. s<sub>min</sub> = minimum spacing distance for reduced load (inches).
- 5.  $f_s$  = adjustment factor for allowable load at actual spacing distance.
- 6. f<sub>scr</sub> = adjustment factor for allowable load at critical spacing distance. fscr is always
- 7. f<sub>smin</sub> = adjustment factor for allowable load at minimum spacing distance.
- 8.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$



# **EDOT** Epoxy Adhesive



Formulated specifically for transportation projects, EDOT adhesive is a two-component, high-solids epoxy system. It is designed for use as a high-strength, non-shrink anchor-grouting material. EDOT adhesive provides an economical solution for transportation applications. *Visit www.strongtie.com/DOT for specific state DOT approvals.* 

#### **Features**

- Meets ASTM C881 and AASHTO M-235 specifications for Type I, II, IV and V, Grade 3, Class C
- Cure times 24 hours at 60°F, 72 hours at 40°F
- Easy hole-cleaning procedure no power-brushing required
- Suitable for use in damp or wet anchor sites
- · When properly mixed, adhesive will be a uniform tan color
- Available in 22 oz. and 56 oz. cartridges for application versatility
- Available in 1-, 10- and 100-gallon bulk kits
- Made in the USA using global materials

#### Applications

- Threaded rod anchoring and rebar doweling into concrete and masonry
- Multiple DOT listings refer to www.strongtie.com/DOT for current approvals

**Codes:** Multiple DOT listings (refer to **www.strongtie.com/DOT** for current approvals)

#### **Chemical Resistance**

See pages 320-321.

#### Installation and Application Instructions

(See also pages 124-127.)

- Surfaces to receive epoxy must be clean.
- Base material temperature must be 40°F or above at the time of installation. For best results, material should be 70°–80°F at time of application.
- To warm cold material, store cartridges in a warm, uniformly heated area or storage container. Do not immerse cartridges in water to facilitate warming.
- Mixed material in nozzle can harden in 30 minutes at temperatures of 70°F and above.

#### Suggested Specifications

See www.strongtie.com for more information.



**EDOT** Adhesive

# **EDOT** Epoxy Adhesive



#### **Test Criteria**

Anchors installed with EDOT adhesive have been tested in accordance with ASTM E1512.

Property	Test Method	Result*
Consistency (77°F)	ASTM C881	Non-sag/thixotropic paste
Heat deflection	ASTM D648	127°F (53°C)
Bond strength (moist cure, 60°F) Hardened concrete to hardened concrete	ASTM C882	2,920 psi (2 days) 3,410 psi (14 days)
Bond strength Fresh concrete to hardened concrete	ASTM C882	2,298 psi (14 days)
Water absorption	ASTM D570	0.11% (24 hours)
Compressive yield strength (cured 60°F)	ASTM D695	10,390 psi (7 days)
Compressive modulus (cured 60°F)	ASTM D695	408,100 psi (7 days)
Shore D Hardness	ASTM D2240	83
Gel time	ASTM C881	60 minutes
Shrinkage coefficient	ASTM D2566	0.002 in./in.
VOC	ASTM D2369	6 g/L

<sup>\*</sup>Material and curing conditions:  $73 \pm 2$ °F, unless otherwise noted.

#### **EDOT Package Systems**

Model No.	Capacity	Cartridge Type	Carton Quantity	Dispensing Tool(s)	Mixing Nozzle
ED0T22	22 ounces	cartridge, side-by-side	10	EDT22S, EDTA22CKT, EDTA22P	EMN22i
EDOT22-N <sup>1</sup>	22 ounces	cartridge, side-by-side	10	EDT22S, EDTA22CKT, EDTA22P	EMN22i
ED0T56	56 ounces	cartridge, side-by-side	6	EMN22i or EMN50	_
EDOT1KT	1-gallon kit	(2) 1/2 gal. pails	1 kit	For bulk applications, use the FMN27A	hulk miving pozzlo
EDOT10KT	10-gallon kit	(2) 5 gal. pails	1 kit	For bulk applications, use the EMN37A bulk mixing noz	
EDOT100KT	100-gallon kit	(2) 50 gal. drums	1 kit	Contact Simpson Strong-Tie for mor	re information.

<sup>1.</sup> Cartridge estimation guidelines are available at www.strongtie.com/apps.

#### Cure Schedule

Base N Tempe	Cure Time	
°F	°C	
40	4	72 hrs
60	16	24 hrs
80	27	24 hrs
100	38	24 hrs

#### In-Service Temperature Sensitivity

Base M Tempe	Percent of	
°F	°C	Allowable Load
40	4	100%
70	21	100%
110	43	100%
135	57	85%

#### Pot Life for 1 Gallon Mixed

Adho Tempa	Pot Life Time	
°F	°C	(min)
60	16	60
70	21	35
80	27	25
90	32	15
100	38	10

Detailed information on dispensing tools, mixing nozzles and other adhesive accessories is available on pages 128 through 135, or at www.strongtie.com.

Use only Simpson Strong-Tie® mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair EDOT adhesive performance.

<sup>4.</sup> One EMN22i mixing nozzle and one nozzle extension are supplied with each cartridge.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC

# **Adhesive Anchoring Installation Instructions**



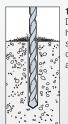


**NOTE:** Always check expiration date on product label. Do not use expired product.

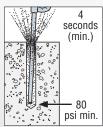


**WARNING:** When drilling and cleaning hole, use eye and lung protection. When installing adhesive, use eye and skin protection.

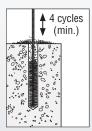
#### 1 Hole Preparation - Horizontal, Vertical and Overhead Applications



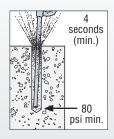
1. Drill.
Drill
hole to
specified
diameter
and depth.



2. Blow.
Remove dust from hole with oil-free compressed air for a minimum of 4 seconds.
Compressed air nozzle must reach the bottom of the hole.



3. Brush.
Clean with a
nylon brush for
a minimum of
4 cycles. Brush
should provide
resistance to
insertion. If no
resistance is felt,
the brush is worn
and must be
replaced.



4. Blow.
Remove dust from hole with oil-free compressed air for a minimum of 4 seconds.
Compressed air nozzle must reach the bottom of the hole.

Refer to page 135 or vist www.strongtie.com for proper brush part number.

#### 2 Cartridge Preparation

#### 1. Check.

Check expiration date on product label. **Do not use expired product.** Product is usable until end of printed expiration month.

Refer to www.strongtie.com for

tool part number.

proper mixing nozzle and dispensing

#### 2. Open.

Open cartridge per package instructions.



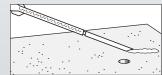
# 3. Attach.

Attach proper Simpson Strong-Tie® nozzle and extension to cartridge. Do not modify nozzle.



4. Insert.

Insert cartridge into dispensing tool.



5. Dispense.

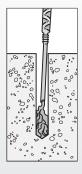
Dispense adhesive to the side until properly mixed (uniform color).

#### FOR SOLID BASE MATERIALS

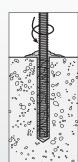
#### 3A Filling the Hole - Vertical Anchorage

Prepare the hole per "Hole Preparation" instructions on product label.

#### DRY AND DAMP HOLES:

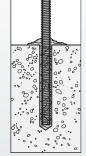


1. Fill.
Fill hole ½ to % full, starting from bottom of hole to prevent air pockets.
Withdraw nozzle as hole fills up.



2. Insert.
Insert clean,
oil-free anchor,
turning slowly
until the anchor
contacts the
bottom of the
hole.

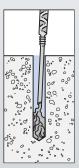
Threaded rod or rebar



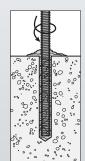
3. Do not disturb.

Do not disturb anchor until fully cured.(See cure schedule for specific adhesive.)

#### WATER-FILLED HOLES:



1. Fill.
Fill hole completely full, starting from bottom of hole to prevent water pockets. Withdraw nozzle as hole fills up.



Insert clean, oil-free anchor, turning slowly until the anchor contacts the bottom of the hole.

2. Insert.

Threaded rod or rebar



disturb.

Do not disturb anchor until fully cured. (See cure schedule.)

3. Do not

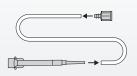
Note: Nozzle extensions may be needed for deep holes.

# Adhesive Anchoring Installation Instructions

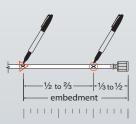


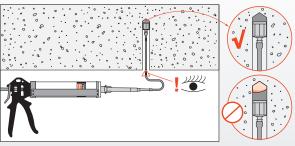
#### 3B Filling the Hole - Piston Plug Delivery System

Prepare the hole per "Hole Preparation" instructions on product label

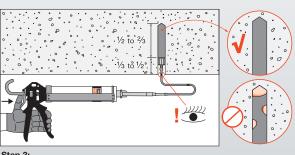


- Attach the piston plug to one end of the flexible tubing (PPFT25)
- Cut tubing to the length needed for the application, mark tubing as noted below and attach other end of tubing to the mixing nozzle
- If using a pneumatic dispensing tool, regulate air pressure to 80-100 psi



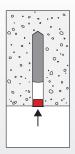


• Insert the piston plug to the back of the drilled hole and dispense adhesive



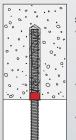
#### Step 3:

- Fill the hole 1/2 to 3/3 full
- Note: as adhesive is dispensed into the drilled hole, the piston plug will slowly displace out of the hole due to back pressure, preventing air gaps



#### Step 4:

Install the appropriate Simpson Strong-Tie adhesive retaining cap

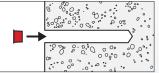


#### Step 5:

- Place either threaded rod or rebar through the adhesive retaining cap and into adhesivefilled hole
- Turn rod/rebar slowly until the insert bottoms out
- Do not disturb until fully cured

### 36 Filling the Hole - Horizontal and Overhead Anchorage with Adhesive Retaining Caps

Prepare the hole per "Hole Preparation" instructions on product label.



Install Simpson Strong-Tie® ARC adhesive retaining cap. Refer to page 132 or visit www.strongtie.com for proper

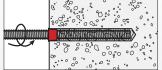
# 000000

Fill hole 1/2-2/3 full, starting from bottom of hole to prevent air pockets. Withdraw nozzle as hole fills up.

ARC size.

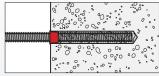
Note: Nozzle extensions may be needed for deep holes.

#### Threaded rod or rebar



Insert clean, oil-free anchor, turning slowly until the anchor contacts the bottom of the hole.

#### Threaded rod or rebar

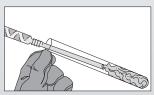


Do not disturb anchor until fully cured (see cure schedule).

#### FOR HOLLOW BASE MATERIALS

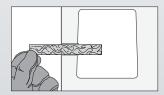
#### 3D Filling the Hole - When Anchoring with Screens: For AT, ET-HP®, SET-XP® and SET Adhesives (except SET1.7KTA)

Prepare the hole per instructions on "Hole Preparation."



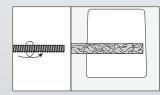
#### 1. Fill.

Fill screen completely. Fill from the bottom of the screen and withdraw the nozzle as the screen fills to prevent air pockets. (Opti-Mesh screens: Close integral cap after filling.)



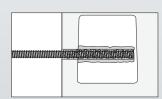
2. Insert.

Insert adhesive-filled screen into hole.



#### 3. Insert.

Insert clean, oil-free anchor, turning slowly until the anchor contacts the bottom of the screen.



#### 4. Do not disturb.

Do not disturb anchor until fully cured. (See cure schedule for specific adhesive.)

Installation instructions continued on page 126.

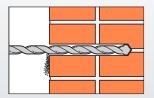


# Adhesive Anchoring Installation Instructions



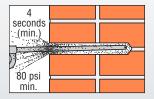
#### FOR UNREINFORCED BRICK MASONRY

1A Hole Preparation – For Configurations A and C (Horizontal) and B (22½-Degree Downward) Installations with a Carbide-Tipped Drill Bit.



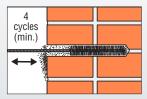
#### 1. Drill.

Drill 1-inch-diameter hole to specified depth with a carbidetipped drill bit, using rotation only mode. For Configurations A and C, drill 8 inches deep. For Configuration B, drill to within 1 inch of the opposite side of wall (minimum 13 inches deep).



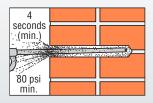
#### 2. Blow.

Remove dust from hole with oil-free compressed air for a minimum of 4 seconds. Compressed air nozzle MUST reach the bottom of the hole.



#### 3. Brush.

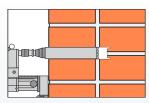
Clean with a nylon brush for a minimum of 4 cycles. Brush MUST reach the bottom of the hole. Brush should provide resistance to insertion. If no resistance is felt, the brush is worn and must be replaced.



#### 4. Blow.

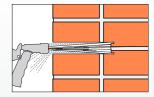
Remove dust from hole with oil-free compressed air for a minimum of 4 seconds. Compressed air nozzle MUST reach the bottom of the hole.

IB Hole Preparation – For using SET Adhesive Configurations A and C (Horizontal) and B (22½-Degree Downward) Installations with a Wet Diamond Core-Drill Bit. (See page 114, footnote 4.)



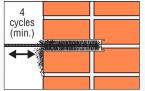
#### 1. Drill.

Drill hole to specified depth with 1-inch-diameter wet diamond core-drill bit. For Configurations A and C. drill 8 inches deep. For Configuration B, drill to within 1 inch of the opposite side of wall (minimum 13 inches deep).



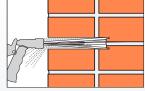
#### 2. Flush.

Flush out hole with pressurized water until water runs clear.



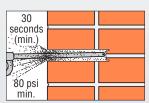
#### 3. Brush.

Clean with a nylon brush (Simpson Strong-Tie part number ETB10) for a minimum of 4 brush strokes. Brush MUST reach the bottom of the hole. Brush should provide resistance to insertion. If no resistance is felt, the brush is worn and must be replaced.



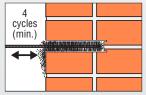
#### 4. Flush.

Flush out hole with pressurized water until water runs clear.



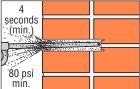
#### 5. Blow.

Remove free standing water from hole with oil-free compressed air and blow out hole for a minimum of 30 seconds. Compressed air nozzle MUST reach the bottom of the hole.



#### 6. Brush.

Clean with a nylon brush (Simpson Strong-Tie part number ETB10) for a minimum of 4 brush strokes. Brush MUST reach the bottom of the hole. Brush should provide resistance to insertion. If no resistance is felt, the brush is worn and must be replaced.



#### 7. Blow.

Blow hole with oil-free compressed air for a minimum of 4 seconds. Compressed air nozzle MUST reach the bottom of the hole.



# **Adhesive Anchoring Installation Instructions**



### 2 Cartridge Preparation

#### 1. Check.

Check cartridge expiration date. Do not use expired product. Product is usable until end of printed expiration month.

#### 2. Open.

Open cartridge per package instructions.



#### 3. Attach.

Attach proper Simpson Strong-Tie® nozzle to cartridge. Do not modify nozzle.



#### 4. Insert.

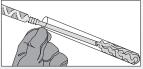
Insert cartridge into dispensing tool.



#### 5. Dispense.

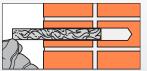
Dispense adhesive to the side until properly mixed (uniform color).

#### 3A Filling the Hole – For Configurations A (Horizontal) and B (22½ - Degree Downward) Installations.



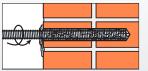
#### 1. Fill.

Fill screen completely. Fill from the bottom of the screen and withdraw the nozzle as the screen fills to prevent air pockets. (Opti-Mesh® screens: Close integral cap after filling.)



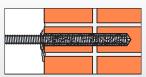
2. Insert.

Insert adhesive filled screen into hole.



#### 3. Insert.

Insert clean, oil-free anchor, turning slowly until the anchor contacts the bottom of the screen.

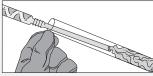


#### 4. Do not disturb.

Do not disturb anchor until fully cured. (See cure schedule for specific adhesive.)

Note: Opti-Mesh® plastic screens or steel wire mesh screens may be used for Configurations A and B.

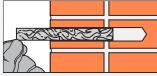
## **3B** Filling the Hole – For Configuration C (Horizontal Through-Bolt) Installation.



1. Fill.

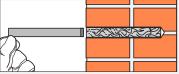
C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

Fill screen completely. Fill from the bottom of the screen and withdraw the nozzle as the screen fills to prevent air pockets.



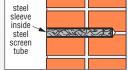
2. Insert.

Insert adhesive filled screen into hole.



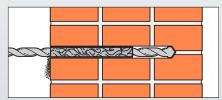
3. Insert.

Insert steel sleeve (capped end first) slowly into screen tube (adhesive will displace).



#### 4. Cure

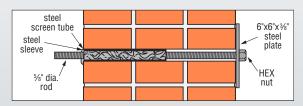
Allow adhesive to cure (see Cure Time Table 1).



#### 5. Drill.

Drill through plastic plug in (inside) end of steel sleeve and completely through the wall with %" carbide tipped concrete drill bit (rotation mode only).

Note: Steel wire mesh screens shall be used for Configuration C.



#### 6. Insert.

Insert %" rod through hole and attach metal plate and nut.



# Adhesive Dispensing Tools



#### CDT10S

Manual dispensing tool for 10 oz. single-cartridge adhesives



#### EDT22S

Manual dispensing tool for 22 oz. cartridges





#### EDTA22CKT

Battery-powered dispensing tool for 22 oz. cartridges (kit includes two battery packs and charger)



#### EDTA22P

Pneumatic dispensing tool for 22 oz. cartridges



#### EDTA56P

Pneumatic dispensing tool for 56 oz. cartridges



#### **ADT813S**

Manual dispensing tool for 12.5 oz. cartridges



#### ADT30S

Manual dispensing tool for 30 oz. cartridges



#### ADTA30CKT

Battery-powered dispensing tool for 30 oz. cartridges (kit includes two battery packs and charger)



#### ADTA30P

Pneumatic dispensing tool for 30 oz. cartridges



# Adhesive Mixing Nozzles

#### EMN22i



An 18-element static mixing nozzle for use with 10 oz., 22 oz. and 56 oz. epoxy adhesive cartridges

#### EMN37A

An 18-element static mixing nozzle for dispensing epoxy adhesive through bulk metering equipment



#### EMN50

High-volume static mixing nozzle for 22 oz. and 56 oz. epoxy adhesive cartridges



#### AMN19Q

A 19-element, static mixing nozzle for use with 10 oz., 13 oz., and 30 oz. acrylic adhesive cartridges

For more information on adhesive dispensing tools and mixing nozzles, including ordering information, visit **www.strongtie.com**.



# Piston Plug Delivery System

The Simpson Strong-Tie® Adhesive Piston Plug Delivery System offers you an easy-to-use, more reliable and less time-consuming means to dispense adhesive into drilled holes for threaded rod and rebar dowel installations at overhead, upwardly inclined and horizontal orientations.

The matched tolerance design between the piston plug and drilled hole virtually eliminates the formation of voids and air pockets during adhesive dispensing.

#### **Features**

- Designed for dispensing adhesive into drilled holes at overhead, upwardly inclined and horizontal orientations, as well as deep embedments
- Suitable for use with all Simpson Strong-Tie anchoring adhesives
- · Adhesive piston plugs are sized to fit each drilled hole diameter
- Model number is embossed on each adhesive piston plug for identification
- A barbed end provides a reliable connection to the flexible extension tubing
- Flexible extension tubing is available in 25-foot-long rolls to be cut to required lengths





Use the piston plug delivery system with Simpson Strong-Tie® adhesive products:



# SIMPSON Strong-Tie

#### Adhesive Piston Plugs

Model No.	Drill Bit Diameter	Pkg. Quantity	Carton Quantity*
PP56-RP10	9/16"	10	100
PP62-RP10	5/8"	10	100
PP68-RP10	11/16"	10	100
PP75-RP10	3/4"	10	100
PP81-RP10	13/16"	10	100
PP87-RP10	7/8"	10	100
PP100-RP10	1"	10	100
PP112-RP10	1 1/8"	10	100
PP137-RP10	13/8"	10	100
PP175-RP10	13/4"	10	100

<sup>\*10</sup> packages of 10

#### Adhesive Tubing

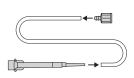
Model No.	Description	Pkg. Quantity
PPFT25	Adhesive Piston Plug Flexible Tubing — 25 ft. roll	1

#### Adhesive Retaining Caps

Model No.	Drill Bit Diameter	Cap Depth	Pkg. Quantity	Carton Quantity*
ARC50A-RP25	9/16"	1/2"	25	200
ARC50-RP25	5/8"	1/2"	25	200
ARC62A-RP25	11/16"	9/16"	25	200
ARC62-RP25	3/4"	9/16"	25	200
ARC75A-RP25	13/16"	9/16"	25	200
ARC75-RP25	7/8"	9/16"	25	200
ARC87-RP25	1"	11/16"	25	200
ARC100-RP25	1 1/8"	11/16"	25	200
ARC125-RP25	13/8"	7/8"	25	200
ARC137-RP25	13/4"	11/16"	25	200

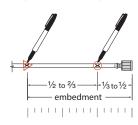
<sup>\*8</sup> packages of 25

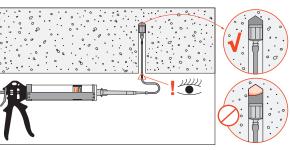
#### Installation Sequence



#### Step 1:

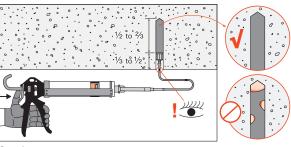
- Attach the piston plug to one end of the flexible tubing (PPFT25)
- Cut tubing to the length needed for the application, mark tubing as noted below and attach other end of tubing to the mixing nozzle
- If using a pneumatic dispensing tool, regulate air pressure to 80–100 psi





#### Step 2:

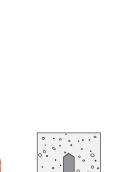
• Insert the piston plug to the back of the drilled hole and dispense adhesive



#### Step 3:

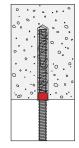
- Fill the hole ½ to ¾ full
- Note: as adhesive is dispensed into the drilled hole, the piston plug will slowly displace out of the hole due to back pressure, preventing air gaps





#### Step 4:

 Install the appropriate Simpson Strong-Tie adhesive retaining cap



#### Step 5:

- Place either threaded rod or rebar through the adhesive retaining cap and into adhesivefilled hole
- Turn rod/rebar slowly until the insert bottoms out
- Do not disturb until fully cured

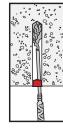
# SIMPSON Strong-Tie

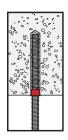
# Adhesive Retaining Caps

Adhesive retaining caps make overhead and horizontal installation easier by preventing the adhesive from running out of the hole. They also center the rod in the hole, making them ideal for applications where precise anchor placement is required. It may be necessary to provide support for the insert during cure time. Adhesive retaining caps are not designed to support the weight of the insert in overhead installations.

#### Material: Plastic







The "X" cut in the cap allows the mixing nozzle and insert to pass through, while containing the adhesive in the hole.

#### Adhesive Retaining Caps

Drill Bit Dia. (in.)	Anchor Diameter (in.)	Rebar Size	Model No.	Cap Depth (in.)	Package Qty.	Carton Qty.* (ea.)
7/16	3/8	"0	ARC37A-RP25	7/16	25	200
1/2	3/8	#3	ARC37-RP25	7/16	25	200
9/16	1/2	#4	ARC50A-RP25	1/2	25	200
5/8	1/2	#4	ARC50-RP25	1/2	25	200
11/16	5/8	#5	ARC62A-RP25	9/16	25	200
3/4	5/8	#3	ARC62-RP25	9/16	25	200
13/16	3/4	#6	ARC75A-RP25	9/16	25	200
7/8	3/4	#0	ARC75-RP25	9/16	25	200
1	7/8	#7	ARC87-RP25	11/16	25	200
1 1/16	1	40	ARC100A-RP25	11/16	25	200
1 1/8	1	#8	ARC100-RP25	11/16	25	200
1 %	1 1/4	#10	ARC125-RP25	7/8	25	200
13/4	_	#11	ARC137-RP25	11/16	25	200

<sup>\*8</sup> packages of 25.

# SIMPSON Strong-Tie

# Steel Adhesive-Anchoring Screen Tubes

Screen tubes are used in hollow base material applications to contain adhesive around the anchor and prevent it from running into voids. Simpson Strong-Tie® screen tubes are specifically designed to work with AT, SET and ET-HP® adhesives in order to precisely control the amount of adhesive that passes through the mesh. This results in thorough coating and bonding of the rod to the screen tube and base material. Order screen tubes based upon rod diameter and adhesive type. The actual outside diameter of the screen tube is larger than the rod diameter.

Material: Acrylic screen tubes: 50 mesh stainless steel Epoxy screen tubes: 60 mesh carbon steel



**Caution:** Screen tubes are designed for a specific adhesive type. Epoxy screen tubes must be used with SET or ET-HP® formulations and acrylic screen tubes must be used with AT.



**Epoxy Screen Tube** (Acrylic screen tubes similar)

Screen tubes are for use in hollow CMU, hollow brick and unreinforced masonry applications. Contact Simpson Strong-Tie for information on special-order sizes.

#### Acrylic Adhesive (AT) Screen Tubes – Stainless Steel

For Rod Dia. (in.)	Hole Size (in.)	Actual Screen Size 0.D./Length (in.)	Model No.	Carton Qty.
3/8	9/16	15/32 X 3 1/2	ATS373	150
78	716	<sup>15</sup> ⁄ <sub>32</sub> x 6	ATS376	150
		19/ <sub>32</sub> X 3 ½	ATS503	100
1/2	11/16	<sup>19</sup> / <sub>32</sub> X 6	ATS506	100
		<sup>19</sup> / <sub>32</sub> x 10	ATS5010	50
	7/8	<sup>25</sup> / <sub>32</sub> X 3	ATS623	50
5/8		<sup>25</sup> / <sub>32</sub> X 6	ATS626	50
78		<sup>25</sup> / <sub>32</sub> x 10	ATS6210	25
		<sup>25</sup> / <sub>32</sub> x 13	ATS6213	25
		<sup>31</sup> / <sub>32</sub> X 8	ATS758	25
3/4	1	<sup>31</sup> / <sub>32</sub> x 13	ATS7513	25
		<sup>31</sup> / <sub>32</sub> x 17	ATS7517	25

#### Epoxy Adhesive (SET and ET-HP®) Screen Tubes - Carbon Steel

For Rod Dia. (in.)	Hole Size (in.)	Actual Screen Size 0.D./Length (in.)	Model No.	Carton Qty.
3/8	9/16	15/32 X 6	ETS376	150
98	716	15⁄32 X 10	ETS3710	100
1/	11/16	<sup>19</sup> / <sub>32</sub> X 6	ETS506	100
1/2	1716	19/ <sub>32</sub> x 10	ETS5010	50
		<sup>25</sup> / <sub>32</sub> x 6	ETS626	50
5/8	7/8	<sup>25</sup> / <sub>32</sub> x 10	ETS6210	25
		<sup>25</sup> / <sub>32</sub> x 13	ETS6213	25
		<sup>31</sup> / <sub>32</sub> x 8	ETS758	25
3/4	4	<sup>31</sup> / <sub>32</sub> x 13	ETS7513	25
		<sup>31</sup> / <sub>32</sub> x 17	ETS7517	25
		<sup>31</sup> / <sub>32</sub> x 21	ETS7521	25

Note: Not for use with SET1.7KTA.

# SIMPSON Strong-Tie

#### Opti-Mesh Adhesive-Anchoring Screen Tubes

Screen tubes are vital to the performance of adhesive anchors in base materials that are hollow or contain voids, such as hollow block and brick. The Simpson Strong-Tie® Opti-Mesh screen tube provides the economical advantage of a plastic screen tube while providing performance comparable to steel screen tubes and better than competitive plastic screen tubes.

#### Material: Plastic

A

Caution: Screen tubes are designed for a specific adhesive type. Epoxy screen tubes must be used with SET-XP®, ET-HP® or SET formulations, and acrylic adhesive screen tubes must be used with AT.



Epoxy Adhesive Screen Tube (mesh is black)

- Integral Cap: Serves to center and secure the rod in the screen tube, while displaying important information such as rod diameter, drill bit diameter and the Simpson Strong-Tie® "#" symbol for easy inspection after installation. The cap also prevents adhesive from running out the front of the screen tube.
- Flanges: Prevents the screen tube from slipping into over-drilled holes. Allows screen tube to function in holes that are drilled too deep.
- Open-Mesh Collar: This section of larger mesh allows extra adhesive to flow out the screen tube behind the face shell of hollow block applications. The extra "collar" of adhesive increases bearing area and results in higher load capacities in hollow concrete block.
- Color-Coded, Formula-Specific Mesh: The screen tube mesh is sized to allow only the right amount of adhesive to flow through the screen tube to bond with the base material while the balance remains in the screen to bond the rod. The acrylic screen tube mesh is white, while the epoxy screen tube mesh is black.



The integral cap centers the rod and displays drill bit and rod diameter.



(mesh is white)

rs drill eter.

#### Epoxy Adhesive (SET-XP®, ET-HP® and SET) Screen Tubes – Plastic

For Rod Dia. (in.)	Hole Size (in.)	Length (in.)	Model No.	Carton Qty.
		3 1/2	ETS373P	150
3/8	9/16	6	ETS376P	150
		10	ETS3710P	100
		3 1/2	ETS503P	100
1/2	3/4	6	ETS506P	100
		10	ETS5010P	50
		3 1/2	ETS623P	50
5/8	7/8	6	ETS626P	50
78	'/8	10	ETS6210P	25
		13	ETS6213P	25
3/4		8	ETS758P	25
	1	13	ETS7513P	25
	ı	17	ETS7517P	25
		21	ETS7521P	25

Not for use with SET1.7KTA.

#### Acrylic Adhesive (AT) Screen Tubes – Plastic

For Rod Dia. (in.)	Hole Size (in.)	Length (in.)	Model No.	Carton Qty.
		31/2	ATS373P	150
3/8	9/16	6	ATS376P	150
		10	ATS3710P	100
		31/2	ATS503P	100
1/2	3/4	6	ATS506P	100
		10	ATS5010P	50
		31/2	ATS623P	50
5/8	7/8	6	ATS626P	50
78	'/8	10	ATS6210P	25
		13	ATS6213P	25
3/4		8	ATS758P	25
	1	13	ATS7513P	25
		17	ATS7517P	25
		21	ATS7521P	25

# SIMPSON Strong-Tie

#### **Hole-Cleaning Brushes**

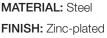
Brushes are used for cleaning drilled holes prior to adhesive anchor installation. Brushes have a twisted wire handle with nylon bristles.

Description	Model No.	For Anchor/Rebar Diameter (in.)	For Hole Diameter (in.)	Ctn Qty
½" dia x 3" brush (8" total length)	ETB4	1/4" — 5/16"	3/8" — 7/16"	24
3/4" x 4" brush (16" total length)	ETB6	3/8" — 5/8"	1/2" — 3/4"	24
1" x 4" brush (16" total length)	ETB8	3/4"	13/16" — 7/8"	24
1" x 4" brush (24" total length)	ETB8L	3/4"	13/16" — 7/8"	24
1 1/4" x 4" brush (29" total length)	ETB10	7⁄8" − 1"	1" – 11/8"	24
15/8" x 6" brush (34" total length)	ETB12	1 1/4"	13/16"- 13/8"	24



#### Adhesive Shear Tubes

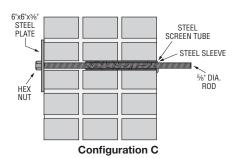
Used in conjunction with anchoring adhesive and screen tubes, adhesive shear tubes transfer anchor shear loads over a larger area, reducing localized crushing in unreinforced masonry installations. Required for through-bolt applications per ICC-ES's unreinforced masonry anchorage "Configuration C" detail. For detailed installation instructions, refer to the appropriate adhesive anchor ICC-ES report.



Description (in.)	Model No.	For use with Simpson Screen Model No. <sup>1</sup>		Threaded Rod Diameter (in.)	Carton Qty.
<sup>13</sup> / <sub>16</sub> X 8	AST800	ETS758, ATS758	1	5/8	1

Screens sold separately. Not for use with Simpson Strong-Tie screen ETS758P or ATS758P plastic Opti-Mesh screen tubes.





#### **Retrofit Bolts**

RFBs are pre-cut threaded rod, supplied with nut and washer. For use with Simpson Strong-Tie® adhesives. May be ordered in bulk without the nut and washer. Use with Simpson Strong-Tie adhesives to anchor into existing concrete and masonry. Each end of the threaded rod is stamped with rod length in inches and our "No-Equal" symbol for easy identification after installation.

MATERIAL: ASTM F1554 Grade 36
COATING: Zinc-plated, hot-dip galvanized

Description Dia. Length	Zinc-Plated Model No.	Hot-Dip Galvanized Model No.	Ctn Qty	Retail² Pack
½" x 4"	RFB#4x4	RFB#4x4HDG	50	_
½" x 5"	RFB#4x5	RFB#4x5HDG	50	10
½" x 6"	RFB#4x6	RFB#4x6HDG	50	10
½" x 7"	RFB#4x7	RFB#4x7HDG	50	10
½" x 8"	_	RFB#4x8HDG		10
½" x 10"	RFB#4x10	RFB#4x10HDG	25	10
%" x 5"	RFB#5x5	RFB#5x5HDG	50	10
5⁄8" x 8"	RFB#5x8	RFB#5x8HDG	50	10
%" x 10"	RFB#5x10	RFB#5x10HDG	50	10
5/8" x 12"	_	RFB#5x12HDG	_	10
%" x 16"	RFB#5x16	RFB#5x16HDG	25	10
3⁄4" x 101⁄2"	RFB#6x10.5	RFB#6x10.5HDG	25	_



- Bulk quantities do not include the nut and washer and must be ordered with a "-B" suffix (example: RFB#4x5-B). Hot-dip galvanized RFBs not available in bulk.
- Retail packs must be ordered with a "-R" suffix (example: RFB#5x12HDG-R).

# **Mechanical** Anchors



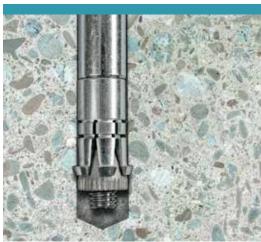




From complex infrastructure projects to do-it-yourself ventures, Simpson Strong-Tie offers a wide variety of anchoring products to meet virtually any need.

Our mechanical anchors are designed to install easily and securely into a variety of base materials — from concrete and brick to hollow and grouted CMU. They offer optimal performance even in the most demanding structural applications. For applications where there is a risk of concrete cracking, specific anchors have been designed and tested to offer reliability under these conditions.







Concrete

#### **Features**

**Mechanical** Anchors

- Code listed under IBC/IRC for cracked and uncracked concrete per ICC-ES ESR-2705
- · Self-undercutting feature provides higher load-carrying capacity than conventional mechanical anchors
- · Qualified for static and seismic loading conditions (seismic design categories A through F)
- Ductile steel rod provides consistent, reliable performance
- · Specially designed, low-friction expansion cone minimizes binding and speeds installation
- Installation requires no special drill bit or secondary drilling operation
- Head is stamped with the Simpson Strong-Tie<sup>®</sup> "≠" sign and anchor size identification for easy post-installation verification

Codes: ICC-ES ESR-2705 (concrete); City of L.A. RR25946

(concrete); Florida FL-15731.3

Material: Carbon steel

Coating: Zinc plated or sherardized\*

#### Torq-Cut™ Setting Tool

The TCAST is the steel setting tool used to install the Torq-Cut self-undercutting anchor, driving the anchor into the pre-drilled hole and protecting the threads on the Torq-Cut anchor from being damaged by hammer blows.

#### Installation Instructions: Pre-Set Version

- 1. Drill a hole in the base material to the specified embedment depth using the appropriate diameter carbide drill bit specified for each diameter.
- 2. Blow the hole clean using compressed air.
- 3. Assemble the anchor with nut and washer, and finger-tighten the nut so all components are snug (spacer sleeve, expansion sleeve and cone). The bottom of the threaded rod should be flush with the bottom of the cone.
- 4. Place the anchor in the drilled hole, and use a hammer and setting tool to drive the anchor until the washer and nut are tight against the surface of the base material.
- 5. Remove the nut and washer and install the fixture. Reassemble the nut and washer over the fixture.
- 6. Tighten to the required installation torque.

# Torq-Cut<sup>™</sup> Torq-Cut™ **Self-Undercutting Anchor** Setting Tool

# Installation Instructions: Through-Set Version

- 1. Drill a hole in the base material to the specified embedment depth using the appropriate diameter carbide drill bit specified for each diameter.
- 2. Blow the hole clean using compressed air.

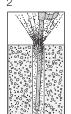
U.S. Patent 7,357,613

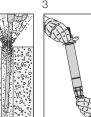
- 3. Assemble the anchor with nut and washer and finger-tighten the nut so all components are snug (spacer sleeve, expansion sleeve and cone). The bottom of the threaded rod should be flush with the bottom of the cone.
- 4. Place the anchor through the fixture and into the drilled hole. Use a hammer and setting tool to drive the anchor until the washer and nut are tight against the fixture.
- 5. Tighten to the required installation torque.

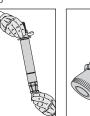
Caution: Oversized holes in the base material will make it difficult to set the anchor and will reduce the anchor's load capacity. Do not install in holes drilled with core drill bit.

#### Pre-Set and Through-Set Version

Step 1

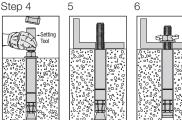


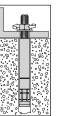




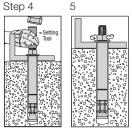


#### **Pre-Set Version**





**Through-Set Version** 



(Sold separately)

# **Torq-Cut**<sup>™</sup> Self-Undercutting Anchor



#### Torq-Cut<sup>™</sup> Anchor Product Data, Pre-Set Version<sup>1</sup>

Size	Model No.	Drill Bit Dia.	Min. Drilled Hole Depth	Min. Nominal Embedment	Max. Fixture Thickness	Min. Fixture Hole Dia.	Threaded Rod Length	Quantity		
(in.)	Model No.	(in.)	(A) (in.)	Depth, h <sub>nom</sub> (B) (in.)	(F) (in.)	(in.)	(D) (in.)	Вох	Carton	
½ x 8¾	TCAP500834	7/8	7	6%	1 1⁄4	9⁄16	8¾	5	10	
½ x 9½	TCAP500912	7/8	7	6%	2	9/16	91/2	5	10	
% x 11½	TCAP621112	1	91/2	87/8	1 ½	11/16	111/2	4	8	
5/8 x 121/2	TCAP621212	1	91/2	87/8	21/2	11/16	12½	4	8	
3/4 x 145/8	TCAP751458	1 1/4	12	11%	2	13/16	14%	4	8	
3/4 x 165/8	TCAP751658	1 1/4	12	11%	4	13/16	16%	4	8	

<sup>1.</sup> See Figure 1 below.

#### Torq-Cut<sup>™</sup> Anchor Product Data, Through-Set Version<sup>1</sup>

Size	Model No.	Drill Bit Dia.	Min. Drilled Hole Depth	Min. Nominal Embedment	Max. Fixture Thickness	Min. Fixture Hole Dia.	Threaded Rod	Qua	ntity
(in.)	Model No.	(in.)	(A) (in.)	Depth, h <sub>nom</sub> (B) (in.)	(F) (in.)	(in.)	Length (D) (in.)	Вох	Carton
½ x 8¾	TCAT500834	7/8	7	6%	1 1⁄4	<sup>15</sup> / <sub>16</sub>	83/4	5	10
½ x 9½	TCAT500912	7/8	7	6%	2	15/16	91/2	5	10
% x 11½	TCAT621112	1	91/2	87/8	1 ½	1 1/16	111/2	4	8
% x 12½	TCAT621212	1	91/2	87/8	21/2	1 1/16	121/2	4	8
3/4 x 145/8	TCAT751458	1 1/4	12	11%	2	1 5/16	14%	4	8
3/4 x 165/8	TCAT751658	1 1/4	12	11%	4	1 5/16	16%	4	8

<sup>1.</sup> See Figure 1 below.

#### Torq-Cut™ Anchor Material Specifications\*

	Carbon Steel Component Materials									
Th	Threaded Rod Nut		Washer	Spacer Sleeve	Undercut Expansion Ring	Expansion Cone				
Material	ASTM A193 Grade B7M	SAE J995, Grade 8	ASTM F436, Type 1	SAE J403 Grade 1045 Steel	SAE J403 Grade 1045 Steel	SAE J403 Grade 1144 Steel				
Coating	Zinc Plated ASTM B633 SC1	Zinc plated	Zinc plated	Zinc Plated ASTM B633 SC1	Zinc Plated ASTM B633 SC1	Zinc Plated ASTM B633 SC1				

<sup>\*</sup>For added corrosion resistance, TCA with a sherardized coating is available by special order.

#### Torq-Cut™ Anchor Installation Data

Nominal Anchor Dia (in.)	1/2	5/8	3/4
Drill Bit Size (in.)	7/8	1	1 1/4
Fixture Hole Dia Range Pre-Set (in.)	9/16-3/4	11/16—7/8	13/16—1 1/8
Min. Fixture Hole Dia Through-Set (in.)	<sup>15</sup> ⁄ <sub>16</sub>	1 1⁄16	15/16
Wrench Size (in.)	3/4	<sup>15</sup> ⁄ <sub>16</sub>	1 1/8
Setting Tool Required	TCAST50	TCAST62	TCAST75

- 1. The Drilled Hole Depth is 1/2" greater than the Nominal Embedment Depth.
- 2. For the Through-Set version of the Torq-Cut anchor, if the actual Fixture Thickness ( $t_{\rm fix}$ ) is less than the Maximum Fixture Thickness (F), the Minimum Drilled Hole Depth (A) must be increased as follows:

Drilled Hole Depth =  $A + (F - t_{fix})$ 

Similarly, the Minimum Nominal Embedment Depth (B) is increased as follows: Nominal Embedment Depth = B + (F -  $t_{\rm fix}$ )

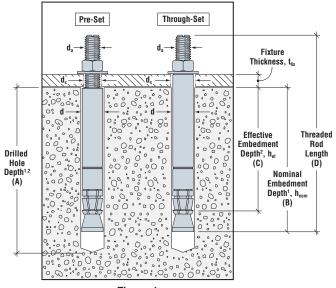


Figure 1
Drilled Hole Depth

# **Torq-Cut**<sup>™</sup> Design Information — Concrete



#### Torq-Cut<sup>™</sup> Anchor Installation and Additional Data<sup>1</sup>

Ohawastawistia	Cumbal	Heite	Nominal Anchor Diameter (in.)			
Characteristic	Symbol	Units	1/2	5/8	3/4	
	Installation Inforn	nation				
Drill Bit Diameter	d	in.	7/8	1	1 1/4	
Pre-Set Fixture Hole Diameter Range <sup>2</sup>	$d_c$	in.	9/16-3/4	11/16—7/8	13/16-1 1/8	
Through-Set Minimum Fixture Hole Diameter <sup>2</sup>	$d_c$	in.	15/16	1 1/16	15/16	
Installation Torque	T <sub>inst</sub>	ftlb.	90	185	240	
Minimum Nominal Embedment Depth	h <sub>nom</sub>	in.	6%	87/8	11 %	
Minimum Overall Depth of Drilled Hole	h <sub>hole</sub>	in.	7	91/2	12	
Critical Edge Distance	Cac	in.	85/8	12	15%	
Minimum Edge Distance	C <sub>min</sub>	in.	7	10	73/4	
Minimum Spacing	S <sub>min</sub>	in.	7	9	73/4	
Minimum Concrete Thickness	h <sub>min</sub>	in.	85%	12	15%	
	Additional Da	ta				
Anchor Category	Category	_	1	1	1	
Yield Strength	f <sub>ya</sub>	ksi	80	80	80	
Tensile Strength	f <sub>uta</sub>	ksi	100	100	100	
Effective Tensile and Shear Stress Area	$A_{Se}$	in <sup>2</sup>	0.142	0.226	0.334	
Axial Stiffness in Service Load Range – uncracked concrete	$\beta_{uncr}$	lb./in.		635,830		
Axial Stiffness in Service Load Range - cracked concrete	$eta_{cr}$	lb./in.	346,694			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D.
- 2. The clearance must comply with applicable code requirements for the connected element.

#### Torg-Cut<sup>™</sup> Tension Strength Design Data<sup>1</sup>



Torq-Cut Tension Strength Design Data					man (managed (managed)		
Characteristic	Symbol	Units	Nomin	Nominal Anchor Diameter (in.)			
บแลเลยเฮเอแบ	Symbol	Units	1/2	5/8	3/4		
Minimum Nominal Embedment Depth	h <sub>nom</sub>	in.	6%	87/8	11%		
5	Steel Strength in T	ension					
Nominal Steel Strength in Tension	N <sub>sa</sub>	lb.	14,190	22,600	33,450		
Strength Reduction Factor - Steel Failure	$\phi_{sa}$	_		$0.75^{2}$			
Concret	e Breakout Streng	th in Tension <sup>6</sup>					
Minimum Effective Embedment Depth	h <sub>ef</sub>	in.	53/4	8	101/4		
Critical Edge Distance	$c_{ac}$	in.	85/8	12	15%		
Effectiveness Factor – Uncracked Concrete	K <sub>uncr</sub>	<u> </u>	24	24	24		
Effectiveness Factor – Cracked Concrete	K <sub>Cr</sub>	<u> </u>	21	17	21		
Modification Factor	$\psi_{c,N}$		1.0	1.0	1.0		
Strength Reduction Factor – Concrete Breakout Failure	$\phi_{cb}$	_		0.655			
Pι	llout Strength in 1	ension <sup>6</sup>					
Pullout Strength Uncracked Concrete	N <sub>p,uncr</sub>	lb	N/A³	N/A <sup>3</sup>	N/A <sup>3</sup>		
Pullout Strength Cracked Concrete	N <sub>p,cr</sub>	lb	N/A <sup>3</sup>	N/A <sup>3</sup>	N/A <sup>3</sup>		
Strength Reduction Factor - Pullout Failure	$\phi_{\scriptscriptstyle D}$	_	N/A <sup>3</sup>	N/A <sup>3</sup>	N/A <sup>3</sup>		
Tension Re	sistance for Seisn	nic Applications	6				
Tension Resistance - Seismic Loads	N <sub>eq</sub>	lb	14,190	22,600	33,450		
Strength Reduction Factor – Steel Failure	$\phi_{sa}$	_		$0.75^{2}$			

- The information presented in this table must be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The tabulated value of  $\phi_{sa}$  applies when the load combinations of Section 1605.2.1 of the IBC, or ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{sa}$  must be determined in accordance with ACI 318 D.4.4. Torq-Cut<sup>™</sup> anchors are ductile steel elements as defined in ACI 318 D.1.
- 3. N/A (Not Applicable) denotes that pullout resistance does not need to be considered.
- 4. The tabulated value of  $\phi_{p}$  applies when the load combinations of Section 1605.2.1 of the IBC, or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, appropriate value of  $\phi$  must be determined in accordance with ACI 318 Section D.4.4(c).
- 5. The tabulated value of  $\phi_{cb}$  applies when both the load combinations of Section 1605.2.1 of the IBC, or ACI 318 Section 9.2 are used and the requirements of ACI 318 Section D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the  $\phi_{cb}$  factors described in ACI 318 D.4.3 for Condition A are allowed. If the load combinations of ACI 318 Section 9.2 are used and the requirements of ACI 318 Section D.4.3 for Condition A are met, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.3(c). If the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.4(c).
- For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout strength, N<sub>p,cr</sub>, N<sub>p,uncr</sub> and N<sub>eq</sub> by 0.6.
   All-lightweight concrete is beyond the scope of this table.
- 7. Pullout strength applies for 2,500 psi  $\leq$  f'<sub>c</sub>  $\leq$  3,500 psi concrete. For f'<sub>c</sub> > 3,500 psi concrete, pullout strength need not be considered since steel controls for concrete strengths greater than 3,500 psi.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **Torq-Cut**<sup>™</sup> Design Information — Concrete



IBC TO TWO

#### Torq-Cut<sup>™</sup> Shear Strength Design Data<sup>1</sup>

Torq-Cut Snear Strength Design Data						
Characteristic	Symbol	Units	Nominal Anchor Diameter (in.)			
जावा बहारा । इसर	Syllibul	Ullits	1/2	5/8	3/4	
Nominal Embedment Depth	h <sub>nom</sub>	in.	6%	87/8	11%	
Steel Strength i	n Shear					
Pre-Set Configuration: Steel Strength in Shear	V <sub>sa</sub>	lb.	8,515	13,560	20,070	
Through-Set Configuration: Steel Strength in Shear	V <sub>sa</sub>	lb.	26,065	38,720	49,235	
Strength Reduction Factor – Steel Failure	$\phi_{sa}$	_		0.652		
Concrete Breakout Stre	ength in Shea	ar <sup>5</sup>				
Outside Diameter	$d_a$	in.	7/8	1	13⁄4	
Load Bearing Length of Anchor in Shear	$\ell_e$	in.	4.3	5.8	7.5	
Strength Reduction Factor – Concrete Breakout Failure	$\phi_{cb}$	_	0.703			
Concrete Pryout Stre	ngth in Shear	r				
Coefficient for Pryout Strength	K <sub>CP</sub>	lb.		2.0		
Strength Reduction Factor — Concrete Pryout Failure	$\phi_{cp}$	_		0.704		
Steel Strength in Shear for S	Seismic Appli	cations				
Pre-Set Configuration: Steel Strength in Shear for Seismic Loads	V <sub>eq</sub>	lb.	8,515	13,560	20,070	
Through-Set Configuration: Steel Strength in Shear for Seismic Loads	$V_{eq}$	lb.	15,640	30,975	44,310	
Strength Reduction Factor – Steel Failure	$\phi_{sa}$	_		0.652		

- The information presented in this table must be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The tabulated value of \$\phi\_{Sa}\$ applies when the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3 (c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, the appropriate value of \$\phi\_{Sa}\$ must be determined in accordance with ACI 318 D.4.4.
  Torq-Cut™ anchors are ductile steel elements as defined in ACI 318 D.1.
- 3. The tabulated value of  $\phi_{cb}$  applies when both the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the  $\phi_{cb}$  factors described in ACI 318 D.4.3 for Condition A are allowed. If the load combinations of ACI 318 Section 9.2 are used and the requirements of ACI 318 Section D.4.3 for Condition A are met, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.3(c). If the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.4(c).
- 4. The tabulated value of  $\phi_{CD}$  applies when both the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. if the load combinations of ACI 318 Appendix C are used, appropriate value of  $\phi_{CD}$  must be determined in accordance with ACI 318 Section D.4.4(c).
- 5. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout strength by 0.6. All-lightweight concrete is beyond the scope of this table.

# Torq-Cut<sup>™</sup> Design Information — Concrete



#### Torq-Cut<sup>™</sup> Tension Design Strengths in Normal-Weight Concrete (f'<sub>C</sub> = 2,500 psi)







		B.02	Outstand	8.00								
Anchor Dia.	Nominal Embed. Depth	Min. Concrete Thickness	Critical Edge Distance	Minimum Edge Distance	Edge Distances = c <sub>ac</sub> on all sides		Edge Distances = c <sub>min</sub> on one side and c <sub>ac</sub> on three sides					
(in.)	(in.)	h <sub>min</sub> (in.)	c <sub>ac</sub> (in.)	c <sub>min</sub> (in.)	SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>		SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>	
		(111.)	(111.)	(111.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
1/2	6%	85%	85/8	7	10,645	9,410	8,065	7,060	9,190	8,040	6,895	6,030
5/8	87/8	12	12	10	16,950	12,500	13,235	9,375	15,370	10,885	11,525	8,165
3/4	11%	15%	15%	73/4	25,090	22,395	19,195	16,800	16,385	14,335	12,290	10,755

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor, φ, is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

#### Torg-Cut™ Allowable Tension Loads in Normal-Weight Concrete $(f'_c = 2,500 \text{ psi})$ — Static Load







1	$\overline{z}$

Anchor Dia. (in.)	Nominal	Min Concrete		Minimum		Allowable Ten	sion Load (lb.)		
	Depth	Min. Concrete Thickness h <sub>min</sub>	Critical Edge Distance c <sub>ac</sub> (in.)	Distance c <sub>min</sub>	Edge Distances	= c <sub>ac</sub> on all sides	Edge Distances = c <sub>min</sub> on one side and c <sub>ac</sub> on three sides		
	(in.)	(in.)	()	(in.)	Uncracked	Cracked	Uncracked	Cracked	
1/2	6%	8%	8%	7	7,605	6,720	6,565	5,745	
5/8	87/8	12	12	10	12,105	8,930	10,980	7,775	
3/4	11%	15%	15%	73/4	17,920	15,995	11,705	10,240	

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = 1.4$ . The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.

# **Torq-Cut**<sup>™</sup> Design Information — Concrete



# Torq-Cut<sup>™</sup> Allowable Tension Loads in Normal-Weight Concrete (f'<sub>C</sub> = 2,500 psi) — Wind Load







					Allowable Tension Load (lb.)							
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)		tances = all sides		s = c <sub>min</sub> on one on three sides				
()	(,	()	(,	(,	Uncracked	Cracked	Uncracked	Cracked				
1/2	6%	85%	8%	7	6,385	5,645	5,515	4,825				
5/8	87/8	12	12	10	10,170	7,500	9,220	6,530				
3/4	11%	15%	15%	73/4	15,055	13,435	9,830	8,600				

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \%.6 = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.

# Torq-Cut<sup>™</sup> Allowable Tension Loads in Normal-Weight Concrete (f'<sub>C</sub> = 2,500 psi) — Seismic Load







		100	0.441	Minimum	Allowable Tension Load (lb.)											
Anchor Dia.	Nominal Embed. Depth	Min. Concrete Thickness	Critical Edge Distance	Edge Distance	Edae	Distances	= c <sub>ac</sub> on all s	ides	Edge Distances = $c_{min}$ on one side and $c_{ac}$ on three sides							
(in.)	(in.)	h <sub>min</sub>	h <sub>min</sub> (in.)	c <sub>ac</sub> (in.)		SDC	A-B <sup>4</sup>	SDC (	C-F <sup>5,6</sup>	SDC	A-B <sup>4</sup>	SDC C-F <sup>5,6</sup>				
		(111.)	(,	(111.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked				
1/2	6%	8%	85%	7	7,450	6,585	5,645	4,940	6,435	5,630	4,825	4,220				
5/8	87/8	12	12	10	11,865	8,750	9,265	9,265 6,565		7,620	8,070	5,715				
3/4	11%	15%	15%	73/4	17,565	15,675	13,435	11,760	11,470	10,035	8,605	7,530				

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \frac{1}{2}$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 5. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 6. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Strong-Bolt® 2 Wedge Anchor



A wedge-type expansion anchor designed for optimal performance in cracked and uncracked concrete as well as uncracked masonry. The Strong-Bolt® 2 is available in carbon steel (1/4" through 1" diameter), Type 304 (1/4" diameter only) and Type 316 stainless steel (1/4" through 3/4" diameter).

#### **Features**

- Code listed under IBC/IRC for cracked and uncracked concrete per ICC-ES ESR-3037
- Code listed under IBC/IRC for masonry per IAPMO UES ER-240
- · Qualified for static and seismic loading conditions (seismic design categories A through F)
- · Suitable for horizontal, vertical and overhead applications
- Qualified for minimum concrete thickness of 31/4", and lightweight concrete-over-metal deck thickness of 21/2" and 31/4"
- · Standard (ANSI) fractional sizes: fits standard fixtures and installs with common drill bit and tool sizes

Codes: ICC-ES ESR-3037 (concrete); IAPMO UES ER-240 (carbon steel in CMU); City of L.A. RR25891 (concrete), RR25936 (carbon steel in CMU); Florida FL-15731.2; FL-16230.4; UL File Ex3605; FM 3043342 and 3047639; Mulitiple DOT listings; meets the requirements of Federal Specifications A-A-1923A, Type 4

Material: Carbon-steel stud with special alloy clip; stainlesssteel stud with stainless-steel clip

Coating: Zinc plated





#### Material Specifications

Anchor Body	Nut	Washer	Clip
Carbon Steel <sup>1</sup>	Carbon Steel, ASTM A 563, Grade A	Carbon Steel ASTM F844	Carbon Steel ASTM A 568
Type 304	Type 304	Type 304	Type 316
Stainless Steel	Stainless Steel	Stainless Steel	Stainless Steel
Type 316	Type 316	Type 316	Type 316
Stainless Steel	Stainless Steel	Stainless Steel	Stainless Steel

<sup>1.</sup> Zinc meets ASTM B 633, Class SC 1 (Fe / Zn 5), Type III.

#### Strong-Bolt® 2 Anchor Installation Data

Strong-Bolt 2 Dia. (in.)	1/4	3/8	1/2	5%	3/4	7∕8	1
Drill Bit Size (in.)	1/4	3/8	1/2	5/8	3/4	7/8	1
Min. Fixture Hole (in.)	5/16	7/16	9/16	11/16	7/8	1	1 1/8
Wrench Size (in.)	7/16	9/16	3/4	15/16	11/8	1 5/16	1 ½

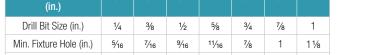




**Head Stamp** 

The head is stamped with the length identification letter, bracketed top and bottom by horizontal lines.





Length Identification Head Marks on Strong-Bolt® 2 Wedge Anchors (corresponds to length of anchor – inches)

Mark	Units	Α	В	С	D	Е	F	G	Н	1	J	K	L	M	N	0	Р	Q	R	S	Т	U	V	W	Х	Υ	Z
From	in.	1 ½	2	21/2	3	3½	4	41/2	5	5½	6	6½	7	7 ½	8	8½	9	9½	10	11	12	13	14	15	16	17	18
Up To But Not Including	in.	2	21/2	3	3½	4	41/2	5	5½	6	61/2	7	71/2	8	81/2	9	91/2	10	11	12	13	14	15	16	17	18	19

Strong-T

# Strong-Bolt® 2 Wedge Anchor

# Strong-Bolt® 2 Anchor Product Data

Size	Carbon Steel	Type 304	Type 316	Drill Bit Dia.	Thread Length	Qua	intity
(in.)	Model No.	Stainless Steel Model No.	Stainless Steel Model No.	(in.)	(in.)	Box	Carton
1⁄4 x 13⁄4	STB2-25134	STB2-251344SS	STB2-251346SS	1/4	<sup>15</sup> / <sub>16</sub>	100	500
1/4 x 21/4	STB2-25214	STB2-252144SS	STB2-252146SS	1/4	17/16	100	500
1/4 x 31/4	STB2-25314	STB2-253144SS	STB2-253146SS	1/4	27/16	100	500
3/8 x 23/4	STB2-37234	_	STB2-372346SS	3/8	1 5/16	50	250
3⁄8 x 3	STB2-37300	_	STB2-373006SS	3/8	1 %16	50	250
% x 3½	STB2-37312	_	STB2-373126SS	3/8	21/16	50	250
% x 3¾	STB2-37334	_	STB2-373346SS	3/8	25/16	50	250
3⁄8 x 5	STB2-37500	_	STB2-375006SS	3/8	3%16	50	200
3/8 x 7	STB2-37700	_	STB2-377006SS	3/8	5%16	50	200
½ x 3¾	STB2-50334	_	STB2-503346SS	1/2	21/16	25	125
½ x 4¾	STB2-50434	_	STB2-504346SS	1/2	31/16	25	100
½ x 5½	STB2-50512	_	STB2-505126SS	1/2	313/16	25	100
½ x 7	STB2-50700	_	STB2-507006SS	1/2	55/16	25	100
½ x 8½	STB2-50812	_	STB2-508126SS	1/2	6	25	50
½ x 10	STB2-50100	_	STB2-501006SS	1/2	6	25	50
% x 4½	STB2-62412	_	STB2-624126SS	5/8	27/16	20	80
% x 5	STB2-62500	_	STB2-625006SS	5/8	215/16	20	80
5/8 x 6	STB2-62600	_	STB2-626006SS	5/8	315/16	20	80
5/8 x 7	STB2-62700	_	STB2-627006SS	5/8	4 15/16	20	80
5⁄8 x 81⁄2	STB2-62812	_	STB2-628126SS	5/8	6	20	40
% x 10	STB2-62100	_	STB2-621006SS	5/8	6	10	20
3/4 x 51/2	STB2-75512	_	STB2-755126SS	3/4	33/16	10	40
3/4 x 61/4	STB2-75614	_	STB2-756146SS	3/4	315/16	10	40
3/4 x 7	STB2-75700	_	STB2-757006SS	3/4	411/16	10	40
3/4 x 81/2	STB2-75812	_	STB2-758126SS	3/4	6	10	20

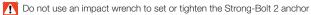
### Installation:

3/4 x 10

1 x 7

1 x 10

1 x 13



STB2-75100

STB2-100700

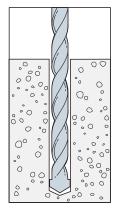
STB2-1001000

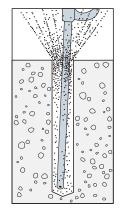
STB2-1001300

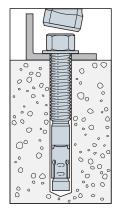


- 1. Drill a hole in the base material using a carbide drill bit the same diameter as the nominal diameter of the anchor to be installed. Drill the hole to the specified minimum hole depth, and blow it clean using compressed air. (Overhead installations need not be blown clean.) Alternatively, drill the hole deep enough to accommodate embedment depth and dust from drilling.
- 2. Assemble the anchor with nut and washer so the top of the nut is flush with the top of the anchor. Place the anchor in the fixture, and drive it into the hole until the washer and nut are tight against the fixture.
- 3. Tighten to the required installation torque.

### Installation Sequence:







3/4

1

6

31/2

31/2

31/2

10

5

5

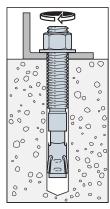
5

20

20

10

10



# SIMPSON Strong-Tie

# Strong-Bolt® 2 Design Information — Concrete

Carbon Steel Strong-Bolt® 2 Installation Information¹

Characteristic	Cumbel	Unito	Nominal Anchor Diameter, d <sub>a</sub> (in.)							(in.)				
Characteristic	Symbol	Units	1/44 3/85			1⁄2 <sup>5</sup> 5⁄8 <sup>5</sup>				3⁄4 <sup>5</sup>			1 <sup>5</sup>	
				Instal	lation Inf	ormation								
Nominal Diameter	da	in.	1/4	3,	⁄8		1/2		5	/8	3	/4		1
Drill Bit Diameter	d	in.	1/4	3,	<b>/</b> 8		1/2		5	/8	3	/4		1
Baseplate Clearance Hole Diameter <sup>2</sup>	$d_{\mathcal{C}}$	in.	5/16	7/	16		9/16		11	/16	7,	/8	1	1/8
Installation Torque	T <sub>inst</sub>	ft-lbf	4	30			60		9	00	1	50	2	30
Nominal Embedment Depth	h <sub>nom</sub>	in.	13⁄4	17/8	27/8	2	3/4	37/8	3%	51/8	41/8	5¾	51/4	93/4
Effective Embedment Depth	h <sub>ef</sub>	in.	1½	1 ½	21/2	2	1/4	3%	23/4	41/2	3%	5	41/2	9
Minimum Hole Depth	h <sub>hole</sub>	in.	17/8	2	3		3	41/8	35/8	5%	43/8	6	51/2	10
Minimum Overall Anchor Length	l <sub>anch</sub>	in.	21/4	23/4	3½	3	3/4	5½	41/2	6	5½	7	7	13
Critical Edge Distance	Cac	in.	2½	61/2	6	61/2	61/2	71/2	7½	9	9	8	18	13½
Minimum Edua Distance	C <sub>min</sub>	in.	13⁄4		3	7	4	4	6	1/2	6	1/2		8
Minimum Edge Distance	for s ≥	in.	_	-	-	_	_	_	-	_		3	-	_
Minimum On a dia a	Smin	in.	21/4	(	3	7 4		4	5			7	8	
Minimum Spacing	for c ≥	in.	_	_	_	_	_	_	_				-	_
Minimum Concrete Thickness	h <sub>min</sub>	in	31/4	31/4	41/2	41/2	5½	6	51/2	77/8	6¾	83/4	9	131⁄2
				A	dditional	Data								
Yield Strength	f <sub>ya</sub>	psi	56,000	92,	000			85,000			70,	000	60,	,000
Tensile Strength	f <sub>uta</sub>	psi	70,000				115,000	)			110	,000	78,000	
Minimum Tensile and Shear Stress Area	A <sub>se</sub>	in.²	0.0318	0.0	514		0.105		0.166		0.2	270	0.4	472
Axial Stiffness in Service Load Range — Cracked and Uncracked Concrete	β	lb./in.	73,700³	34,	820		63,570		91,	370	118	,840	299	),600

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D.
- $\hbox{2. The clearance must comply with applicable code requirements for the connected element.}\\$
- 3. The tabulated value of  $\beta$  for 1/4-inch diameter carbon steel Strong-Bolt 2 anchor is for installations in uncracked concrete only.
- 4. The ¼-inch-diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in this table.
- 5. The %-inch-through 1-inch-diameter (9.5mm through 25.4mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in this table.



**Mechanical** Anchors

Stainless-Steel Strong-Bolt® 2 Installation Information<sup>1</sup>

Characteristic	Cymhol	Mominal Anchor Diameter, d <sub>a</sub> (in.)										
Characteristic	Symbol	Units	1/44	3/	<b>8</b> <sup>5</sup>		1/25		5/6	3 <sup>5</sup>	3,	⁄4 <sup>5</sup>
			Installation Inf	formation								
Nominal Diameter	da	in.	1/4	3,	/8		1/2		5,	8	3,	3/4
Drill Bit Diameter	d	in.	1/4	3,	/8		1/2		5,	<b>8</b>	3	3/4
Baseplate Clearance Hole Diameter <sup>2</sup>	$d_c$	in.	5/16	7/	16		9/16		11/	, 16	7	<b>7</b> /8
Installation Torque	T <sub>inst</sub>	ft-lbf	4	3	0		60		8	80		50
Nominal Embedment Depth	h <sub>nom</sub>	in.	13/4	1 1/8	27/8	2¾	3	7/8	3%	51/8	41/8	53/
Effective Embedment Depth	h <sub>ef</sub>	in.	1½	1 ½	2½	21/4	3	3/8	23/4	41/2	3%	5
Minimum Hole Depth	h <sub>hole</sub>	in.	17/8	2	3	3	4	1/8	35/8	5%	43/8	6
Minimum Overall Anchor Length	$\ell_{anch}$	in.	21/4	23/4	3½	3¾	5	1/2	41/2	6	5½	7
Critical Edge Distance	Cac	in.	2½	61/2	81/2	41/2	-	7	71/2	9	8	8
Misimum Edna Diskaras	C <sub>min</sub>	in.	13/4	(	3	6½	5	4	2	4 (		6
Minimum Edge Distance	for $s \ge$	in.	_	1	0	_	_	8	8	3	_	_
Minimum On sing	S <sub>min</sub>	in.	21/4	3	3	8	5½	4	6	1/4	6	1/2
Minimum Spacing	for $c \ge$	in.	_	1	0		_	8	5	/2	_	_
Minimum Concrete Thickness	h <sub>min</sub>	in.	31/4	31/4	41/2	41/2	(	3	5½	77/8	6¾	83
			Additional	Data								
Yield Strength	f <sub>ya</sub>	psi	96,000	80,	000		92,000		82,0	000	68,	000
Tensile Strength	f <sub>uta</sub>	psi	120,000	100	,000		115,000		108,	000	95,	000
Minimum Tensile and Shear Stress Area	A <sub>se</sub>	in.²	0.0255	0.0	514		0.105		0.166		0.2	270
Axial Stiffness in Service Load Range — Cracked and Uncracked Concrete	β	lb./in.	54,430 <sup>3</sup>	29,	150		54,900		61,2	270	154	,290

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D.
- 2. The clearance must comply with applicable code requirements for the connected element.
- 3. The tabulated value of  $\beta$  for 1/4-inch diameter stainless steel Strong-Bolt 2 anchor is for installtions in uncracked concrete only.
- 4. The ¼-inch-diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in this table.
- 5. The %-inch-through %-inch-diameter (9.5mm through 19.1mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in this table.

0.55

# **Strong-Bolt® 2** Design Information — Concrete



### Ca

Carbon Steel Strong-Bolt® 2 7	Tension S	Streng	jth Design D	ata¹							IBC		LW
Ohovostovistis	Complete	Haita				Nomina	l Anchor I	Diameter	, d <sub>a</sub> (in.)				
Characteristic	Symbol	Units	1/48	3,	/8 <sup>9</sup>	1/	⁄2 <sup>9</sup>	5,	∕8 <sup>9</sup>	3/2	9	1	9
Anchor Category	1, 2 or 3	_				1						7	2
Nominal Embedment Depth	h <sub>nom</sub>	in.	13/4	17/8	21/8	23/4	37/8	3%	51/8	41/8	53/4	51/4	9¾
		S	teel Strength in 1	ension (A	CI 318 Se	ection D.5	i.1)						
Steel Strength in Tension	N <sub>sa</sub>	lb.	2,225	5,6	600	12,	100	19,	070	29,7	700	36,	815
Strength Reduction Factor — Steel Failure <sup>2</sup>	$\phi_{sa}$	_				0.7	75					0.	65
	C	Concrete	Breakout Streng	th in Tens	ion (ACI 3	318 Secti	on D.5.2)	10					
Effective Embedment Depth	h <sub>ef</sub>	in.	1½	1 ½	2½	21/4	3%	23/4	41/2	3%	5	4½	9
Critical Edge Distance	C <sub>ac</sub>	in.	21/2	61/2	6	6½	7½	7½	9	9	8	18	13½
Effectiveness Factor — Uncracked Concrete	K <sub>uncr</sub>	_					24	4					
Effectiveness Factor — Cracked Concrete	k <sub>cr</sub>	_	7					1	7				
Modification Factor	$\psi_{c,N}$	_	7					1.	00				
Strength Reduction Factor — Concrete Breakout Failure <sup>3</sup>	$\phi_{cb}$	_				0.6	35					0.	55
		Pul	lout Strength in 1	Tension (A	CI 318 Se	ection D.5	5.3)10						
Pullout Strength, Cracked Concrete (f' $_c$ =2,500 psi)	N <sub>p,cr</sub>	lb.	7	1,3005	2,7755	N/A <sup>4</sup>	3,7355	N/A <sup>4</sup>	6,9855	N/A <sup>4</sup>	8,5005	7,7005	11,1855
Pullout Strength, Uncracked Concrete (f' <sub>c</sub> =2,500 psi)	N <sub>p,uncr</sub>	lb.	N/A <sup>4</sup>	N/A <sup>4</sup>	3,3405	3,6155	5,2555	N/A <sup>4</sup>	9,0255	7,1155	8,8705	8,3605	9,6905
Strength Reduction Factor — Pullout Failure <sup>6</sup>	$\phi_{ ho}$	_				0.6	35					0.	55
	Te	nsile Str	ength for Seismi	c Applicat	ions (ACI	318 Sect	tion D.3.3	<b>.)</b> <sup>10</sup>					
Tension Strength of Single Anchor for Seismic Loads ( ${\rm f'}_c$ =2,500 psi)	N <sub>p.eq</sub>	lb.	7	1,3005	2,7755	N/A <sup>4</sup>	3,7355	N/A <sup>4</sup>	6,9855	N/A <sup>4</sup>	8,5005	7,7005	11,1855

- The information presented in this table must be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- The tabulated value of  $\phi_{sa}$  applies when the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used. if the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{sa}$  must be determined in accordance with ACI 318 D.4.4. Strong-Bolt 2 anchors are ductile steel elements as defined in ACI 318 D.1.

0.65

- 3. The tabulated value of  $\phi_{cb}$  applies when both the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the  $\phi_{cb}$  factors described in ACI 318 D.4.3 for Condition A are allowed. If the load combinations of ACI 318 Section 9.2 are used and the requirements of ACI 318 Section D.4.3 for Condition A are met, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.3(c). If the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.4(c).
- 4. N/A (not applicable) denotes that pullout resistance does not need to be considered.

 $\phi_{eq}$ 

- 5. The characteristic pullout strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by (f'c/2,500 psi)0-5.
- The tabulated value of  $\phi_p$  or  $\phi_{eq}$  applies when the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. if the load combinations of ACI 318 Appendix C are used, appropriate value of  $\phi$  must be determined in accordance with ACI 318 Section D.4.4(c)
- 7. The 1/4-inch diameter carbon steel Strong-Bolt 2 anchor installation in cracked concrete is beyond the scope of this report.
- The 1/4-inch diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on page 146.
- The %-inch through 1-inch diameter (9.5mm through 25.4mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on page 146.
- 10. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout strength N<sub>D,Cr</sub>, N<sub>D,UnCr</sub> and N<sub>ea</sub> by 0.6. All-lightweight concrete is beyond the scope of this table.

Strength Reduction Factor —

Pullout Failure<sup>6</sup>

<sup>\*</sup> See page 12 for an explanation of the load table icons



**Mechanical** Anchors

### Stainless-Steel Strong-Bolt® 2 Tension Strength Design Data<sup>1</sup>



Characteristic	Cumbal	Units			Nomina	l Anchor	Diameter	; d <sub>a</sub> (in.)			
GHALACTELISTIC	Symbol	UIIILS	1/410	3/	8 <sup>11</sup>	1/:	2 <sup>11</sup>	5,	<b>/</b> 8 <sup>11</sup>	3,	/ <sub>4</sub> <sup>11</sup>
Anchor Category	1, 2 or 3	_					1				
Nominal Embedment Depth	h <sub>nom</sub>	in.	13⁄4	1%	21/8	23/4	37/8	3%	51/8	41/8	5¾
	Steel Stre	ength in T	ension (ACI 318 S	ection D.	5.1)						
Steel Strength in Tension	N <sub>sa</sub>	lb.	3,060	5,1	140	12,	075	17,	930	25,	650
Strength Reduction Factor — Steel Failure <sup>2</sup>	$\phi_{\scriptscriptstyle SA}$	_				0.	75				
Concr	ete Breako	ut Streng	th in Tension (ACI	318 Sect	ion D.5.2	)12					
Effective Embedment Depth	h <sub>ef</sub>	in.	1½	1½	2½	21/4	3%	2¾	41/2	3%	5
Critical Edge Distance	Cac	in.	21/2	6½	81⁄2	41/2	7	71/2	9	8	8
Effectiveness Factor — Uncracked Concrete	k <sub>uncr</sub>					2	4				
Effectiveness Factor — Cracked Concrete	k <sub>cr</sub>	_	9				1	7			
Modification Factor	$\psi_{c,N}$		9				1.0	00			
Strength Reduction Factor — Concrete Breakout Failure <sup>3</sup>	$\phi_{\it cb}$					0.	65				
	Pullout Stre	ength in T	ension (ACI 318 S	ection D.	5.3) <sup>12</sup>						
Pullout Strength, Cracked Concrete (f'c=2,500 psi)	N <sub>p,cr</sub>	lb.	9	1,7206	3,1456	2,5605	4,3055	N/A <sup>4</sup>	6,545 <sup>7</sup>	N/A <sup>4</sup>	8,2305
Pullout Strength, Uncracked Concrete (f'c=2,500 psi)	N <sub>p,uncr</sub>	lb.	1,925 <sup>7</sup>	N/A <sup>4</sup>	4,7706	3,2305	4,4955	N/A <sup>4</sup>	7,6155	7,725 <sup>7</sup>	9,6257
Strength Reduction Factor — Pullout Failure <sup>8</sup>	$\phi_{ ho}$	_				0.	65				
Tensile	Strength fo	r Seismi	Applications (AC	ns (ACI 318 Section D.3.3.) <sup>12</sup>							
Tension Strength of Single Anchor for Seismic Loads (f' $_{\rm c}$ =2,500 psi)	$N_{p.eq}$	lb.	9	1,7206	2,8306	2,5605	4,3055	N/A <sup>4</sup>	6,545 <sup>7</sup>	N/A <sup>4</sup>	8,2305
Strength Reduction Factor — Pullout Failure <sup>8</sup>	$\phi_{eq}$	_				0.	65				

- 1. The information presented in this table must be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The tabulated value of  $\phi_{Sa}$  applies when the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used. if the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{Sa}$  must be determined in accordance with ACI 318 D.4.4. Strong-Bolt 2 anchors are ductile steel elements as defined in ACI 318 D.1.
- 3. The tabulated value of φ<sub>cb</sub> applies when both the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the φ<sub>cb</sub> factors described in ACI 318 D.4.3 for Condition A are allowed. If the load combinations of ACI 318 Section 9.2 are used and the requirements of ACI 318 Section D.4.3 for Condition A are met, the appropriate value of φ<sub>cb</sub> must be determined in accordance with ACI 318 D.4.3(c). If the load combinations of ACI 318 Appendix C are used, the appropriate value of φ<sub>cb</sub> must be determined in accordance with ACI 318 D.4.4(c).
- 4. N/A (not applicable) denotes that pullout resistance does not need to be considered.
- 5. The characteristic pullout strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by (f'<sub>o</sub>/2,500 ps))<sup>0.5</sup>.
- 6. The characteristic pullout strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by (f'<sub>o</sub>/2,500 psi)<sup>0.3</sup>.
- 7. The characteristic pullout strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by (f'<sub>0</sub>/2,500 psi)<sup>0.4</sup>.
- The tabulated value of φ<sub>p</sub> or φ<sub>eq</sub> applies when the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. if the load combinations of ACI 318 Appendix C are used, appropriate value of φ must be determined in accordance with ACI 318 Section D.4.4(c).
- 9. The 1/4-inch diameter stainless steel Strong-Bolt 2 anchor installation in cracked concrete is beyond the scope of this report.
- 10. The ¼-inch diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on page 147.
- 11. The %-inch through %-inch diameter (9.5mm through 19.1mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on page 147.
- 12. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout strength N<sub>p,cr</sub>, N<sub>p,uncr</sub> and N<sub>eq</sub> by 0.6. All-lightweight concrete is beyond the scope of this table.

Carbon Steel Strong-Bolt® 2 Shear Strength Design Data<sup>1</sup>

# **Strong-Bolt® 2** Design Information — Concrete









Chavastavistis	Compleal	Units	Nominal Anchor Diameter, d <sub>a</sub> (in.)											
Characteristic	Symbol	Units	1/46	3,	⁄8 <sup>7</sup>	1/	⁄2 <sup>7</sup>	5/	⁄8 <sup>7</sup>	3/	′4 <sup>7</sup>	1	7	
Anchor Category	1, 2 or 3	_					1					2	2	
Nominal Embedment Depth	h <sub>nom</sub>	in.	13⁄4	17/8	27/8	23/4	37/8	3%	51/8	41/8	5¾	51/4	93/4	
		,	Steel Strength in	Shear (A	CI 318 Se	ection D.6	5.1)							
Steel Strength in Shear	V <sub>sa</sub>	lb.	965	1,8	300	7,2	235	11,	035	14,	480	15,	020	
Strength Reduction Factor — Steel Failure <sup>2</sup>	$\phi_{sa}$	_		'		0.	65			,		0.	60	
		Concret	te Breakout Strei	eakout Strength in Shear (ACI 318 Section D.6.2) <sup>8</sup>										
Outside Diameter	da	in.	0.25	0.25 0.375 0.500 0.625 0.750									00	
Load-Bearing Length of Anchor in Shear	$\ell_e$	in.	1.500	1.500	2.500	2.250	3.375	2.750	4.500	3.375	5.000	4.500	8.000	
Strength Reduction Factor — Concrete Breakout Failure <sup>2</sup>	$\phi_{\it cb}$	_					0.	70						
		Concr	ete Pryout Stren	gth in She	ear (ACI 3	18 Section	on D.6.3)							
Coefficient for Pryout Strength	k <sub>cp</sub>	_	1.0		2.0	1.0				2.0				
Effective Embedment Depth	h <sub>ef</sub>	in.	1½	1½	2½	21/4	3%	23/4	41/2	3%	5	41/2	9	
Strength Reduction Factor — Concrete Pryout Failure <sup>4</sup>	$\phi_{cp}$	_					0.	70						
	Ste	el Strengt	th in Shear for Se	eismic Ap	plications	s(ACI 318	Section	D.3.3.)						
Shear Strength of Single Anchor for Seismic Loads (f'c=2,500 psi)	V <sub>sa.eq</sub>	lb.	5	<b>—</b> ⁵ 1,800 6,510 9,930 11,775									15,020	
Strength Reduction Factor —	феа	_				0.	65					0.	60	

- 1. The information presented in this table must be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The tabulated value of  $\phi_{SB}$  applies when the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. if the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{sa}$  must be determined in accordance with ACI 318 D.4.4. Strong-Bolt 2 anchors are ductile steel elements as defined in ACI 318 D.1.
- 3. The tabulated value of  $\phi_{cb}$  applies when both the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the φ<sub>cb</sub> factors described in ACI 318 D.4.3 for Condition A are allowed. If the load combinations of ACI 318 Section 9.2 are used and the requirements of ACI 318 Section D.4.3 for Condition A are met, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.3(c). If the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.4(c).
- 4. The tabulated value of  $\phi_{CD}$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, appropriate value of  $\phi_{CP}$  must be determined in accordance with ACI 318 Section D.4.4(c).
- 5. The 1/4-inch diameter carbon steel Strong-Bolt 2 anchor installation in cracked concrete is beyond the scope of this report.
- 6. The 1/4-inch diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on page 146.
- 7. The %-inch through 1-inch diameter (9.5mm through 25.4mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on page 146.
- 8. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout by 0.6. All-lightweight concrete is beyond the scope of this table.



## IE





3C	<b>→</b>	LW

### Stainless-Steel Strong-Bolt® 2 Shear Strength Design Data1

Characteristic	Symbol	Units		Nominal Anchor Diameter, d <sub>a</sub> (in.)								
Glidiacteristic	Syllibol	UIIILS	1/46	3,	⁄8 <sup>7</sup>	1/	<sup>′</sup> 2 <sup>7</sup>	5,	⁄8 <sup>7</sup>	3,	⁄4 <sup>7</sup>	
Anchor Category	1, 2 or 3	_					1					
Nominal Embedment Depth	h <sub>nom</sub>	in.	13⁄4	1 1/8	21/8	23/4	37/8	3%	51/8	41/8	5¾	
	Steel Str	ength in	Shear (ACI 318 S	ection D.6	5.1)							
Steel Strength in Shear	V <sub>sa</sub>	lb.	1,605	3,0	085	7,2	245	6,745	10,760	15,	045	
Strength Reduction Factor — Steel Failure <sup>2</sup>	$\phi_{sa}$	_				0.	65					
Con	crete Break	out Stren	gth in Shear (ACI	318 Sect	ion D.6.2)	8						
Outside Diameter	d <sub>a</sub>	in.	0.250 0.375 0.500 0.625 0.750									
Load Bearing Length of Anchor in Shear	$\ell_e$	in.	1.500	1.500	2.500	2.250	3.375	2.750	4.500	3.375	5.000	
Strength Reduction Factor — Concrete Breakout Failure <sup>3</sup>	фcb					0.	70	ı				
Co	ncrete Pryo	ut Streng	th in Shear (ACI	318 Section	on D.6.3)							
Coefficient for Pryout Strength	k <sub>cp</sub>	_	1.0		2.0	1.0			2.0			
Effective Embedment Depth	h <sub>ef</sub>	in.	1½	1 ½	2½	21/4	3%	2¾	41/2	3%	5	
Strength Reduction Factor — Concrete Pryout Failure <sup>4</sup>	$\phi_{cp}$	_				0.	70		,			
Steel Stre	ngth in She	ar for Sei	smic Application	s (ACI 318	Section	D.3.3.)						
Shear Strength of Single Anchor for Seismic Loads (f' <sub>c</sub> =2,500 psi)	V <sub>sa.eq</sub>	lb.	5	3,0	)85	6,1	00	6,745	10,760	13,	620	
Strength Reduction Factor — Steel Failure <sup>2</sup>	$\phi_{sa}$	_				0.	65					

- 1. The information presented in this table must be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The tabulated value of  $\phi_{sa}$  applies when the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) Condition B are met. If the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{sa}$  must be determined in accordance with ACI 318 D.4.3.(c) for Strong-Bolt 2 anchors are ductile steel elements as defined in ACI 318 D.1.
- 3. The tabulated value of  $\phi_{cb}$  applies when both the load combinations of Section 1605.2.1 of the IBC or ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the  $\phi_{cb}$  factors described in ACI 318 D.4.3 for Condition A are allowed. If the load combinations of ACI 318 Section 9.2 are used and the requirements of ACI 318 Section D.4.3 for Condition A are met, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.3(c). If the load combinations of ACI 318 Appendix C are used, the appropriate value of  $\phi_{cb}$  must be determined in accordance with ACI 318 D.4.4(c).
- 4. The tabulated value of  $\phi_{CD}$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of ACI 318 D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, appropriate value of φ<sub>CD</sub> must be determined in accordance with ACI 318 Section D.4.4(c).
- 5. The 1/4-inch diameter stainless-steel Strong-Bolt 2 anchor installation in cracked concrete is beyond the scope of this report.
- 6. The 1/4-inch diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on page 147.
- 7. The %-inch through %-inch diameter (9.5mm through 19.1mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on page 147.
- 8. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout by 0.6. All-lightweight concrete is beyond the scope of this table

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# Strong-Bolt® 2 Design Information — Concrete



Carbon Steel Strong-Bolt® 2 Information for Installation in the Topside of Concrete-Filled Profile Steel Deck Floor and Roof Assemblies<sup>1,2,3,4</sup>



Design Information	Symbol	Units	Nomin	al Anchor Diamet	er (in.)
Design information	Зуппон	Ullits	3,	⁄a	1/2
Nominal Embedment Depth	h <sub>nom</sub>	in.	1	7/8	2¾
Effective Embedment Depth	h <sub>ef</sub>	in.	1	1/2	21/4
Minimum Concrete Thickness <sup>5</sup>	h <sub>min,deck</sub>	in.	21/2	31/4	31/4
Critical Edge Distance	Cac,deck,top	in.	43/4	4	4
Minimum Edge Distance	C <sub>min,deck,top</sub>	in.	43/4	41/2	43/4
Minimum Spacing	S <sub>min,deck,top</sub>	in.	7	61/2	8

For SI: 1 inch = 25.4mm; 1 lbf = 4.45N

- 1. Installation must comply with the table on page 146 and Figure 1 below.
- 2. Design capacity shall be based on calculations according to values in the tables on pages 148 and 150.
- 3. Minimum flute depth (distance from top of flute to bottom of flute) is 11/2 inches.
- 4. Steel deck thickness shall be a minimum 20 gauge.
- 5. Minimum concrete thickness (hmin,deck) refers to concrete thickness above upper flute.

# Stainless-Steel Strong-Bolt® 2 Information for Installation in the Topside of Concrete-Filled Profile Steel Deck Floor and Roof Assemblies<sup>1,2,3,4</sup>



Design Information	Symbol	Units	Nomin	er (in.)	
Design Information	Зуппон	Ullits	3,	8	1/2
Nominal Embedment Depth	h <sub>nom</sub>	in.	13	7/8	2¾
Effective Embedment Depth	h <sub>ef</sub>	in.	1½		21/4
Minimum Concrete Thickness <sup>5</sup>	h <sub>min,deck</sub>	in.	21/2	31/4	31/4
Critical Edge Distance	Cac,deck,top	in.	4¾	4	4
Minimum Edge Distance	C <sub>min,deck,top</sub>	in.	43/4		6
Minimum Spacing	S <sub>min,deck,top</sub>	in.	61	/2	8

For SI: 1 inch = 25.4mm; 1 lbf = 4.45N

- 1. Installation must comply with the table on page 147 and Figure 1 below.
- 2. Design capacity shall be based on calculations according to values in the tables on pages 149 and 151.
- 3. Minimum flute depth (distance from top of flute to bottom of flute) is  $1\frac{1}{2}$  inches.
- 4. Steel deck thickness shall be a minimum 20 gauge.
- 5. Minimum concrete thickness ( $h_{min,deck}$ ) refers to concrete thickness above upper flute.

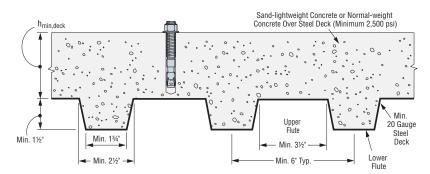
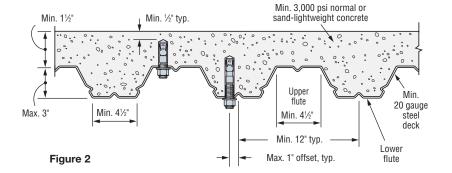


Figure 1



<sup>\*</sup> See page 12 for an explanation of the load table icons.



Carbon Steel Strong-Bolt® 2 Tension and Shear Strength Design Data for the Soffit of Concrete over Profile Steel Deck Floor and Roof Assemblies<sup>1,2,6,8,9</sup>







							Anchor Dia Carbon Ste				
Characteristic	Symbol	Units				_ower Flut		<del>د</del> ا		Uppei	r Flute
			3,	/8	1	/2	5	/8	3/4	3/8	1/2
Nominal Embedment Depth	h <sub>nom</sub>	in.	2	3%	2¾	41/2	3%	5%	41/8	2	23/4
Effective Embedment Depth	h <sub>ef</sub>	in.	15/8	3	21/4	4	23/4	5	3%	15/8	21/4
Installation Torque	T <sub>inst</sub>	ftlbf.	3	0	6	0	9	0	150	30	60
Pullout Strength, concrete on metal deck (cracked)3,4	N <sub>p,deck,cr</sub>	lb.	1,0407	2,615 <sup>7</sup>	2,040 <sup>7</sup>	2,730 <sup>7</sup>	2,615 <sup>7</sup>	4,9907	2,815 <sup>7</sup>	1,340 <sup>7</sup>	3,785 <sup>7</sup>
Pullout Strength, concrete on metal deck (uncracked) <sup>3,4</sup>	N <sub>p,deck,uncr</sub>	lb.	1,765 <sup>7</sup>	3,150 <sup>7</sup>	2,580 <sup>7</sup>	3,8407	3,6857	6,565 <sup>7</sup>	3,8007	2,275 <sup>7</sup>	4,795 <sup>7</sup>
Pullout Strength, concrete on metal deck (seismic) <sup>3,4</sup>	N <sub>p,deck,eq</sub>	lb.	1,040 <sup>7</sup>	2,615 <sup>7</sup>	2,040 <sup>7</sup>	2,730 <sup>7</sup>	2,615 <sup>7</sup>	4,990 <sup>7</sup>	2,815 <sup>7</sup>	1,340 <sup>7</sup>	3,785 <sup>7</sup>
Steel Strength in Shear, concrete on metal deck <sup>5</sup>	V <sub>sa,deck</sub>	lb.	1,595	3,490	2,135	4,580	2,640	7,000	4,535	3,545	5,920
Steel Strength in Shear, concrete on metal deck (seismic) <sup>5</sup>	V <sub>sa,deck,eq</sub>	lb.	1,595	3,490	1,920	4,120	2,375	6,300	3,690	3,545	5,330

- 1. The information presented in this table must be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. Profile steel deck must comply with the configuration in Figure 2 on the previous page, and have a minimum base-steel thickness of 0.035 inch [20 gauge]. Steel must comply with ASTM A 653/A 653M SS Grade 33 with minimum yield strength of 33,000 psi. Concrete compressive strength shall be 3.000 psi minimum.
- 3. For anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies, calculation of the concrete breakout strength may be omitted.
- 4. In accordance with ACI 318 Section D.5.3.2, the nominal pullout strength in cracked concrete for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and rood assemblies N<sub>p,deck,cr</sub> shall be substituted for N<sub>p,cr.</sub> Where analysis indicates no cracking at service
- loads, the normal pullout strength in uncracked concrete  $N_{p,deck,uncr}$  shall be substituted for  $N_{p,uncr}$ . For seismic loads,  $N_{p,deck,eq}$  shall be substituted for  $N_p$
- 5. In accordance with ACI 318 Section D.6.1.2(c), the shear strength for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and rood assemblies  $V_{sa}$ , deck shall be substituted for  $V_{sa}$ . For seismic loads,  $V_{sa,deck,eq}$  shall be substituted for  $V_{sa}$ .
- 6. The minimum anchor spacing along the flute must be the greater of 3.0h<sub>ef</sub> or 1.5 times the flute width.
- 7. The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by (f'<sub>c</sub> / 3,000 psi)<sup>0.5</sup>.
- 8. Concrete shall be normal-weight or structural sand-lightweight concrete having a minimum specified compressive strength, f'c, of 3,000 psi.
- 9. Minimum distance to edge of panel is 2hef.

### Stainless Steel Strong-Bolt® 2 Tension and Shear Strength Design Data for the Soffit of Concrete over Profile Steel Deck Floor and Roof Assemblies 1,2,6,10,11









**Mechanical** Anchors

Characteristic	Symbol	Units				Lower Flut	е			Uppeı	r Flute
			3,	/8	1	/2	5,	/8	3/4	3/8	1/2
Nominal Embedment Depth	h <sub>nom</sub>	in.	2	3%	23/4	41/2	3%	5%	41/8	2	2¾
Effective Embedment Depth	h <sub>ef</sub>	in.	15/8	3	21/4	4	23/4	5	3%	1 5/8	21/4
Installation Torque	T <sub>inst</sub>	ftlbf.	3	0	6	60	8	0	150	30	60
Pullout Strength, concrete on metal deck (cracked) <sup>3</sup>	N <sub>p,deck,cr</sub>	lb.	1,2308	2,6058	1,990 <sup>7</sup>	2,550 <sup>7</sup>	1,750 <sup>9</sup>	4,0209	3,0307	1,5508	2,055 <sup>7</sup>
Pullout Strength, concrete on metal deck (uncracked) <sup>3</sup>	N <sub>p,deck,uncr</sub>	lb.	1,5808	3,9508	2,475 <sup>7</sup>	2,660 <sup>7</sup>	2,470 <sup>7</sup>	5,000 <sup>7</sup>	4,275 <sup>9</sup>	1,9908	2,560 <sup>7</sup>
Pullout Strength, concrete on metal deck (seismic) <sup>5</sup>	N <sub>p,deck,eq</sub>	lb.	1,2308	2,3458	1,990 <sup>7</sup>	2,550 <sup>7</sup>	1,750 <sup>9</sup>	4,0209	3,0307	1,5508	2,055 <sup>7</sup>
Steel Strength in Shear, concrete on metal deck4	V <sub>sa,deck</sub>	lb.	2,285	3,085	3,430	4,680	3,235	5,430	6,135	3,085	5,955
Steel Strength in Shear, concrete on metal deck (seismic) <sup>5</sup>	V <sub>sa,deck,eq</sub>	lb.	2,285	3,085	2,400	3,275	3,235	5,430	5,520	3,085	4,170

- 1. The information presented in this table must be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. Profile steel deck must comply with the configuration in Figure 2 on the previous page, and have a minimum base-steel thickness of 0.035 inch [20 gauge]. Steel must comply with ASTM A 653/A 653M SS Grade 33 with minimum yield strength of 33,000 psi. Concrete compressive strength shall be 3.000 psi minimum.
- 3. For anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies, calculation of the concrete breakout strength may be omitted.
- 4. In accordance with ACI 318 Section D.5.3.2, the nominal pullout strength in cracked concrete for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and rood assemblies N<sub>p,deck,cr</sub> shall be substituted for  $N_{p,cr}$ . Where analysis indicates no cracking at service loads, the normal pullout strength in uncracked concrete  $N_{D,deck,uncr}$  shall be substituted for  $N_{p,uncr}$ . For seismic loads,  $N_{p,deck,eq}$  shall be substituted for  $N_p$ .
- 5. In accordance with ACI 318 Section D.6.1.2(c), the shear strength for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and rood assemblies  $V_{\rm sa}$ , deck shall be substituted for  $V_{sa}$ . For seismic loads,  $V_{sa, deck, eq}$  shall be substituted for  $V_{sa}$ .
- 6. The minimum anchor spacing along the flute must be the greater of 3.0hef or 1.5 times the flute width.
- The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by (f'c / 3,000 psi)0.5
- 8. The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by (f'c / 3,000 psi)0.3
- The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by (f'c / 3,000 psi)0.4
- 10. Concrete shall be normal-weight or structural sand-lightweight concrete having a minimum specified compressive strength, f'c, of 3,000 psi.
- 11. Minimum distance to edge of panel is 2hef-

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Carbon Steel Strong-Bolt® 2 Tension Design Strengths in Normal-Weight Concrete (f'<sub>c</sub> = 2,500 psi)







	Min	Concrete   Edge	Minimum	Tension Design Strength (lb.)										
Anchor Dia.	Nominal Embed. Depth		ncrete Edge ckness Distance	Edge Distance	Edge	Distances	= c <sub>ac</sub> on all s	ides	Edge Distances = $c_{min}$ on one side and $c_{ac}$ on three sides					
(in.)	(in.)	h <sub>min</sub> (in.)	c <sub>ac</sub> (in.)	c <sub>min</sub> (in.)	SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>		SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>			
		(111.)	(111.)	(111.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked		
1/4	13/4	31/4	21/2	13/4	1,435	_	_	_	1,070	_	_	_		
3/8	17/8	31/4	61/2	6	1,435	845	1,075	635	1,325	845	990	635		
9/8	21/8	41/2	6	6	2,170	1,805	1,630	1,355	2,170	1,805	1,630	1,355		
1/2	23/4	41/2	7	7	2,350	1,865	1,760	1,400	2,350	1,865	1,760	1,400		
1/2	37/8	6	71/2	4	3,415	2,430	2,560	1,820	2,740	2,430	2,055	1,820		
5/8	3%	5½	71/2	61/2	3,555	2,520	2,665	1,890	3,085	2,520	2,310	1,890		
9/8	51/8	77/8	9	61/2	5,865	4,480	4,400	3,360	5,420	4,480	4,065	3,360		
3/4	41/8	6¾	9	61/2	4,625	3,425	3,470	2,570	3,495	3,425	2,620	2,570		
94	53/4	83⁄4	8	61/2	5,765	5,525	4,325	4,145	5,765	5,525	4,325	4,145		
-1	51/4	9	18	8	4,600	4,235	3,450	3,175	2,800	4,235	2,100	3,175		
	9¾	131/2	13½	8	5,330	6,150	3,995	4,615	5,330	6,150	3,995	4,615		

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor, φ, is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# Carbon Steel Strong-Bolt® 2 Allowable Tension Loads in Normal-Weight Concrete ( $f'_c = 2,500 \text{ psi}$ ) — Static Load







		, ,		Minimum Edge		Allowable Ten	sion Load (lb.)	
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)	Euge Dis	tances = all sides	Edge Distances = and c <sub>ac</sub> on	
		, ,			Uncracked	Cracked	Uncracked	Cracked
1/4	13/4	31/4	21/2	13/4	1,025	_	765	_
3/-	17/8	31/4	61/2	6	1,025	605	945	605
3/8	27/8	41/2	6	6	1,550	1,290	1,550	1,290
1/	2¾	41/2	7	7	1,680	1,330	1,680	1,330
1/2	37/8	6	71/2	4	2,440	1,735	1,955	1,735
5/8	3%	51/2	71/2	61/2	2,540	1,800	2,205	1,800
78	51/8	77/8	9	61/2	4,190	3,200	3,870	3,200
3/4	41/8	6¾	9	61/2	3,305	2,445	2,495	2,445
94	5¾	83⁄4	8	61/2	4,120	3,945	4,120	3,945
1	51/4	9	18	8	3,285	3,025	2,000	3,025
	9¾	131/2	13½	8	3,805	4,395	3,805	4,395

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.

<sup>2.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>3.</sup> Interpolation between embedment depths is not permitted.



Carbon Steel Strong-Bolt® 2 Allowable Tension Loads in Normal-Weight Concrete (f'c = 2,500 psi) — Wind Load







	Naminal			Minimum Edgo	Allowable Tension Load (lb.)					
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)		tances = all sides	Edge Distances = $c_{min}$ on o side and $c_{ac}$ on three side			
					Uncracked	Cracked	Uncracked	Cracked		
1/4	13/4	31/4	21/2	13⁄4	860	_	640	_		
3/8	17/8	31/4	61/2	6	860	505	795	505		
98	27/8	41/2	6	6	1,300	1,085	1,300	1,085		
1/2	23/4	41/2	7	7	1,410	1,120	1,410	1,120		
72	37/8	6	71/2	4	2,050	1,460	1,645	1,460		
5/8	3%	51/2	71/2	61/2	2,135	1,510	1,850	1,510		
98	51/8	77/8	9	61/2	3,520	2,690	3,250	2,690		
3/4	41/8	6¾	9	61/2	2,775	2,055	2,095	2,055		
94	53/4	8¾	8	61/2	3,460	3,315	3,460	3,315		
1	51/4	9	18	8	2,760	2,540	1,680	2,540		
	93⁄4	131/2	13½	8	3,200	3,690	3,200	3,690		

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \%.6 = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.

- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.

# Carbon Steel Strong-Bolt® 2 Allowable Tension Loads in Normal-Weight Concrete (f' $_{\rm C}=2,\!500$ psi) — Seismic Load







							Al	lowable Ten	ision Load (It	o.)		
Anchor Dia.	Nominal Embed. Depth	Min. Concrete Thickness h <sub>min</sub>	Distance c <sub>ac</sub>	Distance c <sub>min</sub>						Distances = and c <sub>ac</sub> on	= c <sub>min</sub> on one side three sides	
(in.)	(in.)	(in.)	(in.)	(in.)	SDC A-B <sup>4</sup>		SDC (	C-F <sup>5,6</sup>	SDC A-B <sup>4</sup>		SDC C-F <sup>5,6</sup>	
					Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
1/4	13/4	31/4	21/2	13⁄4	1,005	_	_	_	750	_	_	_
2/	1 1/8	31/4	61/2	6	1,005	590	755	445	930	590	695	445
3/8	27/8	41/2	6	6	1,520	1,265	1,140	950	1,520	1,265	1,140	950
1/	2¾	41/2	7	7	1,645	1,305	1,230	980	1,645	1,305	1,230	980
1/2	37/8	6	71/2	4	2,390	1,700	1,790	1,275	1,920	1,700	1,440	1,275
E/	3%	51/2	71/2	61/2	2,490	1,765	1,865	1,325	2,160	1,765	1,615	1,325
5/8	51/8	77/8	9	61/2	4,105	3,135	3,080	2,350	3,795	3,135	2,845	2,350
2/	41/8	6¾	9	61/2	3,240	2,400	2,430	1,800	2,445	2,400	1,835	1,800
3/4	5¾	83⁄4	8	61/2	4,035	3,870	3,030	2,900	4,035	3,870	3,030	2,900
1	51/4	9	18	8	3,220	2,965	2,415	2,225	1,960	2,965	1,470	2,225
	93/4	131/2	131/2	8	3,730	4,305	2,795	3,230	3,730	4,305	2,795	3,230

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \%.7 = 1.43$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>2.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>3.</sup> Interpolation between embedment depths is not permitted.

<sup>4.</sup> The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.

<sup>5.</sup> When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.

<sup>6.</sup> Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

<sup>\*</sup> See page 12 for an explanation of the load table icons.









Stainless Steel Strong-Bolt® 2 Tension Design Strengths in Normal-Weight Concrete (f'c = 2,500 psi)

		Nominal Embed. Thickness Depth (in.)		ļ ļ	Tension Design Strength (lb.)									
Anchor Dia.	Nominal Embed. Denth		Distance c <sub>ac</sub>	Minimum Edge Distance c <sub>min</sub>	Edge	Distances	= c <sub>ac</sub> on all s	sides	Edge Distances = $c_{min}$ on one side and $c_{ac}$ on three sides					
(in.)			(in.)	(in.)	SDC	A-B <sup>5</sup>	SDC (	C-F <sup>6,7</sup>	SDC	A-B <sup>5</sup>	SDC (	C-F <sup>6,7</sup>		
					Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked		
1/4	13/4	31/4	21/2	1 3/4	1,250	_	_	_	1,070	_	_	_		
3/8	17/8	31/4	61/2	6	1,435	1,015	1,075	760	1,325	1,015	990	760		
9/8	21/8	41/2	81/2	6	3,085	2,045	2,090	1,380	2,175	2,045	1,630	1,380		
1/	23/4	41/2	61/2	61/2	2,100	1,665	1,575	1,250	2,100	1,665	1,575	1,250		
1/2	37/8	6	7	5	2,920	2,800	2,190	2,100	2,920	2,800	2,190	2,100		
5/8	3%	51/2	71/2	4	3,555	2,520	2,665	1,890	1,910	2,460	1,430	1,845		
7/8	51/8	77/8	9	4	4,950	4,255	3,710	3,190	3,905	3,685	2,925	2,765		
3/4	41/8	6¾	8	6	4,835	3,425	3,625	2,570	3,625	3,425	2,720	2,570		
9/4	5¾	8¾	8	6	6,255	5,350	4,690	4,010	6,255	5,225	4,690	3,920		

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor, φ, is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# Stainless Steel Strong-Bolt® 2 Allowable Tension Loads in Normal-Weight Concrete (f' $_{\rm C}=2,\!500$ psi) — Static Load



				Minimum Edge		Allowable Ten	sion Load (lb.)		
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete h Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)	Edge Distances :	= c <sub>ac</sub> on all sides	Edge Distances = c <sub>min</sub> on one side and c <sub>ac</sub> on three sides		
					Uncracked	Cracked	Uncracked	Cracked	
1/4	13/4	31/4	21/2	13⁄4	895	_	765	_	
3/	17/8	31/4	61/2	6	1,025	725	945	725	
3/8	27/8	41/2	81/2	6	2,205	1,460	1,555	1,460	
1/	23/4	41/2	61/2	61/2	1,500	1,190	1,500	1,190	
1/2	37/8	6	7	5	2,085	2,000	2,085	2,000	
5/	3%	51/2	71/2	4	2,540	1,800	1,365	1,755	
5/8	51/8	77/8	9	4	3,535	3,040	2,790	2,630	
3/	41/8	6¾	8	6	3,455	2,445	2,590	2,445	
3/4	53/4	8¾	8	6	4,470	3,820	4,470	3,730	

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.

- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.



Stainless Steel Strong-Bolt® 2 Allowable Tension Loads in Normal-Weight Concrete (f'  $_{\rm C}$  = 2,500 psi) — Wind Load







					Allowable Tension Load (lb.)					
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub>	Edge Dis c <sub>ac</sub> on a	tances = all sides	Edge Distances = $c_{min}$ on one side and $C_{ac}$ on three sides			
				(in.)	Uncracked	Cracked	Uncracked	Cracked		
1/4	13/4	31⁄4	21/2	13⁄4	750	_	640	_		
3/8	1 1/8	31/4	61/2	6	860	610	795	610		
98	27/8	41/2	81/2	6	1,850	1,225	1,305	1,225		
1/2	23/4	41/2	61/2	61/2	1,260	1,000	1,260	1,000		
7/2	37/8	6	7	5	1,750	1,680	1,750	1,680		
5/8	3%	51/2	71/2	4	2,135	1,510	1,145	1,475		
9/8	51/8	77/8	9	4	2,970	2,555	2,345	2,210		
3/4	41/8	6¾	8	6	2,900	2,055	2,175	2,055		
9/4	5¾	83/4	8	6	3,755	3,210	3,755	3,135		

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \%.6 = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.

# Stainless Steel Strong-Bolt® 2 Allowable Tension Loads in Normal-Weight Concrete







**Mechanical** Anchors

$(T_{C} = 2,$	$r_c = 2,500$ psi) — Seismic Load												
		Min.	Critical	Minimum			All	owable Ter	ision Load (I	b.)			
Anchor Dia.	Nominal Embed. Depth	Concrete Thickness	Edge Distance	Edge Distance	Edge Fdge Dista		e Distances = c <sub>ac</sub> on all sides				c <sub>min</sub> on on three sides	c <sub>min</sub> on one side hree sides	
(in.)	(in.)	h <sub>min</sub>	C <sub>ac</sub>	Cmin	SDC A-B <sup>4</sup>		SDC C-F <sup>5,6</sup>		SDC A-B⁴		SDC C-F <sup>5,6</sup>		
		(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	
1/4	13/4	31/4	21/2	13/4	875	_	_	_	750	_	_	_	
3/8	17/8	31/4	61/2	6	1,005	710	755	530	930	710	695	530	
9/8	21/8	41/2	81/2	6	2,160	1,430	1,465	965	1,525	1,430	1,140	965	
1/	23/4	41/2	61/2	61/2	1,470	1,165	1,105	875	1,470	1,165	1,105	875	
1/2	3%	6	7	5	2,045	1,960	1,535	1,470	2,045	1,960	1,535	1,470	
5/	3%	5½	71/2	4	2,490	1,765	1,865	1,325	1,335	1,720	1,000	1,290	
5/8	51/8	77/8	9	4	3,465	2,980	2,595	2,235	2,735	2,580	2,050	1,935	
3/	41/8	6¾	8	6	3,385	2,400	2,540	1,800	2,540	2,400	1,905	1,800	
3/4	5¾	83/4	8	6	4,380	3,745	3,285	2,805	4,380	3,660	3,285	2,745	

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = %.7 = 1.43. The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.

<sup>2.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>3.</sup> Interpolation between embedment depths is not permitted.

<sup>2.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>3.</sup> Interpolation between embedment depths is not permitted.

<sup>4.</sup> The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.

<sup>5.</sup> When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.

<sup>6.</sup> Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Carbon Steel Strong-Bolt® 2 Tension Design Strengths in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000$  psi)

IRC		*
IDU	287 282	, U

	Nominal Embed. Depth (in.)	Minimum End Distance c <sub>min</sub> (in.)			T	ension Desig	n Strength (lb	.)					
Anchor Dia.				Lowe	r Flute			Upper Flute					
(in.)			SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>		SDC A-B <sup>5</sup>		SDC C-F <sup>6,7</sup>				
()			Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked			
3/8	2	31/4	1,145	675	860	505	1,480	870	1,110	655			
78	3%	6	2,050	1,700	1,535	1,275	_	_	_	_			
1/2	23/4	41/2	1,675	1,325	1,260	995	3,115	2,460	2,340	1,845			
1/2	41/2	8	2,495	1,775	1,870	1,330	_	_	_	_			
5/8	3%	5½	2,395	1,700	1,795	1,275	_	_	_	_			
9/8	5%	10	4,265	3,245	3,200	2,435	_	_	_	_			
3/4	41/8	63/4	2,470	1,830	1,855	1,370	_	_	_	_			

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 8. Installation must comply with Figure 2 on page 152.

Carbon Steel Strong-Bolt® 2 Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f' $_{\rm c}=3,\!000$  psi) — Static Load



	Nominal	Minimum End		Allowable Ten	sion Load (lb.)		
Anchor Dia. (in.)	Embed. Depth	Distance c <sub>min</sub>	Lower	Flute	Upper Flute		
(,	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	
3/	2	31/4	820	480	1,055	620	
3/8	3%	6	1,465	1,215	_	_	
1/2	23/4	41/2	1,195	945	2,225	1,755	
72	41/2	8	1,780	1,270	_	_	
5/	3%	51/2	1,710	1,215	_	_	
5/8	5%	10	3,045	2,320	_	_	
3/4	41/8	6¾	1,765	1,305	_	_	

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Installation must comply with Figure 2 on page 152.



Carbon Steel Strong-Bolt® 2 Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000~psi$ ) — Wind Load



Anchor	Nominal Embed.	Minimum End		Allowable Ten	sion Load (lb.)	
Dia.	Depth	Distance c <sub>min</sub>	Lower	Flute	Upper	Flute
(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked
3/8	2	31/4	685	405	890	520
78	3%	6	1,230	1,020	_	_
1/2	23/4	41/2	1,005	795	1,870	1,475
7/2	41/2	8	1,495	1,065	_	_
5/	3%	5½	1,435	1,020	_	_
5/8	5%	10	2,560	1,945	_	_
3/4	41/8	6¾	1,480	1,100	_	_

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.67. The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Installation must comply with Figure 2 on page 152.

Carbon Steel Strong-Bolt® 2 Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f'<sub>c</sub> = 3,000 psi) — Seismic Load



D 0 0 1 1 1		0, C - 0,C	500 poi)	COIOITIIC	2 0000					
	Nominal	Minimum			A	llowable Ten	sion Load (lb	)		
Anchor	Embed.	End Distance		Lowe	r Flute			Uppe	r Flute	
Dia. (in.)	Depth	C <sub>min</sub>	SDC	A-B <sup>4</sup>	SDC	C-F <sup>5,6</sup>	SDC	A-B <sup>4</sup>	SDC	C-F <sup>5,6</sup>
()	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
3/8	2	31/4	800	475	600	355	1,035	610	775	460
9/8	3%	6	1,435	1,190	1,075	895	_	_	_	_
1/	23/4	41/2	1,175	930	880	695	2,180	1,720	1,640	1,290
1/2	41/2	8	1,745	1,245	1,310	930	_	_	_	_
5/8	3%	51/2	1,675	1,190	1,255	895	_	_	_	_
7/8	5%	10	2,985	2,270	2,240	1,705	_	_	_	_
3/4	41/8	6¾	1,730	1,280	1,300	960	_	_	_	_

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \frac{1}{2}$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 5. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 6. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 7. Installation must comply with Figure 2 on page 152.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Stainless Steel Strong-Bolt® 2 Tension Design Strengths in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f'<sub>c</sub> = 3,000 psi)

IBC	1	*
-----	---	---

	Nominal				Te	nsion Desig	n Strength (lb	).)		
Anchor	Embed.	Minimum End		Lowe	r Flute			Uppe	r Flute	
Dia. (in.)	Depth	Distance c <sub>min</sub> (in.)	SDC	A-B <sup>5</sup>	SDC (	C-F <sup>6,7</sup>	SDC	A-B <sup>5</sup>	SDC (	C-F <sup>6,7</sup>
(,	(in.)		Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
3/8	2	31/4	1,025	800	770	600	1,295	1,010	970	755
78	3%	6	2,570	1,695	1,735	1,145	_	_	_	_
1/2	23/4	41/2	1,610	1,295	1,205	970	1,665	1,335	1,250	1,000
1/2	41/2	8	1,730	1,660	1,295	1,245	_	_	_	_
5/8	3%	51/2	1,605	1,135	1,205	855	_	_	_	_
7/8	5%	10	3,250	2,615	2,440	1,960	_	_	_	_
3/4	41/8	63/4	2,780	1,970	2,085	1,475		_	_	_

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 8. Installation must comply with Figure 2 on page 152.

Stainless Steel Strong-Bolt® 2 Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f'  $_{\rm C}$  = 3,000 psi) — Static Load



	Nominal	Minimum End		Allowable Ten	sion Load (lb.)	Upper Flute  ced Cracked  720  —
Anchor Dia. (in.)	Embed. Depth	Distance c <sub>min</sub>	Lowe	r Flute	Upper	Flute
(111.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked
3/8	2	31/4	730	570	925	720
98	3%	6	1,835	1,210	_	_
1/2	23/4	41/2	1,150	925	1,190	955
72	41/2	8	1,235	1,185	_	_
5/8	3%	51/2	1,145	810	_	_
78	5%	10	2,320	1,870	_	_
3/4	41/8	6¾	1,985	1,405	_	_

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Installation must comply with Figure 2 on page 152.



Stainless Steel Strong-Bolt® 2 Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000 \text{ psi}$ ) — Wind Load

	Nominal	Minimum End	Allowable Tension Load (lb.)							
Anchor Dia. (in.)	Embed. Depth	Distance c <sub>min</sub>	Lower	Flute	Upper	Flute				
()	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked				
3/8	2	31/4	615	480	775	605				
9/8	3%	6	1,540	1,015	_	_				
1/2	23/4	41/2	965	775	1,000	800				
72	41/2	8	1,040	995	_	_				
5/	3%	5½	965	680	_	_				
5/8	5%	10	1,950	1,570	_	_				
3/4	41/8	6¾	1,670	1,180	_	_				

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.67. The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Installation must comply with Figure 2 on page 152.

Stainless Steel Strong-Bolt® 2 Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f'<sub>c</sub> = 3,000 psi) — Seismic Load



0100. 20	, , , , , , , , ,	1) 00110111	0,000	JO 0.7	, o.	. 0. 0.				
	Nominal	Minimum			A	llowable Ter	ision Load (lb	.)		
Anchor	Embed.	End		Lowe	r Flute			Uppe	r Flute	
Dia. (in.)	Depth	Distance	SDC	A-B <sup>4</sup>	SDC	C-F <sup>5,6</sup>	SDC	A-B <sup>4</sup>	SDC	C-F <sup>5,6</sup>
(,	(in.)	c <sub>min</sub> (in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
3/	2	31/4	720	560	540	420	905	705	680	530
3/8	3%	6	1,800	1,185	1,215	800	_	_	_	_
1/	23/4	41/2	1,125	905	845	680	1,165	935	875	700
1/2	41/2	8	1,210	1,160	905	870	_	_	_	_
5/	3%	5½	1,125	795	845	600	_	_	_	_
5/8	5%	10	2,275	1,830	1,710	1,370	_	_	_	_
3/4	41/8	6¾	1,945	1,380	1,460	1,035	_	_	_	_

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \frac{1}{2}$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 5. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 6. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 7. Installation must comply with Figure 2 on page 152.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Strong-Bolt® 2 Design Information — Masonry



Carbon-Steel Strong-Bolt® 2 Tension and Shear Loads in 8" Lightweight, Medium-Weight and Normal-Weight Grout-Filled CMU

IBC	**************************************	*

Size	Drill Bit Dia.	Min. Embed.	Install. Torque	Critical Edge	Critical End	Critical	Tensio	n Load	Shear	r Load
in. (mm)	(in.)	Depth in. (mm)	ftlb. (N-m)	Dist. in. (mm)	Dist. in. (mm)	Spacing in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
			Anchor	Installed in the	Face of the CN	/IU Wall (See Fi	gure 1)			
<b>1/4</b> (6.4)	1/4	<b>13/4</b> (45)	<b>4</b> (5.4)	<b>12</b> (305)	<b>12</b> (305)	<b>8</b> (203)	<b>1,150</b> (5.1)	<b>230</b> (1.0)	<b>1,500</b> (6.7)	<b>300</b> (1.3)
<b>3/8</b> (9.5)	3/8	<b>25/8</b> (67)	<b>20</b> (27.1)	<b>12</b> (305)	<b>12</b> (305)	<b>8</b> (203)	<b>2,185</b> (9.7)	<b>435</b> (1.9)	<b>3,875</b> (17.2)	<b>775</b> (3.4)
1/2 (12.7)	1/2	<b>3½</b> (89)	<b>35</b> (47.5)	<b>12</b> (305)	<b>12</b> (305)	<b>8</b> (203)	<b>2,645</b> (11.8)	<b>530</b> (2.4)	<b>5,055</b> (22.5)	<b>1,010</b> (4.5)
<b>5%</b> (15.9)	5/8	<b>4</b> 3/8 (111)	<b>55</b> (74.6)	<b>20</b> (508)	<b>20</b> (508)	<b>8</b> (203)	<b>4,460</b> (19.8)	<b>890</b> (4.0)	<b>8,815</b> (39.2)	<b>1,765</b> (7.9)
<b>3/4</b> (19.1)	3/4	<b>5</b> ½ (133)	<b>100</b> (135.6)	<b>20</b> (508)	<b>20</b> (508)	<b>8</b> (203)	<b>5,240</b> (23.3)	<b>1,050</b> (4.7)	<b>12,450</b> (55.4)	<b>2,490</b> (11.1)

- The tabulated allowable loads are based on a safety factor of 5.0 for installation under the IBC and IRC.
- 2. Listed loads may be applied to installations on the face of the CMU wall at least  $1\,\%$  inch away from headjoints.
- 3. Values for 8-inch-wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry,  $t^i_{m}$ , at 28 days is 1,500 psi.
- 4. Embedment depth is measured from the outside face of the concrete masonry unit.
- 5. Tension and shear loads may be combined using the parabolic interaction equation ( $n = \frac{5}{3}$ ).
- 6. Refer to allowable load adjustment factors for edge distance and spacing on page 163.
- 7. Allowable loads may be increased 331/4% for short-term loading due to wind forces or seismic forces where permitted by code.

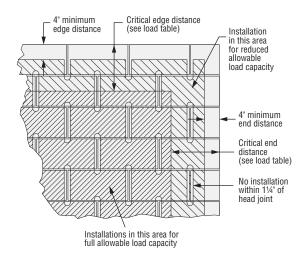


Figure 1

# Carbon-Steel Strong-Bolt® 2 Tension and Shear Loads in 8" Lightweight, Medium-weight and Normal-Weight Grout-Filled CMU

Size	Drill Bit	Min. Embed.	Install.	Min. Edge.	Critical End		Tensio	n Load	Shear Load I	Perp. To Edge		Parallel To ge
in. (mm)	Dia. in.	Depth. in. (mm)	Torque ftlb. (N-m)	Dist. in. (mm)	Dist. in. (mm)	Spacing in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
			А	nchor Install	ed in Cell Ope	ening or Web	(Top of Wall)	(See Figure	2)			
1/2 (12.7)	1/2	<b>3½</b> (89)	<b>35</b> (47.5)	<b>13/4</b> (45)	<b>12</b> (305)	<b>8</b> (203)	<b>2,080</b> (9.3)	<b>415</b> (1.8)	<b>1,165</b> (5.2)	<b>235</b> (1.0)	<b>3,360</b> (14.9)	<b>670</b> (3.0)
<b>5%</b> (15.9)	5/8	<b>4</b> % (111)	<b>55</b> (74.6)	<b>13/4</b> (45)	<b>12</b> (305)	<b>8</b> (203)	<b>3,200</b> (14.2)	<b>640</b> (2.8)	<b>1,370</b> (6.1)	<b>275</b> (1.2)	<b>3,845</b> (17.1)	<b>770</b> (3.4)

- The tabulated allowable loads are based on a safety factor of 5.0 for installation under the IBC and IRC.
- 2. Values for 8-inch-wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry,  $f'_{m}$ , at 28 days is 1,500 psi.
- 3. Tension and shear loads may be combined using the parabolic interaction equation (n =  $\frac{5}{2}$ ).
- 4. Refer to allowable load adjustment factors for edge distance and spacing on page 163.
- 5. Allowable loads may be increased 331/4% for short-term loading due to wind forces or seismic forces where permitted by code.

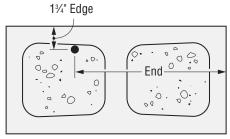


Figure 2

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Strong-Bolt® 2 Design Information — Masonry



Carbon-Steel Strong-Bolt® 2 Allowable Load Adjustment Factors for Face-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance and Spacing, Tension and Shear Loads

### How to use these charts:

- 1. The following tables are for reduced edge distance and spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- Locate the edge distance (c<sub>act</sub>) or spacing (s<sub>act</sub>) at which the anchor is to be installed.
- 5. The load adjustment factor (f  $_{\!c}$  or  $f_{\!s}\!)$  is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load adjustment factor.
- 7. Reduction factors for multiple edges or spacings are multiplied together.

### Edge or End Distance Tension (f<sub>c</sub>)

	Dia.	1/4	3/8	1/2	5/8	3/4
c <sub>act</sub> (in.)	Ε	13/4	25/8	31/2	43/8	51/4
Cact	c <sub>cr</sub>	12	12	12	20	20
(111.)	Cmin	2	4	4	4	4
	f <sub>cmin</sub>	1.00	1.00	1.00	1.00	0.97
2		1.00				
4		1.00	1.00	1.00	1.00	0.97
6		1.00	1.00	1.00	1.00	0.97
8		1.00	1.00	1.00	1.00	0.98
10		1.00	1.00	1.00	1.00	0.98
12		1.00	1.00	1.00	1.00	0.99
14					1.00	0.99
16					1.00	0.99
18					1.00	1.00
20					1.00	1.00

### Edge or End Distance Shear (f<sub>c</sub>)

_490 \		Diotai		- ( ()		
	Dia.	1/4	3/8	1/2	5/8	3/4
	Ε	13/4	25/8	31/2	43/8	51/4
c <sub>act</sub> (in.)	Ccr	12	12	12	20	20
(111.)	C <sub>min</sub>	2	4	4	4	4
	f <sub>cmin</sub>	0.88	0.71	0.60	0.36	0.28
2		0.88				
4		0.90	0.71	0.60	0.36	0.28
6		0.93	0.78	0.70	0.44	0.37
8		0.95	0.86	0.80	0.52	0.46
10		0.98	0.93	0.90	0.60	0.55
12		1.00	1.00	1.00	0.68	0.64
14					0.76	0.73
16					0.84	0.82
18					0.92	0.91
20					1.00	1.00

### Spacing Tension (f<sub>s</sub>)

	Dia.	1/4	3/8	1/2	5/8	3/4	IB
	Ε	13/4	25/8	31/2	43/8	51/4	
s <sub>act</sub> (in.)	Scr	8	8	8	8	8	1
(III.)	Smin	4	4	4	4	4	837
	f <sub>smin</sub>	1.00	1.00	0.93	0.86	0.80	<u></u>
4		1.00	1.00	0.93	0.86	0.80	
6		1.00	1.00	0.97	0.93	0.90	6
8		1.00	1.00	1.00	1.00	1.00	Ų. Į́⊷

### Spacing Shear (f<sub>s</sub>)

	Dia.	1/4	3/8	1/2	5/8	3/4	
	Ε	13/4	25/8	31/2	43/8	51/4	
Sact	Scr	8	8	8	8	8	
(in.)	Smin	4	4	4	4	4	
	f <sub>smin</sub>	1.00	1.00	1.00	1.00	1.00	
4		1.00	1.00	1.00	1.00	1.00	
6		1.00	1.00	1.00	1.00	1.00	
8		1.00	1.00	1.00	1.00	1.00	



Load Adjustment Factors for Carbon-Steel Strong-Bolt® 2 Wedge Anchors in Top-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance and Spacing, Tension and Shear Loads

# End Distance

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

ensio	n (f <sub>c</sub> )			
	Dia.	1/2	5/8	IBC
_	Ε	31/2	43/8	IDU
s <sub>act</sub> (in.)	c <sub>cr</sub>	12	12	<b>1</b>
(111.)	C <sub>min</sub>	4	4	20 22
	f <sub>cmin</sub>	1.00	1.00	(FF)
4		1.00	1.00	
6		1.00	1.00	
8		1.00	1.00	( )
10		1.00	1.00	
12		1.00	1.00	

### End Distance Shear Perpendicular to Edge (f<sub>c</sub>)

Perper	ndicula	ır to Ec	lge (f <sub>c</sub> )	
	Dia.	1/2	5/8	IRC *
	Ε	31/2	43/8	IDO
c <sub>act</sub> (in.)	c <sub>cr</sub>	12	12	<b>→</b>
(111.)	C <sub>min</sub>	4	4	87 B3
	f <sub>cmin</sub>	0.90	0.83	(22)2
4		0.90	0.83	
6		0.93	0.87	
8		0.95	0.92	<b>—</b>
10		0.98	0.96	
12		1.00	1.00	

# End Distance

### Shear Parallel to Edge (f<sub>c</sub>)

Oricai	i aranc	I LO LC	ige (ic)	
	Dia.	1/2	5/8	IRC
_	Ε	31/2	43/8	ibu
c <sub>act</sub> (in.)	C <sub>cr</sub>	12	12	<b>→</b>
(111.)	C <sub>min</sub>	4	4	27 EX
	f <sub>cmin</sub>	0.53	0.50	(F)
4		0.53	0.50	
6		0.65	0.63	
8		0.77	0.75	
10		0.88	0.88	400,000
12		1.00	1.00	

### Spacing Tension (f.

Spacir	ng Tens	sion († <sub>s.</sub>	)	
	Dia.	1/2	5/8	IRC *
	Ε	31/2	43/8	IDO
s <sub>act</sub> (in.)	Scr	<i>s</i> <sub>cr</sub> 8		1
(111.)	Smin	4	4	20 20
	f <sub>cmin</sub>	0.93	0.86	(== =
4		0.93	0.86	H
6		0.97	0.93	<u> </u>
8		1.00	1.00	/ <del>←→</del> \

### Spacing Shear Perpendicular or Parallel to Edge

	Dia.	1/2	5/8	IRC *
_	Ε	31/2	43/8	IDU
s <sub>act</sub> (in.)	Scr	8	8	
()	Smin	4	4	W/ 100
	f <sub>cmin</sub>	1.00	1.00	
4		1.00	1.00	
6		1.00	1.00	n_n
8		1.00	1.00	/ <del>←→</del> \

For footnotes, please see page 200.

# Wedge-All® Wedge Anchor

SIMPSON StrongTie

A non-bottom-bearing, wedge-style expansion anchor for use in solid concrete or grout-filled masonry. The Wedge-All® wedge anchor is available in carbon steel with zinc or mechanically galvanized coating, as well as Types 303/304 and Type 316 stainless steel. Threaded studs are set by tightening the nut to the specified torque. The Wedge-All is code listed for grout-filled masonry applications.

### **Features**

- Code-listed under IBC/IRC for grout-filled CMU per ICC-ES FSR-1396
- One-piece, wrap-around clip ensures uniform holding capacity
- Threaded end is chamfered for ease of starting nut
- · Available in a wide range of diameters and lengths

**Codes:** ICC-ES ESR-1396 (CMU); Florida FL-15730.7; FM 3017082 and 3131136; UL File Ex3605; Mulitiple DOT listings; meets the requirements of Federal Specification A-A-1923A, Type 4

Material: Carbon or stainless steel (Types 303/304; Type 316)

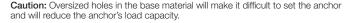
**Coating:** Carbon steel anchors are available zinc plated or mechanically galvanized





### Installation

Do not use an impact wrench to set or tighten anchors.



- 1. Drill a hole in base material using a carbide drill bit the same diameter as the nominal diameter of the anchor to be installed. Drill the hole to the specified embedment depth, and blow it clean using compressed air. (Overhead installations need not be blown clean.) Alternatively, drill the hole deep enough to accommodate the embedment depth and the dust from drilling.
- Assemble the anchor with nut and washer so the top of the nut is flush with the top of the anchor. Place the anchor in the fixture, and drive it into the hole until the washer and nut are tight against the fixture.
- 3. Tighten to the required installation torque.

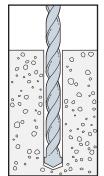


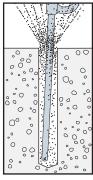


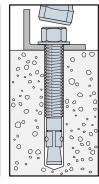
**Head Stamp**The head is stamped with the length identification letter.

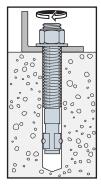
### Wedge-All® Anchor

### Installation Sequence









Wedge-All® Anchor Installation Data

Wedge-All Dia. (in.)	1/4	3/8	1/2	5%	3/4	7/8	1	1¼
Drill Bit Size (in.)	1/4	3/8	1/2	5/8	3/4	7/8	1	1 1/4
Min. Fixture Hole (in.)	5/16	7/16	9/16	11/16	7/8	1	11/8	1%
Wrench Size (in.)	7/16	9/16	3/4	15/16	11/8	15/16	1 ½	1 1//8

Length Identification Head Marks on Wedge-All® Anchors (corresponds to length of anchor — inches).

Mark	Α	В	С	D	Е	F	G	Н		J	K	L	M	N	0	Р	Q	R	S	T	U	٧	W	Х	Υ	Z
From	1½	2	2½	3	3½	4	41/2	5	5½	6	6½	7	7½	8	8½	9	91/2	10	11	12	13	14	15	16	17	18
Up To But Not Including	2	2½	3	3½	4	41/2	5	5½	6	6½	7	7½	8	81/2	9	9½	10	11	12	13	14	15	16	17	18	19

# SIMPSON Strong-Tie

Wedge-All® Anchor Product Data — Carbon Steel: Zinc Plated and Mechanically Galvanized

	Zinc Plated	Mechanically	Drill Bit	Thread	Qua	intity
Size (in.)	Model No.	Galvanized Model No.	Dia. (in.)	Length (in.)	Вох	Carton
1/4 x 1 3/4	_	WA25134MG		15/16	100	500
1/4 x 21/4	_	WA25214MG	1/4	1 7/16	100	500
1/4 x 3 1/4	_	WA25314MG		27/16	100	500
3/8 X 2 1/4	WA37214	WA37214MG		11/8	50	250
3/8 x 23/4	WA37234	WA37234MG		1 5/8	50	250
3% x 3	WA37300	WA37300MG		1 1/8	50	250
3/8 x 3 1/2	WA37312	WA37312MG	3/8	21/2	50	250
3/8 x 33/4	WA37334	WA37334MG		2%	50	250
3% x 5	WA37500	WA37500MG		37/8	50	200
3/8 x 7	WA37700	WA37700MG		5%	50	200
½ x 2¾	WA50234	WA50234MG		1 5/16	25	125
½ x 3¾	WA50334	WA50334MG		25/16	25	125
½ x 41/ <sub>4</sub>	WA50414	WA50414MG		213/16	25	100
½ x 5½	WA50512	WA50512MG	1/	41/16	25	100
½ x 7	WA50700	WA50700MG	1/2	4%16	25	100
½ x 8½	WA50812	WA50812MG		6	25	50
½ x 10	WA50100	WA50100MG		6	25	50
½ x 12	WA50120	WA50120MG		6	25	50
5% x 3½	WA62312	WA62312MG		1%	20	80
5/8 x 4 1/2	WA62412	WA62412MG		27/8	20	80
5⁄8 x 5	WA62500	WA62500MG		3%	20	80
5⁄8 x 6	WA62600	WA62600MG	E/	43/8	20	80
5/8 x 7	WA62700	WA62700MG	5/8	5%	20	80
5/8 X 8 1/2	WA62812	WA62812MG		6	20	40
5⁄8 x 10	WA62100	WA62100MG		6	10	20
% x 12	WA62120	WA62120MG		6	10	20
3/4 X 4 1/4	WA75414	WA75414MG		2%	10	40
3/4 x 43/4	WA75434	WA75434MG		27/8	10	40
3/4 x 51/2	WA75512	WA75512MG		3%	10	40
3/4 x 6 1/4	WA75614	WA75614MG	3/	43/8	10	40
3/4 x 7	WA75700	WA75700MG	3/4	51/8	10	40
3/4 x 8 1/2	WA75812	WA75812MG		6	10	20
3/4 x 10	WA75100	WA75100MG		6	10	20
3/4 x 12	WA75120	WA75120MG		6	5	10
7⁄8 x 6	WA87600	WA87600MG		21/8	5	20
7/8 x 8	WA87800	WA87800MG	7/	21/8	5	10
7⁄8 x 10	WA87100	WA87100MG	7/8	21/8	5	10
7⁄8 x 12	WA87120	WA87120MG		21/8	5	10
1 x 6	WA16000	WA16000MG		21/4	5	20
1 x 9	WA19000	WA19000MG	1	21/4	5	10
1 x 12	WA11200	WA11200MG		21/4	5	10
11/4 x 9	WA12590	_	11/	23/4	5	10
11/4 x 12	WA12512	_	11/4	23/4	5	10

<sup>1.</sup> The published length is the overall length of the anchor. Allow one anchor diameter for the nut and washer thickness plus the fixture thickness when selecting the minimum length.

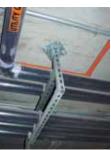
### Material Specifications

Carbon Steel — Zinc Plated											
Component Materials											
Anchor Body	Nut	Washer	Clip								
Material Meets minimum 70,000 psi tensile strength	Carbon Steel ASTM A 563, Grade A	Carbon Steel	Carbon Steel								



### Application:

Interior environment, low level of corrosion resistance. See page 316 for more corrosion information.



### Material Specifications

Carbon Steel - Mechanically Galvanized <sup>1</sup>											
Component Materials											
Anchor Body	Nut	Washer	Clip								
Material Meets minimum 70,000 psi tensile strength	Carbon Steel ASTM A 563, Grade A	Carbon Steel	Carbon Steel								

1. Mechanical Galvanizing meets ASTM B695, Class 55, Type 1.



### Application:

Exterior unpolluted environment, medium level of corrosion resistance. Well suited to humid environments. See page 316 for more corrosion information.

# Wedge-All® Wedge Anchor



### Wedge-All® Anchor Product Data - Stainless Steel

veage-Ai	1 7 (1101101 1 10	Juuci Dala - C	rtaii iiooo t	01001		
Size (in.)	Type 303/304 Stainless	Type 316 Stainless	Drill Bit Dia.	Thread Length	Qua	antity
	Model No. <sup>2</sup>	Model No.	(in.)	(in.)	Box	Carton
3/8 X 2 1/4	WA37214 <b>4SS</b>	WA37214 <b>6SS</b>		11/8	50	250
3/8 x 23/4	WA37234 <b>4SS</b>	WA37234 <b>6SS</b>		15/8	50	250
3⁄8 X 3	WA37300 <b>4SS</b>	WA37300 <b>6SS</b>		17/8	50	250
3/8 x 3 1/2	WA37312 <b>4SS</b>	WA37312 <b>6SS</b>	3/8	21/2	50	250
3/8 x 33/4	WA37334 <b>4SS</b>	WA37334 <b>6SS</b>		2%	50	250
3⁄8 x 5	WA37500 <b>4SS</b>	WA37500 <b>6SS</b>		37/8	50	200
3/8 x 7	WA37700 <b>4SS</b>	WA37700 <b>6SS</b>		57/8	50	200
½ x 2¾	WA50234 <b>4SS</b>	WA50234 <b>6SS</b>		1 5/16	25	125
½ x 3¾	WA50334 <b>4SS</b>	WA50334 <b>6SS</b>		25/16	25	125
½ x 4¼	WA50414 <b>4SS</b>	WA50414 <b>6SS</b>		213/16	25	100
½ x 5½	WA50512 <b>4SS</b>	WA50512 <b>6SS</b>	1/	41/16	25	100
½ x 7	WA50700 <b>4SS</b>	WA50700 <b>6SS</b>	1/2	5%16	25	100
½ x 8½	WA50812 <b>4SS</b>	WA50812 <b>6SS</b>		2	25	50
½ x 10	WA50100 <b>SS</b>	WA50100 <b>3SS</b>		2	25	50
½ x 12	WA50120 <b>SS</b>	WA50120 <b>3SS</b>		2	25	50
% x 3½	WA62312 <b>4SS</b>	WA62312 <b>6SS</b>		17/8	20	80
5/8 x 4 1/2	WA62412 <b>4SS</b>	WA62412 <b>6SS</b>		27/8	20	80
% x 5	WA62500 <b>4SS</b>	WA62500 <b>6SS</b>		3%	20	80
% x 6	WA62600 <b>4SS</b>	WA62600 <b>6SS</b>		43/8	20	80
5⁄8 x 7	WA62700 <b>4SS</b>	WA62700 <b>6SS</b>	5/8	5%	20	80
% x 8½	WA62812 <b>4SS</b>	WA62812 <b>6SS</b>		2	20	40
% x 10	WA62100 <b>SS</b>	WA62100 <b>3SS</b>		2	10	20
% x 12	WA62120 <b>SS</b>	WA62120 <b>3SS</b>		2	10	20
3/4 x 4 1/4	WA75414 <b>4SS</b>	WA75414 <b>6SS</b>		23/8	10	40
3/4 x 43/4	WA75434 <b>4SS</b>	WA75434 <b>6SS</b>		27/8	10	40
3/4 x 51/2	WA75512 <b>4SS</b>	WA75512 <b>6SS</b>		35/8	10	40
3/4 x 6 1/4	WA75614 <b>4SS</b>	WA75614 <b>6SS</b>	2/	43/8	10	40
3/4 x 7	WA75700 <b>4SS</b>	WA75700 <b>6SS</b>	3/4	51/8	10	40
3/4 x 8 1/2	WA75812 <b>4SS</b>	WA75812 <b>6SS</b>		21/4	10	20
3/4 x 10	WA75100 <b>SS</b>	WA75100 <b>3SS</b>		21/4	10	20
3/4 x 12	WA75120 <b>SS</b>	WA75120 <b>3SS</b>		21/4	5	10
7⁄8 x 6	WA87600 <b>SS</b>	WA87600 <b>3SS</b>		21/8	5	20
7⁄8 x 8	WA87800 <b>SS</b>	WA87800 <b>3SS</b>	7/	21/8	5	10
7⁄8 x 10	WA87100 <b>SS</b>	WA87100 <b>3SS</b>	7/8	21/8	5	10
7⁄8 x 12	WA87120 <b>SS</b>	_		21/8	5	10
1 x 6	WA16000 <b>SS</b>	WA16000 <b>3SS</b>		21/4	5	20
1 x 9	WA19000 <b>SS</b>	WA19000 <b>3SS</b>	1	21/4	5	10
1 x 12	WA11200 <b>SS</b>	WA11200 <b>3SS</b>		21/4	5	10

- 1. The published length is the overall length of the anchor. Allow one anchor diameter for the nut and washer thickness plus the fixture thickness when selecting a length.
- 2. Anchors with the "SS" suffix in the model number are manufactured from Type-303 stainless steel; the remaining anchors (with the "4SS" suffix) are manufactured from Type 304 stainless steel. Types 303 and 304 stainless steel perform equally well in certain corrosive environments.

### Material Specifications

Type 303/304 Stainless Steel <sup>1</sup>								
Component Materials								
Anchor Body	Nut	Washer	Clip					
Type 303 or 304 Stainless Steel	Type 18-8 Stainless Steel	Type 18-8 Stainless Steel	Type 304 or 316 Stainless Steel					

 Types 303 and 304 stainless steels perform equally well in certain corrosive environments. Larger sizes are manufactured from Type 303.

### Application:

Exterior environment, high level of corrosion resistance. Resistant to organic chemicals, many inorganic chemicals, mild atmospheric pollution and mild marine environments (not in direct contact with salt water). See page 316 for more corrosion information.

### Material Specifications

Type 316 Stainless Steel <sup>1</sup>									
Component Materials									
Anchor Body	Nut	Washer	Clip						
Type 316 Stainless Steel	Type 316 Stainless Steel	Type 316 Stainless Steel	Type 316 Stainless Steel						

<sup>1.</sup> Type-316 stainless steel provides the greatest degree of corrosion resistance offered by Simpson Strong-Tie.

### Application:

Exterior environment, high level of corrosion resistance. Resistant to chlorides, sulfuric acid compounds and direct contact with salt water. See page 316 for more corrosion information.









### Carbon-Steel Wedge-All® Allowable Tension Loads in Normal-Weight Concrete

IBC		1	1
	, ,	12.00	180



	Critical	Tension Load									
Size in.	Embed. Depth in.	Edge Dist.	Dist. Spacing	(13.	f' <sub>c</sub> ≥ 2,000 ps .8 MPa) Conc	i rete	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Concrete	(27	f' <sub>c</sub> ≥ 4,000 ps .6 MPa) Conc	i rete	Install. Torque ftlb.
(mm)	(mm)	in. (mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	(N-m)
1/4	<b>1</b>	<b>2½</b> (64)	<b>1</b> % (41)	<b>680</b> (3.0)	<b>167</b> (0.7)	<b>170</b> (0.8)	<b>205</b> (0.9)	<b>960</b> (4.3)	<b>233</b> (1.0)	<b>240</b> (1.1)	8
(6.4)	<b>21/4</b> (57)	<b>2½</b> (64)	<b>3</b> 1/8 (79)	<b>1,920</b> (8.5)	<b>286</b> (1.3)	<b>480</b> (2.1)	<b>530</b> (2.4)	<b>2,320</b> (10.3)	<b>105</b> (0.5)	<b>580</b> (2.6)	(10.8)
	<b>13/4</b> (44)	<b>3¾</b> (95)	<b>2</b> % (60)	<b>1,560</b> (6.9)	<b>261</b> (1.2)	<b>390</b> (1.7)	<b>555</b> (2.5)	<b>2,880</b> (12.8)	<b>588</b> (2.6)	<b>720</b> (3.2)	
<b>3/8</b> (9.5)	<b>2</b> % (67)	<b>3¾</b> (95)	<b>3</b> % (92)	<b>3,360</b> (14.9)	<b>464</b> (2.1)	<b>840</b> (3.7)	<b>1,100</b> (4.9)	<b>5,440</b> (24.2)	<b>553</b> (2.5)	<b>1,360</b> (6.0)	<b>30</b> (40.7)
	<b>3</b> % (86)	<b>3¾</b> (95)	<b>4¾</b> (121)	<b>3,680</b> (16.4)	<b>585</b> (2.6)	<b>920</b> (4.1)	<b>1,140</b> (5.1)	<b>5,440</b> (24.2)	<b>318</b> (1.4)	<b>1,360</b> (6.0)	
	<b>21/4</b> (57)	<b>5</b> (127)	<b>3</b> 1/8 (79)	<b>3,280</b> (14.6)	<b>871</b> (3.9)	<b>820</b> (3.6)	<b>1,070</b> (4.8)	<b>5,280</b> (23.5)	<b>849</b> (3.8)	<b>1,320</b> (5.9)	
<b>½</b> (12.7)	<b>3</b> % (86)	<b>5</b> (127)	<b>4¾</b> (121)	<b>6,040</b> (26.9)	<b>654</b> (2.9)	<b>1,510</b> (6.7)	<b>1,985</b> (8.8)	<b>9,840</b> (43.8)	<b>1,303</b> (5.8)	<b>2,460</b> (10.9)	<b>60</b> (81.3)
	<b>4½</b> (114)	<b>5</b> (127)	<b>61/4</b> (159)	<b>6,960</b> (31.0)	<b>839</b> (3.7)	<b>1,740</b> (7.7)	<b>2,350</b> (10.5)	<b>11,840</b> (52.7)	<b>2,462</b> (11.0)	<b>2,960</b> (13.2)	
	<b>2¾</b> (70)	<b>61/4</b> (159)	<b>3</b> % (98)	<b>4,520</b> (20.1)	<b>120</b> (0.5)	<b>1,130</b> (5.0)	<b>1,640</b> (7.3)	<b>8,600</b> (38.3)	<b>729</b> (3.2)	<b>2,150</b> (9.6)	
<b>5/8</b> (15.9)	<b>4½</b> (114)	<b>61/4</b> (159)	<b>61/4</b> (159)	<b>8,200</b> (36.5)	<b>612</b> (2.7)	<b>2,050</b> (9.1)	<b>2,990</b> (13.3)	<b>15,720</b> (69.9)	<b>1,224</b> (5.4)	<b>3,930</b> (17.5)	<b>90</b> (122.0)
	<b>5½</b> (140)	<b>61/4</b> (159)	<b>7</b> 3/4 (197)	<b>8,200</b> (36.5)	<b>639</b> (2.8)	<b>2,050</b> (9.1)	<b>2,990</b> (13.3)	<b>15,720</b> (69.9)	<b>1,116</b> (5.0)	<b>3,930</b> (17.5)	
	<b>3</b> % (86)	<b>7½</b> (191)	<b>4¾</b> (121)	<b>6,760</b> (30.1)	<b>1,452</b> (6.5)	<b>1,690</b> (7.5)	<b>2,090</b> (9.3)	<b>9,960</b> (44.3)	<b>1,324</b> (5.9)	<b>2,490</b> (11.1)	
<b>3/4</b> (19.1)	<b>5</b> (127)	<b>7½</b> (191)	<b>7</b> (178)	<b>10,040</b> (44.7)	<b>544</b> (2.4)	<b>2,510</b> (11.2)	<b>3,225</b> (14.3)	<b>15,760</b> (70.1)	<b>1,550</b> (6.9)	<b>3,940</b> (17.5)	<b>150</b> (203.4)
	<b>6¾</b> (171)	<b>7½</b> (191)	<b>9½</b> (241)	<b>10,040</b> (44.7)	<b>1,588</b> (7.1)	<b>2,510</b> (11.2)	<b>3,380</b> (15.0)	<b>17,000</b> (75.6)	<b>1,668</b> (7.4)	<b>4,250</b> (18.9)	
7/8	<b>3</b> 7/8 (98)	<b>8¾</b> (222)	<b>5</b> % (137)	<b>7,480</b> (33.3)	<b>821</b> (3.7)	<b>1,870</b> (8.3)	<b>2,275</b> (10.1)	<b>10,720</b> (47.7)	<b>1,253</b> (5.6)	<b>2,680</b> (11.9)	200
(22.2)	<b>7</b> % (200)	<b>8¾</b> (222)	<b>11</b> (279)	<b>17,040</b> (75.8)	<b>1,566</b> (7.0)	<b>4,260</b> (18.9)	<b>4,670</b> (20.8)	<b>20,320</b> (90.4)	<b>2,401</b> (10.7)	<b>5,080</b> (22.6)	(271.2)
1	<b>4½</b> (114)	<b>10</b> (254)	<b>61⁄4</b> (159)	<b>15,400</b> (68.5)	<b>2,440</b> (10.9)	<b>3,850</b> (17.1)	<b>3,885</b> (17.3)	<b>15,680</b> (69.7)	<b>1,876</b> (8.3)	<b>3,920</b> (17.4)	300
(25.4)	<b>9</b> (229)	<b>10</b> (254)	<b>12</b> % (321)	<b>20,760</b> (92.3)	<b>3,116</b> (13.9)	<b>5,190</b> (23.1)	<b>6,355</b> (28.3)	<b>30,080</b> (133.8)	<b>1,612</b> (7.2)	<b>7,520</b> (33.5)	(406.7)
11/4	<b>5</b> % (143)	<b>12½</b> (318)	<b>7</b> 7/8 (200)	<b>15,160</b> (67.4)	<b>1,346</b> (6.0)	<b>3,790</b> (16.9)	<b>4,990</b> (22.2)	<b>24,760</b> (110.1)	<b>625</b> (2.8)	<b>6,190</b> (27.5)	400
(31.8)	91/2	121/2	131/4	20,160	3,250	5,040	8,635	48,920	1,693	12,230	(542.3)

(22.4)

(38.4)

(217.6)

(7.5)

(54.4)

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>(14.5)</sup> (241) (318) (89.7) (337)1. The allowable loads listed are based on a safety factor of 4.0.

<sup>2.</sup> Refer to allowable load-adjustment factors for edge distance and spacing on pages 172 and 174.

<sup>3.</sup> Drill bit diameter used in base material corresponds to nominal anchor diameter.

<sup>4.</sup> Allowable loads may be linearly interpolated between concrete strengths listed.

<sup>5.</sup> The minimum concrete thickness is 1  $\!\!\!\!/_2$  times the embedment depth.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Carbon-Steel Wedge-All® Allowable Shear Loads in Normal-Weight Concrete

_		_		
	- 1		_	1
			7	
וטפנון				
		200	9.73	

	Embed.	Critical	Critical	Shear Load						
Size in.	Depth in.	Edge Dist.	Spacing in.	(1:	$f'_c \ge 2,000 \text{ psi}$ 3.8 MPa) Concr	i rete	$f'_c \ge 3,000 \text{ psi}$ (20.7 MPa) Concrete	$f'_c \ge 4,000 \text{ psi}$ (27.6 MPa) Concrete	Install. Torque ftlb.	
(mm)	(mm)	in. (mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	(N-m)	
1/4	<b>1 1/8</b> (29)	<b>2½</b> (64)	<b>1</b> % (41)	<b>920</b> (4.1)	<b>47</b> (0.2)	<b>230</b> (1.0)	<b>230</b> (1.0)	<b>230</b> (1.0)	8	
(6.4)	<b>21/4</b> (57)	<b>2½</b> (64)	<b>3</b> 1/8 (79)	_	_	<b>230</b> (1.0)	<b>230</b> (1.0)	<b>230</b> (1.0)	(10.8)	
	<b>13/4</b> (44)	<b>3¾</b> (95)	<b>2</b> % (60)	<b>2,280</b> (10.1)	<b>96</b> (0.4)	<b>570</b> (2.5)	<b>570</b> (2.5)	<b>570</b> (2.5)		
<b>3/8</b> (9.5)	<b>2</b> 5/8 (67)	<b>3¾</b> (95)	<b>3</b> 5/8 (92)	<b>4,220</b> (18.8)	<b>384</b> (1.7)	<b>1,055</b> (4.7)	<b>1,055</b> (4.7)	<b>1,055</b> (4.7)	<b>30</b> (40.7)	
	<b>3</b> % (86)	<b>3¾</b> (95)	<b>4¾</b> (121)	_	_	<b>1,055</b> (4.7)	<b>1,055</b> (4.7)	<b>1,055</b> (4.7)		
	<b>21/4</b> (57)	<b>5</b> (127)	<b>3</b> 1/8 (79)	<b>6,560</b> (29.2)	<b>850</b> (3.8)	<b>1,345</b> (6.0)	<b>1,485</b> (6.6)	<b>1,625</b> (7.2)		
<b>½</b> (12.7)	<b>3</b> % (86)	<b>5</b> (127)	<b>4¾</b> (121)	<b>8,160</b> (36.3)	<b>880</b> (3.9)	<b>1,675</b> (7.5)	<b>1,850</b> (8.2)	<b>2,020</b> (9.0)	<b>60</b> (81.3)	
	<b>4½</b> (114)	<b>5</b> (127)	<b>6</b> ½ (159)	_	_	<b>1,675</b> (7.5)	<b>1,850</b> (8.2)	<b>2,020</b> (9.0)		
	<b>2¾</b> (70)	<b>61⁄4</b> (159)	<b>3</b> 7/8 (98)	<b>8,720</b> (38.8)	<b>1,699</b> (7.6)	<b>1,620</b> (7.2)	<b>1,900</b> (8.5)	<b>2,180</b> (9.7)	<b>90</b> (122.0)	
<b>5%</b> (15.9)	<b>4½</b> (114)	<b>61⁄4</b> (159)	<b>61/4</b> (159)	<b>12,570</b> (55.9)	<b>396</b> (1.8)	<b>2,330</b> (10.4)	<b>2,740</b> (12.2)	<b>3,145</b> (14.0)		
	<b>5½</b> (140)	<b>61/4</b> (159)	<b>7¾</b> (197)	_	_	<b>2,330</b> (10.4)	<b>2,740</b> (12.2)	<b>3,145</b> (14.0)		
	<b>3</b> % (86)	<b>7½</b> (191)	<b>4¾</b> (121)	<b>11,360</b> (50.5)	<b>792</b> (3.5)	<b>2,840</b> (12.6)	<b>2,840</b> (12.6)	<b>2,840</b> (12.6)		
<b>3/4</b> (19.1)	<b>5</b> (127)	<b>7½</b> (191)	<b>7</b> (178)	<b>18,430</b> (82.0)	<b>1,921</b> (8.5)	<b>4,610</b> (20.5)	<b>4,610</b> (20.5)	<b>4,610</b> (20.5)	<b>150</b> (203.4)	
	<b>6¾</b> (171)	<b>7½</b> (191)	<b>9½</b> (241)	_	_	<b>4,610</b> (20.5)	<b>4,610</b> (20.5)	<b>4,610</b> (20.5)		
7/8	<b>3</b> 7/8 (98)	<b>8¾</b> (222)	<b>5</b> % (137)	<b>13,760</b> (61.2)	<b>2,059</b> (9.2)	<b>3,440</b> (15.3)	<b>3,440</b> (15.3)	<b>3,440</b> (15.3)	200	
(22.2)	<b>7</b> % (200)	<b>8¾</b> (222)	<b>11</b> (279)	<b>22,300</b> (99.2)	<b>477</b> (2.1)	<b>5,575</b> (24.8)	<b>5,575</b> (24.8)	<b>5,575</b> (24.8)	(271.2)	
1	<b>4½</b> (114)	<b>10</b> (254)	<b>6</b> ½ (159)	<b>22,519</b> (100.2)	<b>1,156</b> (5.1)	<b>5,730</b> (25.5)	<b>5,730</b> (25.5)	<b>5,730</b> (25.5)	300	
(25.4)	<b>9</b> (229)	<b>10</b> (254)	<b>12</b> % (321)	<b>25,380</b> (112.9)	<b>729</b> (3.2)	<b>6,345</b> (28.2)	<b>6,345</b> (28.2)	<b>6,345</b> (28.2)	(406.7)	
11/4	<b>5</b> % (143)	<b>12½</b> (318)	<b>7</b> <sup>7</sup> / <sub>8</sub> (200)	<b>29,320</b> (130.4)	<b>2,099</b> (9.3)	<b>7,330</b> (32.6)	<b>7,330</b> (32.6)	<b>7,330</b> (32.6)	400	
(31.8)	<b>9½</b> (241)	<b>12½</b> (318)	<b>13</b> 1/ <sub>4</sub> (337)	_	_	<b>7,330</b> (32.6)	<b>7,330</b> (32.6)	<b>7,330</b> (32.6)	(542.3)	

<sup>1.</sup> The allowable loads listed are based on a safety factor of 4.0.

168

<sup>2.</sup> Refer to allowable load-adjustment factors for spacing and edge distance on pages 172, 173 and 175.

<sup>3.</sup> Drill bit diameter used in base material corresponds to nominal anchor diameter.

<sup>4.</sup> Allowable loads may be linearly interpolated between concrete strengths listed.

<sup>5.</sup> The minimum concrete thickness is 1½ times the embedment depth.



Stainless-Steel Wedge-All® Allowable Tension Loads in Normal-Weight Concrete

Cino	Embed.	Critical	Critical	Allo	wable Tension Load lb.	(kN)	Install.	
Size in. (mm)	Depth in. (mm)	Edge Dist. in. (mm)	Spacing in. (mm)	f' <sub>c</sub> ≥ 2,000 psi (13.8 MPa) Concrete	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Concrete	f' <sub>c</sub> ≥ 4,000 psi (27.6 MPa) Concrete	Torque ftlb. (N-m)	
1/4	<b>1</b> 1/8 (29)	<b>2½</b> (64)	<b>1</b> % (41)	<b>155</b> (0.7)	<b>185</b> (0.8)	<b>215</b> (1.0)	8	
(6.4)	<b>21/4</b> (57)	<b>2½</b> (64)	<b>3</b> 1⁄8 (79)	<b>430</b> (1.9)	<b>475</b> (2.1)	<b>520</b> (2.3)	(10.8)	
	<b>1</b> 3/4 (44)	<b>3¾</b> (95)	<b>2</b> % (60)	<b>350</b> (1.6)	<b>500</b> (2.2)	<b>650</b> (2.9)		
3/8 (9.5)	<b>2</b> 5/8 (67)	<b>3¾</b> (95)	<b>3</b> 5⁄8 (92)	<b>755</b> (3.4)	<b>990</b> (4.4)	<b>1,225</b> (5.4)	<b>30</b> (40.7)	
	<b>3</b> % (86)	<b>3¾</b> (95)	<b>43/4</b> (121)	<b>830</b> (3.7)	<b>1,025</b> (4.6)	<b>1,225</b> (5.4)		
	<b>2½</b> (57)	<b>5</b> (127)	<b>3½</b> (79)	<b>740</b> (3.3)	<b>965</b> (4.3)	<b>1,190</b> (5.3)		
<b>½</b> (12.7)	<b>3</b> % (86)	<b>5</b> (127)	<b>4</b> 3⁄ <sub>4</sub> (121)	<b>1,360</b> (6.0)	<b>1,785</b> (7.9)	<b>2,215</b> (9.9)	<b>60</b> (81.3)	
	<b>4½</b> (114)	<b>5</b> (127)	<b>6 ½</b> (159)	<b>1,565</b> (7.0)	<b>2,115</b> (9.4)	<b>2,665</b> (11.9)		
	<b>2¾</b> (70)	<b>6½</b> (159)	<b>3</b> 7/8 (98)	<b>1,015</b> (4.5)	<b>1,475</b> (6.6)	<b>1,935</b> (8.6)	<b>90</b> (122.0)	
<b>5/8</b> (15.9)	<b>4½</b> (114)	<b>61⁄4</b> (159)	<b>6 1/4</b> (159)	<b>1,845</b> (8.2)	<b>2,690</b> (12.0)	<b>3,535</b> (15.7)		
	<b>5½</b> (140)	<b>61⁄4</b> (159)	<b>7</b> 3⁄4 (197)	<b>1,845</b> (8.2)	<b>2,690</b> (12.0)	<b>3,535</b> (15.7)		
	<b>3</b> % (86)	<b>7½</b> (191)	<b>43/4</b> (121)	<b>1,520</b> (6.8)	<b>1,880</b> (8.4)	<b>2,240</b> (10.0)		
<b>3/4</b> (19.1)	<b>5</b> (127)	<b>7½</b> (191)	<b>7</b> (178)	<b>2,260</b> (10.1)	<b>2,905</b> (12.9)	<b>3,545</b> (15.8)	<b>150</b> (203.4)	
	<b>6¾</b> (171)	<b>7½</b> (191)	<b>9½</b> (241)	<b>2,260</b> (10.1)	<b>3,040</b> (13.5)	<b>3,825</b> (17.0)		
7/8	<b>3</b> % (98)	<b>8¾</b> (222)	<b>5</b> % (137)	<b>1,685</b> (7.5)	<b>2,050</b> (9.1)	<b>2,410</b> (10.7)	200	
(22.2)	<b>7</b> % (200)	<b>83/4</b> (222)	<b>11</b> (279)	<b>3,835</b> (17.1)	<b>4,205</b> (18.7)	<b>4,570</b> (20.3)	(271.2)	
1	<b>4½</b> (114)	<b>10</b> (254)	<b>61/4</b> (159)	<b>3,465</b> (15.4)	<b>3,495</b> (15.5)	<b>3,530</b> (15.7)	300	
(25.4)	<b>9</b> (229)	<b>10</b> (254)	<b>12</b> % (321)	<b>4,670</b> (20.8)	<b>5,720</b> (25.4)	<b>6,770</b> (30.1)	(406.7)	
11/4	<b>5</b> % (143)	<b>12½</b> (318)	<b>7</b> % (200)	<b>3,410</b> (15.2)	<b>4,490</b> (20.0)	<b>5,570</b> (24.8)	400	
(31.8)	<b>9½</b> (241)	<b>12½</b> (318)	<b>131/4</b> (337)	<b>4,535</b> (20.2)	<b>7,770</b> (34.6)	<b>11,005</b> (49.0)	(542.3)	

<sup>1.</sup> The allowable loads listed are based on a safety factor of 4.0.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>2.</sup> Refer to allowable load-adjustment factors for edge distance and spacing on pages 172 and 174.

<sup>3.</sup> Drill bit diameter used in base material corresponds to nominal anchor diameter.

<sup>4.</sup> Allowable loads may be linearly interpolated between concrete strengths listed.

<sup>5.</sup> The minimum concrete thickness is 1½ times the embedment depth.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Stainless-Steel Wedge-All® Allowable Shear Loads in Normal-Weight Concrete

IBC	<b>→</b>	*
	Inst	tall.

Q:	Embed.	Critical	Critical		owable Shear Load lb. (	kN)	Install.	
Size in. (mm)	Depth in. (mm)	Edge Dist. in. (mm)	Spacing in. (mm)	f' <sub>c</sub> ≥ 2,000 psi (13.8 MPa) Concrete	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Concrete	f' <sub>c</sub> ≥ 4,000 psi (27.6 MPa) Concrete	Torque ftlb. (N-m)	
1/4	<b>1</b>	<b>2½</b> (64)	<b>1</b> 5⁄8 (41)	<b>265</b> (1.2)	<b>265</b> (1.2)	<b>265</b> (1.2)	8	
(6.4)	<b>21/4</b> (57)	<b>2½</b> (64)	<b>3½</b> (79)	<b>265</b> (1.2)	<b>265</b> (1.2)	<b>265</b> (1.2)	(10.8)	
	<b>13/4</b> (44)	<b>3¾</b> (95)	<b>2</b> 3/8 (60)	<b>655</b> (2.9)	<b>655</b> (2.9)	<b>655</b> (2.9)		
<b>3/8</b> (9.5)	<b>25%</b> (67)	<b>3¾</b> (95)	<b>35/8</b> (92)	<b>1,215</b> (5.4)	<b>1,215</b> (5.4)	<b>1,215</b> (5.4)	<b>30</b> (40.7)	
(2-1)	<b>3</b> % (86)	<b>3¾</b> (95)	<b>4³⁄4</b> (121)	<b>1,215</b> (5.4)	<b>1,215</b> (5.4)	<b>1,215</b> (5.4)		
	<b>2½</b> (57)	<b>5</b> (127)	<b>3½</b> (79)	<b>1,545</b> (6.9)	<b>1,710</b> (7.6)	<b>1,870</b> (8.3)		
1/2 (12.7)	<b>3</b> % (86)	<b>5</b> (127)	<b>4³/</b> 4 (121)	<b>1,925</b> (8.6)	<b>2,130</b> (9.5)	<b>2,325</b> (10.3)	<b>60</b> (81.3)	
	<b>4½</b> (114)	<b>5</b> (127)	<b>6½</b> (159)	<b>1,925</b> (8.6)	<b>2,130</b> (9.5)	<b>2,325</b> (10.3)		
	<b>2¾</b> (70)	<b>6½</b> (159)	<b>37/8</b> (98)	<b>1,865</b> (8.3)	<b>2,185</b> (9.7)	<b>2,505</b> (11.1)	<b>90</b> (122.0)	
<b>5%</b> (15.9)	<b>4½</b> (114)	<b>6½</b> (159)	<b>6½</b> (159)	<b>2,680</b> (11.9)	<b>3,150</b> (14.0)	<b>3,615</b> (16.1)		
	<b>5½</b> (140)	<b>61/4</b> (159)	<b>7</b> <sup>3</sup> ⁄ <sub>4</sub> (197)	<b>2,680</b> (11.9)	<b>3,150</b> (14.0)	<b>3,615</b> (16.1)	(12210)	
	<b>3</b> % (86)	<b>7½</b> (191)	<b>4³⁄4</b> (121)	<b>3,265</b> (14.5)	<b>3,265</b> (14.5)	<b>3,265</b> (14.5)		
<b>3/4</b> (19.1)	<b>5</b> (127)	<b>7½</b> (191)	<b>7</b> (178)	<b>5,300</b> (23.6)	<b>5,300</b> (23.6)	<b>5,300</b> (23.6)	<b>150</b> (203.4)	
	<b>6¾</b> (171)	<b>7½</b> (191)	<b>9½</b> (241)	<b>5,300</b> (23.6)	<b>5,300</b> (23.6)	<b>5,300</b> (23.6)		
7/8	<b>3</b> 7/ <sub>8</sub> (98)	<b>8³/4</b> (222)	<b>5</b> % (137)	<b>3,955</b> (17.6)	<b>3,955</b> (17.6)	<b>3,955</b> (17.6)	200	
(22.2)	<b>7</b> <sup>7</sup> / <sub>8</sub> (200)	<b>8³/4</b> (222)	<b>11</b> (279)	<b>6,410</b> (28.5)	<b>6,410</b> (28.5)	<b>6,410</b> (28.5)	(271.2)	
1	<b>4½</b> (114)	<b>10</b> (254)	<b>6½</b> (159)	<b>6,590</b> (29.3)	<b>6,590</b> (29.3)	<b>6,590</b> (29.3)	300	
(25.4)	<b>9</b> (229)	<b>10</b> (254)	<b>12</b> 5/8 (321)	<b>7,295</b> (32.4)	<b>7,295</b> (32.4)	<b>7,295</b> (32.4)	(406.7)	
11/4	<b>5</b> % (143)	<b>12½</b> (318)	<b>7</b> <sup>7</sup> / <sub>8</sub> (200)	<b>8,430</b> (37.5)	<b>8,430</b> (37.5)	<b>8,430</b> (37.5)	400	
(31.8)	<b>9½</b> (241)	<b>12½</b> (318)	<b>131/4</b> (337)	<b>8,430</b> (37.5)	<b>8,430</b> (37.5)	<b>8,430</b> (37.5)	(542.3)	

<sup>1.</sup> The allowable loads listed are based on a safety factor of 4.0.

<sup>2.</sup> Refer to allowable load-adjustment factors for spacing and edge distance on pages 172, 173 and 175.

<sup>3.</sup> Drill bit diameter used in base material corresponds to nominal anchor diameter.

<sup>4.</sup> Allowable loads may be linearly interpolated between concrete strengths listed.

<sup>5.</sup> The minimum concrete thickness is  $1\frac{1}{2}$  times the embedment depth.

# Strong

# **Wedge-All®** Design Information — Concrete and Masonry

Carbon-Steel Wedge-All® Allowable Tension Loads in Sand-Lightweight Concrete over Metal Deck

IBC	1	*

0:	Embed.	Embed. Critical		Tension Load (Install in Concrete)			I (Install t	Install.		
Size in. (mm)	Depth in.	Depth Dist.	Critical Spacing in.	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Concrete			$f'_c \ge 3$ ,	Torque ftlb. (N-m)		
()	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	(,
1/ <sub>4</sub> (6.4)	<b>1 ½</b> (38)	<b>3</b> % (86)	<b>2¾</b> (70)	_	_	_	<b>1,440</b> (6.4)	<b>167</b> (0.7)	<b>360</b> (1.6)	
1/2 (12.7)	<b>21/4</b> (57)	<b>6¾</b> (171)	<b>4½</b> (105)	<b>3,880</b> (17.3)	<b>228</b> (1.0)	<b>970</b> (4.3)	<b>3,860</b> (17.2)	<b>564</b> (2.5)	<b>965</b> (4.3)	<b>60</b> (81.3)
<b>5%</b> (15.9)	<b>2¾</b> (70)	<b>8</b> % (213)	<b>5</b> (127)	<b>5,920</b> (26.3)	<b>239</b> (1.1)	<b>1,480</b> (6.6)	<b>5,220</b> (23.2)	<b>370</b> (1.6)	<b>1,305</b> (5.8)	<b>90</b> (122.0)
3/ <sub>4</sub> (19.1)	<b>3</b> % (>86)	<b>10</b> (254)	<b>6</b> 1/8 (156)	<b>7,140</b> (31.8)	<b>537</b> (2.4)	<b>1,785</b> (7.9)	<b>6,600</b> (29.4)	<b>903</b> (4.0)	<b>1,650</b> (7.3)	<b>150</b> (203.4)

See notes 1-7 below.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

### Carbon-Steel Wedge-All® Allowable Shear Loads in Sand-Lightweight Concrete over Metal Deck

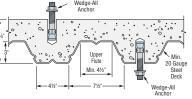
		Critical	a		Shear Load tall in Conci			Shear Load hrough Met		Install.
Size Depth Dist.		Edge	Critical Spacing in.	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Concrete			$f'_c \ge 3$ ,	Torque ftlb. (N-m)		
()	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	(1111)
1/4 (6.4)	<b>1 ½</b> (38)	<b>3</b> % (86)	<b>2¾</b> (70)	_	_	_	<b>1,660</b> (7.4)	<b>627</b> (2.8)	<b>415</b> (1.8)	_
1/2 (12.7)	<b>21/4</b> (57)	<b>6</b> 3⁄4 (171)	<b>4</b> 1/ <sub>8</sub> (105)	<b>5,575</b> (24.8)	<b>377</b> (1.7)	<b>1,395</b> (6.2)	<b>7,260</b> (32.3)	<b>607</b> (2.7)	<b>1,815</b> (8.1)	<b>60</b> (81.3)
<b>5%</b> (15.9)	<b>2¾</b> (70)	<b>8</b> % (213)	<b>5</b> (127)	<b>8,900</b> (39.6)	<b>742</b> (3.3)	<b>2,225</b> (9.9)	<b>8,560</b> (38.1)	<b>114</b> (0.5)	<b>2,140</b> (9.5)	<b>90</b> (122.0)
<b>3/4</b> (19.1)	<b>3</b> % (86)	<b>10</b> (254)	<b>6</b> 1/8 (156)	<b>10,400</b> (46.3)	<b>495</b> (2.2)	<b>2,600</b> (11.6)	<b>11,040</b> (49.1)	<b>321</b> (1.4)	<b>2,760</b> (12.3)	150 (203.4)

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Refer to allowable load-adjustment factors for edge distance on page 176.
- 3. 100% of the allowable load is permitted at critical spacing. Loads at reduced spacing have not been determined.
- 4. Drill bit diameter used in base material corresponds to
- nominal anchor diameter.
- 5. The minimum concrete thickness is 11/2 times the embedment depth.
- 6. Metal deck must be minimum 20 gauge.
- 7. Anchors installed in the bottom flute of the steel deck must have a minimum allowable edge distance of 11/21 from the inclined edge of the bottom flute.

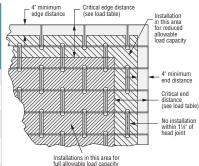
### Carbon-Steel Wedge-All® Allowable Tension and Shear Loads in Grout-Filled CMU

III OI	Jul I III	od Oivi	0							Services Contract	
0:	Embed.	Critical	Critical	Critical	8" Grout	t-Filled CMI	J Allowable	Load Base	ed on CMU S	Strength	Install.
Size in.	Depth	Edge Dist.	End Dist.	Spacing	T	ension Loa	d		Shear Load		Torque
(mm)	in. (mm)	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	ftlb. (N-m)
	Ancho	r Installe	d on the	Face of th	e CMU Wal	l at Least 1	1/4 inch Aw	ay from He	ad Joint (Se	ee Figure)	
<b>3/8</b> (9.5)	<b>25/8</b> (67)	<b>10½</b> (267)	<b>10½</b> (267)	<b>10½</b> (267)	<b>1,700</b> (7.6)	<b>129</b> (0.6)	<b>340</b> (1.5)	<b>3,360</b> (14.9)	<b>223</b> (1.0)	<b>670</b> (3.0)	<b>30</b> (40.7)
<b>½</b> (12.7)	<b>3½</b> (89)	<b>14</b> (356)	<b>14</b> (356)	<b>14</b> (356)	<b>2,120</b> (9.4)	<b>129</b> (0.6)	<b>425</b> (1.9)	<b>5,360</b> (23.8)	<b>617</b> (2.7)	<b>1,070</b> (4.8)	<b>35</b> (47.4)
<b>5/8</b> (15.9)	<b>4</b> % (111)	<b>17½</b> (445)	<b>17½</b> (445)	<b>17½</b> (445)	<b>3,120</b> (13.9)	<b>342</b> (1.5)	<b>625</b> (2.8)	<b>8,180</b> (36.4)	<b>513</b> (2.3)	<b>1,635</b> (7.3)	<b>55</b> (74.5)
<b>3/4</b> (19.1)	<b>5½</b> (133)	<b>21</b> (533)	<b>21</b> (533)	<b>21</b> (533)	<b>4,320</b> (19.2)	<b>248</b> (1.1)	<b>865</b> (3.8)	<b>10,160</b> (45.2)	<b>801</b> (3.6)	<b>2,030</b> (9.0)	<b>120</b> (162.6)

- 1. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.
- 2. Listed loads may be applied to installations on the face of the CMU wall at least 1% inch away from headjoints.
- 3. Values for 8-inch wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry, f'm, at 28 days is 1,500 psi.
- 4. Embedment depth is measured from the outside face of the concrete masonry unit.
- 5. Drill bit diameter used in base material corresponds to nominal anchor diameter.
- 6. Allowable loads may be increased 331/3% for shortterm loading due to wind and seismic forces, where permitted by code.
- 7. Tension and shear loads for the Wedge-All® anchor may be combined using the parabolic interaction equation (n=5/3).
- 8. Refer to allowable load-adjustment factors for edge distance on page 176.



Lightweight Concrete on **Metal Deck** 



Shaded area = Placement for Full and Reduced **Allowable Load Capacity** in Grout-Filled CMU

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Allowable Load-Adjustment Factors for Carbon-Steel and Stainless-Steel Wedge-All® Anchors in Normal-Weight Concrete: Edge Distance, Tension and Shear Loads

### How to use these charts:

- 1. The following tables are for reduced edge distance.
- Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the edge distance ( $c_{act}$ ) at which the anchor is to be installed.
- 4. The load adjustment factor (f<sub>c</sub>) is the intersection of the row and column.
- 5. Multiply the allowable load by the applicable load adjustment factor.
- 6. Reduction factors for multiple edges are multiplied together.

### Edge Distance Tension (f<sub>c</sub>)

Edge	Size	1/4	3/8	1/2	5/8	3/4	7/8	1	1 1/4
Dist.	C <sub>cr</sub>	21/2	3¾	5	61/4	71/2	83/4	10	121/2
c <sub>act</sub> (in.)	C <sub>min</sub>	1	1 1/2	2	21/2	3	31/2	4	5
(in.)	f <sub>cmin</sub>	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70
1		0.70							
1 ½		0.80	0.70						
2		0.90	0.77	0.70					
21/2		1.00	0.83	0.75	0.70				
3			0.90	0.80	0.74	0.70			
31/2			0.97	0.85	0.78	0.73	0.70		
3¾			1.00	0.88	0.80	0.75	0.71		
4				0.90	0.82	0.77	0.73	0.70	
41/2				0.95	0.86	0.80	0.76	0.73	
5				1.00	0.90	0.83	0.79	0.75	0.70
51/2					0.94	0.87	0.81	0.78	0.72
6					0.98	0.90	0.84	0.80	0.74
61/4					1.00	0.92	0.86	0.81	0.75
61/2						0.93	0.87	0.83	0.76
7						0.97	0.90	0.85	0.78
71/2						1.00	0.93	0.88	0.80
8							0.96	0.90	0.82
81/2							0.99	0.93	0.84
8¾							1.00	0.94	0.85
10								1.00	0.90
121/2									1.00
15									



### Edge Distance Shear (f<sub>c</sub>) (Shear Applied Perpendicular to Edge)

Edge	Size	1/4	3/8	1/2	5/8	3/4	7/8	1	1 1/4
Dist.	C <sub>cr</sub>	21/2	3¾	5	61/4	71/2	83/4	10	121/2
Cact	Cmin	1	1 1/2	2	21/2	3	31/2	4	5
(in.)	f <sub>cmin</sub>	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30
1		0.30							
1 1/2		0.53	0.30						
2		0.77	0.46	0.30					
21/2		1.00	0.61	0.42	0.30				
3			0.77	0.53	0.39	0.30			
31/2			0.92	0.65	0.49	0.38	0.30		
33/4			1.00	0.71	0.53	0.42	0.33		
4				0.77	0.58	0.46	0.37	0.30	
41/2				0.88	0.67	0.53	0.43	0.36	
5				1.00	0.77	0.61	0.50	0.42	0.30
51/2					0.86	0.69	0.57	0.48	0.35
6					0.95	0.77	0.63	0.53	0.39
61/4					1.00	0.81	0.67	0.56	0.42
61/2						0.84	0.70	0.59	0.44
7						0.92	0.77	0.65	0.49
71/2						1.00	0.83	0.71	0.53
8							0.90	0.77	0.58
81/2							0.97	0.83	0.63
83/4							1.00	0.85	0.65
10								1.00	0.77
121/2									1.00
15									



- 1.  $c_{act}$  = actual edge distance at which anchor is installed (inches).
- 2.  $c_{cr}$  = critical edge distance for 100% load (inches).
- 3.  $c_{min}$  = minimum edge distance for reduced load (inches).
- $4. f_C = adjustment factor for allowable load at actual edge distance.$
- 5.  $f_{ccr}$  = adjustment factor for allowable load at critical edge distance.  $f_{ccr}$  is always = 1.00.
- 6. f<sub>cmin</sub> = adjustment factor for allowable load at minimum edge distance.
- 7.  $f_c = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min} / (c_{cr} c_{min})].$

### Load-Adjustment Factors for Reduced Spacing:

Critical spacing is listed in the load tables. No adjustment in load is required when the anchors are spaced at critical spacing. No additional testing has been performed to determine the adjustment factors for spacing dimensions less than those listed in the load tables.

<sup>\*</sup> See page 12 for an explanation of the load table icons



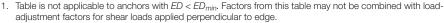
Allowable Load-Adjustment Factors for Carbon-Steel and Stainless-Steel Wedge-All® Anchors in Normal-Weight Concrete: Edge Distance and Shear Load Applied Parallel to Edge

### How to use these charts:

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for a shear load application.
- 3. Locate the edge distance  $(c_{act||})$  at which the anchor is to be installed.
- 4. The load adjustment factor  $(\phi_{c/l})$  is the intersection of the row and column.
- 5. Multiply the allowable load by the applicable load adjustment factor.
- 6. Reduction factors for multiple edges are multiplied together.

### Edge Distance Shear (f<sub>cll</sub>) (Shear Applied Parallel to Edge with End Distance ≥ ED<sub>min</sub>

	Size	1/4	3/8	1/2	5/8	3/4	7/8	1	11/4
Edgo	Ε	21/4	3%	41/2	51/2	6¾	77/8	9	91/2
Edge Dist.	ED <sub>min</sub>	9	131/2	18	22	27	31 1/2	36	38
c <sub>actll</sub> (in.)	C <sub>CrII</sub>	21/2	3¾	5	61/4	71/2	8¾	10	121/2
(111.)	C <sub>min  </sub>	1	1 1/2	2	21/2	3	31/2	4	5
	f <sub>cmin//</sub>	1.00	0.93	0.70	0.62	0.62	0.62	0.62	0.62
1		1.00							
1 ½		1.00	0.93						
2		1.00	0.95	0.70					
21/2		1.00	0.96	0.75	0.62				
3			0.98	0.80	0.67	0.62			
31/2			0.99	0.85	0.72	0.66	0.62		
4			1.00	0.90	0.77	0.70	0.66	0.62	
5				1.00	0.87	0.79	0.73	0.68	0.62
6					0.97	0.87	0.80	0.75	0.67
7					1.00	0.96	0.87	0.81	0.72
8						1.00	0.95	0.87	0.77
9							1.00	0.94	0.82
10								1.00	0.87
11									0.92
12									0.97
13									1.00



- c<sub>act||</sub> = actual edge distance (measured perpendicular to direction of shear load) at which anchor is installed (inches)
- 3.  $c_{crll}$  = critical edge distance (measured perpendicular to direction of shear load) for 100% load (inches).
- 4.  $c_{min||}$  = minimum edge distance (measured perpendicular to direction of shear load) for reduced load (inches).
- 5. *ED* = actual end distance (measured parallel to direction of shear load) at which anchor is installed (inches).
- 6. ED<sub>min</sub> = minimum edge distance (measured parallel to direction of shear load).
- 7.  $f_{c/l}$  = adjustment factor for allowable load at actual edge distance.
- 8.  $f_{ccr|l}$  = adjustment factor for allowable load at critical edge distance.  $f_{ccr|l}$  is always = 1.00.
- 9. f<sub>cmin||</sub> = adjustment factor for allowable load at minimum edge distance.
- 10.  $f_{c||} = f_{cmin||} + [(1 f_{cmin||}) (c_{act||} c_{min||}) / (c_{cr||} c_{min||})].$

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Allowable Load-Adjustment Factors for Carbon-Steel and Stainless-Steel Wedge-All® Anchors in Normal-Weight Concrete: Spacing, Tension Loads

### How to use these charts:

- 1. The following tables are for reduced spacing.
- 2. Locate the anchor size to be used for a tension load application.
- 4. Locate the spacing (s<sub>act</sub>) at which the anchor is to be installed.
- 5. The load adjustment factor (f<sub>s</sub>) is the intersection of the row and column.
- 3. Locate the anchor embedment (E) used for a tension load application. 6. Multiply the allowable load by the applicable load adjustment factor.
  - 7. Reduction factors for multiple spacings are multiplied together.

### Spacing Tension (f<sub>s</sub>)

	Dia.	1,	/4		3/8			1/2			5/8	
	Ε	11/8	21/4	13/4	25/8	3%	21/4	3%	41/2	23/4	41/2	51/2
s <sub>act</sub> (in.)	Scr	1%	31/8	2%	35/8	43/4	31/8	43/4	61/4	31/8	61/4	73/4
()	Smin	5/8	11/8	7/8	1%	13/4	11/8	13/4	21/4	1%	21/4	23/4
	f <sub>smin</sub>	0.43	0.70	0.43	0.43	0.70	0.43	0.43	0.70	0.43	0.43	0.70
3/4		0.50										
1		0.64		0.48								
11/4		0.79	0.72	0.57			0.47					
1 ½		0.93	0.76	0.67	0.46		0.54			0.46		
13/4		1.00	0.79	0.76	0.53	0.70	0.61	0.43		0.52		
2			0.83	0.86	0.59	0.73	0.68	0.48		0.57		
21/4			0.87	0.95	0.65	0.75	0.75	0.53	0.70	0.63	0.43	
21/2			0.91	1.00	0.72	0.78	0.82	0.57	0.72	0.69	0.47	
2¾			0.94		0.78	0.80	0.89	0.62	0.74	0.74	0.50	0.70
3			0.98		0.84	0.83	0.96	0.67	0.76	0.80	0.54	0.72
31/2			1.00		0.97	0.88	1.00	0.76	0.79	0.91	0.61	0.75
4					1.00	0.93		0.86	0.83	1.00	0.68	0.78
41/2						0.98		0.95	0.87		0.75	0.81
5						1.00		1.00	0.91		0.82	0.84
6									0.98		0.96	0.90
7									1.00		1.00	0.96
8												1.00



### Spacing Tension (f<sub>s</sub>)

	Dia.		3/4		7,	/8	1	I	1	1/4
_	Ε	3%	5	6¾	37/8	77/8	41/2	9	5%	91/2
s <sub>act</sub> (in.)	Scr	43/4	7	91/2	5%	11	61/4	12%	77//8	131/4
(111.)	Smin	1¾	21/2	3%	2	4	21/4	41/2	27/8	43/4
	f <sub>smin</sub>	0.43	0.43	0.70	0.43	0.70	0.43	0.70	0.43	0.70
2		0.48			0.43					
3		0.67	0.49		0.60		0.54		0.46	
4		0.86	0.62	0.73	0.77	0.70	0.68		0.57	
5		1.00	0.75	0.78	0.94	0.74	0.82	0.72	0.68	0.71
6			0.87	0.83	1.00	0.79	0.96	0.76	0.79	0.74
7			1.00	0.88		0.83	1.00	0.79	0.90	0.78
8				0.93		0.87		0.83	1.00	0.81
9				0.98		0.91		0.87		0.85
10				1.00		0.96		0.90		0.89
11						1.00		0.94		0.92
12								0.98		0.96
13								1.00		0.99
14										1.00



 $<sup>2.</sup> s_{act} = actual spacing distance at which anchors are installed (inches).$ 



 $<sup>3.</sup> s_{cr}$  = critical spacing distance for 100% load (inches).

<sup>4.</sup>  $s_{min}$  = minimum spacing distance for reduced load (inches).

<sup>5.</sup>  $f_s$  = adjustment factor for allowable load at actual spacing distance.

 $<sup>6.\,</sup>f_{SCr}$  = adjustment factor for allowable load at critical spacing distance.  $f_{SCr}$  is always = 1.00.

<sup>7.</sup>  $f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.

<sup>8.</sup>  $f_s = f_{smin} + [(1 - f_{smin}) (s_{act} - s_{min}) / (s_{cr} - s_{min})].$ 

<sup>\*</sup> See page 12 for an explanation of the load table icons



Allowable Load-Adjustment Factors for Carbon-Steel and Stainless-Steel Wedge-All® Anchors in Normal-Weight Concrete: Spacing, Shear Loads

### How to use these charts:

- 1. The following tables are for reduced spacing.
- 2. Locate the anchor size to be used for a shear load application.
- 3. Locate the anchor embedment (E) used for a shear load application.
- 4. Locate the spacing (s<sub>act</sub>) at which the anchor is to be installed.
- 5. The load adjustment factor (f<sub>s</sub>) is the intersection of the row and
- 6. Multiply the allowable load by the applicable load adjustment factor.
- 7. Reduction factors for multiple spacings are multiplied together.

### Spacing Shear (f<sub>a</sub>)

	Dia.	1,	/4		3/8			1/2			5/8	
	E	11/8	21/4	13/4	25/8	3%	21/4	3%	41/2	23/4	41/2	51/2
s <sub>act</sub> (in.)	Scr	1%	31/8	2%	35/8	43/4	31/8	43/4	61/4	31/8	61/4	73/4
(111.)	Smin	5/8	11/8	7/8	1%	13/4	11/8	13/4	21/4	1%	21/4	23/4
	f <sub>smin</sub>	0.79	0.79	0.79	0.79	0.79	0.79	0.79	0.79	0.79	0.79	0.79
3/4		0.82										
1		0.87		0.81								
1 1/4		0.92	0.80	0.84			0.80					
1 ½		0.97	0.83	0.88	0.80		0.83			0.80		
13/4		1.00	0.86	0.91	0.83	0.79	0.86	0.79		0.82		
2			0.88	0.95	0.85	0.81	0.88	0.81		0.84		
21/4			0.91	0.98	0.87	0.83	0.91	0.83	0.79	0.86	0.79	
21/2			0.93	1.00	0.90	0.84	0.93	0.84	0.80	0.88	0.80	
23/4			0.96		0.92	0.86	0.96	0.86	0.82	0.91	0.82	0.79
3			0.99		0.94	0.88	0.99	0.88	0.83	0.93	0.83	0.80
31/2			1.00		0.99	0.91	1.00	0.91	0.86	0.97	0.86	0.82
4					1.00	0.95		0.95	0.88	1.00	0.88	0.84
41/2						0.98		0.98	0.91		0.91	0.86
5						1.00		1.00	0.93		0.93	0.88
6									0.99		0.99	0.93
7									1.00		1.00	0.97
8												1.00









**Mechanical** Anchors

See notes below.

### Spacing Shear (f<sub>s</sub>)

	Dia.		3/4		7	/8	1		1	1/4
_	Ε	3%	5	6¾	31//8	<b>7</b> ½	41/2	9	5%	91/2
s <sub>act</sub> (in.)	Scr	43/4	7	91/2	5%	11	61/4	12%	<b>7</b> ½	131/4
(,	Smin	1¾	21/2	3%	2	4	21/4	41/2	27/8	43/4
	f <sub>smin</sub>	0.79	0.79	0.79	0.79	0.79	0.79	0.79	0.79	0.79
2		0.81			0.79					
3		0.88	0.81		0.85		0.83		0.80	
4		0.95	0.86	0.81	0.91	0.79	0.88		0.84	
5		1.00	0.91	0.85	0.98	0.82	0.93	0.80	0.88	0.80
6			0.95	0.88	1.00	0.85	0.99	0.83	0.92	0.82
7			1.00	0.91		0.88	1.00	0.85	0.96	0.85
8				0.95		0.91		0.88	1.00	0.87
9				0.98		0.94		0.91		0.90
10				1.00		0.97		0.93		0.92
11						1.00		0.96		0.94
12								0.98		0.97
13								1.00		0.99
14										1.00



 $<sup>2.</sup> s_{act} = actual spacing distance at which anchors are installed (inches).$ 

<sup>3.</sup>  $s_{cr}$  = critical spacing distance for 100% load (inches).

<sup>4.</sup>  $s_{min}$  = minimum spacing distance for reduced load (inches).

 $<sup>5.</sup> f_s = adjustment factor for allowable load at actual spacing distance.$ 

<sup>6.</sup> f<sub>scr</sub> = adjustment factor for allowable load at critical spacing distance. f<sub>scr</sub> is always = 1.00.

<sup>7.</sup> f<sub>smin</sub> = adjustment factor for allowable load at minimum spacing distance.

<sup>8.</sup>  $f_s = f_{smin} + [(1 - f_{smin}) (s_{act} - s_{min}) / (s_{cr} - s_{min})].$ 

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# Wedge-All® Design Information — Concrete



Allowable Load-Adjustment Factors for Carbon-Steel Wedge-All® Anchors in Sand-Lightweight Concrete: Edge Distance, Tension and Shear Loads

### How to use these charts:

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the edge distance (cact) at which the anchor is to be installed.
- The load adjustment factor (f<sub>c</sub>) is the intersection of the row and column.
- 5. Multiply the allowable load by the applicable load adjustment factor.
- 6. Reduction factors for multiple edges are multiplied together.

### Edge Distance Shear (f<sub>c</sub>) (Shear Applied Perpendicular to Edge

Edge	Size	1/4	1/2	5/8	3/4
Dist.	c <sub>cr</sub>	3%	6¾	8%	10
Cact	C <sub>min</sub>	1%	23/4	3%	4
(in.)	f <sub>cmin</sub>	0.30	0.30	0.30	0.30
1%		0.30			
1 1/2		0.34			
2		0.52			
21/2		0.69			
23/4		0.78	0.30		
3		0.87	0.34		
3%		1.00	0.41	0.30	
31/2			0.43	0.32	
4			0.52	0.39	0.30
41/2			0.61	0.46	0.36
5			0.69	0.53	0.42
5½			0.78	0.60	0.48
6			0.87	0.67	0.53
61/2			0.96	0.74	0.59
6¾			1.00	0.77	0.62
7				0.81	0.65
71/2				0.88	0.71
8				0.95	0.77
8%				1.00	0.81
81/2					0.83
9					0.88
91/2					0.94
10					1.00



### Edge Distance Tension (f<sub>c</sub>)

Edge	Size	1/4	1/2	5/8	3/4
Dist.	Ccr	3%	63/4	8%	10
Cact	C <sub>min</sub>	1%	23/4	3%	4
(in.)	f <sub>cmin</sub>	0.70	0.70	0.70	0.70
13/8		0.70			
1 ½		0.72			
2		0.79			
21/2		0.87			
23/4		0.91	0.70		
3		0.94	0.72		
3%		1.00	0.75	0.70	
31/2			0.76	0.71	
4			0.79	0.74	0.70
41/2			0.83	0.77	0.73
5			0.87	0.80	0.75
51/2			0.91	0.83	0.78
6			0.94	0.86	0.80
61/2			0.98	0.89	0.83
63/4			1.00	0.90	0.84
7				0.92	0.85
71/2				0.95	0.88
8				0.98	0.90
83/8				1.00	0.92
81/2					0.93
9					0.95
91/2					0.98
10					1.00

See Notes Below

# Load Adjustment Factors for Carbon-Steel Wedge-All® Anchors in Face-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance, Tension and Shear Loads

### Edge Distance Tension (f<sub>a</sub>)

Eage L	Jistanic	e rensi	O(1)			
	Size	3/8	1/2	5/8	3/4	IRC
Edge	Ccr	101/2	14	171/2	21	
Dist. c <sub>act</sub> (in.)	C <sub>min</sub>	4	4	4	4	1
()	f <sub>cmin</sub>	1.00	1.00	0.80	0.80	20 20
4		1.00	1.00	0.80	0.80	(22)
6		1.00	1.00	0.83	0.82	
8		1.00	1.00	0.86	0.85	
101/2		1.00	1.00	0.90	0.88	
12			1.00	0.92	0.89	
14			1.00	0.95	0.92	
16				0.98	0.94	
171/2				1.00	0.96	
21					1.00	

### Edge Distance Shear (f<sub>a</sub>)

Luge L	istal ic		" (IC)			
	Size	3/8	1/2	5/8	3/4	IBC
Edge	C <sub>cr</sub>	101/2	14	171/2	21	
Dist. cact (in.)	C <sub>min</sub>	4	4	4	4	<b>→</b>
()	f <sub>cmin</sub>	0.79	0.52	0.32	0.32	39 BS
4		0.79	0.52	0.32	0.32	(== =
6		0.85	0.62	0.42	0.40	
8		0.92	0.71	0.52	0.48	_n
101/2		1.00	0.83	0.65	0.58	( )
12			0.90	0.72	0.64	The state of the s
14			1.00	0.82	0.72	
16				0.92	0.80	
171/2				1.00	0.86	
21					1.00	

- 1.  $c_{act}$  = actual edge distance at which anchor is installed (inches).
- $2.c_{cr}$  = critical edge distance for 100% load (inches).
- $3. c_{min}$  = minimum edge distance for reduced load (inches).
- $4. f_C = adjustment factor for allowable load at actual edge distance.$
- 5.  $f_{\it ccr}$  = adjustment factor for allowable load at critical edge distance.  $f_{\it ccr}$  is always = 1.00.
- $6. f_{cmin}$  = adjustment factor for allowable load at minimum edge distance.
- $7.\,f_{c} = f_{cmin} + \left[ (1-f_{cmin})(c_{act}-c_{min}) \,/\, (c_{cr}-c_{min}) \right]$

### Load-Adjustment Factors for Reduced Spacing:

Critical spacing is listed in the load tables. No adjustment in load is required when the anchors are spaced at critical spacing. No additional testing has been performed to determine the adjustment factors for spacing dimensions less than those listed in the load tables.

<sup>\*</sup> See page 12 for an explanation of the load table icons

# Tie-Wire Wedge Anchor



The Tie-Wire anchor is a wedge-style expansion anchor for use in normal-weight concrete or in concrete over metal deck. With a tri-segmented, dual-embossed clip, the Tie-Wire anchor is ideal for the installation of acoustic ceiling grid and is easily set with the claw of a hammer.

### **Features**

- 1/4" eyelet for easy threading of wire
- · Sets with claw of hammer
- Tri-segmented clip each segment adjusts independently to hole irregularities
- Dual embossments on each clip segment enable the clip to undercut into the concrete, increasing follow-up expansion
- Wedge-style expansion anchor for use in normal weight concrete or concrete over metal deck

Material: Carbon steel
Coating: Zinc plated

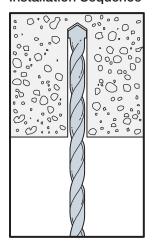
### Installation

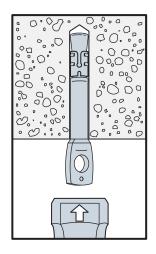
- 1. Drill a hole at least 11/2" deep using a 1/4" diameter carbide tipped bit.
- 2. Drive the anchor into the hole until the bottom of the head is flush with the base material.
- Set the anchor by prying/pulling the head with the claw end of the hammer.

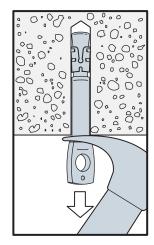
Size	Model No.	Drill Bit Dia.	Eyelet Hole Size	Qua	ntity
(in.)	Model No.	(in.)	(in.)	Вох	Carton
1/4" x 1 1/2"	TW25112	1/4	1/4	100	500

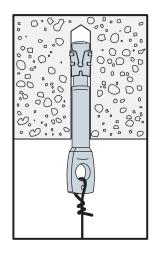


### Installation Sequence









# **Tie-Wire** Design Information — Concrete



Allowable Tension and Shear Loads for Tie-Wire Anchor in Normal-Weight Concrete

IRC			
الحرا	20 00	250 850	

		Embed		Critical	Critical	Tension Load		Shear Load	
	Size in.	Drill Bit Dia.	Depth	End Dist.		f' <sub>c</sub> ≥ 2,500 psi (17.2 MPa)		f' <sub>c</sub> ≥ 2,500 psi (17.2 MPa)	
	(mm)	in.	in. (mm)			Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
	1/4 (6.4)	1/4	<b>1½</b> (38)	<b>2½</b> (64)	<b>5</b> (127)	<b>1,155</b> (5.1)	<b>290</b> (1.3)	<b>380</b> (1.7)	<b>95</b> (0.4)

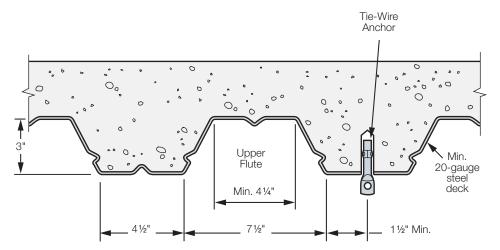
- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. The minimum concrete thickness is  $1\frac{1}{2}$  times the embedment depth.

Allowable Tension and Shear Loads for Tie-Wire Anchor in the Soffit of Normal-Weight Concrete or Sand-Lightweight Concrete over Metal Deck

IBC	<b>1</b>	<b>→</b>	*
-----	----------	----------	---

		Drill Bit Embed Critical Critical Dia Depth End Dist. <sup>5</sup> Spacing		Critical	Tension Load		Shear Load	
Size in.	Drill Bit Dia			End Dist. <sup>5</sup> Spacing	f' <sub>c</sub> ≥ 3,000 ps	si (20.7 MPa)	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa)	
(mm)	in.	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
1/4 (6.4)	1/4	<b>1½</b> (38)	<b>2½</b> (64)	<b>5</b> (127)	<b>1,155</b> (5.1)	<b>290</b> (1.3)	<b>460</b> (2.0)	<b>115</b> (0.5)

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. The minimum concrete thickness is  $1\frac{1}{2}$  times the embedment depth.
- 3. Metal deck must be minimum 20-gauge thick with minimum yield strength of 33 ksi.
- 4. Anchors installed in the bottom flute of the steel deck must have a minimum edge distance of 1½" away from inclined edge of the bottom flute. See the figure below.
- 5. Critical end distance is defined as the distance from the end of the slab in the direction of the flute.



Installation in the Soffit of Concrete over Metal Deck

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Easy-Set Pin-Drive Expansion Anchor



The Easy-Set is a pin-drive expansion anchor for medium- and heavy-duty fastening applications into concrete and grout-filled block. Integrated nut and washer help keep track of parts.

Material: Carbon steel

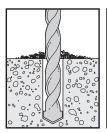
Coating: Yellow zinc dichromate plated

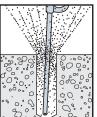
### Installation

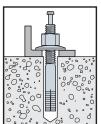
Caution: Oversized holes in the base material will make it difficult to set the anchor and will reduce the anchor's load capacity.

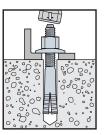
- 1. Drill a hole in the base material using a carbide drill bit the same diameter as the nominal diameter of the anchor to be installed. Drill the hole to the specified embedment depth plus ¼" to allow for pin extension and blow it clean using compressed air. (Overhead installations need not be blown clean.) Alternatively, drill the hole deep enough to accommodate embedment depth and the dust from drilling.
- 2. Adjust the nut for required embedment. Place the anchor through the fixture and into the hole.
- 3. Hammer the center pin until the bottom of the head is flush with top of anchor.

### Installation Sequence









### **EZAC Product Data**

Size	Model	Thread Length	Quanity		
(in.)	No.	(in.)	Вох	Carton	
3/8 x 23/8	EZAC37238	1	50	250	
3/8 X 31/2	EZAC37312	1 1/8	50	250	
3/8 x 43/4	EZAC37434	1 ½	50	200	
½ x 2¾	EZAC50234	1	25	125	
½ x 3½	EZAC50312	1 1/8	25	125	
½ x 4¾	EZAC50434	1 ½	25	100	
½ x 6	EZAC50600	2	25	100	
5% x 4	EZAC62400	1 %	15	60	
5/8 x 43/4	EZAC62434	1 %	15	60	
5⁄8 x 6	EZAC62600	2	15	60	

### Easy-Set Anchor Installation Data

Lady Oct / World Wild	tanatioi	Data	
Easy-Set Dia. (in)	3/8	1/2	5%
Drill Bit Size (in.)	3/8	1/2	5/8
Min. Fixture Hole Size (in.)	7/16	9/16	11/16
Wrench Size (in.)	9/16	3/4	15/16

Easy-Set

(EZAC)

### EZAC Allowable Tension and Shear Loads in Normal-Weight Concrete

	Embed.		Critical Edge	Critical	Tension Load	Shear Load	
Size in.	Size Depth	Drill Bit Dia. In.	Dist. In.	Spacing Dist. In.	f¹ <sub>C</sub> ≥ 2,000 psi (13.8 MPa) Concrete		
			(mm)	(mm)	Allowable lb. (kN)		
3/8	<b>1</b> 3/4 (44)	3/8	<b>2¾</b> (70)	<b>51⁄4</b> (133)	<b>630</b> (2.8)	<b>645</b> (2.9)	
1/2	<b>2½</b> (64)	1/2	<b>3</b> % (86)	<b>6¾</b> (171)	<b>1,005</b> (4.5)	<b>1,230</b> (5.5)	
5/8	<b>3</b> (76)	5/8	<b>4½</b> (108)	<b>9</b> (229)	<b>1,515</b> (6.7)	<b>1,325</b> (5.9)	

<sup>\*</sup> See page 12 for an explanation of the load table icons.



- 1. The allowable loads listed are based on a safety factor of 4.0.
- 100% of the allowable load is permitted at critical spacing and critical edge distance. Allowable loads at lesser spacings and edge distance have not been determined.
- 3. The minimum concrete thickness is 1  $\frac{1}{2}$  times the embedment depth.
- 4. Tension and shear loads for the EZAC anchor may be combined using the straight-line interaction equation (n = 1).

## Sleeve-All® Sleeve Anchor

Sleeve-All® expanding anchors are pre-assembled, expanding sleeve anchors for use in all types of solid base materials. This anchor is available in acorn, hex, rod coupler, flat or round head style for a wide range of applications.

**Codes:** Factory Mutual 3017082, 3026805 and 3029959 (%" – ½" diameter); Underwriters Laboratories File Ex3605 (%" – ¾" diameter); Mulitiple DOT listings; meets the requirements of Federal Specification A-A-1922A

Material: Carbon steel or stainless steel

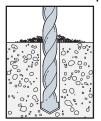
Coating: Carbon steel anchors are zinc plated

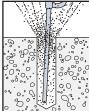
### Installation

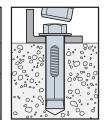
- 1. Drill a hole in the base material using a carbide drill bit the same diameter as the nominal diameter of the anchor to be installed.
- Drill the hole to the specified embedment depth, and blow it clean using compressed air. (Overhead installations need not be blown clean.) Alternatively, drill the hole deep enough to accommodate embedment depth and the dust from drilling.
- 3. Place the anchor in the fixture, and drive it into the hole until the washer and nut are tight against the fixture.
- 4. Tighten to required installation torque.

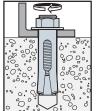
Caution: Oversized holes will make it difficult to set the anchor and will reduce the anchor's load capacity.

### Installation Sequence









### Material Specifications

Anchor Component	Zinc-Plated Carbon Steel	304 Stainless Steel
Anchor Body	Material meets minimum 50,000 psi tensile	Type 304
Sleeve	SAE J403, Grade 1008 Cold-Rolled Steel	Type 304
Nut	Commercial Grade, meets requirements of ASTM A563 Grade A	Type 304
Washer	SAE J403, Grade 1008/1010 Cold-Rolled Steel	Type 304

### Sleeve-All® Anchor Installation Data

Sleeve-All Dia. (in.)	1/4	<sup>5</sup> ⁄16	3/8	1/2	5/8	3/4
Drill Bit Size (in.)	1/4	5/16	3/8	1/2	5/8	3/4
Wrench Size <sup>1</sup> (in.)	3/8	7/16	1/2	9/16	3/4	15/16
Wrench Size for Coupler Nu	t (in.)		1/2	5/8	3/4	_

<sup>1.</sup> Applies to acorn- and hex-head configurations only.







# Sleeve-All® Sleeve Anchor



# Sleeve-All® Anchor Product Data — Zinc-Plated Carbon Steel

Sieeve-Ali®	Anchorrio	duct Data			on otec	71
Size	Model	Head	Bolt Diameter –	Max. Fixture	Qua	ntity
(in.)	No.	Style	Threads per inch	Thickness (in.)	Вох	Carton
1/4 x 13/8	SL25138A	Acorn	3/ 04	1/4	100	500
1/4 x 21/4	SL25214A	Head	3/16-24	1 1/8	100	500
5/16 X 1 1/2*	SL31112H		1/ 00	3/8	100	500
5/16 X 21/2	SL31212H		1/4-20	1 1/16	50	250
3/8 X 1 7/8	SL37178H			3/8	50	250
3/8 X 3	SL37300H		5/16-18	1 1/2	50	200
3/8 X 4	SL37400H			21/4	50	200
½ x 21/4*	SL50214H			1/2	50	200
½ x 3	SL50300H		3⁄8 <b>–</b> 16	3/4	25	100
½ x 4	SL50400H	Hex Head	98-10	13/4	25	100
½ x 6	SL50600H			3%	20	80
5/8 x 2 1/4*	SL62214H			1/2	25	100
5⁄8 x 3	SL62300H		1/2–13	3/4	20	80
5/8 X 4 1/4	SL62414H		1/2-13	1 1/2	10	40
5/8 x 6	SL62600H			31/4	10	40
3/4 x 21/2*	SL75212H			1/2	10	40
3/4 X 4 1/4	SL75414H		5/8-11	7/8	10	40
3/4 x 61/4	SL75614H			27/8	5	20
1/4 x 2	SL25200PF		3/16-24	7/8	100	500
1/4 x 3	SL25300PF		916-24	1 1/8	50	250
5/16 X 21/2	SL31212PF		1/. 00	1 1/16	50	250
5/16 X 3 1/2	SL31312PF	Phillips	1/4-20	21/16	50	250
3/8 X 23/4	SL37234PF	Flat Head		1 1/4	50	200
3/8 x 4	SL37400PF		5/ 10	21/2	50	200
3/8 X 5	SL37500PF		5/16-18	31/2	50	200
3% x 6	SL37600PF			41/2	50	200
1/4 x 23/4	SL25234	Round Head	3/16-24	7/8	50	250

<sup>\*</sup>These models do not meet minimum embedment requirements for rated load values.

# Sleeve-All® Anchor Product Data – Stainless Steel

Size	Model	Head	Bolt Diameter –	Max. Fixture	Quantity		
(in.)	No.	Style	Threads per inch	Thickness (in.)	Box	Carton	
3/8 x 17/8	SL37178HSS		5/16—18	3/8	50	250	
3% x 3	SL37300HSS	Hex Head	916-10	1 1/2	50	200	
½ x 3	SL50300HSS		3 <sub>8</sub> –16	3/4	25	100	
½ x 4	SL50400HSS		%-16	13/4	25	100	

# Sleeve-All® Anchor (with rod coupler) Product Data – Zinc-Plated Carbon Steel

	Size	Model	Accepts Rod	Wrench	Qua	ntity
	(in.)	No.	Dia. (in.)	Size	Вох	Carton
Ī	3% x 17%	SL37178C	3/8	1/2	50	200
	½ x 21/4	SL50214C	1/2	5/8	25	100
	5/8 x 21/4	SL62214C	5/8	3/4	20	80

# Length Identification Head Marks on Sleeve-All Anchors (corresponds to length of anchor – inches)

Mark	Α	В	С	D	Е	F	G	Н	1	J	K	L	M	N	0	Р	Q	R	S	Т	U	٧	W	Х	Υ	Z
From	1½	2	2½	3	3½	4	41/2	5	5½	6	6½	7	71/2	8	8½	9	9½	10	11	12	13	14	15	16	17	18
Up To But Not Including	2	2½	3	3½	4	41/2	5	5½	6	6½	7	7½	8	81/2	9	9½	10	11	12	13	14	15	16	17	18	19

# **Sleeve-All®** Design Information — Concrete and Masonry



### d Shoar Loads for Sloovo-All® in Normal-Woight Concrete Allowable Tens

);	sion and	d Shear	Loads to	or Sieeve	-Aliº in in	ormai-vv	eignt Cor	ncrete				4 608	
	Critical	Critical			Tensio	n Load				Shear Load		Install.	
	Edge Dist.	Spacing Dist.	f¹ <sub>c</sub> ≥ 2	,000 psi (13. Concrete	8 MPa)	f' <sub>c</sub> ≥ 4,	f' <sub>c</sub> ≥ 4,000 psi (27.6 MPa) Concrete			f' <sub>c</sub> ≥ 2,000 psi (13.8 MPa) Concrete			
	in. (mm)	in. (mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)	(N-m)	
	<b>2½</b> (64)	<b>4½</b> (114)	<b>880</b> (3.9)	<b>94</b> (0.4)	<b>220</b> (1.0)	<b>1,320</b> (5.9)	<b>189</b> (0.8)	<b>330</b> (1.5)	<b>1,440</b> (6.4)	<b>90</b> (0.4)	<b>360</b> (1.6)	<b>5</b> (7)	
	<b>3</b> 1/8 (79)	<b>5¾</b> (146)	<b>1,120</b> (5.0)	<b>113</b> (0.5)	<b>280</b> (1.2)	<b>1,320</b> (5.9)	<b>350</b> (1.6)	<b>330</b> (1.5)	<b>2,160</b> (9.6)	<b>113</b> (0.5)	<b>540</b> (2.4)	8 (11)	
	<b>3¾</b> (95)	<b>6</b> (152)	<b>1,600</b> (7.1)	<b>294</b> (1.3)	<b>400</b> (1.8)	<b>2,680</b> (11.9)	<b>450</b> (2.0)	<b>670</b> (3.0)	<b>3,080</b> (13.7)	<b>223</b> (1.0)	<b>770</b> (3.4)	<b>15</b> (20)	
	<b>5</b> (127)	<b>9</b> (229)	<b>3,160</b> (14.1)	<b>254</b> (1.1)	<b>790</b> (3.5)	<b>4,760</b> (21.2)	<b>485</b> (2.2)	<b>1,190</b> (5.3)	<b>5,000</b> (22.2)	<b>473</b> (2.1)	<b>1,250</b> (5.6)	<b>25</b> (34)	
	61/4	11	4,200	681	1,050	6,160	1,772	1,540	8,520	713	2,130	50	

(7.9)

674

(3.0)

(6.9)

2.380

(10.6)

(37.9)

10.040

(44.7)

(3.2)

955

(4.2)

(9.5)

2,510

(11.2)

(68)

90

(122)

(27.4)

9.520

(42.3)

(4.7)

1,600

(7.1)

(343)1. The tabulated allowable loads are based on a safety factor of 4.0.

(279)

131/2

2. Allowable loads may not be increased for short-term loading due to wind or seismic forces.

(18.7)

6.400

(28.5)

(3.0)

665

(3.0)

- 3. Refer to allowable load-adjustment factors for spacing and edge distance on page 183.
- 4. Drill bit diameter used in base material corresponds to nominal anchor diameter.
- 5. Allowable tension loads may be linearly interpolated between concrete strengths listed.
- 6. The minimum concrete thickness is 11/2 times the embedment depth.

# Allowable Tension and Shear Loads for %" Sleeve-All® in Grout-Filled CMU (Anchor Installed in Horizontal Mortar Joint or Face Shell)

Size	Embed. Depth	Min. Edge Dist.	Min. End Dist.	Min. Spacing	Tensio	n Load	Shear	Load	Install. Torque
in. (mm)	in. (mm)	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Allow. lb. (kN)	ftlb. (N-m)
<b>3/8</b> (9.5)	<b>1½</b> (38)	<b>16</b> (406)	<b>16</b> (406)	<b>24</b> (610)	<b>2,000</b> (8.9)	<b>400</b> (1.8)	<b>2,300</b> (10.2)	<b>460</b> (2.0)	<b>15</b> (20)



See notes beneath following table.

Embed.

Depth

(mm) 11/8

> (29)17/16

(37)11/2

(38)

21/4

(57)23/4

(70)

3%

(86)

(159)

71/2

(191)

Size

in. (mm)

(6.4)

(7.9)

(9.5)

(12.7)

(15.9)

3/4

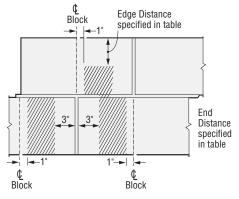
(19.1)

# Allowable Tension and Shear Loads for Sleeve-All® in Grout-Filled CMU

Size	Embed. Depth	Min. Edge Dist.	Min. End Dist.	Min. Spacing	Tensio	n Load	Shear	Load	Install. Torque
in. (mm)	in. (mm)	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Allow. lb. (kN)	ftlb. (N-m)
			Anchor I	nstalled in	a Single Fa	ce Shell			
<b>3/8</b> (9.5)	<b>1½</b> (38)	<b>12</b> (305)	<b>12</b> (305)	<b>24</b> (610)	<b>1,746</b> (7.8)	<b>350</b> (1.6)	<b>2,871</b> (12.8)	<b>575</b> (2.6)	<b>15</b> (20)
<b>½</b> (12.7)	<b>21/4</b> (57)	<b>12</b> (305)	<b>12</b> (305)	<b>24</b> (610)	<b>3,384</b> (15.1)	<b>675</b> (3.0)	<b>5,670</b> (25.2)	<b>1,135</b> (5.0)	<b>25</b> (34)
<b>5/8</b> (15.9)	<b>2¾</b> (70)	<b>12</b> (305)	<b>12</b> (305)	<b>24</b> (610)	<b>3,970</b> (17.7)	<b>795</b> (3.5)	<b>8,171</b> (36.3)	<b>1,635</b> (7.3)	<b>50</b> (68)
<b>3/4</b> (19.1)	<b>3</b> % (86)	<b>12</b> (305)	<b>12</b> (305)	<b>24</b> (610)	<b>6,395</b> (28.4)	<b>1,280</b> (5.7)	<b>12,386</b> (55.1)	<b>2,475</b> (11.0)	<b>90</b> (122)
			Ancho	Installed i	n Mortar "T	" Joint			
<b>3/8</b> (9.5)	<b>1 ½</b> (38)	<b>8</b> (203)	<b>8</b> (203)	<b>24</b> (610)	<b>1,927</b> (8.6)	<b>385</b> (1.7)	<b>3,436</b> (15.3)	<b>685</b> (3.0)	<b>15</b> (20)
<b>½</b> (12.7)	<b>21/4</b> (57)	<b>8</b> (203)	<b>8</b> (203)	<b>24</b> (610)	<b>3,849</b> (17.1)	<b>770</b> (3.4)	<b>5,856</b> (26.0)	<b>1,170</b> (5.2)	<b>25</b> (34)
<b>5/8</b> (15.9)	<b>2¾</b> (70)	<b>8</b> (203)	<b>8</b> (203)	<b>24</b> (610)	<b>4,625</b> (20.6)	<b>925</b> (4.1)	<b>7,040</b> (31.3)	<b>1,410</b> (6.3)	<b>50</b> (68)
<b>3/4</b> (19.1)	<b>3</b> % (86)	<b>8</b> (203)	<b>8</b> (203)	<b>24</b> (610)	<b>5,483</b> (24.4)	<b>1,095</b> (4.9)	<b>7,869</b> (35.0)	<b>1,575</b> (7.0)	<b>90</b> (122)

- 1. The tabulated allowable loads are based on a safety factor of 5.0.
- 2. Listed loads may be applied to installations through a face shell with the following placement guidelines: a. Minimum 3" from vertical mortar joint.
  - b. Minimum 1" from vertical cell centerline.
- 3. Values for 6- and 8-inch-wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry, f'm, at 28 days is 1,500 psi.
- 4. Embedment depth is measured from the outside face of the concrete masonry unit.
- 5. Drill bit diameter used in base material corresponds to nominal anchor diameter.





## **Face Shell Installation**

Allowable Anchor Placement in grout-filled CMU shown by shaded areas.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **Sleeve-All®** Design Information — Concrete



Allowable Load-Adjustment Factors for Sleeve-All® Anchors in Normal-Weight Concrete: Edge Distance and Spacing, Tension and Shear Loads

# How to use these charts:

- 1. The following tables are for reduced edge distance and spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load
- 3. Locate the edge distance ( $c_{act}$ ) or spacing ( $s_{act}$ ) at which the anchor is to be installed.

# 4. The load adjustment factor (f<sub>c</sub> or f<sub>s</sub>) is the intersection of the row and

- 5. Multiply the allowable load by the applicable load adjustment factor.
- 6. Reduction factors for multiple edges or spacing are multiplied

# Edge Distance Tension (f<sub>c</sub>)

Edge	Size	1/4	5/16	3/8	1/2	5/8	3/4
Dist.	c <sub>cr</sub>	21/2	31/8	3¾	5	61/4	71/2
cact	C <sub>min</sub>	1 1/4	1 %16	11//8	21/2	31/8	3¾
(in.)	f <sub>cmin</sub>	0.60	0.60	0.60	0.60	0.60	0.60
11/4		0.60					
1 1/2		0.68					
1 %16		0.70	0.60				
11//8		0.80	0.68	0.60			
2		0.84	0.71	0.63			
21/2		1.00	0.84	0.73	0.60		
3			0.97	0.84	0.68		
31/8			1.00	0.87	0.70	0.60	
3½				0.95	0.76	0.65	
3¾				1.00	0.80	0.68	0.60
4					0.84	0.71	0.63
41/2					0.92	0.78	0.68
5					1.00	0.84	0.73
5½						0.90	0.79
6						0.97	0.84
61/4						1.00	0.87
61/2							0.89
7							0.95
71/2							1.00

See notes below.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

### Edge Distance Shear (f.)

Euge	Distai	ice oi	iear (i <sub>c</sub>	)			
Edge	Size	1/4	5/16	3/8	1/2	5/8	3/4
Dist.	Ccr	21/2	31/8	3¾	5	61/4	71/2
Cact	C <sub>min</sub>	11/4	1%16	11//8	21/2	31/8	3¾
(in.)	f <sub>cmin</sub>	0.30	0.30	0.30	0.30	0.30	0.30
1 1/4		0.30					
1 1/2		0.44					
1 %16		0.48	0.30				
11//8		0.65	0.44	0.30			
2		0.72	0.50	0.35			
21/2		1.00	0.72	0.53	0.30		
3			0.94	0.72	0.44		
31/8			1.00	0.77	0.48	0.30	
31/2				0.91	0.58	0.38	
3¾				1.00	0.65	0.44	0.30
4					0.72	0.50	0.35
41/2					0.86	0.61	0.44
5					1.00	0.72	0.53
51/2						0.83	0.63
6						0.94	0.72
61/4						1.00	0.77
61/2							0.81
7							0.91
71/2							1.00

- 1.  $c_{act}$  = actual edge distance at which anchor is installed (inches).
- 2.  $c_{cr}$  = critical edge distance for 100% load (inches).
- 3.  $c_{min}$  = minimum edge distance for reduced load (inches).
- $4. f_C = adjustment factor for allowable load at actual edge distance.$
- 5. f<sub>cccr</sub> = adjustment factor for allowable load at critical edge distance.  $f_{cccr}$  is always = 1.00.
- 6. f<sub>cmin</sub> = adjustment factor for allowable load at minimum edge distance.
- 7.  $f_c = f_{cmin} + [(1 f_{smin}) (c_{act} c_{min}) / (c_{cr} c_{min})]$

# Spacing Tension and Shear (f<sub>a</sub>)

	Size	1/4	5/16	3/8	1/2	5/8	3/4
	E	11/8	17/16	11/2	21/4	23/4	3%
s <sub>act</sub> (in.)	Scr	41/2	5¾	6	9	11	131/2
(111.)	Smin	21/4	21/8	3	41/2	51/2	63/4
	f <sub>smin</sub>	0.50	0.50	0.50	0.50	0.50	0.50
21/4		0.50					
21/2		0.56					
27/8		0.64	0.50				
3		0.67	0.52	0.50			
31/2		0.78	0.61	0.58			
4		0.89	0.70	0.67			
41/2		1.00	0.78	0.75	0.50		
5			0.87	0.83	0.56		
5½			0.96	0.92	0.61	0.50	
5¾			1.00	0.96	0.64	0.52	
6				1.00	0.67	0.55	
6½					0.72	0.59	
6¾					0.75	0.61	0.50
7					0.78	0.64	0.52
8					0.89	0.73	0.59
9					1.00	0.82	0.67
10						0.91	0.74
11						1.00	0.81
12							0.89
13							0.96
13½							1.00

- 1. E = Embedment depth (inches).
- 2.  $s_{act}$  = actual spacing distance at which anchors are installed (inches).
- 3.  $s_{cr}$  = critical spacing distance for 100% load (inches).
- 4.  $s_{min}$  = minimum spacing distance for reduced load (inches).
- 5.  $f_s$  = adjustment factor for allowable load at actual spacing distance.
- 6.  $f_{scr}$  = adjustment factor for allowable load at critical spacing distance.  $f_{SCr}$  is always = 1.00.
- $7.\,f_{\text{Smin}} = \text{adjustment factor for allowable load at minimum spacing distance}.$
- 8.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$

<sup>\*</sup> See page 12 for an explanation of the load table icons.

Cracked

Concrete

# Titen HD® Heavy-Duty Screw Anchor

The original high-strength screw anchor for use in cracked and uncracked concrete, as well as uncracked masonry. The Titen HD® offers low installation torque and outstanding performance. Designed and tested in dry, interior, non-corrosive environments or temporary outdoor applications, the Titen HD® demonstrates industry-leading performance even in seismic conditions.

### **Features**

- Code listed under IBC/IRC in accordance with ICC-ES AC193 for cracked and uncracked concrete per ICC-ES ESR-2713
- Code listed under IBC/IRC in accordance with ICC-ES AC106 for masonry per ICC-ES ESR-1056
- · Qualified for static and seismic loading conditions
- Thread design undercuts to efficiently transfer the load to the base material
- Standard fractional sizes
- Specialized heat-treating process creates tip hardness for better cutting without compromising the ductility
- No special drill bit required designed to install using standard-sized ANSI tolerance drill bits
- Testing shows the Titen HD® installs in concrete with 50% less torque than competitor anchors
- Hex-washer head requires no separate washer and provides a clean installed appearance
- Removable ideal for temporary anchoring (e.g., formwork, bracing) or applications where fixtures may need to be moved (reuse of the anchor to achieve listed load values is not recommended)

Codes: ICC-ES ESR-2713 (concrete); ICC-ES ESR-1056 (masonry); City of L.A. RR25741 (concrete), RR25560 (masonry); Florida FL-15730.6; FM 3017082, 3035761 and 3043442; Multiple DOT listings

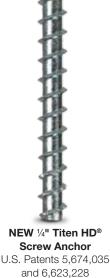
Material: Carbon steel

Coating: Zinc plated or mechanically galvanized









Serrated teeth on the tip of the Titen HD® screw anchor facilitate cutting and reduce installation torque.

# Installation

Mechanical Anchors

Holes in metal fixtures to be mounted should match the diameter specified in the table below. Use a Titen HD® screw anchor one time only - installing the anchor multiple times may result in excessive thread wear and reduce load capacity.



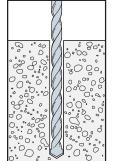
Do not use impact wrenches to install into hollow CMU.

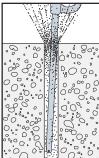


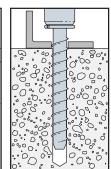
Caution: Oversized holes in base material will reduce or eliminate the mechanical interlock of the threads with the base material and reduce the anchor's load capacity.

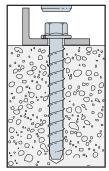
- 1. Drill a hole in the base material using a carbide drill bit the same diameter as the nominal diameter of the anchor to be installed. Drill the hole to the specified embedment depth plus minimum hole depth overall (see table below right) to allow the thread tapping dust to settle, and blow it clean using compressed air. (Overhead installations need not be blown clean.) Alternatively, drill the hole deep enough to accommodate embedment depth and the dust from drilling and tapping.
- 2. Insert the anchor through the fixture and into the hole.
- 3. Tighten the anchor into the base material until the hex-washer head contacts the fixture.

# Installation Sequence









# Additional Installation Information

Titen HD® Diameter (in.)	Wrench Size (in.)	Recommended Fixture Hole Size (in.)	Min. Hole Depth Overdrill (in.)
1/4	3/8	3% to 7/16	1/8
3/8	9/16	½ to %16	1/4
1/2	3/4	5% to 11/16	1/2
5/8	15/16	3⁄4 to 13⁄16	1/2
3/4	11/8	7⁄8 to 15∕16	1/2

# Titen HD® Heavy-Duty Screw Anchor



# Titen HD® Anchor Product Data — Zinc Plated

Size	Model No.	Drill Bit Dia.	Wrench Size	Qua	ntity
(in.)	Model No.	(in.)	(in.)	Вох	Carton
1/4 x 1 7/8	THDB25178H	1/4	3/8	100	500
1/4 x 23/4	THDB25234H	1/4	3/8	50	250
1/4 x 3	THDB25300H	1/4	3/8	50	250
1/4 x 3 1/2	THDB25312H	1/4	3/8	50	250
1/4 x 4	THDB25400H	1/4	3/8	50	250
3/8 X 1 3/4	THD37134H*	3/8	9/16	50	250
3/8 X 2 1/2	THD37212H*	3/8	9/16	50	200
3/8 x 3	THD37300H	3/8	9/16	50	200
3/8 x 4	THD37400H	3/8	9/16	50	200
3/8 x 5	THD37500H	3/8	9/16	50	100
3/8 x 6	THD37600H	3/8	9/16	50	100
½ x 3	THD50300H	1/2	3/4	25	100
½ x 4	THD50400H	1/2	3/4	20	80
½ x 5	THD50500H	1/2	3/4	20	80
½ x 6	THD50600H	1/2	3/4	20	80
½ x 6½	THD50612H	1/2	3/4	20	40
½ x 8	THD50800H	1/2	3/4	5	25
½ x 12	THD501200H	1/2	3/4	5	25
½ x 13	THD501300H	1/2	3/4	5	25
½ x 14	THD501400H	1/2	3/4	5	25
½ x 15	THD501500H	1/2	3/4	5	25
5⁄8 x 4	THDB62400H	5/8	15/16	10	40
5⁄8 x 5	THDB62500H	5/8	15/16	10	40
% x 6	THDB62600H	5/8	15/16	10	40
5/8 x 6 1/2	THDB62612H	5/8	15/16	10	40
5⁄8 x 8	THDB62800H	5/8	15/16	10	20
3/4 x 4	THD75400H	3/4	11/8	10	40
3/4 x 5	THD7500H	3/4	11/8	5	20
3/4 x 6	THDT75600H	3/4	11/8	5	20
3/4 x 7	THD75700H	3/4	11/8	5	10
3/4 X 8 1/2	THD75812H	3/4	11/8	5	10
3/4 x 10	THD75100H	3/4	11/8	5	10

<sup>\*</sup>These models do not meet minimum embedment depth requirements for strength design and require maximum installation torque of 25 ft. – lb. using a torque wrench, driver drill or cordless  $^{1/4}$ " impact driver with a maximum permitted torque rating of 100 ft. – lb.

# Titen HD® Anchor Product Data — Mechanically Galvanized

Size	Model	Drill Bit Dia.	Wrench	Qua	ntity
(in.)	No.	(in.)	Size (in.)	Вох	Carton
3% x 5	THD37500HMG	3/	9/	50	100
3% x 6	THD37600HMG	3/8	9⁄16	50	100
½ x 5	THD50500HMG			20	80
½ x 6	THD50600HMG	1/	3/	20	80
½ x 6½	THD50612HMG	1/2	3/4	20	40
½ x 8	THD50800HMG			20	40
5⁄8 x 5	THD62500HMG			10	40
5⁄8 x 6	THD62600HMG	E/	45/	10	40
5/8 x 6 1/2	THD62612HMG	5/8	15/16	10	40
5% x 8	THD62800HMG			10	20
5⁄8 x 5	THDB62500HMG			10	40
5⁄8 x 6	THDB62600HMG	E/	45/	10	40
5/8 x 6 1/2	THDB62612HMG	5/8	15/16	10	40
5⁄8 x 8	THDB62800HMG			10	20
3/4 x 8 1/2	THD75812HMG	2/	44/	5	10
3/4 x 10	THD75100HMG	3/4	11/8	5	10

Mechanical galvanizing meets ASTM B695, Class 65, Type 1. Intended for some pressure-treated wood sill plate applications. Not for use in other corrosive or outdoor environments. See page 316 or visit www.strongtie.com/info for more corrosion information.

# Titen HD® Installation Information and Additional Data<sup>1</sup>

Characteristic	Cumbal	Units				Nomina	I Anchor	Diamete	r, d <sub>a</sub> (in.)			
Characteristic	Symbol	UIIILS	1/	⁄4 <sup>4</sup>	3,	<b>/</b> 8	1,	/2	5/	5/8 <sup>4</sup> 5/8 3/4 100 <sup>2</sup>	3	3/4
		Install	ation Info	rmation								
Drill Bit Diameter	d <sub>bit</sub>	in.	1,	4	3,	8	1,	/2	5	/8	3	3/4
Baseplate Clearance Hole Diameter	$d_c$	in.	3	/8	1,	⁄2	5,	/8			7	<b>7</b> /8
Maximum Installation Torque	T <sub>inst,max</sub>	ftlbf	2	<b>4</b> <sup>2</sup>	50	<b>)</b> 2	6	5 <sup>2</sup>	10	)O <sup>2</sup>	15	50 <sup>2</sup>
Maximum Impact Wrench Torque Rating	T <sub>impact,max</sub>	ftlbf	12	25 <sup>3</sup>	15	iO <sup>3</sup>	34				38	35³
Minimum Hole Depth	h <sub>hole</sub>	in.	13/4	25/8	23/4	31/2	3¾	41/2	41/2	6	6	63/4
Nominal Embedment Depth	h <sub>nom</sub>	in.	15/8	21/2	21/2	31/4	31/4	4	4	51/2	51/2	61/4
Critical Edge Distance	Cac	in.	3	6	211/16	35/8	3%16	41/2	41/2	6%	6%	75/1
Minimum Edge Distance	C <sub>min</sub>	in.	1	1/2				1	13/4			
Minimum Spacing	Smin	in.					3	3				
Minimum Concrete Thickness	h <sub>min</sub>	in.	31/4	31/2	4	5	5	61/4	6	81/2	83/4	10
		Ad	dditional I	Data								
Anchor Category	Category	_						1				
Yield Strength	$f_{va}$	psi	100	,000				97,	000			
Tensile Strength	f <sub>uta</sub>	psi	125	,000				110	,000			
Minimum Tensile & Shear Stress Area	A <sub>se</sub>	in <sup>2</sup>	0.0	)42	0.0	199	0.1	83	0.2	276	0.4	414
Axial Stiffness in Service Load Range – Uncracked Concrete	$eta_{\mathit{uncr}}$	lb./in.	202	,000		715,000						
Axial Stiffness in Service Load Range – Cracked Concrete	$eta_{cr}$	lb./in.	173	,000				345	,000			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D.
- 2. Tinst, max is the maximum permitted installation torque for the embedment depth range covered by this table using a torque wrench.
- 3. T<sub>impact,max</sub> is the maximum permitted torque rating for impact wrenches for the embedment depth range covered by this table.
- 4. Data for 1/4" anchor is only valid for THDB25 series. Data for the 1/8" anchor is valid only for the THDB62 series.



# Titen HD® Tension Strength Design Data<sup>1</sup>



Characteristic	Cumbal	Symbol Units Nominal Anchor Diameter, d <sub>a</sub> (in.)										
Characteristic	Syllibol	UIIILS	1,	⁄4 <sup>9</sup>	3,	/8	20,130 0.65 <sup>2</sup> 2.35 2.99 3%6 4½ 24 17 1.0 0.65 <sup>7</sup>	5/	8 <sup>9</sup>	3	1/4	
Nominal Embedment Depth	h <sub>nom</sub>	in.	15/8	21/2	21/2	31/4	31/4	4	4	51/2	5½	61/4
		Steel S	Strength	in Tensio	1							
Tension Resistance of Steel	N <sub>sa</sub>	lb.	5,								45,540	
Strength Reduction Factor — Steel Failure	$\phi_{sa}$	_					0.0	35 <sup>2</sup>				
Concrete Breakout Strength in Tension <sup>6,8</sup>												
Effective Embedment Depth	h <sub>ef</sub>	in.	1.19	1.94	1.77	2.40	2.35	2.99	2.97	4.24	4.22	4.86
Critical Edge Distance <sup>6</sup>	$c_{ac}$	in.	3	6	211/16	35/8	3%16	41/2	41/2	6 %	6%	75/16
Effectiveness Factor — Uncracked Concrete	k <sub>uncr</sub>		30					24				
Effectiveness Factor — Cracked Concrete	k <sub>cr</sub>						1	7				
Modification Factor	$\psi_{c,N}$						1	.0				
Strength Reduction Factor — Concrete Breakout Failure	$\phi_{cb}$						0.0	35 <sup>7</sup>				
		Pullout 9	Strength	in Tensio	n <sup>8</sup>							
Pullout Resistance, Uncracked Concrete (f'c=2,500 psi)	N <sub>p,uncr</sub>	lb.	3	3	2,7004	3	3	3	3	9,8104	3	3
Pullout Resistance, Cracked Concrete (f'c=2,500 psi)	$N_{p,cr}$	lb.	3	1,9054	1,2354	2,7004	3	3	3,2604	5,5704	6,0704	7,1954
Strength Reduction Factor — Concrete Pullout Failure	$\phi_{\scriptscriptstyle D}$	_	- 0.65 <sup>5</sup>									
Breako	ut or Pullo	ut Streng	th in Ten	sion for S	Seismic A	pplication	1S <sup>8</sup>					
Nominal Pullout Strength for Seismic Loads (f'c=2,500 psi)	nal Pullout Strength for Seismic Loads (f' $_c$ =2,500 psi) $N_{p,eq}$   lb. $-3$   1,905 $^4$   1,235 $^4$   2,700 $^4$   $-3$   $-3$   3,260 $^4$   5,570 $^4$   6,						6,0704	7,1954				
Strength Reduction Factor — Breakout or Pullout Failure	$\phi_{eq}$	_					0.0	35 <sup>5</sup>				

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ . Anchors are considered brittle steel elements.
- 3. Pullout strength is not reported since concrete breakout controls.
- Adjust the characteristic pullout resistance for other concrete compressive strengths by multiplying the tabular value by (f'<sub>c,Specified</sub> / 2,500)<sup>0.5</sup>.
- 5. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 6. The modification factor  $\Psi_{Cp,N} = 1.0$  for cracked concrete. Otherwise, the modification factor for uncracked concrete without supplementary reinforcement to control splitting is either:

(1) 
$$\psi_{cp,N} = 1.0 \text{ if } c_{a,min} \ge c_{ac} \text{ or } (2) \ \psi_{cp,N} = \frac{c_{a,min}}{c_{ac}} \ge \frac{1.5 h_{ef}}{c_{ac}} \text{ if } c_{a,min} < c_{ac}$$

The modification factor,  $\mathit{V_{cp,N}}$  is applied to the nominal concrete breakout strength,  $N_{cb}$  or  $N_{cba}$ .

- 7. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 8. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout strength,  $N_{p,cr}$   $N_{p,uncr}$  and  $N_{eq}$  by 0.6. All-lightweight concrete is beyond the scope of this table.
- 9. Data for 1/4" anchor is valid only for THDB25 series. Data for 1/4" anchor is valid only for THDB62 series.

# Titen HD® Shear Strength Design Data<sup>1</sup>









Characteristic	Symbol	Units				Nomina	l Anchor	Diameter	r, d <sub>a</sub> (in.)			
Gildideleristic	Syllibol	UIIILS	1/	⁄4 <sup>5</sup>	3	<sup>3</sup> /8	1,	/2	5/8	3 <sup>5</sup>	3,	4
Nominal Embedment Depth	h <sub>nom</sub>	in.	15/8	21/2	21/2	31/4	31/4	4	4	51/2	51/2	61/4
		Steel	Strength	in Shear	•							
Shear Resistance of Steel	V <sub>sa</sub>	lb.	2,0	020	4,4	4,460 7,455			10,0	000	16,	840
Strength Reduction Factor — Steel Failure	$\phi_{sa}$	_					0.6	30 <sup>2</sup>				
	Con	crete Bre	akout St	rength in	Shear <sup>6</sup>							
Outside Diameter	d <sub>a</sub>	in.	0.	25	0.3	0.375		0.500		0.625		'50
Load Bearing Length of Anchor in Shear	$\ell_e$	in.	1.19	1.94	1.77	2.40	2.35	2.99	2.97	4.24	4.22	4.86
Strength Reduction Factor — Concrete Breakout Failure	$\phi_{cb}$						0.7	70 <sup>4</sup>				
	Co	ncrete P	ryout Str	ength in	Shear							
Coefficient for Pryout Strength	k <sub>cp</sub>	lb.		1.0				2.0				
Strength Reduction Factor — Concrete Pryout Failure	$\phi_{cp}$	_					0.7	70 <sup>4</sup>				
	Steel Stre	ength in S	Shear for	Seismic	Applicati	ons						
Shear Resistance for Seismic Loads	V <sub>eq</sub>	lb.	1,6	695	2,8	355	4,790		8,000		9,350	
Strength Reduction Factor — Steel Failure	$\phi_{eq}$	_		$0.60^{2}$								

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The value of  $\phi$  applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ . Anchors are considered brittle steel elements.
- 3. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used, and the requirements of Section D.4.3(c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used,
- \* See page 12 for an explanation of the load table icons.

- refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 4. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- Data for ¼" anchor is valid only for THDB25 series. Data for ¾" anchor is valid only for THDB62 series.
- 6. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout strength by 0.6. All-lightweight concrete is beyond the scope of this table.



Titen HD® Tension and Shear Strength Design Data for the Soffit of Normal-Weight or Sand-Lightweight Concrete over Metal Deck<sup>1,6,8</sup>

$\overline{}$		_
BC	<b>→</b>	ı

		Nominal Anchor Diameter, d <sub>a</sub> (in.)										
Characteristic	Symbol	Units			Lowe	r Flute				Upper	Flute	
Gildideletistic	Зунион	UIIILS	Figu	ire 2		Figu	ire 1		Figu	ire 2	Figu	ıre 1
			1/	4 <sup>8</sup>	3,	3/8 1/2		⁄2	1/.	48	3/8	1/2
Nominal Embedment Depth	h <sub>nom</sub>	in.	1%	21/2	1 1/8	21/2	2	31/2	15/8	21/2	1 1/8	2
Effective Embedment Depth	h <sub>ef</sub>	in.	1.19	1.94	1.23	1.77	1.29	2.56	1.19	1.94	1.23	1.29
Pullout Resistance, concrete on metal deck (cracked) <sup>2,3,4</sup>	$N_{p,deck,cr}$	lb.	420	535	375	870	905	2,040	655	1,195	500	1,700
Pullout Resistance, concrete on metal deck (uncracked) <sup>2,3,4</sup>	N <sub>p,deck,uncr</sub>	lb.	995	1,275	825	1,905	1,295	2,910	1,555	2,850	1,095	2,430
Steel Strength in Shear, concrete on metal deck <sup>5</sup>	V <sub>sa, deck</sub>	lb.	1,335	1,745	2,240	2,395	2,435	4,430	2,010	2,420	4,180	7,145
Steel Strength in Shear, Seismic	V <sub>sa, deck,eq</sub>	lb.	870	1,135	1,434	1,533	1,556	2,846	1,305	1,575	2,676	4,591

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. Concrete compressive strength shall be 3,000 psi minimum. The characteristic pullout resistance for greater compressive strengths shall be increased by multiplying the tabular value by  $(f^i_{c,specified}/3,000)^{0.5}$ .
- 3. For anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies, as shown in Figure 1 and Figure 2, calculation of the concrete breakout strength may be omitted.
- 4. In accordance with ACI 318 Section D.5.3.2, the nominal pullout strength in cracked concrete for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies  $N_{p,deck,cr}$
- shall be substituted for  $N_{p,cr}$ . Where analysis indicates no cracking at service loads, the normal pullout strength in uncracked concrete  $N_{p,deck,uncr}$  shall be substituted for  $N_{p,uncr}$ .
- 5. In accordance with ACI 318 Section D.6.1.2(c), the shear strength for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies V<sub>sa,deck</sub> and V<sub>sa,deck,eq</sub> shall be substituted for V<sub>sa</sub>.
- 6. Minimum edge distance to edge of panel is 2h<sub>ef</sub>-
- 7. The minimum anchor spacing along the flute must be the greater of  $3h_{\rm ef}$  or 1.5 times the flute width.
- 8. Data for 1/4" anchor is valid only for THDB25 series.

Titen HD® Anchor Tension and Shear Strength Design Data in the Topside of Normal-Weight Concrete over Metal Deck



			Nominal Anchor Diameter, d <sub>a</sub>				
Design Information	Symbol	Units	Figure 3	Figure 2			
Nominal Embedment Depth	h	in.	1/4" 15/8	21/2			
Nominal Embedment Depth	h <sub>nom</sub>	111.	1 7/8	Z 1/2			
Effective Embedment Depth	h <sub>ef</sub>	in.	1.19	1.77			
Minimum Concrete Thickness	h <sub>min,deck</sub>	in.	21/2	31/4			
Critical Edge Distance	Cac,deck,top	in.	3¾	71/4			
Minimum Edge Distance	C <sub>min, deck, top</sub>	in.	31/2	3			
Minimum Spacing	S <sub>min,deck,top</sub>	in.	31/2	3			

- 1. For anchors installed in the topside of concrete-filled deck assemblies, as shown in Figures 2 and 3, the nominal concrete breakout strength of a single anchor or group of anchors in shear,  $V_{cb}$  or  $V_{cbg}$ , respectively, must be calculated in accordance with ACI 318 D.6.2, using the actual member thickness,  $h_{min,deck^*}$  in the determination of  $A_{vc}$ .
- Design capacity shall be based on calculations according to values in the tables featured on pages 185 and 186.
- 3. Minimum flute depth (distance from top of flute to bottom of flute) is  $1\frac{1}{2}$  inch (see Figures 2 and 3).
- 4. Steel deck thickness shall be minimum 20 gauge.
- 5. Minimum concrete thickness ( $h_{min,deck}$ ) refers to concrete thickness above upper flute (see Figures 2 and 3).

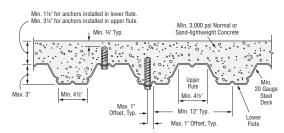


Figure 1. Installation of %" and ½" Diameter Anchors in the Soffit of Concrete over Metal Deck

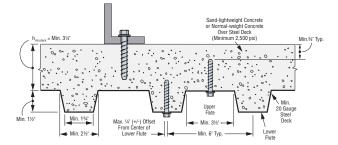


Figure 2. Installation of %" Diameter Anchors in the Topside and ¼" Diameter Anchors in the Soffit of Concrete over Metal Deck

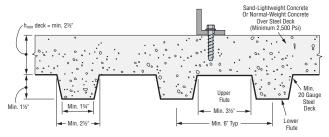


Figure 3. Installation of 1/4" Diameter Anchors in the Topside of Concrete over Metal Deck

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **Titen HD®** Design Information — Concrete



# Titen HD® Tension Design Strengths in Normal-Weight Concrete (f'<sub>c</sub> = 2,500 psi)





		Min.	Critical	Minimum	Tension Design Strength (lb.)								
Anchor Dia.	Nominal Embed. Depth	Concrete Thickness	Edge Distance	Edge Distance	lge Fdge Distances = c <sub>oo</sub> on al		c <sub>ac</sub> on all si				s = c <sub>min</sub> on one side on three sides		
(in.)	(in.)	h <sub>miņ</sub>	Cac	C <sub>miņ</sub>	SDC A	SDC A-B <sup>5</sup> SDC C-F <sup>6,7</sup>		SDC A-B <sup>5</sup>		SDC C	C-F <sup>6,7</sup>		
	(,	(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	
1/	1 5/8	31/4	3	1 ½	1,265	715	950	540	660	630	495	470	
1/4	21/2	31/2	6	1 ½	2,110	1,240	1,580	930	660	965	495	725	
3/8	21/2	4	211/16	13/4	1,755	805	1,315	600	1,350	805	1,015	600	
98	31/4	5	35/8	13/4	2,900	1,755	2,175	1,315	1,810	1,290	1,360	970	
1/	31/4	5	3%16	13/4	2,810	1,990	2,105	1,495	1,765	1,265	1,325	950	
1/2	4	61/4	41/2	13/4	4,035	2,855	3,025	2,140	2,285	1,620	1,710	1,220	
5/	4	6	41/2	13/4	3,990	1,975	2,995	1,480	2,250	1,610	1,690	1,210	
5/8	51/2	81/2	6%	13/4	6,375	3,620	4,780	2,715	3,390	2,405	2,540	1,805	
3/	51/2	83/4	6%	13/4	6,760	3,945	5,070	2,960	3,355	2,395	2,515	1,795	
3/4	61/4	10	75/16	13/4	8,355	4,675	6,265	3,510	3,990	2,835	2,990	2,125	

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# Titen HD® Allowable Tension Loads in Normal-Weight Concrete ( $f'_c = 2,500 \text{ psi}$ ) — Static Load





27 ES	1915

	Newstreet	Min. Ormanata	0	Minimum Edua		Allowable Tension Load (lb.)					
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)		= c <sub>ac</sub> on all sides	Edge Distances = and c <sub>ac</sub> on	: c <sub>min</sub> on one side three sides			
	(111.)	(111.)	(111.)	()	Uncracked	Cracked	Uncracked	Cracked			
1/	1 5/8	31/4	3	1 1/2	905	510	470	450			
1/4	21/2	31/2	6	1 1/2	1,505	885	470	690			
3/8	21/2	4	211/16	13/4	1,255	575	965	575			
98	31/4	5	35/8	13/4	2,070	1,255	1,295	920			
1/	31/4	5	3%16	13/4	2,005	1,420	1,260	905			
1/2	4	61/4	41/2	13/4	2,880	2,040	1,630	1,155			
5/	4	6	41/2	13/4	2,850	1,410	1,605	1,150			
5/8	51/2	81/2	6%	13/4	4,555	2,585	2,420	1,720			
3/	51/2	8¾	6%	13/4	4,830	2,820	2,395	1,710			
3/4	61/4	10	75/16	13/4	5,970	3,340	2,850	2,025			

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = 1.4$ . The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted

# Titen HD® Allowable Tension Loads in Normal-Weight Concrete ( $f'_c = 2,500$ psi) — Wind Load





	Naminal	Min Consusts	Ovition Ledon	Minimum Edua		Allowable Ten	wable Tension Load (lb.)		
Anchor Dia. (in.)	Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub>			Edge Distances = and c <sub>ac</sub> on	c <sub>min</sub> on one side three sides	
	(111.)	(111.)	(111.)	(111.)	Uncracked	Cracked	Uncracked	Cracked	
1/	15/8	31/4	3	1 ½	760	430	395	380	
1/4	21/2	31/2	6	1 ½	1,265	745	395	580	
3/8	21/2	4	211/16	13/4	1,055	485	810	485	
9/8	31/4	5	35/8	13/4	1,740	1,055	1,085	775	
1/2	31/4	5	3%16	13/4	1,685	1,195	1,060	760	
72	4	61/4	41/2	13/4	2,420	1,715	1,370	970	
5/8	4	6	41/2	13/4	2,395	1,185	1,350	965	
9/8	51/2	81/2	6%	13/4	3,825	2,170	2,035	1,445	
3/4	51/2	8¾	6%	13/4	4,055	2,365	2,015	1,435	
9/4	61/4	10	75/16	13/4	5,015	2,805	2,395	1,700	

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of α = 1.67. The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Titen HD® Allowable Tension Loads in Normal-Weight Concrete ( $f'_C = 2,500 \text{ psi}$ ) — Seismic Load







	Name of Min. Critical Minimum							llowable Tension Load (lb.)					
Anchor Dia.	Nominal Embed.	nbed. Concrete	Edge	Edge Distance	Edge	Distances	= c <sub>ac</sub> on all s	ides	Edge		c <sub>min</sub> on one three sides	side	
(in.)	Depth (in.)	hmin	Cac	C <sub>miņ</sub>	SDC	A-B <sup>4</sup>	SDC (	C-F <sup>5,6</sup>	SDC	A-B <sup>4</sup>	SDC C-F <sup>5,6</sup>		
	()	(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	440 675	Uncracked	Cracked	
1/	1%	31/4	3	1 ½	885	500	665	380	460	440	345	330	
1/4	21/2	31/2	6	1 1/2	1,475	870	1,105	650	460	675	345	510	
2/	21/2	4	211/16	13/4	1,230	565	920	420	945	565	710	420	
3/8	31/4	5	35/8	13/4	2,030	1,230	1,525	920	1,265	905	950	680	
1/	31/4	5	3%16	13/4	1,965	1,395	1,475	1,045	1,235	885	930	665	
1/2	4	61/4	41/2	13/4	2,825	2,000	2,120	1,500	1,600	1,135	1,195	855	
E/	4	6	41/2	13/4	2,795	1,385	2,095	1,035	1,575	1,125	1,185	845	
5/8	51/2	81/2	6%	13/4	4,465	2,535	3,345	1,900	2,375	1,685	1,780	1,265	
2/	51/2	8¾	6%	13/4	4,730	2,760	3,550	2,070	2,350	1,675	1,760	1,255	
3/4	61/4	10	75/16	13/4	5,850	3,275	4,385	2,455	2,795	1,985	2,095	1,490	

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \frac{1}{2}$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>2.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>3.</sup> Interpolation between embedment depths is not permitted.

<sup>4.</sup> The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.

<sup>5.</sup> When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.

<sup>6.</sup> Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# Titen HD® Design Information — Concrete



Titen HD® Tension Design Strengths in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000 \text{ psi}$ )



	Tension Design Strengt							rength (lb.)			
Anchor Dia.	Nominal Embed. Depth (in.)	Minimum End		Lowe	r Flute			Uppe	r Flute		
(in.)		Distance c <sub>min</sub> (in.)	SDC A-B <sup>5</sup>		SDC (	C-F <sup>6,7</sup>	SDC	A-B⁵	SDC (	C-F <sup>6,7</sup>	
	, ,		Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	
1/4	1%	2 1/2	645	275	485	205	1,010	425	760	320	
74	21/2	4	830	350	620	260	1,855	775	1,390	585	
3/8	17/8	21/2	535	245	400	185	710	325	535	245	
98	21/2	35/8	1,240	565	930	425	_	_	_	_	
1/2	2	2 %	840	590	630	440	1,580	1,105	1,185	830	
72	31/2	5 1/4	1,890	1,325	1,420	995	_		_	_	

- 1. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 8. Installation must comply with Figure 1 on page 187.

# Titen HD $^{\odot}$ Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f' $_{\rm C}$ = 3,000 psi) — Static Load



	Nominal Embed.	Minimum End	Allowable Tension Load (lb.)						
Anchor Dia.	Depth	Distance c <sub>min</sub>	Lowe	r Flute	Upper Flute				
(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked			
1/	15/8	21/2	460	195	720	305			
1/4	21/2	4	595	250	1,325	555			
2/	17/8	21/2	380	175	505	230			
3/8	21/2	35/8	885	405	_	_			
1/	2	2%	600	420	1,130	790			
1/2	31/2	51/4	1,350	945	_	_			

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- $2.\,\mbox{Tabulated}$  values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Installation must comply with Figure 1 on page 187.

# Titen HD® Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000 \text{ psi}$ ) — Wind Load







	Nominal Embed.	Minimum End		Allowable Tension Load (lb.)				
Anchor Dia. (in.)	Depth	Distance c <sub>min</sub>	Lower	Flute	Upper	Flute		
()	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked		
1/4	15/8	21/2	385	165	605	255		
74	21/2	4	500	210	1,115	465		
3/8	17/8	21/2	320	145	425	195		
9/8	21/2	3%	745	340	_	_		
1/	2	2%	505	355	950	665		
1/2	31/2	51/4	1,135	795	_	_		

- 1. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = 16.6$  = 1.67. The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.
- 2. Tabulated values are for a single anchor with no influence of another anchor.
- 3. Interpolation between embedment depths is not permitted.
- 4. Installation must comply with Figure 1 on page 187.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Titen HD $^{\circ}$  Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies (f' $_{c}$  = 3,000 psi) — Seismic Load

IBC	1		,
l J		J	

	Nominal	Minimum	Allowable Tension Load (lb.)									
Anchor Dia.	Embed. Depth (in.)	End Distance		Lowe	r Flute			Uppe	r Flute			
(in.)		C <sub>min</sub>	SDC	A-B⁴	SDC (	C-F <sup>5,6</sup>	SDC	SDC A-B⁴		C-F <sup>5,6</sup>		
		(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked		
1/	1 1 1/8	2 1/2	450	195	340	145	705	300	530	225		
1/4	21/2	4	580	245	435	180	1300	545	975	410		
3/8	1 1//8	2 1/2	375	170	280	130	495	230	375	170		
78	21/2	35/8	870	395	650	300	_	_	_	_		
1/2	2	25/8	590	415	440	310	1105	775	830	580		
72	31/2	5 1/4	1325	930	995	695	_	_	_	_		

<sup>1.</sup> Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \frac{1}{0.7} = 1.43$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>2.</sup> Tabulated values are for a single anchor with no influence of another anchor.

<sup>3.</sup> Interpolation between embedment depths is not permitted.

<sup>4.</sup> The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.

<sup>5.</sup> When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.

<sup>6.</sup> Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

<sup>7.</sup> Installation must comply with Figure 1 on page 187.









T': 11D@ A11 11	<b>-</b>	N	
Titen HD® Allowable	: Tension Loads in	ı Normal-VVeight	Concrete

			0.11. 1.5.1	0.111	Tension Load												
Size (in.)	Drill Bit Dia.	Embed. Depth in.	Critical Edge Dist. in.	Critical Spacing in.	f' <sub>c</sub> ≥2,000	osi (13.8 MPa	a Concrete)	f¹ <sub>c</sub> ≥3,000 psi (20.7 MPa Concrete)	f' <sub>c</sub> ≥4,000	osi (27.6 MPa	a Concrete)						
(111.)	(in.)	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)						
		<b>1 ½</b> (38)	<b>6</b> (152)	<b>4</b> (102)	<b>2,070</b> (9.2)	_	<b>520</b> (2.3)	<b>635</b> (2.8)	<b>2,974</b> (13.2)	_	<b>745</b> (3.3)						
3/8 (9.5)	3/8	<b>2¾</b> (70)	3	6	<b>4,297</b> (19.1)	_	<b>1,075</b> (4.8)	<b>1,315</b> (5.8)	<b>6,204</b> (27.6)	_	<b>1,550</b> (6.9)						
		<b>3¾</b> (95)	(76)	(152)	<b>7,087</b> (31.5)	<b>347</b> (1.5)	<b>1,770</b> (7.9)	<b>2,115</b> (9.4)	<b>9,820</b> (43.7)	<b>1,434</b> (6.4)	<b>2,455</b> (10.9)						
		<b>2¾</b> (70)			<b>4,610</b> (20.5)	_	<b>1,155</b> (5.1)	<b>1,400</b> (6.2)	<b>6,580</b> (29.3)	_	<b>1,645</b> (7.3)						
½ (12.7)	1/2	<b>3</b> % (92)	<b>4</b> (102)	<b>8</b> (203)	<b>7,413</b> (33.0)	<b>412</b> (1.8)	<b>1,855</b> (8.3)	<b>2,270</b> (10.1)	<b>10,742</b> (47.8)	<b>600</b> (2.7)	<b>2,685</b> (11.9)						
		<b>5</b> <sup>3</sup> / <sub>4</sub> (146)			<b>10,278</b> (45.7)	<b>297</b> (1.3)	<b>2,570</b> (11.4)	<b>3,240</b> (14.4)	<b>15,640</b> (69.6)	<b>2,341</b> (10.4)	<b>3,910</b> (17.4)						
		<b>2³/4</b> (70)									<b>4,610</b> (20.5)	_	<b>1,155</b> (5.1)	<b>1,400</b> (6.2)	<b>6,580</b> (29.3)	_	<b>1,645</b> (7.3)
5% (15.9)	5/8	<b>4</b> 1/8 (105)	<b>5</b> (127)	<b>10</b> (254)	<b>8,742</b> (38.9)	<b>615</b> (2.7)	<b>2,185</b> (9.7)	<b>2,630</b> (11.7)	<b>12,286</b> (54.7)	<b>1,604</b> (7.1)	<b>3,070</b> (13.7)						
		<b>5</b> <sup>3</sup> ⁄ <sub>4</sub> (146)			<b>12,953</b> (57.6)	<b>1,764</b> (7.8)	<b>3,240</b> (14.4)	<b>3,955</b> (17.6)	<b>18,680</b> (83.1)	_	<b>4,670</b> (20.8)						
		<b>2³/4</b> (70)			<b>4,674</b> (20.8)	_	<b>1,170</b> (5.2)	<b>1,405</b> (6.3)	<b>6,580</b> (29.3)	_	<b>1,645</b> (7.3)						
<sup>3</sup> / <sub>4</sub> (19.1)	3/4	<b>4</b> 5/8 (117)	<b>6</b> (152)	<b>12</b> (305)	<b>10,340</b> (46.0)	<b>1,096</b> (4.9)	<b>2,585</b> (11.5)	<b>3,470</b> (15.4)	<b>17,426</b> (77.5)	<b>1,591</b> (7.1)	<b>4,355</b> (19.4)						
		<b>53%</b> (146)	(555)	<b>13,765</b> (61.2)	<b>1,016</b> (4.5)	<b>3,440</b> (15.3)	<b>4,055</b> (18.0)	<b>18,680</b> (83.1)	<b>1,743</b> (7.8)	<b>4,670</b> (20.8)							

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Refer to allowable load-adjustment factors for spacing and edge distance on pages 198 and 199.
- 3. The minimum concrete thickness is 1½ times the embedment depth.
- 4. Tension and shear loads for the Titen HD anchor may be combined using the elliptical interaction equation (n=%). Allowable load may be interpolated for concrete compressive strengths between 2,000 psi and 4,000 psi.

# Titen HD® Allowable Shear Loads in Normal-Weight Concrete



					Shear Load						
Size (in.)	Drill Bit Dia. (in.)	Embed. Depth in. (mm)	Critical Edge Dist. in. (mm)	Critical Spacing in.	f' <sub>c</sub> ≥2,000 p	osi (13.8 MP	a Concrete)	$f'_c \ge 3,000 \text{ psi}$ (20.7 MPa Concrete)			a Concrete)
	Dia. (iii.)	()	Dist. III. (IIIII)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Ultimate 1b. (kN) 3,668 (16.3) — 9,987 (44.4) 13,027 (57.9) — 9,987 (44.4) 18,607 (82.8) —	Std. Dev. lb. (kN)	Allowable lb. (kN)
		<b>1½</b> (38)	<b>6</b> (152)	<b>4</b> (102)	<b>2,912</b> (13.0)	_	<b>730</b> (3.2)	<b>825</b> (3.7)		_	<b>915</b> (4.1)
<b>3/8</b> (9.5)	3/8	<b>2¾</b> (70)	41/2	6	<b>6,353</b> (28.3)	_	<b>1,585</b> (7.1)	<b>1,665</b> (7.4)	_	_	<b>1,740</b> (7.7)
		<b>3¾</b> (95)	(114)	(152)	<b>6,377</b> (28.4)	<b>1,006</b> (4.5)	<b>1,595</b> (7.1)	<b>1,670</b> (7.4)	_	_	<b>1,740</b> (7.7)
		<b>2¾</b> (70)			<b>6,435</b> (28.6)	_	<b>1,605</b> (7.1)	<b>2,050</b> (9.1)		_	<b>2,495</b> (7.8)
<b>½</b> (12.7)	1/2	<b>3</b> % (92)	<b>6</b> (152)	<b>8</b> (203)	<b>9,324</b> (41.5)	<b>1,285</b> (5.7)	<b>2,330</b> (10.4)	<b>2,795</b> (12.4)		<b>597</b> (2.7)	<b>3,255</b> (14.5)
		<b>5¾</b> (146)			<b>11,319</b> (50.3)	<b>1,245</b> (5.5)	<b>2,830</b> (12.6)	<b>3,045</b> (13.5)	_	_	<b>3,255</b> (14.5)
		<b>2¾</b> (70)			<b>7,745</b> (34.5)	_	<b>1,940</b> (8.6)	<b>2,220</b> (9.9)		_	<b>2,495</b> (7.8)
<b>5%</b> (15.9)	5/8	<b>4</b> 1/8 (105)	<b>7½</b> (191)	<b>10</b> (254)	<b>8,706</b> (38.7)	<b>1,830</b> (8.1)	<b>2,175</b> (9.7)	<b>3,415</b> (15.2)		<b>1,650</b> (7.3)	<b>4,650</b> (20.7)
		<b>5¾</b> (146)			<b>12,498</b> (55.6)	<b>2,227</b> (9.9)	<b>3,125</b> (13.9)	<b>3,890</b> (17.3)	_	_	<b>4,650</b> (20.7)
		<b>2¾</b> (70)			<b>7,832</b> (34.8)	_	<b>1,960</b> (8.7)	<b>2,415</b> (10.7)	<b>11,460</b> (51.0)	_	<b>2,865</b> (12.7)
<b>3/4</b> (19.1)	3/4	<b>4</b> 5/8 (117)	<b>9</b> (229)	<b>12</b> (305)	<b>11,222</b> (49.9)	<b>2,900</b> (12.9)	<b>2,805</b> (12.5)	<b>4,490</b> (20.0)	<b>24,680</b> (109.8)	<b>2,368</b> (10.5)	<b>6,170</b> (27.4)
,		<b>5</b> 3/4 (146)			<b>19,793</b> (88.0)	<b>3,547</b> (15.8)	<b>4,950</b> (22.0)	<b>5,560</b> (24.7)	<b>24,680</b> (109.8)	<b>795</b> (3.5)	<b>6,170</b> (27.4)

- 1. The allowable loads listed are based on a safefy factor of 4.0.
- 2. Refer to allowable load-adjustment factors for spacing and edge distance on pages 198 and 199.
- 3. The minimum concrete thickness is 11/2 times the embedment depth.
- 4. Tension and shear loads for the Titen HD anchor may be combined using the elliptical interaction equation (n=5%). Allowable load may be interpolated for concrete compressive strengths between 2,000 psi and 4,000 psi.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

SIMPSON Strong-Tie

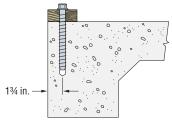
Titen HD® Allowable Shear Loads in Normal-Weight Concrete, Load Applied Parallel to Concrete Edge

LUau F	Load Applied Farallel to Concrete Lage												
Size	Drill Bit	Drill Bit Doubt Edge End Spacing			Shear Load Based on Concrete Edge Distance								
in.	Dia.	Depth in.	Dist.	Dist.	Dist.	f' <sub>c</sub> ≥ 2,500	a) Concrete						
(mm)	in.	(mm)	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)					
		<b>2¾</b> (70)				<b>4,660</b> (20.7)	<b>575</b> (2.6)	<b>1,165</b> (5.2)					
1/2	1/2	<b>31/4</b> (83)	<b>13/4</b> (45)	8	8		_	<b>1,530</b> (6.8)					
(12.7)	1/2	<b>3½</b> (89)		(203)	(203)	<b>6,840</b> (30.4)							
		<b>4½</b> (114)				<b>7,800</b> (34.7)	<b>300</b> (1.3)	<b>1,950</b> (8.7)					
		<b>23/4</b> (70)		<b>4,820</b> (21.4)	<b>585</b> (2.6)	<b>1,205</b> (5.3)							
<b>5%</b> (15.9)	5/8	<b>31/4</b> (83)	<b>13/4</b> (45)	<b>10</b> (254)	<b>10</b> (254)	_	_	<b>1,580</b> (7.0)					
		31/2				7,060	1,284	1,765					

(31.4)

(5.7)

(7.9)



Note: Rebar not shown for clarity.

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. The minimum concrete thickness is 11/2 times the embedment depth.

# Titen HD® Allowable Tension Loads in Normal-Weight Concrete Stemwall

(89)

torriar voight condicto ctornvair										
							Tensio	n Load		
Size in.	Drill Bit Dia. in.	Embed. Depth in. (mm)	Stemwall Width in.	Min. Edge Dist.	Min. End Dist.	f' <sub>c</sub> ≥ 2,5 (17.2 N Concr	ИРа́)	f' <sub>c</sub> ≥ 4,500 psi (31.0 MPa) Concrete		
(mm)			(mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Allow. lb. (kN)	
1/2		10	6	13/4	<b>8</b> (203)	<b>15,420</b> (68.6)	<b>3,855</b> (17.1)	<b>20,300</b> (90.3)	<b>5,075</b> (22.6)	
(12.7)	1/2	(254)	(152)	(45)	<b>4</b> % (111)	<b>14,280</b> (63.5)	<b>3,570</b> (15.9)	<b>19,040</b> (84.7)	<b>4,760</b> (21.2)	

- 1. The allowable loads are based on a safety factor of 4.0.
- 2. The minimum anchor spacing is 15 inches.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

- 3. The minimum concrete thickness (depth) is 12 inches.
- 4. Allowable loads may be interpolated for compressive strengths between 2,500 and 4,500 psi.

Titen HD® Allowable Tension Loads in Normal-Weight Concrete, Load Applied at 60° Angle to Horizontal for Tilt-Up Wall Braces

	Size Drill Bit		Tension Applied at 60 degrees to Horizontal				
Size in. (mm)	Drill Bit Dia. in.	Embed. Depth in. (mm)	f' <sub>c</sub> ≥ 2,500 psi (17.2 M Concrete				
		(11111)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allow. lb. (kN)		
<b>5%</b> (15.9)	5/8	<b>5</b> (127)	<b>13,420</b> (59.7)	<b>1,273</b> (5.7)	<b>3,355</b> (14.9)		
<b>3/4</b> (19.1)	3/4	<b>5</b> (127)	<b>15,180</b> (67.5)	<b>968</b> (4.3)	<b>3,795</b> (16.9)		

- 1. The allowable loads are based on a safety factor of 4.0.
- Anchor must be installed into a concrete floor slab, footing, or deadman with sufficient area, weight, and strength to resist the anchorage load.
- Titen HD<sup>®</sup> has been qualified for temporary outdoor use of up to 90 days through testing for this application.



The Titen HD® screw anchor ¾" x 6" and ¾" x 7" (models THDT75600H and THD75700H) have a 1" section under the head that is unthreaded to allow installation into tilt-up wall braces.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

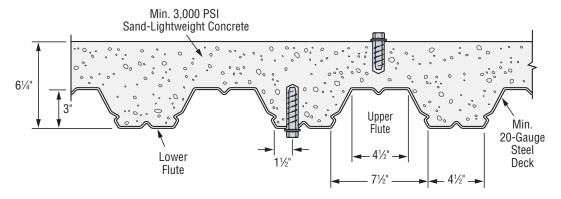


Titen HD® Allowable Tension and Shear Loads in Sand-Lightweight Concrete over Metal Deck

BC	<b>→</b>	

				Critical	Inst	tall in Concrete	(see Figure bel	ow)	Install t	hrough Metal D	eck (see Figure	below)										
Size	Drill	Embed.	Critical Edge	Critical Spacing	Tensio	n Load	Shea	Load	Tensio	n Load	Shear	Load										
in. (mm)	Bit Dia. in.	Depth in. (mm)	Dist. in.	Dist. in.	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Lightweight Concrete		f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Lightweight Concrete		$f'_c \ge 3,000 \text{ psi } (20.7 \text{ MPa})$ Lightweight Concrete		f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Lightweight Concrete											
		(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lbs. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)											
3/8	3/	<b>23/4</b> (70)	6	<b>6</b> (152)	<b>2,560</b> (11.4)	<b>640</b> (2.8)	<b>4,240</b> (18.9)	<b>1,060</b> (4.7)	_	_	_	_										
(9.5)		(152)	(152)	_	_	_	_	<b>5,420</b> (24.1)	<b>1,355</b> (6.0)	<b>4,100</b> (18.2)	<b>1,025</b> (4.6)											
1/2	1/	<b>23/4</b> (70)	8		8	<b>3,040</b> (13.5)	<b>760</b> (3.4)	<b>6,380</b> (28.4)	<b>1,595</b> (7.1)	_	_	_	_									
(12.7)	1/2	(203)	_	_	_		<b>7,020</b> (31.2)	<b>1,755</b> (7.8)	<b>6,840</b> (30.4)	<b>1,710</b> (7.6)												
5/8	5/	<b>2¾</b> (70)	10 10		10 10		10	10	10		0 10	10	10	10	<b>3,100</b> (13.8)	<b>775</b> (3.4)	<b>6,380</b> (28.4)	<b>1,595</b> (7.1)	_	_	_	_
(15.9)			(254)	(254)	_	_	_	_	<b>8,940</b> (39.8)	<b>2,235</b> (9.9)	<b>10,700</b> (47.6)	<b>2,675</b> (11.9)										

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Allowable loads for anchors installed in the lower flute of the steel deck are for flutes with a trapezoidal profile with a depth of 3 inches, and a width varying from 4½ inches at the bottom to 7½ inches at the top. The spacing of the flutes is 12 inches. The metal deck must be minimum 20-gauge with a minimum yield strength of 38 ksi and minimum ultimate strength of 45 ksi.
- 3. Anchors may be installed off-center in the lower flute (up to 11/2" from the edge of the lower flute) without a load reduction.
- 4.100% of the allowable load is permitted at critical edge distance and critical spacing. Testing at smaller edge distances and spacings has not been performed.



Titen HD® screw anchor installed in the top and bottom of a structural sand-lightweight-concrete and metal-deck assembly

# **Titen HD®** Design Information — Masonry



Titen HD® Allowable Tension and Shear Loads in 8" Lightweight, Medium-Weight and Normal-Weight Grout-Filled CMU

Ciout	-1 11160	OIVIO												
Size	Drill	Min. Embed.	Critical Edge	Critical End	Critical Spacing									
in.	Bit Dia.	Depth	Dist.	Dist.	Dist.	Tension Load Shear Load		r Load						
(mm)	in.	in. (mm)	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)					
	Anchor Installed in the Face of the CMU Wall (See Figure 4)													
<b>3/8</b> (9.5)	3/8	<b>2¾</b> (70)	<b>12</b> (305)	<b>12</b> (305)	<b>6</b> (152)	<b>2,390</b> (10.6)	<b>480</b> (2.1)	<b>4,340</b> (19.3)	<b>870</b> (3.9)					
1/2 (12.7)	1/2	<b>3½</b> (89)	<b>12</b> (305)	<b>12</b> (305)	<b>8</b> (203)	<b>3,440</b> (15.3)	<b>690</b> (3.1)	<b>6,920</b> (30.8)	<b>1,385</b> (6.2)					
<b>5/8</b> (15.9)	5/8	<b>4½</b> (114)	<b>12</b> (305)	<b>12</b> (305)	<b>10</b> (254)	<b>5,300</b> (23.6)	<b>1,060</b> (4.7)	<b>10,420</b> (46.4)	<b>2,085</b> (9.3)					
3/4	3/.	51/2	12	12	12	7,990	1,600	15,000	3,000					

1. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.

(35.5)

(7.1)

(66.7)

- 2. Values for 8-inch-wide, lightweight, medium-weight and normal-weight concrete masonry units.
- 3. The masonry units must be fully grouted.
- 4. The minimum specified compressive strength of masonry,  $f'_{m}$ , at 28 days is 1,500 psi.
- 5. Embedment depth is measured from the outside face of the concrete masonry unit.

(140) (305) (305) (305)

- 6. Allowable loads may be increased 331/3% for short-term loading due to wind or seismic forces where permitted by code.
- 7. Grout-filled CMU wall design must satisfy applicable design standards and be capable of withstanding applied loads.
- 8. Refer to allowable load-adjustment factors for spacing and edge distance on page 200.

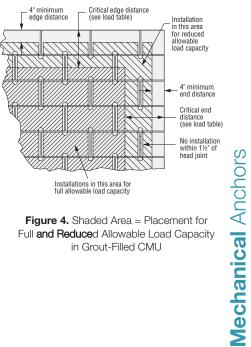
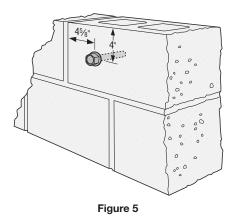


Figure 4. Shaded Area = Placement for Full and Reduced Allowable Load Capacity in Grout-Filled CMU

# Titen HD® Allowable Tension and Shear Loads in 8" Lightweight, Medium-Weight and Normal-Weight Hollow CMU

C:	Drill	Embed.	Min. Edge	Min.	8-ir		MU Loads Based Strength				
Size in. (mm)	Bit Dia.	Depth⁴ in.	Dist. in.	End Dist. in.	Tensio	n Load	oad Shear Load				
()	in.	(mm)	(mm) (mm)		Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)			
	Anchor Installed in Face Shell (See Figure 5)										
<b>3/8</b> (9.5)	3/8	<b>13/4</b> (45)	<b>4</b> (102)	<b>4</b> 5/8 (117)	<b>720</b> (3.2)	<b>145</b> (0.6)	<b>1,240</b> (5.5)	<b>250</b> (1.1)			
<b>½</b> (12.7)	1/2	<b>13/4</b> (45)	<b>4</b> (102)	<b>4</b> 5/8 (117)	<b>760</b> (3.4)	<b>150</b> (0.7)	<b>1,240</b> (5.5)	<b>250</b> (1.1)			
<b>5%</b> (15.9)	5/8	<b>13/4</b> (45)	<b>4</b> (102)	<b>4</b> 5/8 (117)	<b>800</b> (3.6)	<b>160</b> (0.7)	<b>1,240</b> (5.5)	<b>250</b> (1.1)			
<b>3/4</b> (19.1)	3/4	<b>13/4</b> (45)	<b>4</b> (102)	<b>4</b> 5/8 (117)	<b>880</b> (3.9)	<b>175</b> (0.8)	<b>1,240</b> (5.5)	<b>250</b> (1.1)			

- 1. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.
- 2. Values for 8-inch-wide, lightweight, medium-weight and normal-weight concrete masonry units.
- 3. The minimum specified compressive strength of masonry, f'm, at 28 days is 1,500 psi.
- 4. Embedment depth is measured from the outside face of the concrete masonry unit and is based on the anchor being embedded an additional ½" through 1 ¼" thick face shell.
- 5. Allowable loads may not be increased for short-term loading due to wind or seismic forces. CMU wall design must satisfy applicable design standards and be capable of withstanding applied loads.
- 6. Do not use impact wrenches to install in hollow CMU.
- 7. Set drill to rotation-only mode when drilling into hollow CMU.



<sup>\*</sup> See page 12 for an explanation of the load table icons.

(15.9)

# Titen HD® Design Information — Masonry



Titen HD® Allowable Tension and Shear Loads in 8" Lightweight, Medium-Weight and Normal-Weight Grout-Filled CMU Stemwall

							00. 00				
<b>2</b> 1	Drill	Embed.	Min.	Min.	Critical	8-inch	Grout-Filled (	CMU Allowab	le Loads Bas	sed on CMU S	Strength
Size in.	in. Dia.	Depth in.	Dist.	End Dist.	Spacing Dist. in. (mm)	Tension		Shear Per	p. to Edge	Shear Parallel to Edge	
(mm) D	in.	(mm)	in. (mm)			Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
			And	chor Ins	talled in Ce	ell Opening o	r Web (Top o	f Wall) (See F	igure 6)		
<b>½</b> (12.7)	1/2	<b>4½</b> (114)	<b>13/4</b> (45)	<b>8</b> (203)	<b>8</b> (203)	<b>2,860</b> (12.7)	<b>570</b> (2.5)	<b>800</b> (3.6)	<b>160</b> (0.7)	<b>2,920</b> (13.0)	<b>585</b> (2.6)

570

(2.5)

800

(3.6)

(0.7)

3,380

(15.0)

(3.0)

- 1. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.
- 2. Values are for 8-inch-wide, lightweight, medium-weight and normal-weight concrete masonry units.

(254)

3. The masonry units must be fully grouted.

(114)

(45)

(254)

- 4. The minimum specified compressive strength of masonry,  $f'_{\it m}$ , at 28 days is 1,500 psi.
- 5. Allowable loads may be increased 331/4% for short-term loading due to wind or seismic forces where permitted by code.

2,860

(12.7)

- 6. Grout-filled CMU wall design must satisfy applicable design standards and be capable of withstanding applied design loads.
- 7. Loads are based on anchor installed in either the web or grout-filled cell opening in the top of wall.

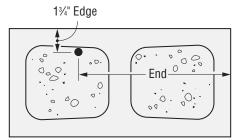


Figure 6. Anchor Installed in top of wall

# Titen HD® Design Information — Masonry



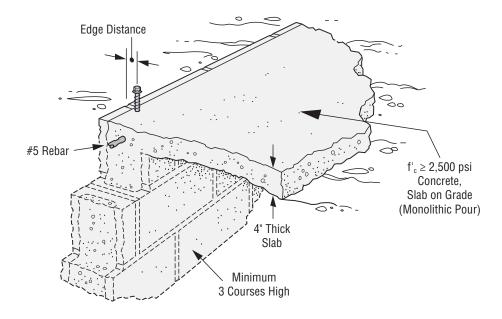
Titen HD $^{\otimes}$  Allowable Tension Loads for 8" Lightweight, Medium-Weight and Normal-Weight CMU Chair Blocks Filled with Normal-Weight Concrete

IBC	<b>1</b>	
-----	----------	--

Size in.	Drill Bit Dia.	Min. Embed. Depth	Min. Edge Dist.	Critical Spacing	8-inch Concrete-Filled CMU Chair Block Allowable Tension Loads Based on CMU Strength				
(mm)	(in.)	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)			
		<b>2</b> % (60)	<b>13/4</b> (44)	<b>9½</b> (241)	<b>3,175</b> (14.1)	<b>635</b> (2.8)			
<b>3/8</b> (9.5)	3/8	<b>3</b> % (86)	<b>1</b> 3/ <sub>4</sub> (44)	<b>13½</b> (343)	<b>5,175</b> (23.0)	<b>1,035</b> (4.6)			
		<b>5</b> (127)	<b>21/4</b> (57)	<b>20</b> (508)	<b>10,584</b> (47.1)	<b>2,115</b> (9.4)			
1/2	1/2	<b>8</b> (203)	<b>21/4</b> (57)	<b>32</b> (813)	<b>13,722</b> (61.0)	<b>2,754</b> (12.2)			
(12.7)	72	<b>10</b> (254)	<b>21/4</b> (57)	<b>40</b> (1016)	<b>16,630</b> (74.0)	<b>3,325</b> (14.8)			
5/8	5/8	<b>5½</b> (140)	<b>13/4</b> (44)	<b>22</b> (559)	<b>9,025</b> (40.1)	<b>1,805</b> (8.1)			
(15.9)	9/8	<b>12</b> (305)	<b>21/4</b> (57)	<b>48</b> (1219)	<b>18,104</b> (80.5)	<b>3,620</b> (16.1)			

<sup>1.</sup> The tabulated allowable loads are based on a safety factor of 5.0.

<sup>3.</sup> Center #5 rebar in CMU cell and concrete slab as shown in the illustration below.



C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>2.</sup> Values are for 8-inch-wide concrete masonry units (CMU) filled with concrete, with minimum compressive strength of 2,500 psi and poured monolithically with the floor slab.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



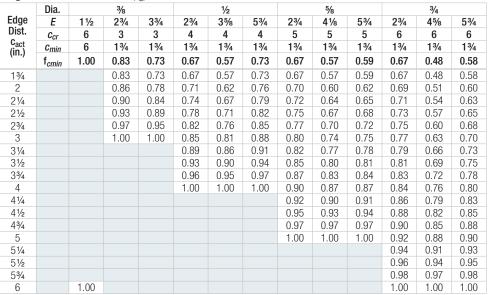
Load Adjustment Factors for Titen HD® Anchors in Normal-Weight Concrete: Edge Distance, Tension and Shear Loads

# How to use these charts:

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- Locate the anchor embedment (E) used for either a tension and/or shear load application.
- 4. Locate the edge distance ( $c_{act}$ ) at which the anchor is to be installed.
- The load adjustment factor (f<sub>c</sub>) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load adjustment factor(s).
- 7. Reduction factors for multiple edges are multiplied together.

I₽Ć

# Edge Distance Tension (f<sub>c</sub>)



See notes below.

# Edge Distance Shear (f<sub>c</sub>)

	Dia.		3/8		1/2				5/8			3/4		
Edge	Ε	11/2	23/4	3¾	23/4	35/8	53/4	23/4	41/8	53/4	23/4	45/8	5¾	
Dist.	Ccr	6	41/2	41/2	6	6	6	71/2	71/2	71/2	9	9	9	
c <sub>act</sub> (in.)	Cmin	6	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	13/4	1¾	
(,	f <sub>cmin</sub>	1.00	0.25	0.24	0.25	0.20	0.17	0.19	0.16	0.19	0.19	0.14	0.13	
13/4			0.25	0.24	0.25	0.20	0.17	0.19	0.16	0.19	0.19	0.14	0.13	
2			0.32	0.31	0.29	0.25	0.22	0.23	0.20	0.23	0.22	0.17	0.16	
21/2			0.45	0.45	0.38	0.34	0.32	0.30	0.27	0.30	0.27	0.23	0.22	
3			0.59	0.59	0.47	0.44	0.41	0.37	0.34	0.37	0.33	0.29	0.28	
31/2			0.73	0.72	0.56	0.53	0.51	0.44	0.42	0.44	0.39	0.35	0.34	
4			0.86	0.86	0.65	0.62	0.61	0.51	0.49	0.51	0.44	0.41	0.40	
41/2			1.00	1.00	0.74	0.72	0.71	0.58	0.56	0.58	0.50	0.47	0.46	
5					0.82	0.81	0.80	0.65	0.63	0.65	0.55	0.53	0.52	
51/2					0.91	0.91	0.90	0.72	0.71	0.72	0.61	0.58	0.58	
6		1.00			1.00	1.00	1.00	0.79	0.78	0.79	0.66	0.64	0.64	
61/2								0.86	0.85	0.86	0.72	0.70	0.70	
7								0.93	0.93	0.93	0.78	0.76	0.76	
71/2								1.00	1.00	1.00	0.83	0.82	0.82	
8											0.89	0.88	0.88	
81/2											0.94	0.94	0.94	
9											1.00	1.00	1.00	

The tabled adjustment values ( $f_c$ ) have been calculated using the following information:

- 1. E = Embedment depth (inches).
- 2.  $c_{act}$  = actual edge distance at which anchor is installed (inches).
- 3.  $c_{cr}$  = critical edge distance for 100% load (inches).
- 4.  $c_{min}$  = minimum edge distance for reduced load (inches).
- 5.  $f_C$  = percent of allowable load at actual edge distance.
- 6.  $f_{CCT}$  = percentage of allowable load at critical edge distance.  $f_{CCT}$  is always = 1.00.
- 7. f<sub>cmin</sub> = percent of allowable load at minimum edge
- 8.  $f_c = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min}) / (c_{cr} c_{min})].$

<sup>\*</sup> See page 12 for an explanation of the load table icons



Load Adjustment Factors for Titen HD® Anchors in Normal-Weight Concrete: Edge Distance, Tension and Shear Loads

# How to use these charts:

- 1. The following tables are for reduced edge distance.
- 2. Locate the anchor size to be used for either a tension and/or a shear load application.
- 3. Locate the anchor embedment (E) used for either a tension and/or a shear load application.
- 4. Locate the edge distance ( $s_{act}$ ) at which the anchor is to be installed.
- 5. The load adjustment factor (f<sub>s</sub>) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load adjustment factor(s).
- 7. Reduction factors for multiple edges are multiplied together.

# Spacing Tension (f<sub>s</sub>)

	Dia.	3/8				1/2			5/8		3/4		
	Ε	1 1/2	23/4	3¾	23/4	35/8	53/4	23/4	41/8	5¾	23/4	45/8	53/4
s <sub>act</sub> (in)	Scr	4	6	6	8	8	8	10	10	10	12	12	12
(111)	Smin	4	1 1/2	1 1/2	2	2	2	21/2	21/2	21/2	3	3	3
	f <sub>smin</sub>	1.00	0.66	0.56	0.72	0.63	0.76	0.79	0.69	0.73	0.80	0.70	0.72
1													
1 ½			0.66	0.56									
2			0.70	0.61	0.72	0.63	0.76						
21/2			0.74	0.66	0.74	0.66	0.78	0.79	0.69	0.73			
3			0.77	0.71	0.77	0.69	0.80	0.80	0.71	0.75	0.80	0.70	0.72
4		1.00	0.85	0.80	0.81	0.75	0.84	0.83	0.75	0.78	0.82	0.73	0.75
5			0.92	0.90	0.86	0.82	0.88	0.86	0.79	0.82	0.84	0.77	0.78
6			1.00	1.00	0.91	0.88	0.92	0.89	0.83	0.86	0.87	0.80	0.81
7					0.95	0.94	0.96	0.92	0.88	0.89	0.89	0.83	0.84
8					1.00	1.00	1.00	0.94	0.92	0.93	0.91	0.87	0.88
9								0.97	0.96	0.96	0.93	0.90	0.91
10								1.00	1.00	1.00	0.96	0.93	0.94
11											0.98	0.97	0.97
12											1.00	1.00	1.00

See notes below

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# Spacing Shear (f<sub>s</sub>)

	Dia.					1/2			5/8			3/4	
	Ε	1 1/2	23/4	3¾	23/4	35/8	53/4	23/4	41/8	53/4	23/4	45/8	5¾
s <sub>act</sub> (in)	Scr	4	0	0	0	0	0	0	0	0	0	0	0
(111)	Smin	4	0	0	0	0	0	0	0	0	0	0	0
	f <sub>smin</sub>	1.00	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77
1													
1 1/2			0.77	0.77	0.88								
2			0.80	0.80	0.77	0.77	0.77						
21/2			0.82	0.82	0.79	0.79	0.79	0.77	0.77	0.77			
3			0.85	0.85	0.81	0.81	0.81	0.79	0.79	0.79	0.77	0.77	0.77
4		1.00	0.90	0.90	0.85	0.85	0.85	0.82	0.82	0.82	0.80	0.80	0.80
5			0.95	0.95	0.89	0.89	0.89	0.85	0.85	0.85	0.82	0.82	0.82
6			1.00	1.00	0.92	0.92	0.92	0.88	0.88	0.88	0.85	0.85	0.85
7					0.96	0.96	0.96	0.91	0.91	0.91	0.87	0.87	0.87
8					1.00	1.00	1.00	0.94	0.94	0.94	0.90	0.90	0.90
9								0.97	0.97	0.97	0.92	0.92	0.92
10								1.00	1.00	1.00	0.95	0.95	0.95
11											0.97	0.97	0.97
12											1.00	1.00	1.00

The tabled adjustment values  $(f_s)$  have been calculated using the following information:

- 1.E = Embedment depth (inches).
- 2.  $s_{act}$  = actual spacing distance at which anchors are installed (inches).
- 3.  $s_{cr}$  = critical spacing distance for 100% load (inches).
- 4.  $s_{min}$  = minimum spacing distance for reduced load (inches)
- 5. f<sub>s</sub> = adjustment factor for allowable load at actual spacing distance.
- 6.  $f_{SCT}$  = adjustment factor for allowable load at critical spacing distance.  $f_{SCT}$  is always = 1.00.
- 7. f<sub>smin</sub> = adjustment factor for allowable load at minimum spacing distance.
- 8.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **Titen HD®** Design Information — Masonry



# Load-Adjustment Factors for Titen HD® Anchors in Face-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance and Spacing, Tension and Shear Loads

# How to use these charts:

- 1. The following tables are for reduced edge distance and spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the embedment (E) at which the anchor is to be installed.
- 4. Locate the edge distance ( $c_{act}$ ) or spacing ( $s_{act}$ ) at which the anchor is to be installed.
- 5. The load adjustment factor ( $f_c$  or  $f_s$ ) is the intersection of the row and column.
- 6. Multiply the allowable load by the applicable load adjustment factor.
- 7. Reduction factors for multiple edges or spacings are multiplied together.

# Edge or End Distance Tension (f<sub>c</sub>)

0			( 0)			
	Dia.	3F8	1/2	5F8	3F4	IBC *
	E	4 1/2	31/2	4 1/2	4 1/2	
c <sub>act</sub> (in.)	C <sub>cr</sub>	12	12	12	12	
()	C <sub>min</sub>	4	4	4	4	27 22
	f <sub>cmin</sub>	1.00	1.00	0.83	0.66	(==/=
4		1.00	1.00	0.83	0.66	
6		1.00	1.00	0.87	0.75	
8		1.00	1.00	0.92	0.83	/ I
10		1.00	1.00	0.96	0.92	
12		1.00	1.00	1.00	1.00	

See notes below

# Edge or End Distance Shear (f<sub>c</sub>) Shear Load Perpendicular to Edge or End (Directed Towards Edge or End)

Lago o	TENA (BITO)	stoa rovvar	ac Lago or	L 10)		
	Dia.	3/8	1/2	5/8	3/4	IBC '
	E	23/4	3 1/2	4 1/2	5 1/2	IDO
c <sub>act</sub> (in.)	c <sub>cr</sub>	12	12	12	12	<b>→</b>
(111.)	C <sub>min</sub>	4	4	4	4	20 20
	f <sub>cmin</sub>	0.58	0.38	0.30	0.21	(====
4		0.58	0.38	0.30	0.21	
6		0.69	0.54	0.48	0.41	
8		0.79	0.69	0.65	0.61	
10		0.90	0.85	0.83	0.80	
12		1.00	1.00	1.00	1.00	

- 1. E = Embedment depth (inches).
- $2. c_{act}$  = actual end or edge distance at which anchor is installed (inches).
- 3.  $c_{cr}$  = critical end or edge distance for 100% load (inches).
- 4. c<sub>min</sub> = minimum end or edge distance for reduced load (inches).
- 5. f<sub>c</sub> = adjustment factor for allowable load at actual end or edge distance.
- 6.  $f_{ccr}$  = adjustment factor for allowable load at critical end or edge distance.  $f_{ccr}$  is always = 1.00.
- 7. f<sub>cmin</sub> = adjustment factor for allowable load at minimum end or edge distance.
- $8.\,f_{c} = f_{cmin} + \left[ \left( 1 f_{cmin} \right) \left( c_{act} c_{min} \right) / \left( c_{cr} c_{min} \right) \right].$

# Spacing Tension (f<sub>s</sub>)

	Dia.	3/8	1/2	5/8	3/4	IB
	E	2¾	3 1/2	4 1/2	5 1/2	
s <sub>act</sub> (in.)	Scr	6	8	10	12	1
(111.)	S <sub>min</sub>	3	4	5	6	87
	f <sub>smin</sub>	0.87	0.69	0.59	0.50	<u></u>
3		0.87				世
4		0.91	0.69			<u>-</u>
5		0.96	0.77	0.59		14
6		1.00	0.85	0.67	0.50	
8			1.00	0.84	0.67	
10				1.00	0.83	
12					1.00	

- 1. E = Embedment depth (inches).
- $2. s_{act}$  = actual spacing distance at which anchors are installed (inches).
- $3. s_{cr}$  = critical spacing distance for 100% load (inches).
- 4.  $s_{min}$  = minimum spacing distance for reduced load (inches).
- $5.\,f_{\rm S}=$  adjustment factor for allowable load at actual spacing distance.
- $6.\,f_{SCr}$  = adjustment factor for allowable load at critical spacing distance.  $f_{SCr}$  is always = 1.00.
- 7.  $f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.
- 8.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$

# \* See page 12 for an explanation of the load table icons.

# Edge and End Distance Shear (f<sub>c</sub>) Shear Load Parallel to Edge or End

	Dia.	3/8	1/2	5/8	3/4	
_	Е	23/4	31/2	41/2	41/2	
c <sub>act</sub> (in.)	C <sub>cr</sub>	12	12	12	12	
(111.)	C <sub>min</sub>	4	4	4	4	
	f <sub>cmin</sub>	0.77	0.48	0.46	0.44	
4		0.77	0.48	0.46	0.44	
6		0.83	0.61	0.60	0.58	
8		0.89	0.74	0.73	0.72	
10		0.94	0.87	0.87	0.86	
12		1.00	1.00	1.00	1.00	

See notes below

# Edge or End Distance Shear (f<sub>c</sub>) Shear Load Perpendicular to Edge or End (Directed Away From Edge or End)

	Dia.	3/8	1/2	5/8	3/4
_	E	23/4	31/2	4 1/2	51/2
c <sub>act</sub> (in.)	C <sub>cr</sub>	12	12	12	12
(111.)	Cmin	4	4	4	4
	f <sub>cmin</sub>	0.89	0.79	0.58	0.38
4		0.89	0.79	0.58	0.38
6		0.92	0.84	0.69	0.54
8		0.95	0.90	0.79	0.69
10		0.97	0.95	0.90	0.85
12		1.00	1.00	1.00	1.00



# S

Spacin	g Shea	ar (f <sub>s</sub> )				
	Dia.	3/8	1/2	5/8	3/4	IBC
_	Е	23/4	31/2	4 1/2	51/2	ibu
s <sub>act</sub> (in.)	Scr	6	8	10	12	$\Rightarrow$
(111.)	S <sub>min</sub>	3	4	5	6	20 E2
	f <sub>smin</sub>	0.62	0.62	0.62	0.62	(##J#
3		0.62				
4		0.75	0.62			n_n
5		0.87	0.72	0.62		/←→\
6		1.00	0.81	0.70	0.62	
8			1.00	0.85	0.75	
10				1.00	0.87	
12					1.00	

# Titen HD® Rod Coupler

SIMPSON
Strong-Tie

The Titen HD® Rod Coupler is designed to be used in conjunction with a single or multi-story rod tiedown system. This anchor provides a fast and simple way to attach threaded rod to a concrete stem wall or thickened slab footing. Unlike adhesive anchors, the installation requires no special tools, cure time or secondary setting process; just drill a hole and drive the anchor.

# **Features**

- The serrated cutting teeth and patented thread design enable the Titen HD Rod Coupler to be installed quickly and easily. Less installation time translates to lower installed cost
- The specialized heat treating process creates tip hardness to facilitate cutting while the body remain ductile
- No special setting tools are required. The Titen HD Rod Coupler installs with regular or hammer drill, ANSI size bits and standard sockets
- Compatible with threaded rods in 3/8" and 1/2" diameters

Material: Carbon steel

Coating: Zinc plated

# Installation



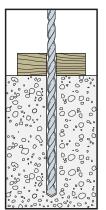
**Caution:** Oversized holes in the base material will reduce or eliminate the mechanical interlock of the threads with base material and will reduce the anchor's load capacity. Use a Titen HD® Rod Coupler one time only. Installing the anchor multiple times may result in excessive thread wear and reduce load capacity.

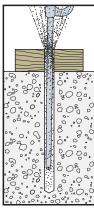
- Drill a hole using the specified diameter carbide bit into the base material to a depth of at least ½" deeper than the required embedment.
- 2. Blow the hole clean of dust and debris using compressed air. Overhead application need not be blown clean.
- 3. Tighten the anchor with appropriate size socket until the head sits flush against base material.

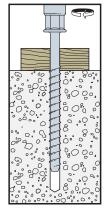


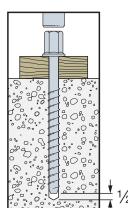
Titen HD® Rod Coupler U.S. Patent 5,674,035 & 6,623,228

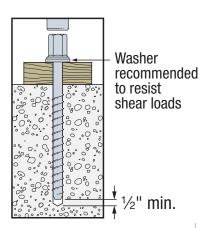
# Installation Sequence:











# Titen HD® Rod Coupler



# Titen HD® Rod Coupler Product Data

Size	Model	Accepts Rod	Drill Bit	Wrench	Quantity		
(in)	No.	Dia. (in.)	Dia. (in)	Size (in)	Вох	Carton	
3/8 x 63/4	THD37634RC	3/8	3/8	9/16	50	100	
½ x 9¾	THD50934RC	1/2	1/2	3/4	20	40	

# Titen HD® Rod Coupler Allowable Tension Loads in Normal-Weight Concrete Stemwall







Size	Drill Bit	Embed. Depth	Stemwall Width	Minimum Edge	Minimum End	Minimum Spacing	acing		Tension Load Based on Connected Rod Strength
in. (mm)	Dia. in.	in. (mm)	in. (mm)	Dist. in. (mm)	Dist. in. (mm)	Dist. in. (mm)		si (17.2 MPa) crete	A307 (SAE 1018)
							Ultimate lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
<b>3/8</b> (9.5)	3/8	<b>5</b> (127)	<b>8</b> (203)	<b>1¾</b> (45)	<b>10</b> (254)	<b>20</b> (508)	<b>8,900</b> (39.6)	<b>2,225</b> (9.9)	<b>2,105</b> (9.4)
1/2 (12.7)	1/2	<b>8</b> (203)	<b>8</b> (203)	<b>1</b> 3/4 (45)	<b>16</b> (406)	<b>32</b> (813)	<b>15,540</b> (69.1)	<b>3,885</b> (17.3)	<b>3,750</b> (16.7)

- 1. Allowable load must be the lesser of the concrete or steel strength.
- 2. The allowable loads based on concrete strength are based on a factor of safety of 4.0.
- 3. The allowable load based on steel strength is limited by the strength of the coupler nut supplied with this anchor. Use of higher strength rod will not increase allowable loads.
- 4. The minimum concrete thickness is 1.5 times the embedment depth.
- 5. Tension and shear loads may be combined using the straight-line interaction equation (n=1).

# Titen HD® Rod Coupler Allowable Shear Loads in Normal-Weight Concrete Stemwall, Load Applied Parallel to Concrete Edge







Size in. (mm)	Drill Bit Dia. in.	Drill Bit Depth Width Edge Dist.  Dia. in in Dist. in in	in.	Minimum Spacing Dist. in.	Shear Load Based on Conc. Edge Dist. f' <sub>c</sub> ≥ 2500 psi (17.2 MPa) Concrete			
(11111)			(mm)		(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)
<b>½</b> (12.7)	1/2	<b>8</b> (203)	<b>8</b> (203)	<b>13/4</b> (45)	<b>16</b> (406)	<b>32</b> (813)	<b>6,200</b> (27.6)	<b>1,550</b> (6.9)

- 1. Install with a washer (not supplied with anchor) when used to resist shear loads.
- 2. The allowable load based on concrete edge distance is based on a factor of safety of 4.0. Steel strength does not control.
- 3. The minimum concrete thickness is 1.5 times the embedment depth.
- 4. Tension and shear loads may be combined using the straight-line interaction equation (n=1).

# Titen® Concrete and Masonry Screw



Titen® screws are hardened screws for attaching all types of components to concrete and masonry. These fasteners are commonly used in applications such as attaching electrical boxes, light fixtures or window frames into concrete or masonry base materials.

# **Features**

- Available in 3/16" and 1/4" diameter sizes
- · Available in hex and Phillips flat-head designs in two colors
- Drill bit included with each box

Material: Carbon steel

Coating: Zinc plated with a baked-on ceramic coating

Codes: Florida FL-2355.1

# Installation



Caution: Industry studies show that hardened fasteners can experience performance problems in wet or corrosive environments. Steps must be taken to prevent inadvertent sustained loads above the listed allowable loads. Overtightening and bending moments can initiate cracks detrimental to the hardened screw's performance. Use the Simpson Strong-Tie installation tool kit. It is designed to reduce the potential for overtightening the screw.

**Caution:** Oversized holes in the base material will reduce or eliminate the mechanical interlock of the threads with the base material and will reduce the anchor's load capacity.

- 1. Drill a hole in the base material using the appropriate diameter carbide drill bit as specified in the table. Drill the hole to the specified embedment depth plus ½" to allow the thread tapping dust to settle and blow it clean using compressed air. Overhead installations need not be blown clean. Alternatively, drill the hole deep enough to accommodate embedment depth and dust from drilling and tapping.
- Position fixture, insert screw and tighten using drill and installation tool fitted with a hex socket or phillips bit.

Preservative-treated wood applications: suitable for use in non-ammonia formulations of CCA, ACQ-C, ACQ-D, CA-B, BX/DOT and zinc borate. Use in dry, interior environments only.

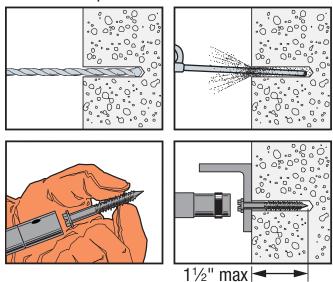
Use caution not to damage ceramic barrier coating during installation. Recommendations are based on testing and experience at time of publication and may change. Simpson Strong-Tie cannot provide estimates on service life of screws.



Titen® Hex-Head Screw (H)

**Titen®**Phillips Flat-Head
Screw (PF)

# Installation Sequence





Titen® Phillips head screw available in white and standard blue

# Titen® Concrete and Masonry Screw



# Blue Titen® Product Data (3/16" diameter)

Size	Model No.1	Drill Bit Diameter	Quantity		
(in.)	Would No.	(in.)	Box <sup>2</sup>	Carton	
3/16 X 1 1/4	TTN18114H			1600	
3/16 X 1 3/4	TTN18134H			500	
3/16 X 2 1/4	TTN18214H			500	
3/16 X 23/4	TTN18234H	5/32	100	500	
3/16 X 3 1/4	TTN18314H			400	
3/16 X 3 3/4	TTN18334H			400	
3/16 X 4	TTN18400H			400	
3/16 X 1 1/4	TTN18114PF			1600	
3/16 X 1 3/4	TTN18134PF			500	
3/16 X 2 1/4	TTN18214PF			500	
3/16 X 23/4	TTN18234PF	5/32	100	500	
3/16 X 3 1/4	TTN18314PF			400	
3/16 X 3 3/4	TTN18334PF			400	
3/16 X 4	TTN18400PF			400	

<sup>1.</sup> H Suffix: Hex-Head, PF Suffix: Phillips Flat-Head.

# Blue Titen® Product Data (1/4" diameter)

Size	Model No.1	Drill Bit Diameter	Quantity			
(in.)	Model No.	(in.)	Box <sup>2</sup>	Carton		
1/4 x 1 1/4	TTN25114H			1600		
1/4 x 1 3/4	TTN25134H			500		
1/4 x 2 1/4	TTN25214H			500		
1/4 x 2 3/4	TTN25234H			500		
1/4 x 3 1/4	TTN25314H	3/16	100	400		
1/4 x 3 3/4	TTN25334H			400		
1/4 x 4	TTN25400H			400		
1/4 x 5	TTN25500H			400		
1/4 x 6	TTN25600H			400		
1/4 x 1 1/4	TTN25114PF			1600		
1/4 x 1 3/4	TTN25134PF			500		
1/4 x 2 1/4	TTN25214PF			500		
1/4 x 2 3/4	TTN25234PF			500		
1/4 x 3 1/4	TTN25314PF	3/16	100	400		
1/4 x 3 3/4	TTN25334PF			400		
1/4 x 4	TTN25400PF			400		
1/4 x 5	TTN25500PF			400		
1/4 x 6	TTN25600PF			400		

<sup>1.</sup> H Suffix: Hex-Head, PF Suffix: Phillips Flat-Head.

# White Titen® Product Data (Phillips Flat-Head)

Size	Model No.	Drill Bit Diameter	Quantity			
(in.)	Model No.	(in.)	Box <sup>1</sup>	Carton		
3/16 X 1 1/4	TTNW18114PF			1600		
3/16 X 1 3/4	TTNW18134PF			500		
3/16 X 2 1/4	TTNW18214PF	5/32	100	500		
3/16 X 23/4	TTNW18234PF	732	100	500		
3/16 X 3 1/4	TTNW18314PF			400		
3/16 X 3 3/4	TTNW18334PF			400		
1/4 x 1 1/4	TTNW25114PF			1600		
1/4 X 1 3/4	TTNW25134PF			500		
1/4 x 2 1/4	TTNW25214PF	2/	100	500		
1/4 x 2 3/4	TTNW25234PF	3/16	100	500		
1/4 x 3 1/4	TTNW25314PF			400		
1/4 x 3 3/4	TTNW25334PF			400		

Titen® Allowable Tension and Shear Loads in Face Shell of Hollow and Grout-Filled CMU



Dia.	Drill Bit	Embed. Depth	Critical Spacing in. (mm)		Values for 6" or 8" Lightweight, Medium-Weight or Normal-Weight CMU					
in. (mm)	Dia. in.	in. (mm)			Tensio	n Load	Shear Load			
					Avg. Ult. lb. (kN)	Allow. lb. (kN)	Avg. Ult. lb. (kN)	Allow. lb. (kN)		
<b>3/16</b> (4.8)	5/32	<b>1</b> (25.4)	<b>2 ½</b> (57.2)	<b>1 1/8</b> (28.6)	<b>542</b> (2.4)	<b>110</b> (0.5)	<b>1,016</b> (4.5)	<b>205</b> (0.9)		
<b>1/4</b> (6.4)	3/16	<b>1</b> (25.4)	<b>3</b> (76.2)	<b>1 ½</b> (38.1)	<b>740</b> (3.3)	<b>150</b> (0.7)	<b>1,242</b> (5.5)	<b>250</b> (1.1)		

- 1. The tabulated allowable loads are based on a safety factor of 5.0.
- 2. Maximum anchor embedment is 1 1/2" (38.1 mm).

# Titen® Allowable Tension and Shear Loads in Normal-Weight Concrete



	Drill Bit Dia. in.	Embed. Depth in. (mm)	Critical Spacing in. (mm)	Critical Edge Dist. in. (mm)		Tensio		Shear Load			
Dia. in.						$f'_c \ge 2,000 \text{ psi}$ (13.8 MPa) Concrete		$f'_c \ge 4,000 \text{ psi}$ (27.6 MPa) Concrete		$f'_c \ge 2,000 \text{ psi}$ (13.8 MPa) Concrete	
(mm)					Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	
3/16 (4.8)	5/32	<b>1</b> (25.4)	<b>2 ½</b> (57.2)	<b>1 1/8</b> (28.6)	<b>500</b> (2.2)	<b>125</b> (0.6)	<b>640</b> (2.8)	<b>160</b> (0.7)	<b>1,020</b> (4.5)	<b>255</b> (1.1)	
3/16 (4.8)	5/32	<b>1 ½</b> (38.1)	<b>2 ½</b> (57.2)	<b>1 </b>	<b>1,220</b> (5.4)	<b>305</b> (1.4)	<b>1,850</b> (8.2)	<b>460</b> (2.0)	<b>1,670</b> (7.4)	<b>400</b> (1.8)	
<b>1/4</b> (6.4)	3/16	<b>1</b> (25.4)	<b>3</b> (76.2)	<b>1 ½</b> (38.1)	<b>580</b> (2.6)	<b>145</b> (0.6)	<b>726</b> (3.2)	<b>180</b> (0.8)	<b>900</b> (4.0)	<b>225</b> (1.0)	
<b>1/4</b> (6.4)	3/16	<b>1 ½</b> (38.1)	<b>3</b> (76.2)	<b>1 ½</b> (38.1)	<b>1,460</b> (6.5)	<b>365</b> (1.6)	<b>2,006</b> (8.9)	<b>500</b> (2.2)	<b>1,600</b> (7.1)	<b>400</b> (1.8)	

- 1. Maximum anchor embedment is 11/2" (38.1 mm).
- 2. Concrete must be minimum 1.5 x embedment.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Titen® Stainless Steel Concrete and Masonry Screw



Stainless Steel Titen® screws are ideal for attaching various types of components to concrete and masonry, such as fastening electrical boxes or light fixtures. They offer the versatility of our standard Titen screws with enhanced corrosion protection. Available in hex and Phillips flat head.

# **Features**

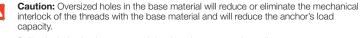
- Suitable for concrete, brick, grout-filled CMU and hollow-block applications
- Suitable for some preservative-treated wood applications
- · Acceptable for exterior use
- Titen drill bits included in each box
- Available in lengths from 11/4"-4"

Material: Type 410 stainless steel

Coating: Zinc plated with a protective overcoat

### Installation

Caution: Industry studies show that hardened fasteners can experience performance problems in wet or corrosive environments. Steps must be taken to prevent inadvertent sustained loads above the listed allowable loads. Overtightening and bending moments can initiate cracks detrimental to the hardened screw's performance. Use the Simpson Strong-Tie Titen installation tool kit as it has a bit that is designed to reduce the potential for overtightening the screw.



- 1. Drill a hole in the base material using the appropriate diameter carbide drill bit as specified in the table. Drill the hole to the specified embedment depth plus ½" to allow the thread tapping dust to settle and blow it clean using compressed air. Overhead installations need not be blown clean. Alternatively, drill the hole deep enough to accommodate embedment depth and dust from drilling and tapping.
- 2. Position fixture, insert screw and tighten using drill and Titen screw installation tool fitted with a hex socket or phillips bit.

Preservative-treated wood applications: suitable for use in non-ammonia formulations of CCA, ACQ-C, ACQ-D, CA-B, SBX/DOT and zinc borate. Acceptable for use in exterior environments. Use caution not to damage coating during installation. The 410 stainless-steel Titen with top coat provides "medium" corrosion protection. Recommendations are based on testing and experience at time of publication and may change. Simpson Strong-Tie cannot provide estimates on service life of screws.

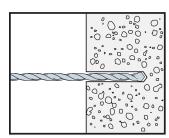


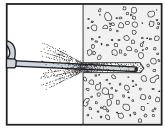
Titen®
Stainless-Steel
Phillips Flat Head Screw
(PFSS)



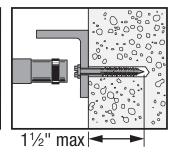
Titen® Stainless-Steel Hex-Head Screw (HSS)

# Installation Sequence









# Titen® Stainless Steel Concrete and Masonry Screw

# Stainless-Steel Titen® Product Data

Size	Head	Model No.	Drill Bit	Qua	ntity
(in.)	Style	wodel No.	Dia. (in.)	Box	Carton
1/4 x 1 1/4		TTN25114HSS		100	1600
1/4 X 1 3/4		TTN25134HSS		100	500
1/4 x 2 1/4		TTN25214HSS		100	500
1/4 x 2 3/4	Hex-Head	TTN25234HSS	3/16	100	500
1/4 x 3 1/4		TTN25314HSS		100	400
1/4 x 3 3/4		TTN25334HSS		100	400
1/4 x 4		TTN25400HSS		100	400
1/4 X 1 1/4		TTN25114PFSS		100	1600
1/4 x 1 3/4		TTN25134PFSS		100	500
1/4 x 2 1/4	DI 1111	TTN25214PFSS		100	500
1/4 x 2 3/4	Phillips Flat-Head	TTN25234PFSS	3/16	100	500
1/4 x 3 1/4		TTN25314PFSS		100	400
1/4 x 3 3/4		TTN25334PFSS		100	400
1/4 x 4		TTN25400PFSS		100	400

One drill bit is included in each box.

Stainless-Steel Titen® Allowable Tension and Shear Loads in Normal-Weight Concrete

|--|

				0		Tensio	n Load		Shear	Load							
Dia. in. (mm)	Drill Bit Dia. in.	Bit Dia.	Bit Dia.	Bit Depth Dia. in.	Depth Spacin. in	Depth in.	Depth Spacing in.	pth Spacing n. in.	pth Spacing in.	Spacing in.	Critical Edge Dist. in.	ge $1^{\circ}_{c} \ge 2,000 \text{ psi}$ st. $(13.8 \text{ MPa})$		f' <sub>c</sub> ≥ 4,000 psi (27.6 MPa) Concrete		f' <sub>c</sub> ≥ 2,000 psi (13.8 MPa) Concrete	
		(mm)	(mm) (mm)	(mm) (mm)		Ultimate lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Allow. lb. (kN)						
1/ <sub>4</sub> (6.4)	3/16	<b>1</b> (25.4)	<b>3</b> (76.2)	<b>1 ½</b> (38.1)	<b>600</b> (2.7)	<b>150</b> (0.7)	<b>935</b> (4.2)	<b>235</b> (1.0)	<b>760</b> (3.4)	<b>190</b> (0.8)							
1/ <sub>4</sub> (6.4)	3/16	<b>1 ½</b> (38.1)	<b>3</b> (76.2)	<b>1 ½</b> (38.1)	<b>1,040</b> (4.6)	<b>260</b> (1.2)	<b>1,760</b> (7.8)	<b>440</b> (2.0)	<b>810</b> (3.6)	<b>200</b> (0.9)							

- 1. Maximum anchor embedment is 11/2" (38.1 mm).
- 2. Minimum concrete thickness is 1.5 x embedment.

# Stainless-Steel Titen® Allowable Tension and Shear Loads in Face Shell of Hollow and Grout-Filled CMU



Dia.	Drill	Embed. Critical Critical Edge				8" Lightwe Normal-Wei		
in.	Bit Dia.	Depth Spacing in.	Spacing in.	Dist.	Tension Load		Shear	Load
(mm)	in.	(mm)	(mm)	in. (mm)	Ultimate lb. (kN)	Allow. lb. (kN)	Ultimate lb. (kN)	Allow. lb. (kN)
<b>1/4</b> (6.4)	3/16	<b>1</b> (25.4)	<b>4</b> (101.6)	<b>1 ½</b> (38.1)	<b>550</b> (2.4)	<b>110</b> (0.5)	<b>495</b> (2.2)	100 (0.4)

- 1. The tabulated allowable loads are based on a safety factor of 5.0.
- 2. Maximum anchor embedment is 1  $\ensuremath{\ensuremath{\%^{\text{\tiny{II}}}}}$  (38.1 mm).

# Titen® Screw - Installation Accessories



# Titen® Screw - Installation Tool

The Simpson Strong-Tie® Titen® screw installation kit makes installation of Titen screws quick and easy. Accessories are compatible with a standard three-jaw style chuck, and the sockets have been designed to prevent over-torquing, which can lead to fastener failure. Comes packaged in a rugged plastic box ideal for storage of the installation kit and Titen screws.

# Eight-piece kit includes:

- Drill bit holder
- · Phillips bit socket
- 5¾" sleeve
- #2 and #3 Phillips bits
- 1/4" and 5/16" hex sockets
- Allen wrench

# Titen® Installation Tool

Model	Quantity				
No.	Вох	Carton			
TTNT01	1	24			



Titen®
Screw Installation Kit
(Model TTNT01)





Special hex adapter (included with the Titen Screw Installation Kit) allows the Titen Installation Tool to slide over the bit and lock in, ready to drive screws.

# Titen® Screw - Drill Bits

The same bits that come included with boxes of Titen screws are also available separately. They work with the Titen Installation Tool as well as drills with a standard three-jaw style chuck.

# Titen® Drill Bits

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

Size	Model	Use With		Qua	ntity
(in.)	No.	Screw	Length	Box	Carton
5/32 X 3 1/2	MDB15312		To 13/4		48
5/ <sub>32</sub> x 4 1/ <sub>2</sub>	MDB15412	3⁄16" dia.	To 31/4	12	
5/32 X 5 1/2	MDB15512	ula.	To 4		
3/16 X 3 1/2	MDB18312	4711	To 13/4	12	48
3/16 X 4 1/2	MDB18412	1⁄4" dia.	To 31/4		
3/16 X 5 1/2	MDB18512	uia.	To 4		



Titen® Screw Drill Bit

# Titen® Screw - SDS-Plus Drill Bit/Driver

This SDS-Plus shank bit works with the Titen Installation Tool to allow pre-drilling and installation of Titen screws using a rotohammer. Rotohammer must be in rotation-only mode before driving screws.

Titen® Drill Bit/Driver Product Data

Size (in.)	Model No.	For Screw Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)
5⁄32 X 5	MDBP15500H		21/4	5
5⁄32 X 6	MDBP15600H	3/16	31/4	6
5⁄32 X 7	MDBP15700H		4 1/4	7
3∕16 X 5	MDBP18500H		21/4	5
3∕16 X 6	MDBP18600H	1/4	31/4	6
3∕16 X 7	MDBP18700H		4 1/4	7

Titen drivers are sold individually.



Titen®
Screw Drill Bit / Driver

# Titen HD® Threaded Rod Hanger

SIMPSON
Strong-Tie

The Titen HD® threaded rod hanger is a high-strength screw anchor designed to suspend threaded rod from concrete slabs and beams or concrete over metal in order to hang pipes, cable trays and HVAC equipment. The anchor offers low installation torque with no secondary setting, and has been tested to offer industry-leading performance in cracked and uncracked concrete – even in seismic loading conditions.

# Cracked Concrete CODE LISTED

### **Features**

- Thread design undercuts to efficiently transfer the load to the base material
- Serrated cutting teeth and patented thread design enable quick and easy installation
- Specialized heat-treating process creates tip hardness to facilitate cutting while the anchor body remains ductile
- Designed to install using a rotary hammer or hammer drill with standard ANSI drill bits – no special tools required
- Installs with standard-sized sockets
- The THD50234RH and THD37212RH are code listed for cracked and uncracked concrete applications under the 2012 and 2009 IBC/IRC, per ICC-ES ESR-2713

**Codes:** ICC-ES ESR-2713 (THD37212RH and THD50234RH); City of L.A. RR25741; Florida FL-15730.6; Factory Mutual 3031136 (THD50234RH and THD37218RH) and 3035761 (THD37212RH)

Material: Carbon steel
Coating: Zinc plated



- Caution: Oversized holes in the base material will reduce or eliminate the mechanical interlock of the threads with base material and will reduce the anchor's load capacity.
  - Caution: Use a Titen HD® Rod Hanger one time only. Installing the anchor multiple times may result in excessive thread wear and reduce load capacity.

    1. Drill a hole using the specified diameter carbide bit into the
  - Drill a hole using the specified diameter carbide bit into the base material to a depth of at least ½" deeper than the required embedment.
  - 2. Blow the hole clean of dust and debris using compressed air.
  - 3. **IMPORTANT:** Install with an applied torque of 15 ft-lbs for the THD25112RH and THD37218RH rod hangers using a torque wrench, driver drill, hammer drill or cordless 1/4" impact driver with a maximum permitted torque rating of 100 ft-lb.



THD50234RH (%" dia. shank)



**THD37218RH** (1/4" dia. shank)



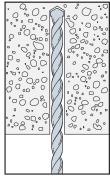
THD37212RH

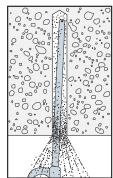
(%" dia. shank)

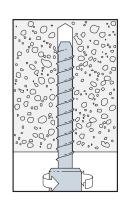
**THD25112RH** (1/4" dia. shank)

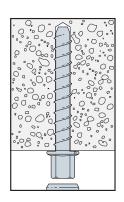
U.S. Patent 5,674,035 & 6,623,228

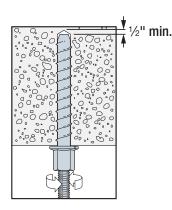
# Installation Sequence











# **Titen HD®** Rod Hanger Design Information — Concrete



Titen HD® Threaded Rod Hanger Product Data

	Size	Model	Accepts Rod Dia.	Drill Bit Dia.	Wrench Size	Min. Embed.	Qua	ntity
	(in.)	No.	(in.)	(in.)	(in.)	(in.)	Вох	Carton
	1/4 x 1 1/2	THD25112RH	1/4	1/4	3/8	1 ½	100	500
	3/8 x 2 1/8	THD37218RH	3/8	1/4	1/2	21/8	50	250
)	3/8 X 21/2	THD37212RH	3/8	3/8	1/2	21/2	50	200
	½ x 2¾	THD50234RH	1/2	3/8	11/16	23/4	50	100

Titen HD® Threaded Rod Hanger Installation Information and Additional Data<sup>1</sup>

Characteristic	Cumbal	Units	Model I	Number
Gnaracteristic	Symbol	Units	THD37212RH	THD50234RH
	Installation Info	ormation		
Rod Hanger Diameter	do	in.	3/8	1/2
Drill Bit Diameter	d <sub>bit</sub>	in.	3/8	3/8
Maximum Installation Torque <sup>2</sup>	T <sub>inst,max</sub>	ftlb.	50	50
Maximum Impact Wrench Torque Rating <sup>3</sup>	T <sub>impact,max</sub>	ftlb.	150	150
Minimum Hole Depth	h <sub>hole</sub>	in.	3	31/4
Embedment Depth	h <sub>nom</sub>	in.	21/2	23/4
Effective Embedment Depth	h <sub>ef</sub>	in.	1.77	1.77
Critical Edge Distance	C <sub>ac</sub>	in.	211/16	211/16
Minimum Edge Distance	C <sub>min</sub>	in.	1:	3/4
Minimum Spacing	S <sub>min</sub>	in.		3
Minimum Concrete Thickness	h <sub>min</sub>	in.	41/4	41/4
	Anchor D	ata		
Yield Strength	f <sub>ya</sub>	psi	97,	000
Tensile Strength	f <sub>uta</sub>	psi	110	,000
Minimum Tensile and Shear Stress Area	$A_{Se}$	in.²	0.099	0.099
Axial Stiffness in Service Load Range – Uncracked Concrete	$eta_{uncr}$	lb./in.	715	,000
Axial Stiffness in Service Load Range – Cracked Concrete	$eta_{cr}$	lb./in.	345	,000

<sup>1.</sup> The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D.

 $<sup>2.</sup>T_{\mathit{inst,max}}$  is the maximum permitted installation torque for installations using a torque wrench.

<sup>3.</sup> T<sub>impact,max</sub> is the maximum permitted torque rating for impact wrenches.

# Titen HD® Rod Hanger Design Information — Concrete



Titen HD® Threaded Rod Hanger Tension Strength Design Data for Installations in Concrete<sup>1,6</sup>

IBC	
	1 1







Characteristic	Cumbal	Unito	Model N	lumber				
Gnaracteristic	Symbol	Units	THD37212RH	THD50234RH				
Anchor Category	1, 2 or 3	_	1					
Embedment Depth	h <sub>nom</sub>	in.	2½	23/4				
Steel St	rength in Tension (ACI 3	18 Section D.5.1)						
Tension Resistance of Steel	N <sub>sa</sub>	lb.	10,890	10,890				
Strength Reduction Factor – Steel Failure <sup>2</sup>	$\phi_{_{SA}}$	_	0.6	65				
Concrete Breakout Strength in Tension (ACI 318 Section D.5.2) <sup>6</sup>								
Effective Embedment Depth	h <sub>ef</sub>	in.	1.77	1.77				
Critical Edge Distance	$c_{ac}$	in.	211/16	211/16				
Effectiveness Factor – Uncracked Concrete	Kuncr	_	24					
Effectiveness Factor – Cracked Concrete	k <sub>cr</sub>	_	17					
Modification Factor	$\psi_{c,N}$	_	1.	0				
Strength Reduction Factor — Concrete Breakout Failure <sup>5</sup>	$\phi_{cb}$	_	0.6	65				
Pullout S	trength in Tension (ACI 3	318 Section D.5.3) <sup>6</sup>						
Pullout Resistance – Uncracked Concrete $(\mathbf{f'}_c = 2,500 \text{ psi})$	N <sub>p,uncr</sub>	lb.	2,025³	2,025³				
Pullout Resistance — Cracked Concrete $(f'_c = 2,500 \text{ psi})$	N <sub>p,cr</sub>	lb.	1,235³	1,235³				
Strength Reduction Factor – Pullout Failure <sup>4</sup>	$\phi_{ ho}$	_	0.65					
Tension Strength	n for Seismic Application	ns (ACI 318 Section D.3.	3) <sup>6</sup>					
Nominal Pullout Strength for Seismic Loads $(f'_c = 2,500 \text{ psi})$	$N_{p,eq}$	lb.	1,235³	1,235³				
Strength Reduction Factor – Pullout Failure <sup>4</sup>	$\phi_{eq}$		0.6	65				

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. The value of φ applies when the load combinations of ACI 318 Section 9.2 are used. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of φ. Anchors are considered brittle steel elements.
- Adjust the characteristic pullout resistance for other concrete compressive strengths by multiplying the tabular value by (f'<sub>c,specified</sub>/2,500)<sup>0.5</sup>.
- 4. The value of  $\phi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 5. The value of  $\varphi$  applies when both the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition B are met. If the load combinations of ACI 318 Section 9.2 are used and the requirements of Section D.4.3(c) for Condition A are met, refer to Section D.4.3 to determine the appropriate value of  $\phi$ . If the load combinations of ACI 318 Appendix C are used, refer to Section D.4.4 to determine the appropriate value of  $\phi$ .
- 6. For sand-lightweight concrete, the modification factor for concrete breakout strength must be taken as 0.6. Additionally, the pullout strength  $N_{p,uncr}$ ,  $N_{p,cr}$  and  $N_{p,eq}$  must be multiplied by 0.6, as applicable.
- 7. For sand-lightweight concrete, in lieu of ACI 318 Section D.3.6, modify the value of concrete breakout strength,  $N_{p,cr}$ ,  $N_{p,uncr}$  and  $N_{eq}$  by 0.6. All-lightweight concrete is beyond the scope of this table.



Titen HD® Threaded Rod Hanger Tension Strength Design Data for Installations in the Lower and Upper Flute of Normal-Weight or Sand-Lightweight Concrete Through Metal Deck<sup>1,2,5,6</sup>

IBC	1	*
	200.2	

Characteristic	Cumbol	Units	Model No.		
Gilai actei istic	Symbol	Units	THD37212RH	THD50234RH	
Minimum Hole Depth	h <sub>hole</sub>	in.	3	31/4	
Embedment Depth	h <sub>nom</sub>	in.	21/2	23/4	
Effective Embedment Depth	h <sub>ef</sub>	in.	1.77	1.77	
Pullout Resistance — Cracked Concrete <sup>2,3,4</sup>	N <sub>p,deck,cr</sub>	lbf.	870	870	
Pullout Resistance – Uncracked Concrete <sup>2,3,4</sup>	N <sub>p,deck,uncr</sub>	lbf.	1,430	1,430	

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318 Appendix D, except as modified below.
- 2. Concrete compressive strength shall be 3,000 psi minimum. The characteristic pullout resistance for greater compressive strengths shall be increased by multiplying the tabular value by (f'<sub>c,specified</sub>/3,000 psi)<sup>0.5</sup>.
- 3. For anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies, as shown in Figure 1, calculation of the concrete breakout strength may be omitted.
- 4. In accordance with ACI 318 Section D.5.3.2, the nominal pullout strength in cracked concrete for anchors installed in the soffit of sand-lightweight or normal-weight-concrete-over-metal-deck floor and roof assemblies N<sub>p,deck,cr</sub> shall be substituted for N<sub>p,cr</sub>. Where analysis indicates no cracking at service loads, the normal pullout strength in uncracked concrete N<sub>p,deck,uncr</sub> shall be substituted for N<sub>p,uncr</sub>.
- 5. Minimum distance to edge of panel is 2hef.
- 6. The minimum anchor spacing along the flute must be the greater of  $3h_{\it ef}$  or 1.5 times the flute width.

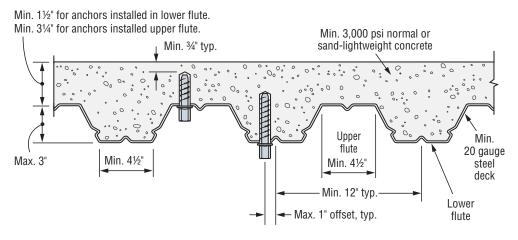


Figure 1. Installation in Concrete Over Metal Deck

Titen HD® Threaded Rod Hanger Allowable Tension Loads in Normal-Weight Concrete



							Tensio	n Load	
Model Number	Rod Hanger Dia.		Depth	Critical Edge Distance (in.)	Critical Spacing Distance (in.)	f' <sub>c</sub> ≥ 2, Con	000 psi crete	$f'_c \ge 4$ , Con	000 psi crete
	(in.)					Ultimate (lb.)	Allowable (lb.)	Ultimate (lb.)	Allowable (lb.)
THD25112RH	1/4	1/4	1½	3	6	1,319	330	2,102	525
THD37218RH	3/8	1/4	21/8	3	6	2,210	555	3,227	805
THD37212RH	3/8	3/8	2½	3	6	3,650	915	5,275	1,320
THD50234RH	1/2	3/8	2¾	3	6	4,297	1,075	6,204	1,550

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Allowable loads may not be increased for short-term loading due to wind or seismic forces.
- 3. Refer to allowable load-adjustment factors for spacing and edge distance on pages 198 and 199.
- 4. The minimum concrete thickness is 11/2 times the embedment depth.
- 5. Allowable load may be interpolated for concrete compressive strengths between 2,000 psi and 4,000 psi.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Wood Rod Hanger Threaded Rod Anchor System



Simpson Strong-Tie's wood rod hanger is a one-piece fastening system for suspending ¼" or %" threaded rod. Vertical rod hangers are designed to suspend threaded rod in overhead applications from wood members. Horizontal rod hangers are available for applications requiring installation into the side of joists, columns and overhead members. Both rod hangers provide attachment points for use in pipe hanging, fire protection, electrical conduit and cable-tray applications. Recommended for use in dry, interior, non-corrosive environments only.

# **Features**

- Threaded anchors for rod-hanging applications in wood
- Suitable for installation horizontally or vertically in overhead applications
- No pre-drilling required
- Easily installed with a drill or screw gun
- Type-17 tip provides for fast starts
- UL/FM Listed

Material: Carbon steel
Coating: Zinc plated







Rod Diameter	Size	Madal Na	Application	Point Style	Quantity	
in.	3126	Model No.	Аррисации	ruiit Style	Box	Carton
1/4	1⁄4" x 2"	RWV25200				
3/8	1⁄4" x 1"	RWV37100	Vertical	Type 17	25	250
3/8	1/4" x 2"	RWV37200	vertical			230
3/8	5/16" X 21/2"	RWV37212				
1/4	1⁄4" x 1"	RWH25100				
3/8	1⁄4" x 2"	RWH37200	Horizontal	Type 17	25	250
3/8	5/16" x 21/2"	RWH37212				

# Nut Driver

Model No.	Description	Quantity			
Model No.	Description	Box	Carton		
RND62	Nut Driver	1 blister	10		



Vertical Wood Rod Hanger (RWV)



Horizontal Wood Rod Hanger (RWH)



Type-17 point for use in wood



Nut Driver RND62

# **Wood Rod Hanger** Design Information — Wood



# **IBC**

IBC

# C 🛊

**Mechanical** Anchors

# Vertical Wood Rod Hanger Allowable Loads

						Loads														
Model No.	Rod Diameter	Size (in.)	Minimum Edge Dist.	Minimum End Dist.	Minimum Spacing	[	)F	5	SP .	S	PF	UL Approval	FM Approval							
(in.)	(in.) (in	(in.)	(in.)	Ultimate lb.	Allowable lb.	Ultimate lb.	Allowable lb.	Ultimate lb.	Allowable lb.	Pipe Size in.	Pipe Size in.									
RWV25200	1/4	1/4 x 2	3/4									1,875	375	2,165	435	1,540	310	_	_	
RWV37100	3/8	1⁄4 x 1		23/4	2¾	2¾	2¾	4 23/4	2¾	23/4	23/4	2¾	765	155	950	190	525	105	_	_
RWV37200	3/8	1/4 x 2				1,875	375	2,165	435	1,540	310	3	_							
RWV37212	3/8	5/16 X 21/2		31/4	31/4	3,015	605	2,960	590	2,470	495	4	4							

- 1. Load values are based on full shank penetration into the wood member.
- 2. Allowable loads may be increased by CD = 1.6 for wind or earthquake.
- 3. Allowable loads are based on a factor of safety of 5.0.
- 4. Mechanical and plumbing design codes may prescribe lower allowable loads. Verify with local codes.
- 5. Allowable loads are based on Douglas Fir-Larch (DF), Southern Pine (SP) and Spruce-Pine-Fir (SPF) wood members having a minimum specific gravity of 0.50, 0.55 and 0.42, respectively.

# Horizontal Wood Rod Hanger Allowable Loads

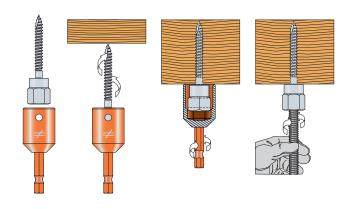
	D. d		ge End	Minimum - Spacing	Loads						III Approval		
	Size						SP		SPF		UL Approval		
	(in.)	(In.)   Dist	Distance (in.)	Distance (in.)	istance   ' <sub>(in )</sub>		Allowable lb.	Ultimate lb.	Allowable lb.	Ultimate lb.	Allowable lb.	Pipe Size (in.)	
RWH25100	1/4	1⁄4 x 1	1	00/	03/ 03/	23/4	555	110	680	135	430	85	_
RWH37200	3/8	1/4 x 2	01/	2¾	294	1,205	240	1,115	225	1,650	330	3	
RWH37212	3/8	5/16 X 2 1/2	21/2	31/4	31/4	1,145	230	1,320	265	1,190	240	3	

- 1. Load values are based on full shank penetration into the wood member.
- 2. Allowable loads may not be increased for short-term loading.
- 3. Allowable loads are based on a factor of safety of 5.0.
- Mechanical and plumbing design codes may prescribe lower allowable loads. Verify with local codes.
- Allowable loads are based on Douglas Fir-Larch (DF), Southern Pine (SP) and Spruce-Pine-Fir (SPF) wood members having a minimum specific gravity of 0.50, 0.55 and 0.42, respectively.

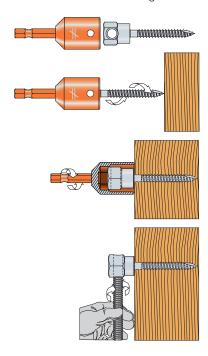
# Installation Sequence

- 1. Attach RND62 nut driver to a drill.
- 2. Insert rod hanger into the RND62 nut driver.
- 3. Using rotation-only mode, drive rod hanger until it contacts the surface. Do not over-tighten. RND62 nut driver will
- disengage the rod hanger at the appropriate depth to prevent over-driving.
- 4. Insert threaded rod. Minimum thread engagement should be equal to the nominal diameter of the threaded insert.

# Vertical Wood Rod Hanger



# Horizontal Wood Rod Hanger



<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Blue Banger Hanger® Cast-In-Place, Internally Threaded Insert



# Wood-Form Insert

Multi-thread, cast-in-place wood-form and metal-deck inserts for cracked and uncracked concrete maximize jobsite efficiency and reduce inventory commitment. Also available in metal-roof-deck insert version, offering a low-profile design that does not interfere with roofing material.

### **Features**

- Code listed under the IBC/IRC in accordance with AC446 for cracked and uncracked concrete applications, per ICC-ES ESR-3707
- Multi-thread design allows insert to accept multiple rod diameters
- Blue plastic ring acts as an insert locator when forms are removed
- Plastic ring creates a countersunk recess to keep internal threads clean from concrete residue
- Nails snap off with a hammer strike after the forms are removed

Material: Carbon steel

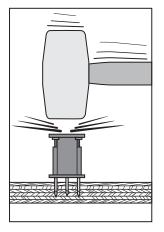
Coating: Yellow zinc dichromate coating

Codes: ICC-ES ESR-3707; Factory Mutual 3024378 (see pipe size limit tables); Underwriters Laboratories File Ex3605 (see pipe size limit tables)

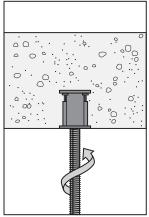
# Installation

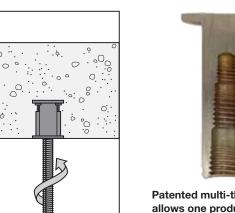
- 1. Strike the top of the hanger and drive the 3 mounting nails into the forming material until the bottom of the hanger is flush with the bottom of the plywood. The hanger should be sitting 90° from the forming material.
- 2. Once concrete is hardened and forms are stripped, strike the mounting nails to break them off.
- 3. Insert the rod into the sleeve and thread it into the hanger.

# Installation Sequence











# **Product Data**

Hanger Type	For Rod Diameter (in)	Model Number	Carton Qty.
	1/4, 3/8, 1/2	BBWF2550	200
Wood-Form Insert	3/8, 1/2, 5/8	BBWF3762	150
	5/8, 3/4	BBWF6275	150







# Blue Banger Hanger® Cast-In-Place, Internally Threaded Insert



# Metal-Deck Insert

## **Features**

- Code-listed under the IBC/IRC in accordance with AC446 for cracked and uncracked concrete applications, per ICC-ES ESR-3707
- Multi-thread design allows insert to accept multiple rod diameters
- Compression spring keeps insert perpendicular to deck, even if bumped or stepped on after installation
- 3" plastic sleeve keeps internal threads clean and provides guidance to align threaded rod with the internal threads
- Extended sleeve length allows easy location of insert even with fireproofing on the underside of the deck
- Installed height of 2" allows insert to be used on top of or between deck flutes

Material: Carbon steel

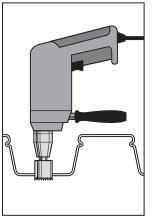
Coating: Yellow zinc dichromate coating

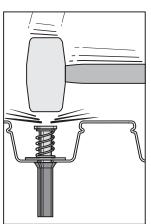
**Codes:** ICC-ES ESR-3707; Factory Mutual 3024378 (see pipe size limit tables); Underwriters Laboratories File Ex3605 (see pipe size limit tables)

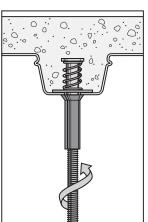
## Installation

- 1. Drill a hole in the metal deck using the appropriate diameter bit as referenced in the table.
- Insert the hanger in the hole and strike the top so that the plastic sleeve is forced through the hole and expands against the bottom side of the deck. The anchor can also be installed by stepping on it.
- 3. Insert the rod into the sleeve and thread it into the hanger.

# Installation Sequence









Patented multi-thread design allows one product to handle up to three rod diameters.

# Product Data

Hanger Type	For Rod Diameter (in)	Deck Hole Diameter (in)	Model Number	Carton Qty.
Metal-Deck Insert	1/4, 3/8, 1/2	13/16 — 7/8	BBMD2550	100
	3/8, 1/2, 5/8	11/8 - 13/16	BBMD3762	50
	5/8, 3/4	13/16 - 11/4	BBMD6275	50





# Blue Banger Hanger® Cast-In-Place, Internally Threaded Insert



# Metal-Roof-Deck Insert

# **Features**

- Multi-thread design: The insert accepts three different rod diameters
- Low-profile design does not interfere with roofing material
- Positive attachment to the roof deck prevents spinning and keeps the hanger in position
- Pre-staked, self-drilling screws allow quick installation

Material: Carbon steel

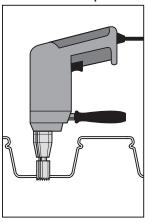
Coating: Yellow zinc dichromate coating

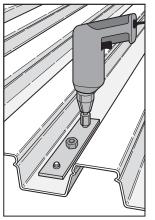
# Installation

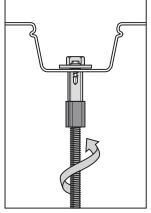
- 1. Drill a hole in the metal deck using the appropriate diameter bit as referenced in the table.
- 2. Insert the hanger into the hole and fasten to the deck with the two pre-staked screws provided.
- 3. Insert the rod into the sleeve and thread it into the hanger.



# Installation Sequence



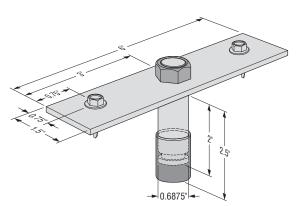






# Product Data

Hanger Type	For Rod Diameter (in.)	Deck Hole Diameter (in.)	Model Number	Carton Qty.
Roof-Deck Insert	1/4, 3/8, 1/2	7/8	BBRD2550	50



**Mechanical** Anchors

# **Blue Banger Hanger®** Design Information — Concrete



### Wood-Form Insert: Tension and Shear Strength Design Data<sup>1,2,3,4,5,6,8</sup>

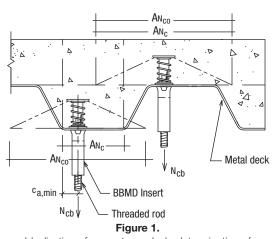


Design Information	Symbol	Units		Model No.	
บิธิรโซที แบบเกิลแบบ	Symbol	Ullita	BBWF2550	BBWF3762	BBWF6275
Insert outside diameter <sup>7</sup>	d <sub>a</sub>	in.	0.811	1.00	1.102
Effective embedment depth	h <sub>ef</sub>	in.	1.875	1.954	1.875
Insert steel characterization	-	_		Non-ductile	
Modification factor for insert tension strength for inserts located in a region of a concrete member where analysis indicates no cracking at service load levels	$\Psi_{c,N}$	-	1.25	1.25	1.25
Nominal tension strength of single insert in tension as governed by steel strength	N <sub>sa,insert</sub>	lb.	8,415	16,755	18,685
Nominal seismic tension strength of single insert in tension as governed by steel strength	N <sub>sa,insert,eq</sub>	lb.	7,695	8,195	7,695
Nominal steel shear strength of single insert	V <sub>sa</sub>	lb.	6,810	8,210	8,760
Nominal steel shear strength of single insert for seismic loading	V <sub>sa,eq</sub>	lb.	6,810	8,210	8,760

- 1. Concrete must be normal-weight or lightweight concrete with f'c of 3,000 psi minimum. 5. Strength reduction factor for load combinations of ACI 318 Section 9.2 governed
- 2. Only the largest size of threaded rod specified for each insert must be used for applications resisting shear loads.
- 3. Design of headed cast-in specialty inserts shall be in accordance with the provisions of ACI 318 Appendix D for cast-in headed anchors. The value of  $k_c$ shall be in accordance with the value for cast-in anchors in D.5.2.2.
- 4. Strength reduction factors shall be taken from ACI 318-11 D.4.3 for cast-in headed anchors.
- by steel strength shall be taken as 0.65 for tension and 0.60 for shear.
- 6. The concrete tension strength of headed cast-in specialty inserts shall be calculated in accordance with ACI 318 Appendix D.
- 7. Insert outside diameter = outside diameter of plastic sleeve.
- 8. The strengths shown in the table are for inserts only. Design professional is responsible for checking threaded rod strength in tension, shear and combined tension and shear, as applicable.

Metal-Deck Insert: Tension and Shear Strength Design Data <sup>1,2</sup>	al-Deck Insert: Tension and Shear Strength Design Data <sup>1,2,3,4,5,6,8</sup>								
Design Information	Symbol	Units		Model No.					
200.3	<b>- - - - - - - - - -</b>	55	BBMD2550	BBMD3762	BBMD6275				
Insert outside diameter <sup>7</sup>	da	in.	0.94	1.16	1.29				
Effective embedment depth	h <sub>ef</sub>	in.	1.98	1.98	1.98				
Insert steel characterization	_	_		Non-ductile					
Modification factor for insert tension strength for inserts located in a region of a concrete member where analysis indicates no cracking at service load levels	$\Psi_{c,N}$	_	1.25	1.25	1.25				
Nominal tension strength of single insert in tension as governed by steel strength	N <sub>sa,insert</sub>	lb.	10,085	16,655	14,200				
lominal seismic tension strength of single insert in tension as governed by steel strength	N <sub>sa,insert,eq</sub>	lb.	7,920	7,920	7,920				
Nominal steel shear strength of single insert in the soffit of concrete on metal deck, lower flute	V <sub>sa,deck,lower</sub>	lb.	3,105	2,610	3,345				
Nominal steel shear strength of single insert in the soffit of concrete on metal deck, upper flute	V <sub>sa,deck,upper</sub>	lb.	3,500	1,710	5,565				
Nominal steel shear strength of single insert in the soffit of concrete on metal deck, for seismic loading, lower flute	V <sub>sa,deck,lower,eq</sub>	lb.	3,105	2,610	3,345				
Nominal steel shear strength of single insert in the soffit of concrete on metal deck, for seismic loading, upper flute	V <sub>sa,deck,upper,eq</sub>	lb.	3,500	1,710	5,565				

- 1. Concrete must be normal-weight or lightweight concrete with f'c of 3,000 psi minimum.
- 2. Only the largest size of threaded rod specified for each insert must be used for applications resisting shear loads.
- 3. Design of headed cast-in specialty inserts shall be in accordance with the provisions of ACI 318 Appendix D for cast-in headed anchors. The value of  $k_c$  shall be in accordance with the value for cast-in anchors in D.5.2.2.
- 4. Strength reduction factors shall be taken from ACI 318-11 D.4.3 for cast-in headed anchors.
- 5. Strength reduction factor for load combinations of ACI 318 Section 9.2 governed by steel strength shall be taken as 0.65 for tension and 0.60 for
- 6. The concrete tension strength of headed cast-in specialty inserts in the sofit of concrete on metal deck assemblies shall be calculated in accordance with ACI 318 Appendix D and Figure 1.
- 7. Insert outside diameter = outside diameter of plastic sleeve.
- 8. The strengths shown in the table are for inserts only. Design professional is responsible for checking threaded rod strength in tension, shear and combined tension and shear, and the influence of bending on tension values when loaded in shear, as applicable.



Idealization of concrete on deck; determination of concrete breakout strength in accordance with ACI 318.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



# Wood-Form Insert: Tension Design Strengths in Normal-Weight Concrete (f'<sub>C</sub> = 3,000 psi)







			Min.		Min.	Min.	Min.	Min.	Min.	Min.	Min.		Critical	Minimum		Tension Design Strength Based on Concrete (lb.)							
Model No.	Threaded Rod Dia.	Rod Dia. Denth	Concrete Thickness	Edge Distance	Edge Distance	Edge Distances = $c_{ac}$ on all sides			Edge Dista	ances = c <sub>m</sub> on thre	<sub>in</sub> on one side and c <sub>ac</sub> ee sides												
	(in.)	(in.)	h <sub>min</sub>		C <sub>ac</sub>	Cac	C <sub>ac</sub>	C <sub>ac</sub>	C <sub>ac</sub> (in.)	C <sub>min</sub>	SDC	A-B <sup>5</sup>	SDC (	C-F <sup>6,7</sup>	SDC	A-B⁵	SDC (	C-F <sup>6,7</sup>					
			(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked										
	1/4																						
BBWF2550	3/8	2	23/4	3	1 1/2	2,955	2,365	2,215	1,770	1,950	1,560	1,460	1,170										
	1/2																						
	3/8																						
BBWF3762	1/2	2	23/4	3	1 %16	3,140	2,515	2,355	1,885	2,070	1,655	1,550	1,240										
	5/8																						
BBWF6275	5/8	2	23/4	3	15/8	2.955	2,365	2.215	1.770	2.040	1.630	1.530	1,225										
DDWI 0273	3/4	2	294	3	1 78	2,900	2,303	2,213	1,770	2,040	1,030	1,550	1,220										

T	Tension Design Strength of Threaded Rod Steel (lb.)											
Threaded Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A307	ASTM A325	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M				
1/4	1,385	1,790	2,980	1,435	2,860	2,625	2,980	1,360				
3/8	3,370	4,360	7,270	3,490	6,975	6,395	7,270	3,310				
1/2	6,175	7,990	13,315	6,390	12,780	11,715	13,315	6,070				
5⁄8	9,835	12,715	21,190	10,170	20,340	18,645	21,190	9,660				
3/4	14,530	18,790	31,315	15,030	30,060	27,555	31,315	14,280				

- 1. Tension design strengh must be the lesser of the concrete or threaded rod strength.
- 2. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Strength reduction factor,  $\phi$ , is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

# Wood-Form Insert: Allowable Tension Loads in Normal-Weight Concrete ( $f'_c = 3,000 \text{ psi}$ ) — Static Load







			Min. Concrete	0 III 1 = 1		Allowable Tension Load Based on Concrete (lb.)					
Model No.	Threaded Rod Dia. (in.)	Nominal Embed. Depth (in.)	Nmin	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)			Edge Distances = $c_{min}$ on or side and $c_{ac}$ on three side:			
	(,	()	(in.)	()	()	Uncracked	Cracked	Uncracked	Cracked		
	1/4										
BBWF2550	3/8	2	2¾	3	1 1/2	2,110	1,690	1,395	1,115		
	1/2										
	3/8										
BBWF3762	1/2	2	2¾	3	1 %16	2,245	1,795	1,480	1,180		
	5/8										
BBWF6275	5/8	2	23/4	3	1 5/8	2.110	1.690	1,455	1,165		
DDWI 027 3	BBWF6275 2	∠74	3	1 78	۷,۱۱۵	1,090	1,433	1,100			

	Allowable Tension Load of Threaded Rod Steel (lb.)											
Threaded Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A307	ASTM A325	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M				
1/4	990	1,280	2,130	1,025	2,045	1,875	2,130	970				
3/8	2,405	3,115	5,195	2,495	4,980	4,570	5,195	2,365				
1/2	4,410	5,705	9,510	4,565	9,130	8,370	9,510	4,335				
5/8	7,025	9,080	15,135	7,265	14,530	13,320	15,135	6,900				
3/4	10,380	13,420	22,370	10,735	21,470	19,680	22,370	10,200				

- 1. Allowable tension load must be the lesser of the concrete or threaded rod steel load.
- 2. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- 3. Tabulated values are for a single anchor with no influence of another anchor.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

# Blue Banger Hanger® Design Information — Concrete



# Wood-Form Insert: Allowable Tension Loads in Normal-Weight Concrete ( $f'_c = 3,000 \text{ psi}$ ) — Wind Load







	Thursday Day	Newstreet	Min Ormanda	Outlined Educ	Maintinum Edua	Allowable Tension Load Based on Concrete (lb.)				
Model No.	Threaded Rod Dia. (in.)	Rod Nominal Embed. Depth (in.)	Min. Concrete Thickness h <sub>min</sub> (in.)	Critical Edge Distance c <sub>ac</sub> (in.)	Minimum Edge Distance c <sub>min</sub> (in.)	Edge Dis c <sub>ac</sub> on a	tances = III sides	Edge Distances = $c_{min}$ on one side and $c_{ac}$ on three sides		
	(111.)	(111.)	(111.)	(111.)	("".)	Uncracked	Cracked	Uncracked	Cracked	
	1/4									
BBWF2550	3/8	2	23/4	3	1 1/2	1,775	1,420	1,170	935	
	1/2									
	3/8									
BBWF3762	1/2	2	23/4	3	1 %16	1,885	1,510	1,240	995	
	5/8		274		. ,					
BBWE6275	5/8		23/4	3	15/8	1.775	1.420	1.225	980	
DDWI 0273	BBWF6275 /8 2		∠74	3	1 78	1,773	1,420	1,220	300	

			Allowable	Tension Load of	Threaded Rod S	teel (lb.)		
Threaded Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A307	ASTM A325	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M
1/4	830	1,075	1,790	860	1,715	1,575	1,790	815
3/8	2,020	2,615	4,360	2,095	4,185	3,835	4,360	1,985
1/2	3,705	4,795	7,990	3,835	7,670	7,030	7,990	3,640
5/8	5,900	7,630	12,715	6,100	12,205	11,185	12,715	5,795
3/4	8,720	11,275	18,790	9,020	18,035	16,535	18,790	8,570

- 1. Allowable tension load must be the lesser of the concrete or threaded rod steel load.
- 2. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \%.6 = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.

# Wood-Form Insert: Allowable Tension Loads in Normal-Weight Concrete ( ${\rm f'}_{\rm C}=3,000~{\rm psi}$ ) — Seismic Load







			Min.	s Distance Distance Cac Cmin			Allowable Te	ension Load	Based on C	oncrete (lb.	.)									
Model No.	Threaded Rod Dia.	Nominal Embed. Depth	Concrete Thickness			Edge Distances = co. on all sides														
	(in.)	(in.)	h <sub>miṇ</sub>		Cac	Cac	Cac	Cac	Cac	Cac	Cac	C <sub>min</sub>	C <sub>ac</sub> C <sub>min</sub>	SDC	A-B <sup>4</sup>	SDC	C-F <sup>5,6</sup>	SDC	A-B <sup>4</sup>	SDC (
		(,	(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked							
	1/4																			
BBWF2550	3/8	2	23/4	3	1 ½	2,070	1,655	1,550	1,240	1,365	1,090	1,020	820							
	1/2																			
	3/8																			
BBWF3762	1/2	2	23/4	3	1 %16	2,200	1,760	1,650	1,320	1,450	1,160	1,085	870							
	5/8																			
RRWE6275	5/8	2	23/	3	15/8	2.070	1.655	1.550	1.240	1.430	1.140	1.070	860							
BBWF6275 78 3/4	3/4	2	2¾	3	1 %	2,070	1,000	1,550	1,240	1,430	1,140	1,070	000							

			Allowa	ble Tension Load (	of Threaded Rod St	eel (lb.)		
Threaded Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A307	ASTM A325	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M
1/4	970	1,255	2,085	1,005	2,000	1,840	2,085	950
3/8	2,360	3,050	5,090	2,445	4,885	4,475	5,090	2,315
1/2	4,325	5,595	9,320	4,475	8,945	8,200	9,320	4,250
5/8	6,885	8,900	14,835	7,120	14,240	13,050	14,835	6,760
3/4	10,170	13,155	21,920	10,520	21,040	19,290	21,920	9,995

- 1. Allowable tension load must be the lesser of the concrete or threaded rod steel load.
- 2. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \%.7 = 1.43$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 5. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 6. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Metal-Deck Insert: Tension Design Strength in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000 \text{ psi}$ )







	Threaded	Nominal	Minimum								
Model No.	Rod Dia.	Embed.	End Distance		Lowe	r Flute			Uppe	r Flute	
Model No.	(in.)	Depth	C <sub>min</sub>	SDC	A-B⁵	SDC (	C-F <sup>6,7</sup>	SDC	A-B⁵	SDC	C-F <sup>6,7</sup>
	(111.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	1/4										
BBMD2550	3/8	2	21/8	1,930	1,545	1,445	1,155	2,510	2,010	1,885	1,505
	1/2										
	3/8										
BBMD3762	1/2	2	21/2	2,075	1,660	1,555	1,245	2,810	2,250	2,110	1,685
	5/8										
BBMD6275	5/8	2	21/2	2.075	1.660	1.555	1.245	2.010	2.250	2 110	1 605
DDIVIDO213	3/4		2 1/2	2,075	1,000	1,000	1,240	2,810	2,250	2,110	1,685

			Tensio	n Design Strength (	of Threaded Rod St	eel (lb.)		
Threaded Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A307	ASTM A325	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M
1/4	1,385	1,790	2,980	1,435	2,860	2,625	2,980	1,360
3/8	3,370	4,360	7,270	3,490	6,975	6,395	7,270	3,310
1/2	6,175	7,990	13,315	6,390	12,780	11,715	13,315	6,070
5/8	9,835	12,715	21,190	10,170	20,340	18,645	21,190	9,660
3/4	14,530	18,790	31,315	15,030	30,060	27,555	31,315	14,280

- 1. Tension design strengh must be the lesser of the concrete or threaded rod strength.
- 2. Tension design strengths are based on the strength design provisions of ACI 318-11 Appendix D.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Strength reduction factor, φ, is based on using a load combination from ACI 318-11 Section 9.2.
- 5. The tension design strength listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 6. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 7. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 8. Installation must comply with Figure 1 on page 223.

# Metal-Deck Insert: Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000 \text{ psi}$ ) — Static Load

	Threaded Rod	Nominal Embed.	Minimum End	Allow	able Tension Load	Tension Load Based on Concrete (lb.)			
Model No.	Dia.	Depth	Distance c <sub>min</sub>	Lowe	r Flute	Uppe	IBC		
	(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked		
	1/4								
BBMD2550	3/8	2	21/8	1,380	1,105	1,795	1,435		
	1/2							_	
	3/8								
BBMD3762	1/2	2	21/2	1,480	1,185	2,005	1,605		
	5/8								
BBMD6275	5/8	2	01/	1,480	1,185	0.005	1.005		
DDIVID0273	3/4	2	21/2	1,400	1,100	2,005	1,605		

			Allowa	Allowable Tension Load of Threaded Rod Steel (lb.)									
Threaded Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A307	ASTM A325	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M					
1/4	990	1,280	2,130	1,025	2,045	1,875	2,130	970					
3/8	2,405	3,115	5,195	2,495	4,980	4,570	5,195	2,365					
1/2	4,410	5,705	9,510	4,565	9,130	8,370	9,510	4,335					
5/8	7,025	9,080	15,135	7,265	14,530	13,320	15,135	6,900					
3/4	10,380	13,420	22,370	10,735	21,470	19,680	22,370	10,200					

- 1. Allowable tension load must be the lesser of the concrete or threaded rod steel load.
- 2. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha$  = 1.4. The conversion factor  $\alpha$  is based on the load combination 1.2D + 1.6L assuming 50% dead load and 50% live load: 1.2(0.5) + 1.6(0.5) = 1.4.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Installation must comply with Figure 1 on page 223.

**Mechanical** Anchors

<sup>\*</sup> See page 12 for an explanation of the load table icons



Metal-Deck Insert: Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000 \text{ psi}$ ) — Wind Load

	Threaded Rod	Nominal		Allowable Tension Load Based on Concrete (lb.)					
Model No.	Dia.	Embed. Depth		Lower	Flute	Upper Flute			
	(in.)	(in.)	(in.)	Uncracked	Cracked	Uncracked	Cracked		
	1/4								
BBMD2550	3/8	2	21/8	1,160	925	1,505	1,205		
	1/2								
	3/8								
BBMD3762	1/2	2	21/2	1,245	995	1,685	1,350		
DDIVIDOT OZ	5/8	_				,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
DDMD6075	5/8	2	21/2	1.245	995	1 605	1 250		
BBMD6275	3/4		2 1/2	1,240	990	1,685	1,350		

		Allowable Tension Load of Threaded Rod Steel (lb.)										
Threaded Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A307	ASTM A325	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M				
1/4	830	1,075	1,790	860	1,715	1,575	1,790	815				
3/8	2,020	2,615	4,360	2,095	4,185	3,835	4,360	1,985				
1/2	3,705	4,795	7,990	3,835	7,670	7,030	7,990	3,640				
5/8	5,900	7,630	12,715	6,100	12,205	11,185	12,715	5,795				
3/4	8,720	11,275	18,790	9,020	18,035	16,535	18,790	8,570				

- 1. Allowable tension load must be the lesser of the concrete or threaded rod steel load.
- 2. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = \%.6 = 1.67$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% wind load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. Installation must comply with Figure 1 on page 223.

# Metal-Deck Insert: Allowable Tension Loads in Soffit of Normal-Weight or Sand-Lightweight Concrete-Filled Profile Steel Deck Assemblies ( $f'_c = 3,000 \text{ psi}$ ) — Seismic Load



				`	,	. ,					
		Nominal	Allowable Tension Load Based on Concrete (lb.)								
Madal No	Threaded	Embod	Minimum Ena		Lowe	r Flute			Uppe	r Flute	
Model No.	Rod Dia. (in.)	Dehm	Distance c <sub>min</sub> (in.)	SDC	A-B <sup>4</sup>	SDC	C-F <sup>5,6</sup>	SDC	A-B <sup>4</sup>	SDC	C-F <sup>5,6</sup>
(11.)		(in.)		Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked	Uncracked	Cracked
	1/4										
BBMD2550	3/8	2	21/8	1,350	1,080	1,010	810	1,755	1,405	1,320	1,055
	1/2										
	3/8										
BBMD3762	1/2	2	21/2	1,455	1,160	1,090	870	1,965	1,575	1,475	1,180
	5/8										
BBMD6275	5/8	2	21/2	1,455	1,160	1,090	870	1.965	1,575	1,475	1,180
DDIVIDUZI J	3/4	2	∠ 72	1,400	1,100	1,090	070	1,303	1,373	1,473	1,100

			Allowable	Tension Load	of Threaded	Rod Steel (lb.)		
Threaded Rod Dia. (in.)	ASTM F1554 GR 36	ASTM F1554 GR 55	ASTM F1554 GR 105	ASTM A307	ASTM A325	ASTM A193 B6	ASTM A193 B7	ASTM A193 B8/B8M
1/4	970	1,255	2,085	1,005	2,000	1,840	2,085	950
3/8	2,360	3,050	5,090	2,445	4,885	4,475	5,090	2,315
1/2	4,325	5,595	9,320	4,475	8,945	8,200	9,320	4,250
5/8	6,885	8,900	14,835	7,120	14,240	13,050	14,835	6,760
3/4	10,170	13,155	21,920	10,520	21,040	19,290	21,920	9,995

- 1. Allowable tension load must be the lesser of the concrete or threaded rod steel load.
- 2. Allowable tension loads are calculated based on the strength design provision of ACI 318-11 Appendix D using a conversion factor of  $\alpha = 1.43$ . The conversion factor  $\alpha$  is based on the load combination assuming 100% seismic load.
- 3. Tabulated values are for a single anchor with no influence of another anchor.
- 4. The allowable tension load listed for SDC (Seismic Design Category) A-B may also be used in SDC C-F when the tension component of the strength-level seismic design load on the anchor does not exceed 20% of the total factored tension load on the anchor associated with the same load combination.
- 5. When designing anchorages in SDC C-F, the designer shall consider the ductility requirements of ACI 318-11 Section D.3.3.
- 6. Tension design strengths in SDC C-F have been adjusted by 0.75 factor in accordance with ACI 318-11 Section D.3.3.4.4.
- 7. Installation must comply with Figure 1 on page 223.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Wood-Form Insert: Allowable Tension Loads in Normal-Weight or Sand-Lightweight Concrete

IBC		LW

Model No.	Threaded Rod Dia.	Embed. Depth in.	Min. Edge Dist. in.	Min. Spacing in.	Tension Load Based on Concrete Strength (Normal Weight)		Tension Load Based on Rod Strength (Normal Weight)	Stre	ased on Concrete ngth ghtweight)	Tension Load Based on Rod Strength (Sand- Lightweight)				
140.	in.	(mm)	(mm)	(mm)	f¹ <sub>c</sub> ≥ 3,000 psi (20.7 MPa)		F1554 Grade 36	f¹ <sub>c</sub> ≥ 3,000 psi (20.7 MPa)		F1554 Grade 36				
					Ultimate lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)				
	1/4						<b>940</b> (4.2)			<b>940</b> (4.2)				
	3/8	<b>2</b> (51)	<b>7</b> (178)	<b>8</b> (203)	<b>6,820</b> (30.3)	<b>1,705</b> (7.6)	<b>2,105</b> (9.4)	<b>4,280</b> (19.0)	<b>1,070</b> (4.8)	<b>2,105</b> (9.4)				
	1/2						<b>3,750</b> (16.7)			<b>3,750</b> (16.7)				
	3/8										<b>2,105</b> (9.4)			_
BBWF3762	1/2	<b>2</b> (51)	<b>7</b> (178)	<b>8</b> (203)	<b>7,360</b> (32.7)	<b>1,840</b> (8.2)	<b>3,750</b> (16.7)	_	_	_				
	5/8	(01)					<b>5,875</b> (26.1)			_				
DDWE007E	5/8	2	7	8	7,420	1,855	<b>5,875</b> (26.1)	4,400	1,100	<b>5,875</b> (26.1)				
BBWF6275	3/4	(51)	(178)	(203)	(33.0)	(8.3)	<b>8,460</b> (37.6)	(19.6)	(4.9)	<b>8,460</b> (37.6)				

Wood-Form Insert: Allowable Shear Loads in Normal-Weight or Sand-Lightweight Concrete







Model No.	Threaded Rod Dia.	Embed. Depth in.	Min. Edge Dist. in.	Min. Spacing in.			Strength on Rod Strength Strength Strength		Strength		
140.	in.	(mm)	(mm)	(mm)	f' <sub>c</sub> ≥ 3,000 p	si (20.7 MPa)	F1554 Grade 36	f' <sub>c</sub> ≥ 3,000 p	si (20.7 MPa)	F1554 Grade 36	
					Ultimate lb. (kN) Allowable lb. (kN)		Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	
BBWF2550	1/2	<b>2</b> (51)	<b>7</b> (178)	<b>8</b> (203)	<b>8,750</b> (38.9)	<b>2,185</b> (9.7)	<b>1,930</b> (8.6)	<b>8,600</b> (38.2)	<b>2,150</b> (9.6)	<b>1,930</b> (8.6)	
BBWF3762	5/8	<b>2</b> (51)	<b>7</b> (178)	<b>8</b> (203)	<b>10,700</b> (47.6)	<b>2,675</b> (11.9)	<b>3,025</b> (13.4)	_	_	_	
BBWF6275	3/4	<b>2</b> (51)	<b>7</b> (178)	<b>8</b> (203)	<b>10,460</b> (46.5)	<b>2,615</b> (11.6)	<b>4,360</b> (19.4)	<b>9,260</b> (41.2)	<b>2,315</b> (38.9)	<b>4,360</b> (19.4)	

- 1. Allowable load must be the lesser of the concrete or steel strength.
- 2. The allowable loads based on concrete strength are based on a factor of safety of 4.0.
- 3. Allowable loads may not be increased for short-term loading due to wind or seismic forces.
- 4. Mechanical and plumbing design codes may prescribe lower allowable loads. Verify with local codes.
- 5. Minimum concrete slab thickness = 2x embedment depth.

Metal-Deck Insert: Allowable Tension Loads in Normal-Weight or Sand-Lightweight Concrete over Metal Deck







	~
660,000	
$\overline{}$	

	Drill Bit	Threaded Rod	Embed. Depth	Min. Edge	Min. Spacing	Tension Load Based on Concrete Strength (Install in High Flute)			ased on Concrete all in Low Flute)	Tension Load Based on Rod Strength						
Model No.	Dia. in.	Dia.	iń.	Dist. in.	in.			$f'_{c} \ge 3,000 \text{ p}$	F1554 Grade 36							
		in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)						
	1/2	1/4								<b>940</b> (4.2)						
BBMD2550 13/16 - 7/8	$^{13}/_{16} - ^{7}/_{8}$	3/8	<b>2</b> (51)				<b>7½</b> (191)	<b>8</b> (203)	<b>9,320</b> (41.5)	<b>2,330</b> (10.4)	<b>3,210</b> (14.3)	<b>800</b> (3.6)	<b>2,105</b> (9.4)			
		1/2	, ,			, ,	, ,	, ,		<b>3,750</b> (16.7)						
		3/8	<b>2</b> (51)			<b>2</b> (51)	71/						<b>2,105</b> (9.4)			
BBMD3762	11/8 – 13/8	1/2												<b>7½</b> (191)	<b>8</b> (203)	<b>10,540</b> (46.9)
	5/8		, ,						<b>5,875</b> (26.1)							
BBMD6275 13/16 - 13/8	12/ 12/	5/8	2	7½	8	12,360	3,090	3,445	860	<b>5,875</b> (26.1)						
	3/4	(51) (191)		(203)	(55.0)	(13.7)	(15.3)	(3.8)	<b>8,460</b> (37.6)							

See notes under "Metal-Deck Insert: Shear Loads" on page 223.

<sup>\*</sup> See page 12 for an explanation of the load table icons.







# Metal-Deck Insert: Allowable Shear Loads in Normal-Weight or Sand-Lightweight Concrete over Metal Deck

	Drill Bit	Threaded Rod	Embed. Depth	Min. Edge	Min. Spacing	Shear Load Based on Concrete Strength (Install in High Flute) Shear Load Based on Concrete Strength (Install in Low Flute)			Shear Load Based on Rod Strength	
Model No. Dia. in.		Dia.	in.	Dist. in.	in.	f¹ <sub>c</sub> ≥ 3,000 ps	si (20.7 MPa)	f¹ <sub>c</sub> ≥ 3,000 psi (20.7 MPa)		F1554 Grade 36
		in.	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
BBMD2550	13/16 - 7/8	1/2	<b>2</b> (51)	<b>7½</b> (191)	<b>8</b> (203)	<b>9,720</b> (43.2)	<b>2,430</b> (10.8)	<b>2,790</b> (12.4)	<b>700</b> (3.1)	<b>1,930</b> (8.6)
BBMD3762	11/8 - 13/8	5/8	<b>2</b> (51)	<b>7½</b> (191)	<b>8</b> (203)	<b>9,400</b> (41.8)	<b>2,350</b> (10.4)	<b>3,360</b> (14.9)	<b>840</b> (3.7)	<b>3,025</b> (13.4)
BBMD6275	13/16 - 13/8	3/4	<b>2</b> (51)	<b>7½</b> (191)	<b>8</b> (203)	<b>9,720</b> (43.2)	<b>2,430</b> (10.8)	<b>3,360</b> (14.9)	<b>840</b> (3.7)	<b>4,360</b> (19.4)

- 1. Allowable load must be the lesser of the concrete or rod strength.
- 2. The allowable loads based on concrete strength are based on a factor of safety of 4.0.
- 3. Allowable loads may not be increased for short-term loading due to wind or seismic forces.
- 4. Anchors may be installed off-center in the flute, up to 1" from the edge of flute.
- 5. Shear loads shall be applied flush with metal deck surface.
- 6. Deck shall be 20-gauge minimum.
- 7. Mechanical and plumbing design codes may prescribe lower allowable loads. Verify with local codes.
- 8. Installation must comply with Figure 1.

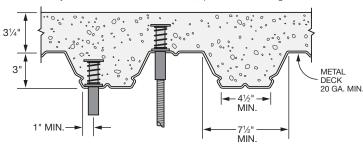


Figure 1. Typical metal deck insert installation in concrete over metal deck

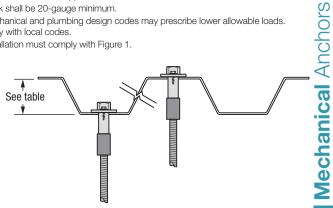


Figure 2. Typical roof deck insert installation in metal deck

### Roof-Deck Insert: Allowable Tension Loads in Metal Deck

1 1001 Doort II 1001t. 7	MOVVADIO TOTICIOTI EC	add ii i woldi Doort			
Model No.	Drill Bit Dia. in.	Threaded Rod Dia in.		sed on Deck Strength b. (kN)	Allowable Tension Load Based on Rod Strength Ib. (kN)
			1½" Deck	3" Deck	F1554 Grade 36
		1/4			<b>940</b> (4.2)
BBRD2550	<sup>13</sup> / <sub>16</sub> — <sup>7</sup> / <sub>8</sub>	3/8	<b>150</b> (0.7)	<b>300</b> (1.3)	<b>2,105</b> (9.4)
		1/2			<b>3,750</b> (16.7)

- 1. The allowable loads are based on a factor of safety of 4.0. 4. Threaded rod strength must be investigated separately.
- 2. Allowable loads may not be increased for short-term loading due to wind or seismic forces.
- 3. Acceptability of deck deflection due to imposed loads must be investigated separately.
- 5. Anchors may be installed in the top or bottom flute of the metal deck.
- 6. Deck shall be 20-gauge minimum.
- 7. See Figure 2 for typical installation.

# Wood-Form Insert: Factory Mutual and Underwriters Laboratories Pipe Size Limits

Model No.	Rod Dia. in.	FM Max. Nominal Pipe Size in.	UL Max. Nominal Pipe Size in.
	1/4	N/L	4
BBWF2550	3/8	4	4
	1/2	8	8
	3/8	4	4
BBWF3762	1/2	8	8
	5/8	N/L	8
BBWF6275	5/8	N.	Л
DDWF0273	3/4	IV.	/L

<sup>1.</sup> N/L = Not listed for this pipe size.

### Metal-Deck Insert:

### Factory Mutual and Underwriters Laboratories Pipe Size Limits

	Dod	FM Max. Nom	inal Pipe Size	UL Max. Nom	inal Pipe Size
Model No.	Rod Dia. in.	Install in High Flute in.	Install in Low Flute in.	Install in High Flute in.	Install in Low Flute in.
	1/4	N/L	N/L	4	4
BBMD2550	3/8	4	4	4	4
	1/2	8	N/L	8	4
	3/8	4	4	4	4
BBMD3762	1/2	8	N/L	8	4
	5/8	N/L	N/L	8	4
DDMDG07E	5/8	12	N/L	12	N/L
BBMD6275	3/4	12	N/L	12	N/L

<sup>1.</sup> N/L = Not listed for this pipe size.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **Drop-In** Internally Threaded Anchor (DIAB)

# Expansion shell anchors for use in solid base materials

Simpson Strong-Tie introduces a new, redesigned Drop-In Anchor (DIAB) that provides easier installation into base materials. Improved geometry in the preassembled expansion plug improves setting capability so the anchor installs with 40% fewer hammer strikes than previous versions. These displacement-controlled expansion anchors are easily set by driving the plug toward the bottom of the anchor using either the hand- or power-setting tools. DIAB anchors feature a positive-set marking indicator at the top of the anchor — helping you see more clearly when proper installation has taken place.

Use a Simpson Strong-Tie fixed-depth stop bit to take the guesswork out of drilling to the correct depth. The fluted design of the tip draws debris away from the hole during drilling, allowing for a cleaner installation.

# Key features

- New design offers easier installation then previous drop-in anchor design - sets with 40% fewer hammer hits
- Positive-set marking system indicates when anchor is
- Lipped drop-in version available for flush installation
- Hand- and power-setting tools available for fast, easy and economical installation
- Fixed-depth stop bit helps you drill to the correct depth every time





Material: Carbon steel

Coating: Zinc plated





Anchor being set with hand setting tool.



Anchor being set with SDS setting tool.



Positive set indicator.

# **Drop-In** Internally Threaded Anchor (DIAB)



# Drop-In Anchor

Rod Size	Model	Drill Bit	Bolt Threads	Body	Thread	Qua	entity
(in.)	No.	Dia. (in.)	(per in.)	Length (in.)	Length (in.)	Box	Carton
1/4	DIAB25	3/8	20	1	3/8	100	500
3/8	DIAB37	1/2	16	1 %16	5/8	50	250
1/2	DIAB50	5/8	13	2	3/4	50	200
5/8	DIAB62	7/8	11	21/2	1	25	100
3/4	DIAB75	1	10	31/8	11⁄4	20	80



Drop-In

# Lipped Drop-In Anchor

Rod Size	Model	Drill Bit	Bolt Threads		Thread	Qua	ıntity
(in.)	No.	Dia. (in.)	(per in.)	Length (in.)	Length (in.)	Box	Carton
1/4	DIABL25	3/8	20	1	3/8	100	500
3/8	DIABL37	1/2	16	1 %16	5/8	50	250
1/2	DIABL50	5/8	13	2	3/4	50	200



Lipped Drop-In

# Drop-In Anchor Hand Setting Tool

Model No.	For Use With	Box Quantity
DIABST25	DIAB25, DIABL25	10
DIABST37	DIAB37, DIABL37	10
DIABST50	DIAB50, DIABL50	10
DIABST62	DIAB62	5
DIABST75	DIAB75	5

<sup>1.</sup> Setting tools sold separately, Tools may be ordered by the piece.



Hand Setting Tool

# Drop-In Anchor Power Setting Tool

Model No.	For Use With	Box Quantity
DIABST25-SDS	DIAB25, DIABL25	10
DIABST37-SDS	DIAB37, DIABL37	10
DIABST50-SDS	DIAB50, DIABL50	10



Power Setting Tool

# Fixed-Depth Drill Bits

Model No	Drill Bit Diameter (in.)	Drill Depth (In.)	For Use With
MDPL037DIA	3/8	1 1/16	DIAB25, DIABL25
MDPL050DIA	1/2	1 11/16	DIAB37, DIABL37
MDPL062DIA	5/8	21/16	DIAB50, DIABL50



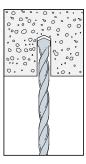
Fixed-Depth Drill Bit

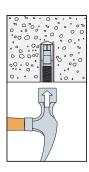
# **Drop-In** Internally Threaded Anchor (DIAB)

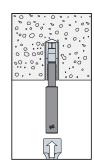
# SIMPSON Strong-Tie

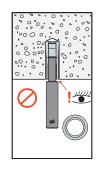
### **DIAB Manual Installation**

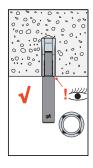
- A
- Caution: Oversized holes will reduce the anchors load capacity
- 1. Drill a hole in the base material using the appropriate diameter carbide drill bit or fixed depth bit as specified in the table. Drill the hole to the specified embedment. For fixed depth bits drill the hole until the shoulder of the bit contacts the surface of the base material. Then blow the hole clean of dust and debris using compressed air. Overhead installations need not be blown clean.
- 2. Insert the anchor into the hole. Tap with hammer until flush against the surface.
- 3. Using the designated Drop-In setting tool, drive expander plug towards the bottom of the anchor until the shoulder of the setting tool makes contact with the top of the anchor. When properly set 4 indentations will be visible on the top of the anchor indicating full expansion.
- Insert bolt or threaded rod. Minimum thread engagement should be equal to the nominal diameter of the threaded insert.

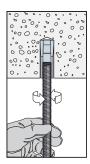






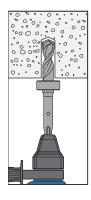


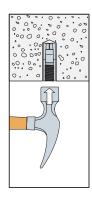


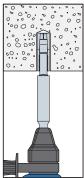


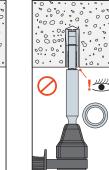
### **DIAB SDS Installation**

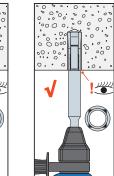
- A
- Caution: Oversized holes will reduce the anchors load capacity
- 1. Drill a hole in the base material using the appropriate diameter carbide drill bit or fixed depth drill bit as specified in the table. Drill the hole to the specified embedment. For fixed depth bits drill the hole until the shoulder of the bit contacts the surface of the base material. Then blow the hole clean of dust and debris using compressed air. Overhead installations need not be blown clean.
- 2. Insert the anchor into the hole. Tap with hammer until flush against the surface.
- 3. Attach SDS Drop-In setting tool a drill. Drive expander plug towards the bottom of the anchor using only hammer mode until the shoulder of the setting tool makes contact with the top of the anchor. When properly set 4 indentations will be visible on the top of the anchor indicating full expansion.
- Insert bolt or threaded rod. Minimum thread engagement should be equal to the nominal diameter of the threaded insert.

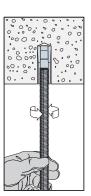












# **Drop-In** (DIAB) Design Information — Concrete





# DIAB Allowable Tension and Shear Loads in Normal-Weight Concrete

	Rod	Drill Bit	Embed	Critical	Critical		f' <sub>c</sub> ≥ 2,500 ps	si (17.2 MPa			f' <sub>c</sub> ≥ 4,000 ps	si (27.6 MPa	)
Model	Size	Dia.	Dia Depth	Edge Dist.	Spacing	Tensio	n Load	Shea	r Load	Tensio	n Load	Shea	r Load
No.	in. (mm)	ln.	In. (mm)	In. (mm)	In. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
DIAB25 DIABL25	<b>1/4</b> (6.4)	3/8	<b>1</b> (25)	<b>3</b> (76)	<b>4</b> (102)	<b>1,565</b> (7.0)	<b>390</b> (1.7)	<b>1,840</b> (8.2)	<b>460</b> (2.0)	<b>1,965</b> (8.7)	<b>490</b> (2.2)	<b>1,840</b> (8.2)	<b>460</b> (2.0)
DIAB37 DIABL37	<b>3/8</b> (9.5)	1/2	<b>1</b> %16 (40)	<b>4½</b> (114)	<b>6</b> (152)	<b>2,950</b> (13.1)	<b>740</b> (3.3)	<b>4,775</b> (21.2)	<b>1,195</b> (5.3)	<b>3,910</b> (17.4)	<b>980</b> (4.4)	<b>4,775</b> (21.2)	<b>1,195</b> (5.3)
DIAB50 DIABL50	<b>½</b> (12.7)	5/8	<b>2</b> (51)	<b>6</b> (152)	<b>8</b> (203)	<b>5,190</b> (23.1)	<b>1,300</b> (5.8)	<b>6,760</b> (30.1)	<b>1,690</b> (7.5)	<b>6,515</b> (29.0)	<b>1,630</b> (7.3)	<b>6,760</b> (30.1)	<b>1,690</b> (7.5)
DIAB62	<b>5/8</b> (15.9)	7/8	<b>2½</b> (64)	<b>7½</b> (191)	<b>10</b> (254)	<b>7,010</b> (31.2)	<b>1,755</b> (7.8)	<b>12,190</b> (54.2)	<b>3,050</b> (13.6)	<b>9,060</b> (40.3)	<b>2,265</b> (10.1)	<b>12,190</b> (54.2)	<b>3,050</b> (13.6)
DIAB75	<b>3/4</b> (19.1)	1	<b>31/8</b> (79)	<b>9</b> (229)	<b>12½</b> (318)	<b>9,485</b> (42.2)	<b>2,370</b> (10.5)	<b>15,960</b> (71.0)	<b>3,990</b> (17.7)	<b>11,660</b> (51.9)	<b>2,915</b> (13.0)	<b>15,960</b> (71.0)	<b>3,990</b> (17.7)

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Refer to allowable load-adjustment factors for edge distance and spacing on page 228.
- 3. Allowable loads may be linearly interpolated between concrete strength listed.
- 4. The minimum concrete thickness is 1 ½ times the embedment depth.
- 5. Allowable loads may not be increased for short-term loading due to wind or seismic forces.

# DIAB Allowable Tension and Shear Loads in Soffit of Sand-Lightweight Concrete over Metal Deck

_	
[ <b>/</b> ]	ſ
IBC	- 1
<i></i>	- 5



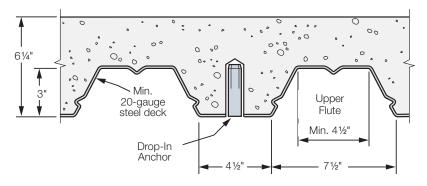




**Mechanical** Anchors

	Rod Size	Drill Bit	Embed	Critical	Critical		f¹ <sub>c</sub> ≥ 3,000. p	si (20.7 MPa)	
Model	in.	Dia.	Depth	End Dist.6	Spacing	Tensio	n Load	Shear	Load
No.	(mm)	In.	In. (mm)	In. (mm) (mm)		Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
DIAB37 DIABL37	<b>3/8</b> (9.5)	1/2	<b>1</b> % (40)	<b>4½</b> (114)	<b>6</b> (152)	<b>2,895</b> (12.9)	<b>725</b> (3.2)	<b>3,530</b> (15.7)	<b>885</b> (3.9)
DIAB50 DIABL50	<b>½</b> (12.7)	5/8	<b>2</b> (51)	<b>6</b> (152)	<b>8</b> (203)	<b>4,100</b> (18.2)	<b>1,025</b> (4.6)	<b>4,685</b> (20.8)	<b>1,170</b> (5.2)

- 1. The allowable loads listed are based on a safety factor of 4.0.
- $2. \, \hbox{Allowable loads may not be increased for short-term loading due to wind or seismic forces}.$
- 3. Refer to allowable load-adjustment factors for edge distance and spacing on page 228.
- 4. Anchors were installed in the center of the bottom flute of the steel deck.
- 5. Metal deck must be minimum 20-gauge thick with minimum yield strength of 33 ksi.
- 6. Critical end distance is defined as the distance from end of the slab in the direction of the flute.



**Lightweight Concrete over Metal Deck** 

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC

# **Drop-In** (DIAB) Design Information — Concrete



Allowable Load-Adjustment Factors for Drop-In Anchor (DIAB) in Normal-Weight Concrete and Sand-Lightweight Concrete over Metal Deck: Edge Distance and Spacing, Tension and Shear Loads

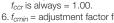
### How to use these charts:

- 1. The following tables are for reduced edge distance and spacing.
- 2. Locate the anchor size to be used for either a tension and/or a shear load application.
- 3. Locate the edge distance ( $c_{act}$ ) or spacing ( $s_{act}$ ) at which the anchor is to be installed.

# Edge Distance Tension (f<sub>c</sub>)

Edge	Size	1/4	3/8	1/2	5/8	3/4
Dist.	Ccr	3	41/2	6	71/2	9
Cact	C <sub>min</sub>	13/4	25/8	31/2	43/8	51/4
(in.)	f <sub>cmin</sub>	0.77	0.77	0.77	0.77	0.77
13/4		0.77				
2		0.82				
21/2		0.91				
25/8		0.93	0.77			
3		1.00	0.82			
31/2			0.88	0.77		
4			0.94	0.82		
43/8			0.98	0.85	0.77	
41/2			1.00	0.86	0.78	
5				0.91	0.82	
51/4				0.93	0.83	0.77
51/2				0.95	0.85	0.79
6				1.00	0.89	0.82
61/2					0.93	0.85
7					0.96	0.88
71/2					1.00	0.91
8						0.94
81/2						0.97
9						1.00

- 1.  $c_{act}$  = actual edge distance at which anchor is installed (inches).
- $2.c_{cr}$  = critical edge distance for 100% load (inches).
- 3.  $c_{min}$  = minimum edge distance for reduced load (inches).
- 4.  $f_c$  = adjustment factor for allowable load at actual edge distance.
- 5.  $f_{ccr}$  = adjustment factor for allowable load at critical edge distance.
- 6. f<sub>cmin</sub> = adjustment factor for allowable load at minimum edge distance.
- 7.  $f_C = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min}) / (c_{cr} c_{min})].$



Spacing Tension (f<sub>s</sub>)

Spacing	Size	1/4	3/8	1/2	5/8	3/4
	$s_{cr}$	4	6	8	10	121/2
s <sub>act</sub> (in.)	Smin	11/2	21/4	3	3¾	43/4
(111.)	f <sub>smin</sub>	0.72	0.72	0.80	0.80	0.80
1 1/2		0.72				
2		0.78				
21/4		0.80	0.72			
21/2		0.83	0.74			
3		0.89	0.78	0.80		
31/2		0.94	0.81	0.82		
3¾		0.97	0.83	0.83	0.80	
4		1.00	0.85	0.84	0.81	
41/2			0.89	0.86	0.82	
43/4			0.91	0.87	0.83	0.80
5			0.93	0.88	0.84	0.81
51/2			0.96	0.90	0.86	0.82
6			1.00	0.92	0.87	0.83
61/2				0.94	0.89	0.85
7				0.96	0.90	0.86
71/2				0.98	0.92	0.87
8				1.00	0.94	0.88
81/2					0.95	0.90
9					0.97	0.91
91/2					0.98	0.92
10					1.00	0.94
101/2						0.95
11						0.96
111/2						0.97
12						0.99
121/6						1.00

- $1. s_{act}$  = actual spacing distance at which anchor is installed (inches).
- $2.s_{cr}$  = critical spacing distance for 100% load (inches).
- $3. s_{min}$  = minimum spacing distance for reduced load (inches).
- 4.  $f_s$  = adjustment factor for allowable load at actual spacing distance.
- 5.  $f_{SCT}$  = adjustment factor for allowable load at critical spacing distance.  $f_{SCr}$  is always = 1.00.
- 6.  $f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.
- 7.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$
- \* See page 12 for an explanation of the load table icons.

- 4. The load adjustment factor ( $f_c$  or  $f_s$ ) is the intersection of the row and column.
- 5. Multiply the allowable load by the applicable load adjustment factor.
- 6. Reduction factors for multiple edges or spacing are multiplied together.

### Edge Distance Shear (f<sub>c</sub>)

Edge	Size	1/4	3/8	1/2	5/8	3/4	IDC
Dist.	Ccr	3	41/2	6	71/2	9	IBC
Cact	C <sub>min</sub>	13/4	25/8	31/2	43/8	51/4	
(in.)	f <sub>cmin</sub>	0.54	0.54	0.64	0.64	0.64	<b>→</b>
13/4		0.54					252 252
2		0.63					
21/2		0.82					
25/8		0.86	0.54				
3		1.00	0.63				
31/2			0.75	0.64			
4			0.88	0.71			
43/8			0.97	0.77	0.64		
41/2			1.00	0.78	0.65		<b>/→</b> i
5				0.86	0.71		(LOUIS AND
51/4				0.89	0.74	0.64	
51/2				0.93	0.77	0.66	
6				1.00	0.83	0.71	
61/2					0.88	0.76	
7					0.94	0.81	
71/2					1.00	0.86	
8						0.90	
81/2						0.95	
9						1.00	

- 1.  $c_{act}$  = actual edge distance at which anchor is installed (inches).
- $2.c_{cr}$  = critical edge distance for 100% load (inches).
- 3.  $c_{min}$  = minimum edge distance for reduced load (inches).
- 4.  $f_c$  = adjustment factor for allowable load at actual edge distance.
- 5.  $f_{ccr}$  = adjustment factor for allowable load at critical edge distance.  $f_{ccr}$  is always = 1.00.
- 6.  $f_{cmin}$  = adjustment factor for allowable load at minimum edge distance.
- 7.  $f_C = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min}) / (c_{cr} c_{min})].$

### Spacing Shear (f<sub>s</sub>)

Spacing	Size	1/4	3/8	1/2	5/8	3/4
	Scr	4	6	8	10	121/2
s <sub>act</sub> (in.)	Smin	11/2	21/4	3	3¾	43/4
	f <sub>smin</sub>	1.00	1.00	1.00	1.00	1.00
1 1/2		1.00				
2		1.00				
21/4		1.00	1.00			
21/2		1.00	1.00			
3		1.00	1.00	1.00		
31/2		1.00	1.00	1.00		
3¾		1.00	1.00	1.00	1.00	
4		1.00	1.00	1.00	1.00	
41/2			1.00	1.00	1.00	
43/4			1.00	1.00	1.00	1.00
5			1.00	1.00	1.00	1.00
51/2			1.00	1.00	1.00	1.00
6			1.00	1.00	1.00	1.00
61/2				1.00	1.00	1.00
7				1.00	1.00	1.00
71/2				1.00	1.00	1.00
8				1.00	1.00	1.00
81/2					1.00	1.00
9					1.00	1.00
91/2					1.00	1.00
10					1.00	1.00
101/2						1.00
11						1.00
11½						1.00
12						1.00
121/2						1.00

- $1. s_{act} = actual spacing distance at which anchor is installed (inches).$
- $2. s_{cr}$  = critical spacing distance for 100% load (inches).
- $3. s_{min}$  = minimum spacing distance for reduced load (inches).
- 4.  $f_s$  = adjustment factor for allowable load at actual spacing distance.
- 5.  $f_{scr}$  = adjustment factor for allowable load at critical spacing distance.  $f_{scr}$  is always = 1.00.
- 6.  $f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.
- 7.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$

# **Drop-In** Internally Threaded Anchor (DIA)



Drop-in anchors are internally threaded drop-in expansion anchors for use in flush-mount applications in solid base materials. Available in stainless steel (DIA), short (DIAS) or coil-thread (DIAC) versions. Minimum thread engagement should be equal to the nominal diameter of the threaded insert.

### **Features**

- Lipped edge (DIAS) eliminates need for precisely drilled hole depth
- Available in coil-thread version for 1/2" and 3/4" coil-threaded rod
- Short length (DIAS) enables shallow embedment to help avoid drilling into rebar or pre-stressed/post-tensioned cables
- Short Drop-In anchors include a setting tool compatible with the anchor to ensure consistent installation

Material: Carbon and stainless steel Coating: Carbon steel; zinc plated

**Codes:** Drop-in: DOT; Factory Mutual 3017082; Underwriters Laboratories File Ex3605. Meets requirements of Federal Specifications A-A-55614, Type I.

Short drop-in: Factory Mutual 3017082 and Underwriters Laboratories File Ex3605.

A

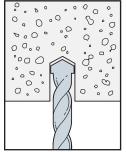
**Caution:** The load tables list values based upon results from the most recent testing and may not reflect those in current code reports. Where code jurisdictions apply, consult the current reports for applicable load values.

### Installation

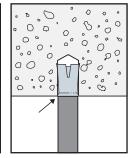
- 1. Drill a hole in the base material using the appropriate diameter carbide drill bit as specified in the table. Drill the hole to the specified embedment depth plus 1/8" for flush mounting. Blow the hole clean using compressed air. Overhead installations need not be blown clean.
- 2. Insert designated anchor into hole. Tap with hammer until flush against surface.
- Using the designated drop-in setting tool, drive expander plug toward the bottom of the anchor until shoulder of setting tool makes contact with the top of the anchor.
- Minimum thread engagement should be equal to the nominal diameter of the threaded insert.

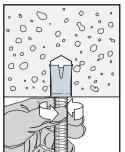


Caution: Oversized holes will make it difficult to set the anchor and will reduce the anchor's load capacity.















Short Drop-In



Coil-Thread Drop-In

# **Drop-In** Internally Threaded Anchor (DIA)



# Drop-In Anchor Product Data - Stainless Steel

Rod Size	Type 303/304	Type 316 Stainless	Drill Bit	_Bolt	Body	Thread	Qua	ntity
	Stainless Model No.		Dia. (in.)	Threads (per in.)	Length (in.)	Length (in.)	Box	Carton
1/4	DIA25SS	DIA256SS	3/8	20	1	3/8	100	500
3/8	DIA37SS	DIA376SS	1/2	16	1%16	5/8	50	250
1/2	DIA50SS	DIA506SS	5/8	13	2	3/4	50	200
5/8	DIA62SS	_	7/8	11	21/2	1	25	100
3/4	DIA75SS	_	1	10	31/8	11/4	20	80

# Short Drop-In Anchor Product Data

Rod	Model	Drill Bit Bolt Body Thread		Quantity			
Size (in.)	No.	Diameter (in.)	Threads (per in.)	Length (in.)	Length (in.)	Вох	Carton
3/8	DIA37S1	1/2	16	3/4	1/4	100	500
1/2	DIA50S1	5/8	13	1	5/16	50	200

<sup>1.</sup> A dedicated setting tool is included with each box of DIA37S and DIA50S.

# Coil-Thread Drop-In Anchor Product Data

Rod Size	Carbon Steel	Drill Bit Diameter	Bolt Threads	Body Length	Thread Length	Quantity		
(in.)	Model No.	(in.)	(per in.)	(in.)	(in.)	Вох	Ctn.	
1/2	DIA50C1	5/8	6	2	3/4	50	200	
3/4	DIA75C1	1	5	31/8	1 1/4	20	80	

<sup>1.</sup> DIA50C and DIA75C accept  $\frac{1}{2}$ " and  $\frac{3}{4}$ " coil-thread rod, respectively.

# Drop-In Anchor Setting Tool Product Data

Model No.	For Use With	Box Qty.
DIAST25	DIA25SS, DIA256SS	10
DIAST37	DIA37SS, DIA376SS	10
DIAST50	DIA50SS, DIA506SS, DIA50C	10
DIAST62	DIA62SS	5
DIAST75	DIA75SS, DIA75C	5

- 1. Setting tools sold separately except for DIA37S and DIA50S.
- 2. Setting tools for use with carbon and stainless-steel drop-in anchors.
- 3. Setting tools may be ordered by the piece.



o. Setting tools may be ordered by the piece.

# Drop-In Anchor (DIA) Power Setting Tool

Model No.	For Use With	Box Qty.
DIAST37S-SDS	DIA37S	10
DIAST50S-SDS	DIA50S	10

Also sold by the piece



**Power Setting Tool** 

# Drop-In Anchor Stop Bit

Model No.	Drill Bit Diameter (in.)	Drop-In Anchor (in.)	Drill Depth (in.)
MDPL037DIA	3/8	1/4	1 1/16
MDPL050DIA	1/2	3/8	13/16
MDPL062DIA	1/2	1/2	1 11/16
MDPL050DIAS	5/8	3/8	1 1/16
MDPL062DIAS	5%	1/2	21/16



Stop Bit

# **Drop-In** (DIA) Design Information — Concrete



Allowable Tension Loads for Drop-In (Stainless Steel) and Coil-Thread Drop-In (Carbon Steel) Anchors in Normal-Weight Concrete







Rod	Drill	Embed.	Critical	Critical				Tension Load			
Size in.	Bit Dia.	Depth in.	Edge Dist.	Spacing in.		$c \ge 2,000 \text{ p}$ B MPa) Cond		$f'_c \ge 3,000 \text{ psi}$ (20.7 MPa) Concrete	$f'_c \ge 4,000 \text{ psi}$ (27.6 MPa) Concrete		
(mm)	(in.)	(mm)	in. (mm)	(mm)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Std. Dev. lb. (kN)	Allowable lb. (kN)
<b>1/4</b> (6.4)	3/8	<b>1</b> (25)	<b>3</b> (76)	<b>4</b> (102)	<b>1,400</b> (6.2)	<b>201</b> (0.9)	<b>350</b> (1.6)	<b>405</b> (1.8)	<b>1,840</b> (8.2)	<b>451</b> (2.0)	<b>460</b> (2.0)
<b>3/8</b> (9.5)	1/2	<b>1%</b> 6 (40)	<b>4½</b> (114)	<b>6</b> (152)	<b>2,400</b> (10.7)	<b>251</b> (1.1)	<b>600</b> (2.7)	<b>795</b> (3.5)	<b>3,960</b> (17.6)	<b>367</b> (1.6)	<b>990</b> (4.4)
<b>½</b> (12.7)	5/8	<b>2</b> (51)	<b>6</b> (152)	<b>8</b> (203)	<b>3,320</b> (14.8)	<b>372</b> (1.7)	<b>830</b> (3.7)	<b>1,178</b> (5.2)	<b>6,100</b> (27.1)	<b>422</b> (1.9)	<b>1,525</b> (6.8)
<b>5%</b> (15.9)	7/8	<b>2½</b> (64)	<b>7½</b> (191)	<b>10</b> (254)	<b>5,040</b> (22.4)	<b>689</b> (3.1)	<b>1,260</b> (5.6)	<b>1,715</b> (7.6)	<b>8,680</b> (38.6)	<b>971</b> (4.3)	<b>2,170</b> (9.7)
<b>3/4</b> (19.1)	1	<b>3</b> 1/8 (79)	<b>9</b> (229)	<b>12½</b> (318)	<b>8,160</b> (36.3)	<b>961</b> (4.3)	<b>2,040</b> (9.1)	<b>2,365</b> (10.5)	<b>10,760</b> (47.9)	<b>1,696</b> (7.5)	<b>2,690</b> (12.0)

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Refer to allowable load-adjustment factors for edge distance and spacing on page 234.
- 3. Allowable loads may be linearly interpolated between concrete strengths listed.
- 4. The minimum concrete thickness is 11/2 times the embedment depth.

# Allowable Shear Loads for Drop-In (Stainless Steel) and Coil-Thread Drop-In (Carbon Steel) Anchors in Normal-Weight Concrete







(Carbon Steel) Anchors in Normal-Weight Concrete										
				Critical				S	hear Load	
	Rod Size in.	Drill Bit Dia.	Embed. Depth in.	Edge Dist.	Critical Spacing in.		f' <sub>c</sub> ≥ 2,000 psi 3.8 MPa) Concr		$f'_c \ge 3,000 \text{ psi}$ (20.7 MPa) Concrete	$f'_c \ge 4,000 \text{ psi}$ (27.6 MPa) Concrete
	(mm)	in.	(mm)	in. (mm)	(mm)	Ultimate Std. Dev. Allowable lb. (kN) lb. (kN) lb. (kN)		Allowable lb. (kN)	Allowable lb. (kN)	
	<b>1/4</b> (6.4)	3/8	<b>1</b> (25)	<b>3½</b> (89)	<b>4</b> (102)	<b>1,960</b> (8.7)	<b>178</b> (0.8)	<b>490</b> (2.2)	<b>490</b> (2.2)	<b>490</b> (2.2)
	<b>3/8</b> (9.5)	1/2	<b>1</b> %16 (40)	<b>5½</b> (133)	<b>6</b> (152)	<b>3,240</b> (14.4)	<b>351</b> (1.6)	<b>810</b> (3.6)	<b>925</b> (4.1)	<b>1,040</b> (4.6)
	<b>½</b> (12.7)	5/8	<b>2</b> (51)	<b>7</b> (178)	<b>8</b> (203)	<b>7,000</b> (31.1)	<b>562</b> (2.5)	<b>1,750</b> (7.8)	<b>1,750</b> (7.8)	<b>1,750</b> (7.8)
	<b>5/8</b> (15.9)	7/8	<b>2½</b> (64)	<b>8¾</b> (222)	<b>10</b> (254)	<b>11,080</b> (49.3)	<b>923</b> (4.1)	<b>2,770</b> (12.3)	<b>2,770</b> (12.3)	<b>2,770</b> (12.3)
	<b>3/4</b> (19.1)	1	<b>3</b> 1/8 (79)	<b>10½</b> (267)	<b>12½</b> (318)	<b>13,800</b> (61.4)	<b>1,781</b> (7.9)	<b>3,450</b> (15.3)	<b>3,725</b> (16.6)	<b>4,000</b> (17.8)

- 1. The allowable loads listed are based on a safety factor of 4.0.
- $2.\, \text{Refer to allowable load-adjustment factors for edge distance and spacing on page 234}.$
- 3. Allowable loads may be linearly interpolated between concrete strengths listed.
- 4. The minimum concrete thickness is 1½ times the embedment depth.

# Material Specifications

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

Anchor		Component Material						
Component	Zinc Plated Carbon Steel	Type 303/304 Stainless Steel	Type 316 Stainless Steel					
Anchor Body	Meets minimum 70,000 psi tensile	AISI 303. Meets chemical requirements of ASTM A582	Type 316					
Expander Plug	Meets minimum 50,000 psi tensile	AISI 303	Type 316					
Thread	UNC/Coil-thread	UNC	UNC					

Note: DIA37S, DIA50C and DIA75C are not available in stainless steel.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **Drop-In** (DIA) Design Information — Concrete



Allowable Tension and Shear Loads for %" and  $\frac{1}{2}$ " Short Drop-In Anchor in Sand-Lightweight Concrete Fill over Metal Deck



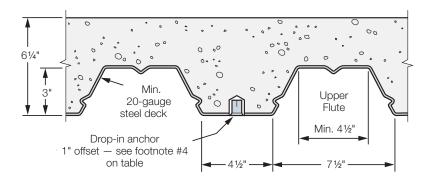






Rod Drill			DIII Emb Critical Criti		Shear Critical	Critical	Install through the Lower Flute or Upper Flute of Metal Deck, $f'_c \ge 3,000$ psi Concrete (20.7 MPa)				
Model No.	Size	Bit Dia.	Depth	End Distance	End	Spacing Tension Load		cing Tension Load Shea		Load	
(in.)	(in.)	(in.)	(in.)	Distance (in.)	(in.)	Ultimate (lb.)	Allowable (lb.)	Ultimate (lb.)	Allowable (lb.)		
DIA37S	3/8	1/2	3/4	6	7	8	1,344	335	1,649	410	
DIA50S	1/2	5/8	1	8	9%	10%	1,711	430	2,070	515	

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Allowable loads may not be increased for short-term loading due to wind or seismic forces.
- 3. Refer to allowable load-adjustment factors for edge distances and spacing on page 235.
- 4. Anchors were installed with a 1" offset from the centerline of the flute.



**Lightweight Concrete over Metal Deck** 

### **Drop-In** (DIA) Design Information -Concrete

Critical

Edge

Distance

(in.)

51/4

7

Critical

(in.)

3

4



Allowable Tension and Shear Loads for 3/8" and 1/2" Short Drop-In Anchor in Normal-Weight Concrete



(lb.)

540

855

Norm

Ter

Ultima

(lb.)

2,170

3,420





(lb.)

870

1,295

nal-Weight Concrete, f' <sub>c</sub> ≥ 4,000 psi							
sion Load Shear Load							
-	Allowable	Illtimate	Allos	vahla			

(lb.)

3,482

5,173

1 1. The allowable loads listed are based on a safety factor of 4.0.

Emb.

Depth

3/4

Drill

Bit Dia.

(in.)

1/2

5/8

Rod Size

(in.)

3/8

1/2

Model No.

DIA37S

DIA50S

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

- 2. Allowable loads may not be increased for short-term loading due to wind or seismic forces.
- 3. Refer to allowable load-adjustment factors for edge distances and spacing on page 234.

Critical

Edge

Distance

(in.)

41/2

6

- 4. Allowable loads may be linearly interpolated between concrete strengths.
- 5. The minimum concrete thickness is 11/2 times the embedment depth.

# Allowable Tension and Shear Loads for %" and 1/2" Short Drop-In Anchor in Hollow-Core Concrete Panel



		Drill Tension Shear		Нс	Hollow Core Concrete Panel, $\mathbf{f}'_c \ge 4,000 \; \mathrm{psi}$					
Model	Rod Size	Bit	Emb. Depth	Critical Edge	Critical Edge	Critical Spacing	Tensio	ı Load	Shear	Load
No.	(in.)	Dia. (in.)	(in.)	Distance (in.)	Distance (in.)	stance (in.)	Ultimate (lb.)	Allowable (lb.)	Ultimate (lb.)	Allowable (lb.)
DIA37S	3/8	1/2	3/4	41/2	51/4	3	1,860	465	3,308	825
DIA50S	1/2	5/8	1	6	7	4	2,650	660	4,950	1,235

Normal-Weight Concrete, f'<sub>C</sub> ≥ 2500 psi

**Shear Load** 

Allowable

(lb.)

570

805

Ultimate

(lb.)

2,274

3.224

**Tension Load** 

Allowable

(lb.)

375

510

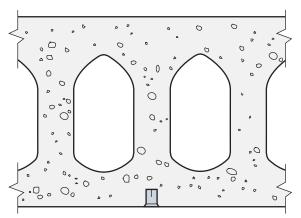
Ultimate

(lb.)

1,500

2,039

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. Allowable loads may not be increased for short-term loading due to wind or seismic forces.
- 3. Refer to allowable load-adjustment factors for edge distances and spacing on page 234.
- 4. Allowable loads may be linearly interpolated between concrete strengths.



**Hollow-Core Concrete Panel** 

(Anchor can be installed below web or hollow core)

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **Drop-In** (DIA) Design Information — Concrete



Allowable Load-Adjustment Factors for Drop-In (Stainless Steel), Coil Thread (Carbon Steel) and Short Drop-In Anchors in Normal-Weight Concrete: Edge Distance and Spacing, Tension and Shear Loads

### How to use these charts:

- 1. The following tables are for reduced edge distance and spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load application.
- 3. Locate the edge distance ( $c_{act}$ ) or spacing ( $s_{act}$ ) at which the anchor is to be installed.
- 4. The load adjustment factor ( $f_c$  or  $f_s$ ) is the intersection of the row and column.
- 5. Multiply the allowable load by the applicable load adjustment factor.
- 6. Reduction factors for multiple edges or spacing are multiplied together.

### Edge Distance Tension (f<sub>c</sub>)

Edge	Size	1/4	3/8	1/2	5/8	3/4	
Dist.	C <sub>cr</sub>	3	41/2	6	71/2	9	2
Cact	C <sub>min</sub>	13/4	25/8	31/2	4%	51/4	
(in.)	f <sub>cmin</sub>	0.65	0.65	0.65	0.65	0.65	33
13/4		0.65					٦
2		0.72					
21/2		0.86					٦
25/8		0.90	0.65				
3		1.00	0.72				6
31/2			0.81	0.65			
4			0.91	0.72			
43/8			0.98	0.77	0.65		
41/2			1.00	0.79	0.66		
5				0.86	0.72		
51/4				0.90	0.75	0.65	
51/2				0.93	0.78	0.67	
6				1.00	0.83	0.72	
61/2					0.89	0.77	
7					0.94	0.81	
71/2					1.00	0.86	
8						0.91	
81/2						0.95	
9						1.00	

See notes below.

### Edgo Dietanco Shoar (f.)

Edge	Size	1/4	3/8	1/2	5/8	3/4
Dist.	C <sub>cr</sub>	31/2	51/4	7	8¾	101/2
Cact	C <sub>min</sub>	13/4	25/8	31/2	43/8	51/4
(in.)	f <sub>cmin</sub>	0.45	0.45	0.45	0.45	0.45
13/4		0.45				
2		0.53				
21/2		0.69				
25/8		0.73	0.45			
3		0.84	0.53			
31/2		1.00	0.63	0.45		
4			0.74	0.53		
43/8			0.82	0.59	0.45	
41/2			0.84	0.61	0.47	
5			0.95	0.69	0.53	
51/4			1.00	0.73	0.56	0.45
51/2				0.76	0.59	0.48
6				0.84	0.65	0.53
61/2				0.92	0.72	0.58
7				1.00	0.78	0.63
71/2					0.84	0.69
8					0.91	0.74
81/2					0.97	0.79
83/4					1.00	0.82
9						0.84
91/2						0.90
10						0.95
101/2						1.00

- 1.  $c_{act}$  = actual edge distance at which anchor is installed (inches).
- 2.  $c_{cr}$  = critical edge distance for 100% load (inches).
- 3.  $c_{min}$  = minimum edge distance for reduced load (inches).
- 4.  $f_{\rm C}$  = adjustment factor for allowable load at actual edge distance.
- 5.  $f_{ccr}$  = adjustment factor for allowable load at critical edge distance.  $f_{ccr}$  is always = 1.00.
- 6.  $f_{cmin}$  = adjustment factor for allowable load at minimum edge distance.
- 7.  $f_C = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min}) / (c_{cr} c_{min})].$

# Spacing Tension and Shear (f<sub>s</sub>)

	Size	1/4	3/8 9	3/8	1/210	1/2	5/8	3/4
	Ε	1	3/4	11/2	1	2	21/2	31/8
s <sub>act</sub> (in.)	Scr	4	3	6	4	8	10	121/2
(111.)	S <sub>min</sub>	2	1 1/2	3	2	4	5	61/4
	f <sub>smin</sub>	0.50	0.50	0.50	0.50	0.50	0.50	0.50
1 1/2			0.50					
2		0.50	0.67		0.50			
21/2		0.63	0.83		0.63			
3		0.75	1.00	0.50	0.75			
31/2		0.88		0.58	0.88			
4		1.00		0.67	1.00	0.50		
41/2				0.75		0.56		
5				0.83		0.63	0.50	
5½				0.92		0.69	0.55	
6				1.00		0.75	0.60	
61/4						0.78	0.63	0.50
7						0.88	0.70	0.56
8						1.00	0.80	0.64
9							0.90	0.72
10							1.00	0.80
11								0.88
12								0.96
121/2								1.00

- 1. E = Embedment depth (inches).
- 2.  $s_{act}$  = actual spacing distance at which anchors are installed (inches).
- 3.  $s_{cr}$  = critical spacing distance for 100% load (inches).
- 4.  $s_{min}$  = minimum spacing distance for reduced load (inches).
- 5.  $f_s$  = adjustment factor for allowable load at actual spacing distance.
- 6.  $f_{SCT} =$  adjustment factor for allowable load at critical spacing distance.  $f_{SCT}$  is always = 1.00.
- 7.  $f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.
- 8.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$
- 9. %" short drop-in (DIA37S).
- 10.1/2" short Drop-in (DIA50S)



# **Drop-In** (DIA) Design Information — Concrete



**Mechanical** Anchors

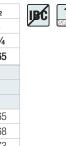
Allowable Load-Adjustment Factors for Short Drop-in Anchors in Sand-Lightweight Concrete over Metal Deck: Edge Distance and Spacing, Tension and Shear Loads

### How to use these charts:

- 1. The following tables are for reduced edge distance and spacing.
- 2. Locate the anchor size to be used for either a tension and/or shear load
- 3. Locate the edge distance ( $c_{act}$ ) or spacing ( $s_{act}$ ) at which the anchor is to be installed.
- 4. The load adjustment factor ( $f_c$  or  $f_s$ ) is the intersection of the row and column.
- 5. Multiply the allowable load by the applicable load adjustment factor.
- 6. Reduction factors for multiple edges or spacing are multiplied

### Edge Distance Tension (f<sub>c</sub>)

Edge	Size	3/8	1/2
Dist.	c <sub>cr</sub>	6	8
Cact	C <sub>min</sub>	31/2	43/4
(in.)	f <sub>cmin</sub>	0.65	0.65
31/2		0.65	
4		0.72	
41/2		0.79	
43/4		0.83	0.65
5		0.86	0.68
51/2		0.93	0.73
6		1.00	0.78
61/2			0.84
7			0.89
71/2			0.95
8			1.00



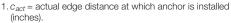
See notes below

### Edge Distance Shear (f<sub>c</sub>)

Edgo	Size	3/8	1/2
Edge Dist.	c <sub>cr</sub>	7	9%
c <sub>act</sub>	C <sub>min</sub>	31/2	43/4
(in.)	f <sub>cmin</sub>	0.45	0.45
31/2		0.45	
4		0.53	
41/2		0.61	
43/4		0.65	0.45
5		0.69	0.48
51/2		0.76	0.54
6		0.84	0.60
61/2		0.92	0.66
7		1.00	0.72
71/2			0.78
8			0.84
81/2			0.90
9			0.96
9%			1.00



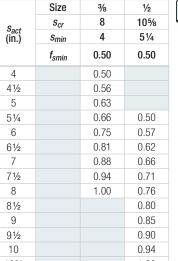
Edge	Size	3/8	1/2	
Dist.	c <sub>cr</sub>	7	9%	
cact	C <sub>min</sub>	31/2	43/4	
(in.)	f <sub>cmin</sub>	0.45	0.45	
31/2		0.45		
4		0.53		
41/2		0.61		
43/4		0.65	0.45	
5		0.69	0.48	
51/2		0.76	0.54	
6		0.84	0.60	
61/2		0.92	0.66	
7		1.00	0.72	
71/2			0.78	
8			0.84	
81/2			0.90	
9			0.96	
9%			1.00	



- $2.c_{cr}$  = critical edge distance for 100% load (inches).
- $3.c_{min}$  = minimum edge distance for reduced load (inches).
- 4.  $f_{\rm G}$  = adjustment factor for allowable load at actual edge distance.
- 5.  $f_{ccr}$  = adjustment factor for allowable load at critical edge distance.  $f_{ccr}$  is always = 1.00.
- 6.  $f_{cmin}$  = adjustment factor for allowable load at minimum edge distance.
- 7.  $f_c = f_{cmin} + [(1 f_{cmin}) (c_{act} c_{min}) / (c_{cr} c_{min})].$

# Spacing Tension and Shear (f<sub>s</sub>)

	Size	3/8	1/2
c .	S <sub>cr</sub>	8	10%
s <sub>act</sub> (in.)	Smin	4	51/4
	f <sub>smin</sub>	0.50	0.50
4		0.50	
41/2		0.56	
5		0.63	
51/4		0.66	0.50
6		0.75	0.57
61/2		0.81	0.62
7		0.88	0.66
71/2		0.94	0.71
8		1.00	0.76
81/2			0.80
9			0.85
91/2			0.90
10			0.94
10%			1.00





- $2. s_{cr}$  = critical spacing distance for 100% load (inches).
- 3. s<sub>min</sub> = minimum spacing distance for reduced load (inches).
- 4.  $f_S$  = adjustment factor for allowable load at actual spacing
- 5.  $f_{SCT}$  = adjustment factor for allowable load at critical spacing distance.  $f_{SCI}$  is always = 1.00.
- 6.  $f_{smin}$  = adjustment factor for allowable load at minimum spacing distance.
- 7.  $f_s = f_{smin} + [(1 f_{smin}) (s_{act} s_{min}) / (s_{cr} s_{min})].$

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Hollow Drop-In Internally Threaded Anchor



The Simpson Strong-Tie® Hollow Drop-In Anchor (HDIA) is an internally threaded, flush-mount expansion anchor for use in hollow materials such as CMU and hollow-core plank, as well as in solid base materials such as brick, normal-weight and lightweight concrete.

### Features:

- Suitable for suspending conduit, cable trays, pipe supports, fire sprinklers and suspended lighting into concrete
- Expansion design allows HDIA to anchor into CMU, hollow-core plank, brick, normal-weight concrete and lightweight concrete
- Internally threaded anchor allows for easy bolt removal

**Material:** Die-cast Zamac 3 alloy shell with carbon-steel cone or 304 stainless-steel cone

Codes: Factory Mutual 3053987 (%"-1/2" diameter) Underwriters Laboratories EX3605 (%"-1/2" diameter)





# Hollow Drop-In Anchor

		Drill Bit	Threads	Overall	Quantity	
Size	Model No.	Diameter (in.)	(per in.)	Anchor Length (in.)	Pkg. Quantity	Carton Quantity
1/4"	HDIA25	3/8	20	3/4	100	1600
1/4"	HDIA25SS	3/8	20	3/4	100	1600
5/16"	HDIA31	5/8	18	1 1/4	50	200
3/8"	HDIA37	5/8	16	1 1/4	50	200
3/8"	HDIA37SS	5/8	16	1 1/4	50	200
1/2"	HDIA50	3/4	13	13/4	50	250
5/8"	HDIA62	1	11	2	25	125

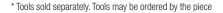


### Setting Tool for Hollow Materials\*

			Quantity		
Size	Model No.	For Use With	Pkg. Quantity	Carton Quantity	
1/4"	HDIASTH25	HDIA25, HDIA25SS	_	25	
5/16"	HDIASTH31	HDIA31	_	25	
3/8"	HDIASTH37	HDIA37, HDIA37SS	_	25	
1/2"	HDIASTH50	HDIA50		25	
5/8"	HDIASTH62	HDIA62	_	10	

### Setting Tool for Solid Materials\*

			Quantity		
Size	Model No.	For Use With Pkg. Quantity		Carton Quantity	
1/4"	HDIASTS25	HDIA25, HDIA25SS	25	125	
5/16" - 3/8"	HDIASTS31 - 37	HDIA31, HDIA37, HDIA37SS	10	50	
1/2"	HDIASTS50	HDIA50	10	50	
5/8"	HDIASTS62	HDIA62	5	20	





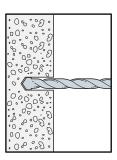


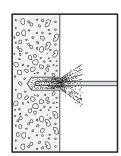
# Hollow Drop-In Internally Threaded Anchor

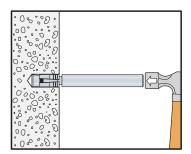


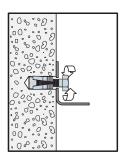
# Installation Instructions - Solid Base (using solid setting tool)

- Drill a hole in the base material using the appropriate diameter carbide drill bit as specified in the table. Drill the hole to the specified embedment depth.
- Blow the hole clean using compressed air. Overhead installations need not be blown clean.
- Insert the HDIA into hole. Tap with hammer until flush against surface.
- Using the designated setting tool, drive the anchor to the bottom of the drilled hole. After the anchor reaches the bottom of the drilled hole, perform an additional 3 hammer blows against the setting tool to drive the anchor body over the cone.
- Position fixture; insert fastener and tighten.



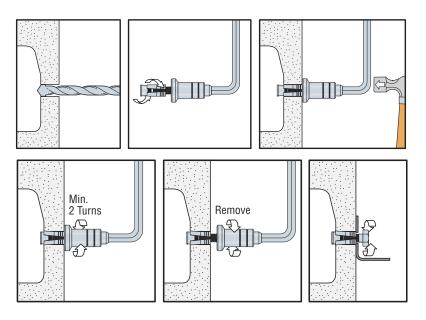






# Installation Instructions — Hollow Base (using hollow setting tool)

- Drill a hole in the base material using the appropriate diameter carbide drill bit as specified in the table.
- Thread the HDIA onto the designated setting tool for hollow base materials.
- Insert the HDIA into the hole. Tap the setting tool until the face of the tool contacts the surface.
- Rotate the setting tool a minimum of 2 turns to set the anchor.
- · Remove the setting tool.
- Position fixture; insert fastener and tighten.



# Hollow Drop-In Design Information — Concrete and Masonry



# Allowable Tension Loads for Hollow Drop-In Anchor in Normal-Weight Concrete



	0:	Drill Bit	Drill Bit Embed Critical Critical Tension L				n Load	Load		
Model	Size in.	Dia.	Depth	Edge Dist.	1 . 0   1 t = 2,000 por		si (17.2 MPa)	f' <sub>c</sub> ≥ 4,000 p	si (27.6 MPa)	
No.	(mm)	in. (mm)	in. (mm)	in. (mm)	in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	
HDIA25, HDIA25SS	1/4 (6.4)	3/8 (9.5)	7/8 (22)	<b>2</b> 5/8 (67)	<b>3½</b> (89)	<b>1,180</b> (5.2)	<b>295</b> (1.3)	<b>1,220</b> (5.4)	<b>305</b> (1.4)	
HDIA31	5/16 (7.9)	5 <b>%</b> (15.9)	<b>1 ½</b> (38)	<b>4½</b> (114)	<b>6</b> (152)	<b>3,000</b> (13.3)	<b>750</b> (3.3)	<b>3,420</b> (15.2)	<b>855</b> (3.8)	
HDIA37, HDIA37SS	<b>3/8</b> (9.5)	<b>5%</b> (15.9)	<b>1 ½</b> (38)	<b>4½</b> (114)	<b>6</b> (152)	<b>3,000</b> (13.3)	<b>750</b> (3.3)	<b>3,420</b> (15.2)	<b>855</b> (3.8)	
HDIA50	<b>½</b> (12.7)	<b>3/4</b> (19.1)	<b>2</b> (51)	<b>6</b> (152)	<b>8</b> (203)	<b>4,260</b> (18.9)	<b>1,065</b> (4.7)	<b>5,500</b> (24.5)	<b>1,375</b> (6.1)	
HDIA62	<b>5/8</b> (15.9)	<b>1</b> (25.4)	<b>21/4</b> (57)	<b>6¾</b> (171)	<b>9</b> (229)	<b>6,100</b> (27.1)	<b>1,525</b> (6.8)	<b>6,300</b> (28.0)	<b>1,575</b> (7.0)	

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. The minimum concrete thickness is 11/2 times the embedment depth.
- 3. Allowable loads may be linearly interpolated between concrete strengths listed.

# Allowable Shear Loads for Hollow Drop-In Anchor in Normal-Weight Concrete



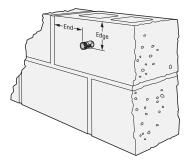
	c: Drill Bit	Embed	Critical	Critical		d Based on Strength	Shear Load Based on Steel Strength		
Model No.	Size in. (mm)	Dia. in.	Depth in.	Edge Dist. in.	Spacing in.	Spacing   f' > 2 500 psi (17 2 MPa)		F1554 Grade 36	A193 Grade B7
	()	(mm)	(mm)	(mm)	(mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)	Allowable lb. (kN)
HDIA25, HDIA25SS	1/4 (6.4)	<b>3/8</b> (9.5)	<b>7/8</b> (22)	<b>25/8</b> (67)	<b>3½</b> (89)	<b>1,840</b> (8.2)	<b>460</b> (2.0)	<b>485</b> (2.2)	<b>1,045</b> (4.6)
HDIA31	<b>5/16</b> (7.9)	<b>5%</b> (15.9)	<b>1½</b> (38)	<b>4½</b> (114)	<b>6</b> (152)	<b>2,660</b> (11.8)	<b>665</b> (3.0)	<b>755</b> (3.4)	<b>1,630</b> (7.3)
HDIA37, HDIA37SS	3/8 (9.5)	<b>5%</b> (15.9)	<b>1½</b> (38)	<b>4½</b> (114)	<b>6</b> (152)	<b>3,580</b> (15.9)	<b>895</b> (4.0)	<b>1,085</b> (4.8)	<b>2,340</b> (10.4)
HDIA50	<b>½</b> (12.7)	<b>3/4</b> (19.1)	<b>2</b> (51)	<b>6</b> (152)	<b>8</b> (203)	<b>8,220</b> (36.6)	<b>2,055</b> (9.1)	<b>1,930</b> (8.6)	<b>4,160</b> (18.5)
HDIA62	<b>5%</b> (15.9)	<b>1</b> (25.4)	<b>21/4</b> (57)	<b>6¾</b> (171)	<b>9</b> (229)	<b>10,180</b> (45.3)	<b>2,545</b> (11.3)	<b>3,025</b> (13.5)	<b>6,520</b> (29.0)

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. The minimum concrete thickness is 1  $\frac{1}{2}$  times the embedment depth.
- 3. Allowable load must be the lesser of the load based on anchor strength or steel strength.

# Allowable Tension and Shear Loads for Hollow Drop-In Anchor in 8" Lightweight, Medium-Weight and Normal-Weight Hollow CMU



	Size	Drill Bit	Embed	Minimum	Minimum	Minimum	Tensio	n Load	Shea	Shear Load		
Model No.	in. (mm)	Dia. in. (mm)	Depth <sup>4</sup> in. (mm)	Edge Dist. in. (mm)	End Dist. in. (mm)	Spacing in. (mm)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)		
HDIA25, HDIA25SS	<b>1/4</b> (6.4)	<b>3/8</b> (9.5)	<b>3/4</b> (19)	<b>4</b> (102)	<b>4</b> % (117)	<b>8</b> (203)	<b>500</b> (2.2)	<b>100</b> (0.4)	<b>975</b> (4.3)	<b>195</b> (0.9)		
HDIA31	<b>5/16</b> (7.9)	<b>5%</b> (15.9)	<b>1 1/4</b> (32)	<b>4</b> (102)	<b>4</b> % (117)	<b>8</b> (203)	<b>500</b> (2.2)	<b>100</b> (0.4)	<b>1,450</b> (6.4)	<b>290</b> (1.3)		
HDIA37, HDIA37SS	<b>3/8</b> (9.5)	<b>5%</b> (15.9)	<b>1 1/4</b> (32)	<b>4</b> (102)	<b>4</b> % (117)	<b>8</b> (203)	<b>500</b> (2.2)	<b>100</b> (0.4)	<b>1,450</b> (6.4)	<b>290</b> (1.3)		
HDIA50	<b>½</b> (12.7)	<b>3/4</b> (19.1)	<b>13/4</b> (44)	<b>4</b> (102)	<b>4</b> % (117)	<b>8</b> (203)	<b>1,525</b> (6.8)	<b>305</b> (1.4)	<b>2,300</b> (10.2)	<b>460</b> (2.0)		
HDIA62	<b>5%</b> (15.9)	<b>1</b> (25.4)	<b>2</b> (51)	<b>4</b> (102)	<b>4</b> 5/8 (117)	<b>8</b> (203)	<b>1,525</b> (6.8)	<b>305</b> (1.4)	<b>2,325</b> (10.3)	<b>465</b> (2.1)		



- 1. The allowable loads listed are based on a safety factor of 5.0.
- 2. Values for 8-inch wide lightweight, medium-weight, and normal-weight CMU.
- 3. The minimum specified compressive strength of masonry,  $f'_m$ , at 28 days with a minimum face shell thickness of 11/4" is 1,500 psi.
- 4. The installed end of the anchor may extend into the CMU cavity depending upon face shell thickness.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **LSES** Lag Screw Expansion Shield



The Lag Screw Expansion Shield is a die-cast zinc alloy expansion shield for anchoring lag screws in a variety of base materials, including concrete, concrete block, brick and mortar joints. Radial ribs provide additional holding power in softer material.

Material: Die-cast Zamac 3 alloy

### Installation



**Caution:** Oversized holes may make it impossible to set the anchor and will reduce the anchor's load capacity.

- 1. Drill a hole in the base material using the appropriate diameter carbide drill bit as specified in the table. Drill the hole to the specified embedment depth plus 1/8" for flush mounting and blow it clean using compressed air. Alternatively, drill the hole deep enough to accommodate embedment depth and dust from drilling. Overhead installations need not be blown clean.
- 2. Insert anchor into hole. Tap with hammer until flush with surface of base material.
- 3. Position fixture, insert screw and tighten.



**LSES** 

# LSES Product Data and Allowable Tension Loads in Normal-Weight Concrete

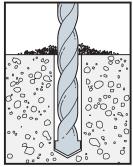


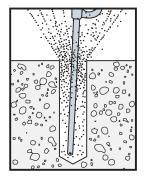


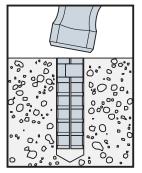


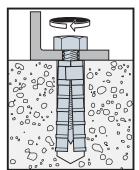
Eddad ii i voight dendicte — — —									
Size (in.)	Model No.	Drill Bit Dia.	Embed. Depth	Allowable Tension Load (lb.)	Quantity				
(,	140.	(in.)	(in.) $f'_c \ge 3,000 \text{ psi}$		Box	Carton			
1/4 Short	LSES25S	1/2	1	90	100	500			
5/16 Short	LSES31S	1/2	1 1/4	100	100	500			
3/8 Short	LSES37S	5/8	13/4	220	50	250			
½ Short	LSES50S	3/4	2	250	25	125			
1/4 Long	LSES25L	1/2	1 ½	120	50	250			
5∕16 Long	LSES31L	1/2	13/4	150	50	250			
% Long	LSES37L	5/8	21/2	260	50	200			
½ Long	LSES50L	3/4	3	310	25	100			

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. The minimum concrete thickness is 11/2 times the embedment depth.
- 3. Screw is not included.









<sup>\*</sup> See page 12 for an explanation of the load table icons.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **ESA** Expansion Screw Anchor



The ESA was the original internally threaded mechanical anchor design. The malleable lead shield allows for secure mounting.

**Material:** Cone: Die-cast Zamac 3 alloy; expander shield: 3–5% antimonial lead

**Code:** Meets Federal Specifications A-A-1922A, Type 1, except ESA50.

### Installation

- 1. Drill a hole in the base material using the appropriate-diameter carbide drill bit as specified in the table. Drill the hole to the specified embedment depth plus 1/8" for flush mounting. Blow the hole clean using compressed air. Overhead installations need not be blown clean.
- 2. Insert anchor into hole.
- 3. Using a piloted setting punch, drive expander shield over cone.
- 4. Position fixture, insert fastener and tighten.

# ESA Product Data and Allowable Tension Loads in Normal-Weight Concrete



Internal Thread Size	Model No.	Drill Bit	Embed.	Allowable Tension Load (lb.)	Quantity	
(dia threads per in.)		Dia. (in.)	Depth (in.)	f' <sub>c</sub> ≥ 3,000 psi	Box	Carton
1/4 - 20	ESA25	1/2	7/8	190	100	500
<b>%</b> - 16	ESA37	3/4	1 1/4	380	50	200
1⁄2 - 13	ESA50	7/8	1 ½	400	50	200

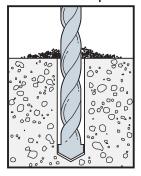


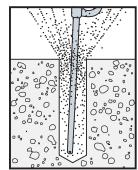
**ESA** 

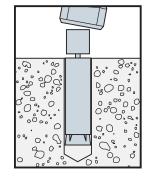
**Piloted Setting Punch** 

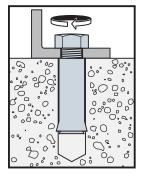
# Piloted Setting Punch Product Data

Model No.	For Use With	Box Qty.
PSP25	ESA25	10
PSP37	ESA37	10
PSP50	ESA50	10









<sup>\*</sup> See page 12 for an explanation of the load table icons.

# SIMPSON Strong-Tie

Zinc Nailon™ anchors are low-cost, easy-to-install anchors for applications under static loads.

### **Features**

- Available with carbon and stainless-steel pins
- Pin and head configuration designed to make anchor tamperresistant

### **Materials**

- Body Die-cast Zamac 3 alloy
- Pin Carbon steel; Type 304 stainless steel

Code: Meets Federal Specification A-A-1925A, Type 1

### Installation

Caution: Not for use in overhead applications.

 $\overline{\Lambda}$ 

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

Caution: Nailon anchors are not recommended for eccentric tension (prying) loads — capacity will be greatly reduced in such applications

- 1. Drill a hole in base material using a carbide drill bit the same diameter as the nominal diameter of the anchor to be installed. Drill the hole to specified embedment depth, plus ¼" for pin extension, and blow hole clean using compressed air. Alternatively, drill the hole deep enough to accommodate embedment depth and dust from drilling.
- 2. Position fixture and insert Nailon anchor.
- 3. Tap with hammer until flush with fixture, then drive pin until flush with top of head.



Zinc Nailon™ Anchor (Mushroom)

# Zinc Nailon™ Product Data

Carbon Steel	Stainless Steel	Quantity			
Pin Model No.	Pin Model No.	Box	Carton	Bulk	
ZN18078	_	100	1,600	3,000	
ZN25034	ZN25034SS	100	500	2,000	
ZN25100	ZN25100SS	100	500	1,500	
ZN25114	ZN25114SS	100	500	1,500	
ZN25112	ZN25112SS	100	500	1,000	
ZN25200	ZN25200SS	100	400	1,000	
ZN25212	ZN25212SS	100	400	1,000	
ZN25300	ZN25300SS	100	400	1,000	
	Pin Model No.  ZN18078  ZN25034  ZN25100  ZN25114  ZN25112  ZN25200  ZN25212	Pin Model No.         Pin Model No.           ZN18078         —           ZN25034         ZN25034SS           ZN25100         ZN25100SS           ZN25114         ZN25114SS           ZN25112         ZN25112SS           ZN25200         ZN25200SS           ZN25212         ZN25212SS	Pin Model No.         Pin Model No.         Box           ZN18078         —         100           ZN25034         ZN25034SS         100           ZN25100         ZN25100SS         100           ZN25114         ZN25114SS         100           ZN25112         ZN25112SS         100           ZN25200         ZN25200SS         100           ZN25212         ZN25212SS         100	Pin Model No.         Pin Model No.         Box         Carton           ZN18078         —         100         1,600           ZN25034         ZN25034SS         100         500           ZN25100         ZN25100SS         100         500           ZN25114         ZN25114SS         100         500           ZN25112         ZN25112SS         100         500           ZN25200         ZN25200SS         100         400           ZN25212         ZN25212SS         100         400	

# Allowable Tension and Shear Loads for Zinc Nailon™ in Normal-Weight Concrete

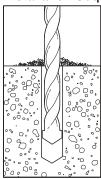
	- 2	
	l ſ	
106		
III.		
IDU	L	
	l F	

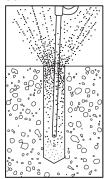


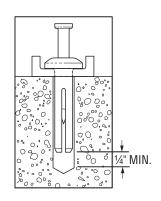


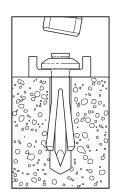
	5 W 50		Ultimate I	oads (lb.)	Allowable Loads (lb.)¹		
Size (in.) Drill Bit	Embed. Depth (in.)	$f'c \geq 3$ ,	000 psi	f' <i>c</i> ≥ 3,000 psi			
	Dia. (iii.)	Dopar ()	Tension	Shear	Tension	Shear	
3/16	3/16	5/8	460	465	115	115	
		5/8	590	635	150	160	
1/4	/ <sub>4</sub> 1/ <sub>4</sub>	3/4	780	765	195	190	
		1 1/2	1,050	1,050	265	265	

<sup>1.</sup> The allowable loads are based on a safety factor of 4.0.









<sup>\*</sup> See page 12 for an explanation of the load table icons.

# Crimp Drive® Anchor



The Crimp anchor is an easy-to-install expansion anchor for use in concrete and grout-filled block. The pre-formed curvature along the shaft creates an expansion mechanism that secures the anchor in place and eliminates the need for a secondary tightening procedure. This speeds up anchor installation and reduces the overall cost.

Five crimp anchor head styles are available to handle different applications that include fastening wood or light-gauge steel, attaching concrete formwork, hanging overhead support for sprinkler pipes or suspended ceiling panels.

Material: Carbon steel

Coating: Zinc plated and mechanically galvanized

Codes: Factory Mutual 3031136 for the %" Rod Coupler.

Head Styles: Mushroom, rod coupler, countersunk, tie-wire and duplex

### Installation



**Warning:** Industry studies show that hardened fasteners can experience performance problems in wet or corrosive environments. Accordingly, with the exception of the duplex anchor, use these products in dry, interior and non-corrosive environments only.

- Drill a hole using the specified diameter carbide bit into the base material to a depth of at least ½" deeper than the required embedment.
- Blow the hole clean of dust and debris using compressed air. Overhead application need not be blown clean. Where a fixture is used, drive the anchor through the fixture into the hole until the head sits flush against the fixture.
- Be sure the anchor is driven to the required embedment depth. The rod coupler and tie-wire models should be driven in until the head is seated against the surface of the base material.

# Crimp Drive® Anchor Product Data

0:		111 05-1-6	Drill	Min.	Min.	Qua	ntity
Size (in.)	Model No.	Head Style/ Finish	Bit Dia. (in.)	Fixture Hole Size	Embed. (in.)	Pkg. Quantity	Carton Quantity
3/16 X 1 1/4	CD18114M				7/8	100	1600
3∕16 X 2	CD18200M				1 1/4	100	500
3/16 X 21/2	CD18212M		3/16	1/4	1 1/4	100	500
3∕16 X 3	CD18300M		/16	/4	11/4	100	500
3/16 X 3 1/2	CD18312M	Mushroom			11/4	100	500
3/16 X 4	CD18400M				1 1/4	100	500
1/4 x 1	CD25100M				7/8	100	1,600
1/4 x 1 1/4	CD25114M	Head/			7/8	100	1,600
1/4 x 1 1/2	CD25112M	Zinc Plated			1 1/4	100	1,600
1/4 x 2	CD25200M	ZIIIC FIAIGU	1/	5/16	1 1/4	100	500
1/4 x 21/2	CD25212M		1/4	9/16	11/4	100	500
1/4 x 3	CD25300M				11/4	100	500
1/4 x 31/2	CD25312M				11/4	100	500
1/4 x 4	CD25400M				11/4	100	500
3/8 x 2	CD37200M		0.4	7/	13/4	25	125
3% x 3	CD37300M		3/8	7/16	13/4	25	125
1/4 x 3	CD25300MG	Mushroom Head/ Mechanically Galvanized	1/4	5/16	11⁄4	100	500
1/4" Rod Coupler	CD25114RC	Rod Coupler/	3/16	N/A	1 1/4	100	500
3%" Rod Coupler	CD37112RC	Zinc Plated	1/4	N/A	1 ½	50	250
3/16 X 21/2	CD18212C				11/4	100	500
3/16 X 3	CD18300C		3/16	1/4	1 1/4	100	500
3∕16 X 4	CD18400C				1 1/4	100	500
1/4 X 1 1/2	CD25112C	Countersunk			1 1/4	100	500
1/4 X 2	CD25200C	Head/			11/4	100	500
1/4 X 21/2	CD25212C	Zinc Plated	1/4	5/16	11/4	100	500
1/4 x 3 1/4 x 31/2	CD25300C CD25312C				1 ½ 1 ½	100 100	500 400
1/4 X 4	CD25312C				1 1/4	100	400
1/4 x 3	CD25300CMG	Countersunk Head/			1 1/4	100	500
1/4 x 4	CD25400CMG	Mechanically Galvanized <sup>1</sup>	1/4	5/16	11/4	100	400
1/4" Tie Wire	CD25118T	Tie Wire/Zinc Plated	1/4	N/A	11/8	100	500
1/4" Duplex	CD25234D	Duplex Head/ Zinc Plated	1/4	5/16	11⁄4	100	500

 Mechanical galvanizing meets ASTM B695, Class 55, Type 1. Intended for some pressure-treated wood sill plate applications. Not for use in other corrosive or outdoor environments. See page 316 for details.



Mushroom Head

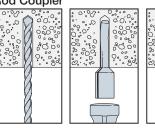
Rod Countersunk Coupler Head

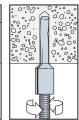
Tie-Wire

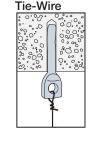
Duplex

# Installation Sequence

### **Rod Coupler**







### Mushroom Head





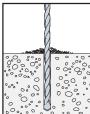


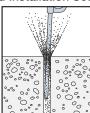
### **Duplex**

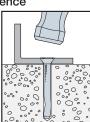


Duplex-head anchor may be removed with a claw hammer

# Countersunk Head Installation Sequence







**Mechanical** Anchors

# **Crimp Drive®** Design Information — Concrete



### Allowable Tension and Shear Loads in Normal-Weight Concrete



					Tensio	on Load	Shear	Load		
Size (in.)	Size Bit. De	Embed. Depth	Min. Spacing	Min. Edge Dist. (in.)	f' <sub>c</sub> ≥ 2,000 psi Concrete	$f'_c \ge 4,000 \text{ psi}$ Concrete	f' <sub>c</sub> ≥ 2,000 psi Concrete	f' <sub>c</sub> ≥ 4,000 psi Concrete		
(arry		(in.)	(in.)		Allowable Load (lb.)	Allowable Load (lb.)	Allowable Load (lb.)	Allowable Load (lb.)		
	Mushroom/Countersunk Head									
3/16	3/16	11/4	3	3	145	250	340	450		
1/4	1/4	11/4	3	3	175	275	395	610		
3/8	3/8	13/4	4	4	365	780	755	1,305		
				Duplex H	lead					
1/4	1/4	11/4	3	3	175	275	395	610		
				Tie Wi	re					
1/4	1/4	11/8	3	3	155	215	265	325		
				Rod Cou	pler <sup>4</sup>					
1/4	3/16	11/4	3	3	145	250	_	_		
3/8	1/4	1½	4	4	265	600	_	_		

- 1. The allowable loads listed are based on a safety factor of 4.0.
- 2. The minimum concrete thickness is 11/2 times the embedment depth.
- 3. Allowable loads may be linearly interpolated between concrete strengths listed.
- 4. For rod coupler, mechanical and plumbing design codes may prescribe lower allowable loads; verify with local codes.

# Allowable Tension and Shear Loads in Sand-Lightweight Concrete over Metal Deck

5



5

300

280

1. The allowable loads listed are based on a safety factor of 4.0.

1/4

3/8

- 3. Anchors may be installed off-center in the flute, up to 1" from the center of flute.

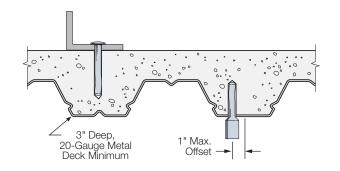
11/2

- 4. Anchor may be installed in either upper or lower flute.
- 5. Deck profile shall be 3" deep, 20-gauge minimum.
- For rod coupler, mechanical and plumbing design codes may prescribe lower allowable loads; verify with local codes.

### Length Identification Head Marks on Mushroom, Countersunk and Duplex-Head Crimp Drive Anchors (corresponds to length of anchor – inches)

		_					
Mark	0	Α	В	C	D	E	F
From	1	1 1/2	2	21/2	3	31/2	4
Up To But Not Including	1½	2	2½	3	3½	4	41/2

<sup>\*</sup> See page 12 for an explanation of the load table icons.



Sand-Lightweight Concrete
On Metal Deck

# **CSD/DSD** Split-Drive Anchors



The Split-Drive anchor is a one-piece expansion anchor that can be installed in concrete, grout-filled block and stone. As the anchor is driven in, the split-type expansion mechanism on the working end compresses and exerts force against the walls of the hole.

### **Features**

- Available in countersunk (CSD) and duplex-head (DSD) styles
- DSD anchor can be removed with a claw hammer for temporary applications

Material: Carbon steel

Coating: Zinc plated; mechanically galvanized

### Installation



Warning (CSD only): Industry studies show that hardened fasteners can experience performance problems in wet or corrosive environments. Accordingly, use these products in dry, interior and non-corrosive environments only.



Caution: Oversized holes in the base material will greatly reduce the anchor's load capacity. For CSD, embedment depths greater than 11/2" may cause bending during



- 1. Drill a hole in base material using a 1/4"-diameter carbide-tipped drill. Drill hole to specified embedment depth and blow clean using compressed air. (Overhead installation need not be blown clean.) Alternatively, drill hole deep enough to accommodate embedment depth and dust from drilling. Position fixture and insert split-drive anchor through fixture hole.
- 2. For CSD, %" diameter fixture hole is recommended for hard fixtures such as steel. For DSD, 5/16"-diameter fixture hole is recommended.
- 3. Drive anchor until head is flush against fixture.



(Duplex)

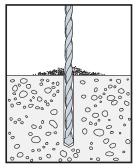
(Countersunk)

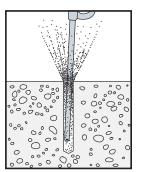
### CSD/DSD Product Data

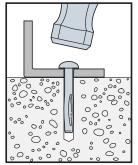
Size (in.)	Model No.	Head Style/Finish	Drill Bit	Qua	ntity
Size (III.) Would No.		ricau Style/Fillisii	Dia. (in.)	Box	Carton
1/4 X 1 1/2	CSD25112	Countersunk Head – Zinc Plated		100	500
1/4 x 2	CSD25200			100	500
1/4 x 2 1/2	CSD25212		1/	100	500
1/4 x 3	CSD25300		1/4	100	400
1/4 x 3 1/2	CSD25312			100	400
1/4 x 4	CSD25400			100	400
1/4 x 3	CSD25300MG	Countersunk Head – Mechanically	1/.	100	400
1/4 x 4	CSD25400MG	Galvanized1	1/4	100	400
1/4 x 3	DSD25300	Duplex Head – Zinc Plated	1/4	100	400

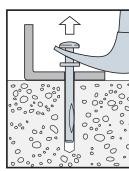
1. Mechanical galvanizing meets ASTM B695, Class 55, Type 1. Intended for some preservative-treated wood sill plate applications. Not for use in other corrosive or outdoor environments. See page 316 for details.

# Installation Sequence









DSD anchor may be removed with a claw hammer

# CSD Allowable Tension and Shear Loads in Normal-Weight Concrete

	Drill	Forth and	DAT:-	Min.	Tension	Load (lb.)	Shear L	oad (lb.)
Size	Bit	Embed. Depth	Spacing	Mill. Edge $f'_c \ge 2,000 \text{ psi}$ $f'_c \ge 2,000 \text{ psi}$		f' <sub>c</sub> ≥ 2,000 psi		000 psi
(in.)	Dia. (in.)	Dia. (in )	(in.)	Dist. (in.)	Ultimate Load	Allowable Load		
1/4	1/4	1 1/4	21/2	3	655	165	970	240

# DSD Allowable Tension and Shear Loads in Normal-Weight Concrete

Size	Drill Bit	Embea.	Min.	Min.	Concrete Compressive Tension Load (lb.) Shear Lo			oad (lb.)	
(in.)	Dia. (in.)	Depth (in.)	Spacing (in.)	Dist. (in.)	Strength (psi)	Ultimate Allowable Load		Ultimate Load	Allowable Load
1/4	1/4	11/4	21/2	3	2,500	800	200	2,480	620
1/4	1/4	11/4	21/2	3	4,000	1,060	265	2,740	685

<sup>\*</sup> See page 12 for an explanation of the load table icons.

SIMPSON Strong-Tie

Sure Wall anchors are self-drilling drywall anchors and provide excellent holding value and greater capacity than screws alone. This anchor cuts threads into drywall, greatly increasing the bearing surface and strength of the fastening.

### **Features**

- Self-drilling may be installed in gypsum board drywall with only a screwdriver
- Easy to remove and reinstall

Material: Die-cast zinc or reinforced nylon

# Sure Wall Product Data — Packaged with Screws

Screw	Model	Ctulo	Qua	ntity	Applications	
Size	No.	Style	Вох	Carton	Аррисация	
#6 x 7/8	SWN06S-R100	Nylon	100	500	3/8", 1/2" drywall, ceiling tile	
#8 x 1 1/4	SWN08LS-R100	Nylon	100	500	3/8", 1/2" drywall, ceiling tile	
#6 x 7⁄8	SWZ06S-R100	Zinc	100	500	3/8", 1/2" drywall, ceiling tile, plaster, pegboard	
#8 x 11/4	SWZ08LS-R100	Zinc	100	500	3/8", 1/2", 5/8" drywall, plaster	



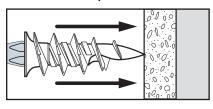


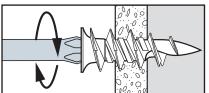
Sure Wall Nylon

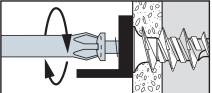
Sure Wall Zinc

# Sure Wall Product Data — Packaged Without Screws

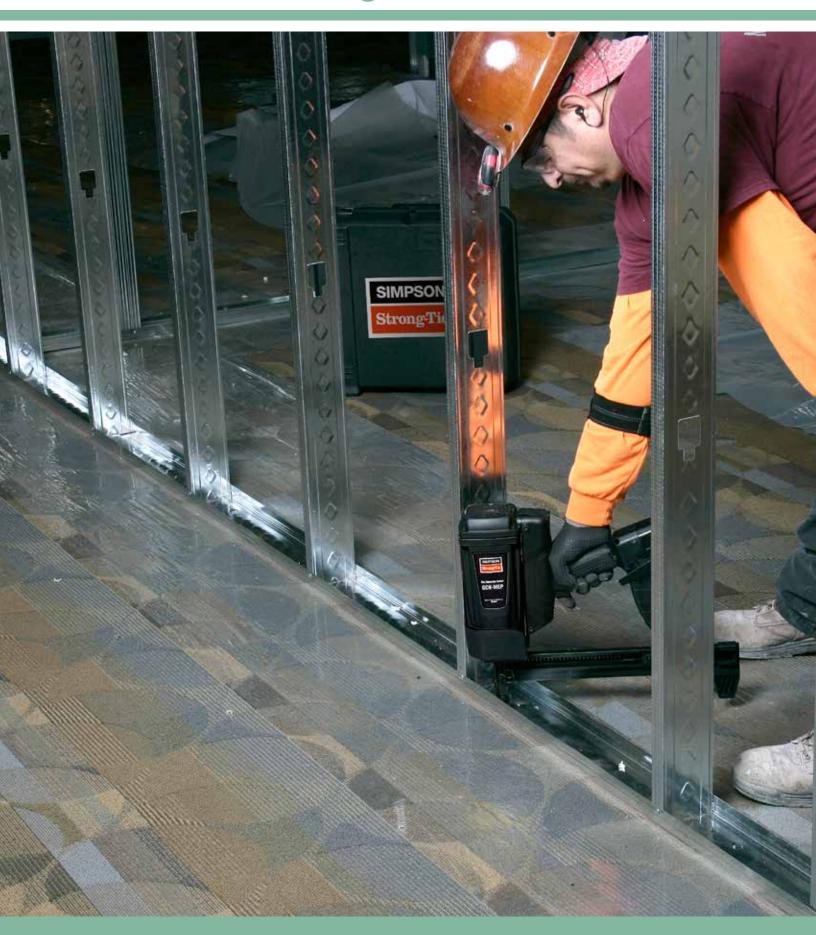
Screw	Model	Style	Quantity		Applications
Size	No.	Otylo	Box	Carton	Арріїсаціона
#6 x 7/8	SWN06-R100	Nylon	100	500	3/8", 1/2" drywall, ceiling tile
#8 x 11/4	SWN08L-R100	Nylon	100	500	3/8", 1/2" drywall, ceiling tile
#6 x 1	SWZ06-R100	Zinc	100	500	%", ½" drywall, ceiling tile, plaster, pegboard
#8 x 11⁄4	SWZ08L-R100	Zinc	100	500	3/8", 1/2", 5/8" drywall, plaster







# **Direct** Fastening Solutions







On the jobsite, time is money. That's why Simpson Strong-Tie offers a full range of gas- and powder-actuated tools and fasteners designed to maximize jobsite productivity and operator comfort in most applications.

Single-shot and fully automatic tool options efficiently drive our line of fasteners into concrete and steel. We also offer free online Powder-Actuated Tool certification at www.strongtie.com/pat.







# **GCN-MEPMAG** Gas-Actuated Concrete Nailer

SIMPSON
Strong-Tie

The GCN-MEPMAG and GCN-MEP gas-actuated concrete nailers are portable fastener tools for attaching light-duty fixtures to concrete, steel, concrete block (CMU), lightweight concrete over metal deck, and cold-formed steel. As a magazine tool, GCN-MEPMAG is ideal for attaching drywall track, furring strips, hat track and angle track using GDP and GDPS collated pins.

GCN-MEPMAG offers you the flexibility of having two tools in one convenient package — a magazine tool and a single-shot tool, since the magazine is easily removed without additional assembly tools. As a single-shot tool, the GCN-MEP is great for attaching mechanical, electrical and plumbing fixtures with pre-assembled pins/accessories such as washer pins, ceiling clips, tophats and threaded studs. The pre-assembled pins for the single-shot tool use 0.300"-headed fasteners with 0.125"-diameter shanks for stronger fastening performance.

Both the single-shot and magazine tool offer portability without the need for cords or hoses, and are actuated with GFC34 gas fuel cells.

### **Features**

- Power to drive 0.125"-diameter pins
- Flexibility to drive 1/2" to 11/2" pins
- Flexibility to drive 0.250" and 0.300" dia. headed pins
- Pin-depth adjustment dial
- · Battery charge indicator light
- Comfortable "sure-grip" rubber handle and ladder hook
- Easy start-up procedure: Insert fuel cell, insert battery, load pins, and begin use
- FREE tool first-aid repair program (see back cover of operators manual)

### **Specifications**

- Tool dimensions:
  - Length 12.5" (317.5 mm), 17" (432.8 mm)
  - Tool weight: 6.6 lb. (3 kg),8.3 lb. (3.7 kg) with magazine
  - Height 15.3" (389 mm)
- · Compatible fasteners:
  - Length: ½" (12.7 mm) to 1½" (38 mm)
  - Head diameter: 0.250" and 0.300"
  - Shank diameter: 0.106"
     to 0.125"

- Average number of shots per battery charge: 3,300
- Average number of shots per fuel cell: 1,200
- Average cyclic firing rate:2 shots per second
- Average battery charge time (6V NiMH): 2 hours
- Operation temperature range: 20°-120°F (-6°-49°C)
- Magazine capacity: 42
- Maximum fastenings before reloading: 40

The magazine is designed to retain two pins during use to prevent the tool from discharging without a fastener (which can damage the tool and possibly cause injury). The tool will resume normal operation when additional pins are loaded.

### Minimum Cleaning Required

The GCN-MEP has a very efficient ignition system that provides complete fuel combustion. This results in a cleaner operating tool, which, in turn, results in more tool energy and higher productivity. To maintain maximum level of productivity, periodic cleaning is recommended.

- Only requires cleaning every 20,000 shots
- Easy access to the air filter and piston chamber

# The GCN-MEP MAG gas-actuated concrete nailer is ideal for fastening:

- Drywall track
- · Lath wire for stucco
- Water-proofing membrane
- Furring strips









GCN-MEPKT or GCN-MEPMAGKT (with magazine)





# **Gas-Actuated** Concrete Nailing

# SIMPSON Strong-Tie

# **GDP Pins**

GDP concrete pins are designed to work with the GCN-MEPMAG gas-actuated concrete nailer as well as with most major-brand gas-actuated concrete-nailer tools. The patented 10-fastener strip is designed with break-away plastic. The pins are designed for use in A36 and A572 steel, concrete, CMU block and sand-lightweight concrete over metal deck.



**GDP** (U.S. Patent 605,016)

Codes: ICC-ES ESR-2811; Florida FL-15730; City of L.A. RR25837

### 0.106"-Diameter Shank Drive Pins

Model No.	Length (in.)	Qty. Pins / Pack +1 Fuel Cell	Packs/ Carton	Compatible with These Tools
GDP-50KT	1/2	1,000	5	
GDP-62KT	5/8	1,000	5	
GDP-75KT	3/4	1,000	5	Simpson Strong-Tie GCN-MEPMAG,
GDP-100KT	1	1,000	5	Others: TF1100, C3, TF1200
GDP-125KT	11/4	1,000	5	
GDP-150KT	1½	1,000	5	

# **GDPS** Pins

The GDPS pins are also designed to work in the GCN-MEPMAG gas-actuated nailer tool for installation into steel and concrete. The step-shank pin, with a smaller-diameter tip, facilitates easier penetration, while the larger-diameter upper shank provides more shear resistance and successful installation.



# 0.118"/0.102"-Diameter Stepped-Shank Drive Pins

Model	Length	Qty. Pins / Pack	Packs/	Compati	ble Tools	
No.	(in.)	+ 1 fuel cell	I fuel cell Carton Simpson Strong-Tie		Others	
GDPS-50KT	1/2	1,000	5			
GDPS-62KT	5/8	1,000	5	GCN-MEPMAG	TF1100, C3, TF1200	
GDPS-75KT	3/4	1,000	5			

# **Gas-Actuated** Concrete Nailing

# Spiral Knurl Gas Pins

GDPSK gas pins are designed for attaching plywood and OSB to cold-formed-steel studs. The spiral knurl provides a positive lock and resists back-out. Installed with the GCN-MEPMAG, the GDPSK-138 gas pin provides faster installation and setup times, which contributes to lower labor costs. The hardened pins quickly and cleanly pierce the cold-formed steel and leave the pin head flush with the wood fixture. The 1%" length pin can be used for ½"-¾" thick plywood, and 14-22 gauge steel.



Strong-Tie

### Spiral Knurl Gas Pins

Model	Length	Qty. Pins / Pack	Packs/	Compatible with
No.	(in.)	+ 1 fuel cell	Carton	These Tools
GDPSK-138KT	1%	1,000	5	

# GWL-100 Lathing Washer and **GMR-2 Magnetic Ring**

The GWL-100 lathing washer is used with the GCN-MEPMAG tool and attaches lath to the wall surface for overlaying scratch coats, brown coats and stucco. The washers are held onto the nose of the tool with the new GMR-2 magnetic ring and are attached to the substrate (including concrete and CMU) with GDP pins, which fasten through the washer. No extra tools are needed to install the magnetic ring to the nosepiece of the tool.



GMR-2

### Lathing Washer and Magnetic Ring

Model No.	Description	Pack Qty.	Carton Qty.
GWL-100 Lathing Washer, 1" Diameter		1,000	5,000
GMR-2	Magnetic Ring for GCN150	10	900

Lathing Washer and Magnetic Rings are sold separately.

# Fuel Cell

The GFC34 fuel cell is designed to operate with the GCN-MEPMAG and GCN-MEP, and with many major-brand gas-actuated concrete-nailer tools. The fuel cell provides 1,200 shots and can operate at temperatures between 20° and 120°F (-6°-49°C). The fuel cells are offered individually or in a two-per-pack clamshell. Additionally, one fuel cell is included with each pack of 1,000 pins.

### Gas Fuel Cells for the GCN-MEP

Model No.	Description	Pack Qty.	Packs/ Carton	Compatible with These Tools
GFC34	34-gram fuel cells	12	_	Simpson Strong-Tie <sup>®:</sup> GCN-MEP and GCN-MEPMAG
GFC34-RC2	(2) 34-gram fuel cells	2	6	Others: TrakFast® TF1100, Trak-It® C3



**GFC Fuel Cell** 

# **Gas-Actuated** Concrete Nailing



# GCN-MEP Gas-Actuated Pins and Assemblies for Mechanical, Electrical and Plumbing (MEP) Applications

Pre-assembled MEP fasteners are available for use with the GCN-MEP concrete nailer designed for high-volume applications, such as affixing conduit clips, rod hangers, cable ties and ceiling clips.

With their 0.300" heads, these versatile pins and assemblies can also be used with common powder-actuated tools when fastening into harder substrates (structural steel or extra-hard concrete) when required.

Codes: ICC-ES ESR-2811; Florida FL-15730



# Mechanical, Electrical and Plumbing Pins

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

All single-shot pins are 0.125" diameter x 1" except where specified.

Model No.	Description	Pack Qty.	Compatible Gas-Actuated Nailer
GRH25-R100	1/4" Rod hanger with pin	100	GCN-MEP, T3
GRH37-R100	%" Rod hanger with pin	100	GCN-MEP, T3
GCC50-R100	½" Conduit clip with pin	100	GCN-MEP, T3
GCC75-R100	3/4" Conduit clip with pin	100	GCN-MEP, T3
GCC100-R100	1" Conduit clip with pin	100	GCN-MEP, T3
GCC125-R50	1" Conduit clip (13 gauge steel) with pin	50	GCN-MEP, T3
GCL50-R50	½" Conduit clamp with pin	50	GCN-MEP, T3
GCL75-R25	3/4" Conduit clamp with pin	25	GCN-MEP, T3
GAC-R100	Angle clip with pin	100	GCN-MEP, T3
GCT-R50	Tie-strap holder with pin	50	GCN-MEP, T3
GW50-R200	1/2" Dome washer with 0.110" or 0.128" x 1/2" step-shank pin	200	GCN-MEP, T3
GW75-R200	½" Dome washer with 0.125 x ¾" pin	200	GCN-MEP, T3
GW100-R100	½" Dome washer with pin	100	GCN-MEP, T3
GTS4-5075-R200	$1\!/\!4$ Threaded stud, $1\!/\!2$ length $1\!/\!4$ -20 thread, $3\!/\!4$ length shank (0.127" dia.)	200	GCN-MEP, T3
GTH-R200	Tophat pin	200	GCN-MEP, T3

# **Extension Pole Tools**





# Advantages

- Modular lengths 2 ft., 6 ft., 8 ft.
- Lightweight

- Eliminates need for scaffolding
- Rugged and durable design

# Extension Poles for PT-27

Model	Description	Quantity
PEPT6	Complete 6 ft. pole	1
PEPT8	Complete 8 ft. pole	1

Extension poles for PTP-27L, PTP-27S, PTP-27SMAGR, PTP-27LMAGR, GCN-MEPMAG and GCN-MEP

Model	Description	Quantity
PEPT6LR	Complete 6 ft. pole	1
PEPT8LR	Complete 8 ft. pole	1

# **PAT Tool / Fastener Matrix**

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.



This matrix matches Simpson Strong-Tie powder-acutated tools with the powder loads and fasteners typically used with each tool.

		Premium Tools		Heavy-Duty Tool	Heavy-Duty Tool General-Purpose Tools					
Fasteners	Page No.	PTP-27L (page 256)	PTP- 27LMAGR (page 256)	PTP-27S (page 258)	PTP- 27SMAGR (page 258)	PT-27HDA (page 260)	PT-27 (page 261)	PT-22A (page 262)	PT-22HA (page 263)	PT-22P (page 264)
				Load	S					
P22AC (levels 2, 3, 4)	265							ALL	ALL	ALL
P22LRSC (levels 4, 5, 6, 7)	265									
P25SL (levels 3, 4, 5)	265									
P27LVL (levels 4, 5, 6)	265					ALL				
P27SL (levels 2, 3, 4, 5)	265	ALL	ALL	ALL	ALL		ALL			
P27SL6	265	✓	✓	✓	✓					
		0.300	"-Headed Fa	steners wit	h 0.157" Sh	ank Diamet	er			
PDPA-XXX	266	✓		✓		✓	✓	✓	Max 21/2"	✓
PDPAW-XXX	266	✓		✓			✓	✓	✓	✓
PDPAWL-XXX	266	✓		✓			✓	✓	✓	✓
PDPAS-XXX	267	✓		✓						
PDPAT-XXX	267	✓		✓		✓	✓	✓	✓	✓
PCLDPA-XXX	267	✓		✓			✓	✓	✓	✓
PECLDPA-XXX	267	✓		✓			✓	✓	✓	✓
PTRHA3-XXX	267	✓		✓			✓	✓	✓	✓
		0.300	"-Headed Fa	steners wit	h 0.145" Sh	ank Diamet	er			
PDPWL-XXSS	268	✓		Max 2"			✓	✓	✓	✓
PINW-XXX	268	✓		Max 2"			✓	✓	✓	✓
PINWP-XXX	268			Max 1 1/2"			Max 21/2"	✓	✓	Max 21/2"
PHBC-XXX	269	Max 21/2"		Max 1 1/2"			Max 21/2"	✓	✓	Max 21/2"
PCC-XXX	269	✓		✓			✓	✓	✓	✓
PBXDP-100	269	✓		✓			✓	✓	✓	✓
			8 n	nm-Headed	Fasteners					
PHN-XXX	270	Max 21/2"		Max 1%"		✓	Max 21/2"	✓	✓	Max 21/2"
PHNW-XXX	271			Max 2"			✓	✓	✓	✓
PHNT-XXX	271						✓	✓	✓	✓
PKP-250	271						✓	✓		✓
			%"-Heade	d Fasteners	/ Threaded	Studs				
PSLV3-XXX	270					✓				
	1/4"-Headed Fasteners / Threaded Studs									
PSLV4-XXX	269	✓		Max 11/2"		✓	✓	✓	✓	✓

# PAT Tool Matrix Powder-Actuated Fastening Systems



This matrix matches Simpson Strong-Tie® powder-actuated tools with the trades that would typically use each tool. The selection is based upon the features of the tool matching the needs of the trade.

	Premium Tools				
	PTP-27L	PTP-27LMAGR	PTP-27S	PTP-27SMAGR	
			1		
Features	<ul> <li>Adjustable Power</li> <li>Low Recoil/Noise</li> <li>2½" Pin Capacity (4" Pin with Washer)</li> </ul>	<ul> <li>Fully Automatic</li> <li>10-Fastener Magazine</li> <li>Adjustable Power</li> <li>Low Recoil/Noise</li> <li>27/6" Pin Capacity</li> </ul>	<ul> <li>Automatic</li> <li>Adjustable Power</li> <li>Low Recoil/Noise</li> <li>Drywall Track Tool</li> <li>1%" Pin Capacity</li> </ul>	<ul> <li>Fully Automatic</li> <li>Rotating Fastener Magazine</li> <li>10-Fastener Magazine</li> <li>Adjustable Power</li> <li>Low Recoil/Noise</li> <li>11/4" Pin Capacity</li> </ul>	
Cold-Formed Steel	Best	Better	Best	Better	
Drywall	Good	Good	Best	Best	
Electrical	Better		Better		
General	Best	Best			
Framer	Best	Best			
Plumbing/ Fire Sprinkler					
Acoustical/ Overhead	Good		Best		
Remodeling	Better	Better			
Carpentry	Better	Better			
Flooring	Better	Better	Good	Good	
Glazing			Better		
HVAC	Better		Best		
Rental	Better				

Premium Tools

# PAT Tool Matrix Powder-Actuated Fastening Systems



This matrix matches Simpson Strong-Tie® powder-actuated tools with the trades that would typically use each tool. The selection is based upon the features of the tool matching the needs of the trade.

	Heavy-Duty Tool	General-Purpose Tools			
	PT-27HDA	PT-27	PT-22A	PT-22HA	PT-22P
		1			
Features	Heavy-Duty     Single .27 Caliber Shot     Long     Reliable Design     %" Threaded     Stud Sprinkler Tool with     Stop Spall	<ul> <li>Semi-Automatic</li> <li>Versatile</li> <li>Reliable Professional Grade Tool</li> <li>2½" Pin Capacity (4" Pin with Washer)</li> </ul>	Single-Shot  Economical Professional-Grade Tool  3" Pin Capacity (4" Pin with Washer)	<ul><li>Single-Shot</li><li>Hammer-Activated</li><li>Medium-Duty</li><li>3" Pin Capacity</li></ul>	Single-Shot Versatile, Professional-Grade Tool 11/2" Pin Capacity 2" Pin with Washer
Drywall		Good			Best
Electrical		Good	Good	Good	Better
General		Better	Good		
Framer		Good	Good		
Plumbing/ Fire Sprinkler	Best				Good
Acoustical/ Overhead		Better	Good		Better
Remodeling		Better	Best	Best	Good
Carpentry		Best	Better	Better	
Flooring	Best				
Glazing		Good	Good		Better
Hvac		Better			
Rental					

**Direct** Fastening

### PTP-27L and PTP-27LMAGR Premium Tools



The PTP-27L and the PTP-27LMAGR are powder-actuated fastening tools designed to provide versatility and ease of use on the jobsite. Both tools deliver productive fastening with automatic piston reset, which enables the user to simply load and shoot. The PTP-27L is a single-shot tool with a longer barrel that can be easily affixed with a fastener magazine. The PTP-27LMAGR is a fully automatic tool with a fastener magazine that can rotate for easier access, or it can be quickly changed to a single-shot tool.

### **Features**

- Adjustable power for fastening versatility: 1-1½ power-level range from a single strip
- · Easy disassembly for cleaning and maintenance
- · No manual resetting of piston required
- Operator comfort: cushioned grip, reduced recoil and sound-dampening muffler for quiet operation

### **Key Fastening Applications**

- Sill plate installation
- Washered-pin installation (PTP-27L only)
- Insulation fastening (PTP-27L only)
- · Forming work
- · Cold-formed steel

### Specifications

• Fastener Length:

PTP-27L: 1/2" - 21/2" (3" or 4" washered)

PTP-27LMAGR: 5%" - 27%"

- Fastener Type: 0.300" (or 8 mm) diameter headed
- Firing Action:

PTP-27L: Automatic

PTP-27LMAGR: Fully automatic

- Load Caliber: 0.27 strip loads, brown through purple (levels 2-6)
- Length: 173/4" (PTP-27L), 191/2" (PTP-27LMAGR)
- Weight: PTP-27L 6.5 lb., PTP-27LMAGR - 8.8 lb.

### Available Kit Combinations

PTP-27L: Single-shot configuration with accessories

PTP-LMAGR: Parts to convert PTP-27L into magazine configuration

PTP-27LMAGR: Magazine configuration

with accessories

PTP-LCONKT: Parts to convert PTP-27LMAGR into a single-shot configuration

PTP-27LMAGRKT: Combination kit; includes tool and components for both single-shot and magazine configurations





The full line of Simpson Strong-Tie® powder loads and fasteners begins on page 265

### Tool is sold in a rugged tool box complete with

- · Operator's manual
- Spall suppressor
- Tools for disassembly
- · Safety glasses / ear plugs
- Tool lubricant
- · Cleaning brushes
- Operator's exam and caution sign
- · Tool box also sold separately
- Gloves

# PTP-27L and PTP-27LMAGR Premium Tools











Quick-disconnect baseplate makes it easy to convert the PTP-27LMAGR from a magazine to a single-shot tool.

### **Complementary Products**

Extension pole tool for the PTP-27L and PTP-27LMAGR available in 6' and 8' lengths



C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

PEPT6LR - 6' Tool and PEPT8LR - 8' Tool



Extension Pole Tool (for the PTP-27L) - See page 252 for details.

### Replacement Parts – PTP-27L

Description	Model No.
Baseplate	PTP-274800
Nosepiece	PTP-273820
Piston	PTP-273320
Piston Disc	PTP-273306
Rubber Returner	PTP-274305

### Replacement Parts - PTP-27LMAGR

Description	Model No.
Magazine (Complete)	PTP-LMAGR
Nosepiece	PTP-276820
Nosepiece Screw	PTP-275826
Piston	PTP-276320
Piston Disc	PTP-273306
Rubber Returner	PTP-274305

Complete tool schematics, tool repair, maintenance kits and parts list are available at www.strongtie.com.

### PTP-27S and PTP-27SMAGR Premium Tools



The PTP-27S and the PTP-27SMAGR are powder-actuated fastening tools designed to provide versatility and ease of use on jobs that require shorter fasteners. Both tools deliver productive fastening with automatic piston reset, which enables the user to simply load and shoot. The PTP-27S is a single-shot tool with a shorter barrel that can be easily affixed with a fastener magazine. The PTP-27SMAGR is a fully automatic tool with rotational fastener magazine that can be quickly changed to a single-shot tool.

### **Features**

- Adjustable power for fastening versatility: 1-11/2 power-level range from a single strip
- Operator comfort from cushioned grip, reduced recoil and sound-dampening muffler for quiet operation
- No manual resetting of piston required
- Easy disassembly for cleaning and maintenance

### **Key Fastening Applications**

### PTP-27S:

- · Conduit clips
- Ceiling clips
- Drywall track
- · Metal Decking

### PTP-27SMAGR:

- Drywall track
- Hat channel
- HVAC duct straps
- · Cold-formed steel
- Furring strips

### **Specifications**

· Fastener Length: PTP-27S: 1/2"-15/8" PTP-27SMAGR: 1/2"-11/4"

• Fastener Type: 0.300" or 8 mm diameter

• Firing Action:

PTP-27S: Automatic

PTP-27SMAGR: Fully automatic

- Load Caliber: 0.27 strip loads, brown through purple (levels 2-6)
- Length: 16¾" (PTP-27S), 17½" (PTP-27SMAGR)
- Weight: PTP-27S 6.25 lb., PTP-27SMAGR 8.1 lb.

# **PTP-27S** PTP-27SMAGR Adjustable power increases versatility



The full line of Simpson Strong-Tie® powder loads and fasteners begins on page 265.

### **Available Kit Combinations:**

PTP-27S: Single-shot configuration

with accessories

PTP-SMAGR: Parts to convert PTP-27S into magazine configuration

PTP-27SMAGR: Magazine configuration

with accessories

PTP-SCONKT: Parts to convert PTP-27SMAGR into a single-shot

configuration

PTP-27SMAGRKT: Combination kit: includes tool and components for both single-shot and magazine configurations

### Tool is sold in a rugged tool box complete with

- · Operator's manual
- Spall suppressor
- Tools for disassembly
- Safety glasses / ear plugs
- Tool lubricant
- · Cleaning brushes
- · Operator's exam and caution sign
- · Tool box also sold separately
- Gloves

# PTP-27S and PTP-27SMAGR Premium Tools







Rotating magazine allows for installation flexibility.



Quick-disconnect baseplate makes it easy to convert the PTP-27SMAGR from a magazine to a single-shot tool.



Collated pins make for fully automatic fastening and quick loading.

### **Complementary Products**

Extension pole tool for the PTP-27S and PTP-27SMAGR available in 6' and 8' lengths



C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

PEPT6LR - 6' Tool and PEPT8LR - 8' Tool



Extension Pole Tool (for the PTP-27S)  $-\,$  See page 252 for details.

### Replacement Parts - PTP-27S

riopideorrient raite i ii 210			
Description	Model No.		
Baseplate	PTP-273800		
Nosepiece	PTP-273820		
Piston	PTP-273320		
Piston Disc	PTP-273306		
Rubber Returner	PTP-273305		

### Replacement Parts - PTP-27SMAGR

Description	Model No.
Magazine Body (Complete)	PTP-SMAGR
Nosepiece	PTP-275800
Nosepiece Screw	PTP-275826
Piston	PTP-273320
Piston Disc	PTP-273306
Rubber Returner	PTP-273305

# PT-27HDA Powder-Actuated Heavy-Duty Stud Driver



The PT-27HDA is a low-velocity, heavy-duty powder-actuated tool designed for installing fasteners into poured and precast concrete, grout-filled concrete masonry block and horizontal grouted joints, as well as structural steel. This tool offers easy-cycling, single-shot firing action for continuous use, high reliability and low maintenance. The PT-27HDA features a spall suppressor, which reduces concrete spalling and helps keep the tool perpendicular to the work surface.

### Key features

- Heavy-duty stud driver for installing fasteners into steel or hard concrete
- Easy cycling pulling on the barrel ejects the shell and resets the piston
- Low recoil for greater operator comfort
- Spall suppressor to reduce concrete spalling and keep tool perpendicular to work surface
- Consistent and reliable performance
- Easy disassembly for cleaning and maintenance

### **Specifications**

- Fastener length: %" through 3"
- Fastener types: 1/4" 20-threaded studs, %" 16-threaded studs, 8 mm-headed fasteners and 0.300"-headed fasteners with 0.157" shank diameter
- Firing action: Single shot
- Load caliber: 0.27 long single loads, yellow through purple (levels 3–6)
- Length: 14½"Weight: 8 lb., 13 oz.

### **Key Fastening Applications**

- %" sprinkler fastenings
- Heavy-duty fastening in concrete strengths up to 8,000 psi
- Structural steel

# PT-27HDA is sold in a durable box complete with

- · Operator's manual
- Spall suppressor
- 8 mm fastener guide and pistons for use with PDPA, PSLV4 and PHN pins
- 10 mm fastener guide and pistons for use with PSLV3 pins
- Safety glasses / ear plugs
- Tool lubricant
- · Cleaning brushes
- · Operator's exam and caution sign
- 2 extra stop rings









Easy cycling: simply pull to eject the shell

### Replacement Parts - PT-27HDA

Description	Model No.	
8 mm Piston	PTHDA-700320	
8 mm Guide Assembly	PTHDA-700340	
10 mm Piston	PTHDA-700310	
10 mm Guide Assembly	PTHDA-700330	
Stop Ring / Buffer	PTHDA-700302	

# PT-27 General Purpose Tool



The PT-27 is a semi-automatic and fast-cycling fastening tool that is engineered for continuous use, high reliability and low maintenance. This versatile tool fires a variety of fastener types and lengths.

### **Key Fastening Applications**

- Acoustical ceilings
- Electrical applications
- Sill plates
- Drywall track
- Water proofing material and/or lathing

### **Specifications**

- Fastener Length: 1/2" 21/2" (3" or 4" washered)
- Fastener Type: .300" or 8 mm-headed fasteners or 1/4"-20 threaded studs
- Firing Action: Semi-automatic
- Load Caliber: 0.27 strip loads, brown through red (levels 2–5)
- Length: 131/2"
- Weight: 5 lb., 4 oz.

### Tool is sold in a rugged tool box complete with

- Operator's manual
- Spall suppressor
- Tools for disassembly
- Safety glasses / ear plugs
- Tool lubricant

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

- Cleaning brushes
- Operator's exam and caution sign



The full line of Simpson Strong-Tie® powder loads and fasteners begins on page 265

### Replacement Parts - PT-27

Description	Model No.
Annular Spring	PT-301014
Ball Bearing (6 mm)	PT-301013
Barrel	PT-301006
Baseplate	PT-301009
Piston – Concave (includes ring)	PT-301217
Piston – Flat (includes ring)	PT-301903
Piston Ring	PT-301208
Piston Stop	PT-301012
Shear Clip	PT-301011

For tool repair and maintenance kits and complete tool schematics and parts list, visit www.strongtie.com.

### **Complementary Products**

Extension pole tool for the PT-27 available in 6' and 8' lengths



PEPT6 Tool and PEPT8 Tool



# PT-22A General-Purpose Tool



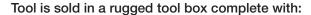
The PT-22A is a powder-actuated tool that uses 0.22 caliber "A" crimp loads, has single-shot firing action and is engineered for continuous use, high reliability and low maintenance.

### **Key Fastening Applications**

- Furring strips
- Framing pins
- Electrical boxes
- · Ceiling clips



- $\bullet$  Fastener Length:  $1\!\!/_2$  " 3" (3" and 4" washered)
- Fastener Type: 0.300" or 8-mm headed fasteners or 1/4"-20 threaded studs
- Firing Action: Single shot
- Load Caliber: 0.22 single "A" crimp loads, brown through yellow (levels 2–4). Note: Not for use with 0.22-caliber straight wall loads.
- Length: 13%"Weight: 4.4 lb.



- Operator's manual
- Spall guard
- Tools for disassembly\*
- Safety glasses / ear plugs\*
- Cleaning brushes\*
- Operator's exam and caution sign\*

### PT-22A Retail Package Product Data

Description	Model No.	Qty. of Tools Per Retail Package	Qty. of Retail Packages Per Carton
.22 Caliber, Single-Shot Trigger- Activated Tool	PT-22A-RB	1	2

### Replacement Parts

Description	Model No.
Nosepiece	PT22A-01
Piston Buffer	PT22A-02
Piston Reset Cap	PT22A-13
Piston Reset Pin	PT22A-11
Piston Reset Spring	PT22A-12
Piston with Ring	PT22A-03

- 1. Model PT-DC108 for tools with a serial number below 5000.
- 2. Model PT-DC107 for tools with a serial number below 5000.
- 3. Model PT-DC122 for tools with a serial number below 5000.
- 4. Complete tool schematics and parts list available at www.strongtie.com.





The PT-22A is sold individually in a tool box with accessories or in a retail package (see below).

The full line of Simpson Strong-Tie® powder loads and fasteners begins on page 265



PT-22A-RB

<sup>\*</sup>These items not supplied with the PT-22A-RB retail package.

# PT-22HA General-Purpose Tool



The PT-22HA is a hammer-activated tool engineered for low maintenance and economy. The tool offers three levels of power: Brown through yellow loads (levels 2–4).

### **Key Fastening Applications**

- Remodeling
- Maintenance
- Electricians
- Telecommunications



### **Specifications**

- Fastener Length: ½"–3"
  (4" washered)
- Fastener Type: 0.300" or 8 mm-headed fasteners or 1/4"-20 threaded studs
- Firing Action: Single shot, hammer activated
- Load Caliber: 0.22 single "A" crimp loads, brown through yellow (levels 2–4). Note: Not for use with 0.22-caliber straight wall loads.
- Length: 14¼"Weight: 2 lb., 12 oz.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

### PT-22H Retail Package Product Data

Description	Model No.	Qty. of Tools Per Retail Package	Qty. of Retail Packages Per Carton
0.22 Caliber, Single-Shot Hammer- Activated Tool	PT-22HA-RB	1	4



The PT-22HA-RB comes packaged in a retail clamshell ready for merchandising.



# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# PT-22P Powder-Actuated Tool

Strong-Tie

The PT-22P is a single-shot fastening tool engineered for continuous use, high reliability and low maintenance. The all-aluminum body of the PT-22P also provides rugged durability.

### **Key Fastening Applications**

- Drywall track
- Furring strips
- Framing pins
- Electrical boxes
- · Ceiling clips

### **Specifications**

- Fastener Length: 1/2"-11/2"
- Fastener Type: 0.300" or 8 mm-headed fasteners or 1/4"-20 threaded studs
- Firing Action: Single shot
- Load Caliber: 0.22 single "A" crimp loads, brown through yellow (levels 2-4). Note: Not for use with 0.22-caliber straight wall loads.
- Length: 14"
- Weight: 4 lb. 7 oz.

### Tool is sold in a rugged tool box complete with

- Operator's manual
- Spall guard
- Tools for disassembly
- Safety glasses / ear plugs
- Cleaning brushes
- Operator's exam and caution sign
- One additional piston

### Replacement Parts

Description	Model No.
Nosepiece	PT-22P-01
Stop Pin Cover	PT-22P-17
Barrel Stop Pin	PT-22P-20
Barrel Stop Pin Spring	PT-22P-21
Piston with Ring	PT-22P-02







The PT-22P is sold individually in a tool box with accessories.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **Powder Loads** for Powder-Actuated Tools

# SIMPSON Strong-Tie

### 0.22-Caliber "A" Crimp Loads - Single Shot

Description	Model	Dook Oty	Carton Oty	Oty Compatible Tools	
Description	Model	Pack Qty.	Carton Qty.	Simpson	Others
22 Cal Provin (Loval 2)	P22AC2	100	10,000		704 11 0000
.22 Cal. – Brown (Level 2)	P22AC2A	100	10,000	PT-22A	721, U-2000, DX-37E, DX72E,
.22 Cal. – Green (Level 3)	P22AC3	100	10,000	PT-22GS	4170 and model 70,
.22 Gal. — Green (Level 3)	P22AC3A	100	10,000	PT-22HA	System 3 and
22 Cal Vallous (Laval 4)	P22AC4	100	10,000	PT-22P	most low-velocity, single-shot tools
.22 Cal. – Yellow (Level 4)	P22AC4A	100	10.000		origio oriot toolo



0.22-Caliber Straight Wall Loads - Single Shot

Description	Model	Pack Qty.	Carton Qty.	Compatible Tools
.22 Cal Yellow (Level 4)	P22LRSC4	100	10,000	
.22 Cal. – Red (Level 5)	P22LRSC5	100	10,000	Ladd Tools,
.22 Cal Purple (Level 6)	P22LRSC6	100	10,000	and some special application tools
.22 Cal Gray (Level 7)	P7LRSC	100	10,000	4,



Note: Not for use with Simpson Strong-Tie PT-22, PT-22GS, or PT-22H tools.

### 0.25-Caliber Plastic 10-Shot Strip Loads

Description	Model	Pack Qty.	Carton Qty.	Compatible Tools
.25 Cal. – Green (Level 3)	P25SL3	100	10,000	
.25 Cal. – Green BULK PACK	P25SL3M	1,000	5,000	
.25 Cal. – Yellow (Level 4)	P25SL4	100	10,000	DX35, R355
.25 Cal. – Yellow BULK PACK	P25SL4M	1,000	5,000	DA30, N300
.25 Cal. – Red (Level 5)	P25SL5	100	10,000	
.25 Cal. – Red BULK PACK	P25SL5M	1,000	5,000	



P25SL

### 0.27-Caliber Single-Shot Loads - Long

Description	Model	Pack Qty.	Carton Qty.	Compatible Tools
.27 Cal Yellow (Level 4)	P27LVL4	100	10,000	DT OFFICE A DV4400
.27 Cal. – Red (Level 5)	P27LVL5	100	10,000	PT-27HDA, DX460, and Hilti DX600
.27 Cal Purple (Level 6)	P27LVL6	100	10,000	and mill DA000



P27I V

### 0.27-Caliber Plastic, 10-Shot Strip Loads

		D 1 01		Comp	atible Tools
Description	Model	Pack Qty.	Carton Qty.	Simpson Strong-Tie	Others
07 Cal Prove (Laval 0)	P27SL2	100	10,000		
.27 Cal. – Brown (Level 2)	P27SL2A	100	10,000		
07 Col Croop (Lovel 2)	P27SL3	100	10,000		DX-350, DX-351,
.27 Cal. – Green (Level 3)	P27SL3A	100	10,000	PTP-27L.	DX-36, DX-A40 (except PT27SL2), DX-A41 (except PT27SL2 and PT27SL3), DX-460, DX-450, DX-451, DX-460, System 1H, P-36B,
.27 Cal. – Green BULK PACK	P27SL3M	1,000	5,000		
O7 Cel Velley (Level 4)	P27SL4	100	10,000	PTP-27MAGR,	
.27 Cal. – Yellow (Level 4)	P27SL4A	100	10,000	PTP-27S,	
.27 Cal. – Yellow BULK PACK	P27SL4M	1,000	5,000	PTP-27SMAGR, PT-27	A-40B, A-41B, Cobra
O7 Cal Dad /Laval E)	P27SL5	100	10,000		and most 0.27-caliber
.27 Cal. – Red (Level 5)	P27SL5A	100	10,000		clone tools
.27 Cal. – Red BULK PACK	P27SL5M	1,000	5,000		
.27 Cal. – Purple (Level 6)	P27SL6	100	10,000		DX-450, DX-451, DX-A41

Note: An "A" in a part number denotes imported load. No "A" indicates a domestic load.



# PDPA Drive Pins

- Manufactured with tight tolerances for superior performance
- Code-listed per ICC-ES ESR-2138; City of L.A. RR25469; Florida FL-15730

### 0.300"-Headed Fasteners with 0.157" Shank Diameter

Length	Model		Pack	Carton	Compat	ible Tools
(in.)	No.	Description	Qty.	Qty.	Simpson Strong-Tie	Others
1/2	PDPA-50	0.157 x ½"	100	1,000		
½ knurled	PDPA-50K	0.157 x ½" knurl	100	1,000		
% knurled	PDPA-62K	0.157 x %" knurl	100	1,000		
3/4	PDPA-75	0.157 x ¾"	100	1,000	PTP-27L	721, D-60, U-2000
1	PDPA-100	0.157 x 1"	100	1,000	PTP-27S	
1 1/16	PDPA-106	0.157 x 1½16"	100	1,000	PT-27	
1 1/4	PDPA-125	0.157 x 11/4"	100	1,000	PT-27HDA PT-22A	and most other
1 5/16	PDPA-131	0.157 x 15/16"	100	1,000	PT-22GS	low-velocity tools
1 ½	PDPA-150	0.157 x 1½"	100	1,000	PT-22P	
1 1//8	PDPA-187	0.157 x 11/8"	100	1,000	PT-22HA	
2	PDPA-200	0.157 x 2"	100	1,000		
21/2	PDPA-250	0.157 x 2½"	100	1,000		
27/8	PDPA-287	0.157 x 21/8"	100	1,000		



This model available in mechanically galvanized finish (PDPA-287MG).

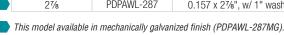
### 0.300"-Headed Fasteners with 0.157" Shank Diameter and 3/4" Metal Washers

Length	Model		Pack	Carton	Compat	ble Tools
(in.)	No.	Description	Qty.	Qty.	Simpson Strong-Tie	Others
1/2	PDPAW-50	0.157 x 1/2", w/ 3/4" washer	100	1,000		
½ knurled	PDPAW-50K	0.157 x 1/2" knurl, w/ 3/4" washer	100	1,000		
% knurled	PDPAW-62K	0.157 x %" knurl, w/ 3/4" washer	100	1,000		
3/4	PDPAW-75	0.157 x 3/4", w/ 3/4" washer	100	1,000	PTP-27L PTP-27S	721,
1	PDPAW-100	0.157 x 1", w/ 3/4" washer	100	1,000	PT-275	D-60, U-2000, System 1.
1 1/4	PDPAW-125	0.157 x 11/4", w/3/4" washer	100	1,000	PT-22P	System 3
1 ½	PDPAW-150	0.157 x 11/2", w/ 3/4" washer	100	1,000	PT-22A PT-22GS	and most other
1 1/8	PDPAW-187	0.157 x 11%", w/ 3/4" washer	100	1,000	PT-22GS PT-22HA	low-velocity tools
2	PDPAW-200	0.157 x 2", w/ 3/4" washer	100	1,000		
21/2	PDPAW-250	0.157 x 21/2", w/ 3/4" washer	100	1,000		
21/8	PDPAW-287	0.157 x 21/8", w/ 3/4" washer	100	1,000		



### 0.300"-Headed Fasteners with 0.157" Shank Diameter and 1" Metal Washers

Length	Model		Pack	Carton	Compat	ble Tools
(in.)	No.	Description	Qty.	Qty.	Simpson Strong-Tie	Others
1/2	PDPAWL-50	0.157 x 1/2", w/ 1" washer	100	1,000		
½ knurled	PDPAWL-50K	0.157 x 1/2" knurl, w/ 1" washer	100	1,000		
% knurled	PDPAWL-62K	0.157 x %" knurl, w/ 1" washer	100	1,000		
3/4	PDPAWL-75	0.157 x 3/4", w/ 1" washer	100	1,000	PTP-27L PTP-27S	721,
1	PDPAWL-100	0.157 x 1", w/ 1" washer	100	1,000	PT-275	D-60, U-2000, System 1.
11/4	PDPAWL-125	0.157 x 11/4", w/ 1" washer	100	1,000	PT-22P	System 3
1½	PDPAWL-150	0.157 x 11/2", w/ 1" washer	100	1,000	PT-22A PT-22GS	and most other
17/8	PDPAWL-187	0.157 x 11/8", w/ 1" washer	100	1,000	PT-22HA	low-velocity tools
2	PDPAWL-200	0.157 x 2", w/ 1" washer	100	1,000		
21/2	PDPAWL-250	0.157 x 21/2", w/ 1" washer	100	1,000		
27/8	PDPAWL-287	0.157 x 21/8", w/ 1" washer	100	1,000		





0.300"-Headed Fasteners with 0.157" Shank Diameter — 10-Pin Collation

Lawadh	Medel		Dools	Carton	Compat	ible Tools
Length (in.)	Model No.	Description	Pack Qty.	Qty.	Simpson Strong-Tie	Others
1/2	PDPAS-50	0.157 x ½"	100	1,000		
½ knurled	PDPAS-50K	0.157 x ½" knurl	100	1,000		
% knurled	PDPAS-62K	0.157 x %" knurl	100	1,000		DX-460 MAG and most other low-velocity
3/4	PDPAS-75	0.157 x ¾"	100	1,000		
1	PDPAS-100	0.157 x 1"	100	1,000		
1 1/4	PDPAS-125	0.157 x 11/4"	100	1,000	PTP-27SMAGR PT-27LMAGR	
1 1/2	PDPAS-150	0.157 x 1½"	100	1,000	1 1 Z1 LIVIAGIT	magazine tools
17/8	PDPAS-187	0.157 x 1%"	100	1,000		
2	PDPAS-200	0.157 x 2"	100	1,000		
21/2	PDPAS-250	0.157 x 2½"	100	1,000		
27/8	PDPAS-287	0.157 x 21/8"	100	1,000		



0.300"-Headed Tophat Fasteners with 0.157" Shank Diameter

Length	Model		Pack	Carton	Compat	tible Tools	
(in.)	No.	Description	Qty.	Qty.	Simpson Strong-Tie	Others	
½ knurled	PDPAT-50K	0.157 x ½" knurl	100	1,000	PTP-27L PTP-27S	PTP-27L PTP-27S	
% knurled	PDPAT-62K	0.157 x %" knurl	100	1,000	PT-27 PT-27HDA	721, D-60, U-2000 and most other low-velocity tools	
3/4	PDPAT-75	0.157 x ¾"	100	1,000	PT-22A PT-22GS PT-22P PT-22HA		
1	PDPAT-100	0.157 x 1"	100	1,000			





Pre-Assembled Ceiling Clips – 0.300"-Headed Fasteners with 0.157" Shank Diameter

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

Longth	Model		Pack	Carton	Compatible Tools	
Length (in.)	No.	Description	Qty.	Qty.	Simpson Strong-Tie	Others
7/8	PCLDPA-87	Ceiling Clip with %" Pin	100	1,000		DX-350 System 1 721 DX-351, DX-460, Ramset Viper, Reamset Viper 4 and most other tools
1 1/16	PCLDPA-106	Ceiling Clip with 11/16" Pin	100	1,000	PTP-27L	
15/16	PCLDPA-131	Ceiling Clip with 15⁄16" Pin	100	1,000	PTP-27S PT-27 PT22A	
1 1⁄16	PECLDPA-106	Compact Ceiling Clip with 11/16" Pin	100	1,000	PT-22GS PT-22GS PT-22P PT-22HA	
1 5⁄16	PECLDPA-131	Compact Ceiling Clip with 15/16" Pin	100	1,000		



**PCLDPA** 



**PECLDPA** 

Threaded Rod Hangers - 0.300" - Headed Fasteners with 0.157" Shank Diameter

Threaded Fled Fled 91000 Fledded Factoriol With 51101 Chairle Diameter								
Longth Model	Model		Pack	Carton	Compatible Tools			
Length (in.)	No.	Description	Qty. Carton Qty.	Simpson Strong-Tie	Others			
1 5/16, 1/4 – 20 Threaded Rod Hanger	PTRHA4-131	0.157 x 15⁄16"	50	500	PTP-27L PTP-27S PT-27 PT-22P	DX-350 DX-36		
15/16, 3% – 16 Threaded Rod Hanger	PTRHA3-131	0.157 x 15⁄16"	50	500	PT-22P PT-22A PT-22GS PT-22HA	DX-35 DX-A40 DX-460		



# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# **Fasteners** for Powder-Actuated Tools

Type-304 Stainless-Steel 0.300"-Headed Fasteners with 0.145" Shank Diameter and 1" Metal Washers\*

Length	Model	Pack	Carton	Compa	atible Tools	
(in.)	No.	Qty.	Qty.	Cimpoon	Others	
1	PDPWL-1004SS	100	1,000	PTP-27L PTP-27S**	721**, D-60, DX-460, U-2000, System 1, System 3 and most other low-velocity tools	
1 1/4	PDPWL-1254SS	100	1,000	PT-275 PT-27 PT-22P		
1½	PDPWL-1504SS	100	1,000	PT-22P PT-22A PT-22GS PT-22HA		
2	PDPWL-2004SS	100	1,000			

<sup>\*</sup>Washers are Type-304 Stainless-Steel



PDPWL-SS

### 0.300"-Headed Fasteners with 0.145" Shank Diameter and 17/16" Metal Washers

Length	Model	Pack	Carton	Compati	npatible Tools	
(in.)	No.		Qty.	Simpson Strong-Tie	Others	
1	PINW-100	50	500			
1 1/4	PINW-125	50	500	PTP-27L	721, D-60, U-2000, System 1, System 3 and most other low-velocity tools	
1 ½	PINW-150	50	500	PT-27 PT-22P		
21/4	PINW-225	50	500	PT-22A PT-22GS		
21/2	PINW-250	50	500	PT-22HA		
3	PINW-300	50	500			



### 0.300"-Headed Fasteners with 0.145" Shank Diameter and 1%" Plastic White Washers

Length	Model	Pack	Carton	Compat	ble Tools
(in.)	No.	Qty.		Simpson Strong-Tie	Others
1	PINWP-100W	50	500	_	
1 1/4	PINWP-125W	50	500	PTP-27L	721*, D-60, DX-460, U-2000, System 1, System 3 and most other low-velocity tools
1 ½	PINWP-150W	50	500	PT-27	
13⁄4	PINWP-175W	50	500	PT-22P PT-22A	
2	PINWP-200W	50	500	PT-22GS PT-22HA	
21/2	PINWP-250W	50	500		
3	PINWP-300W	50	500		



\*Up to 21/2"

# SIMPSON Strong-Tie

Highway Basket Clips - 0.300"-Headed Fasteners with 0.145" Shank Diameter

	Model	Dools	Corton	Compatil	ole Tools
Description Model No.		Pack Qty.	Carton Qty.	Simpson Strong-Tie	Others
Clip with 11/2" Pin	PHBC-150	100	1,000	PTP-27L, PT-27	
Clip with 2" Pin	PHBC-200	100	1,000	PT-22P, PT-22A	DX-A41, Autofast
Clip with 21/2" Pin	PHBC-250	50	1,000	PT-22GS PT-22HA	



Pre-Assembled BX Cable Straps and Conduit Straps – 0.300"-Headed Fasteners with 0.145" Shank Diameter

Description	Model	Pack	Carton	Compati	ble Tools
	No.	Qty.	Qty.	Simpson Strong-Tie	Others
BX Cable Strap with 1" Pin	PBXDP-100	100	1,000	PTP-27L PTP-27S PT-27 PT-22P PT-22A PT-22GS PT-22HA	D-60, 721, System 1, System 3, DX-350 and most other tools
Conduit Clip ½" EMT with 1" Pin	PCC50-DP100	100	1,000		
Conduit Clip ¾" EMT with 1" Pin	PCC75-DP100	50	500		
Conduit Clip 1" EMT with 1" Pin	PCC100-DP100	50	500		



1/4" - 20 Threaded Studs\*

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

Longth	Model	Pack	Carton	Compatible Tools		
Length (in.)	No.	Qty.	Qty.	Simpson Strong-Tie	Others	
1/4 - 20 Knurled (T-1/2, S-1/2)	PSLV4-5050K	100	1,000			
½ - 20 (T-½, S-¾)	PSLV4-5075	100	1,000			
1/4 - 20 (T-1/2, S-1)	PSLV4-50100	100	1,000			
1/4 - 20 (T-1/2, S-1 1/4)	PSLV4-50125	100	1,000	DTD 07		
½ - 20 (T-¾, S-¾)	PSLV4-7575	100	1,000	PTP-27 PTP-27L	Most	
1/4 - 20 Knurled (T-3/4, S-1/2)	PSLV4-7550K	100	1,000	PT-27 PT-22A	low-velocity	
1/4 - 20 (T-3/4, S-1)	PSLV4-75100	100	1,000	PT-22GS PT-22HA	tools	
1/4 - 20 (T-3/4, S-1 1/4)	PSLV4-75125	100	1,000	I I-ZZIIA		
1/4 - 20 (T-1, S-1)	PSLV4-100100	100	1,000			
1/4 - 20 Knurled (T-1 1/4, S-1/2)	PSLV4-12550K	100	1,000			
1/4 - 20 (T-1 1/4, S-1 1/4)	PSLV4-125125	100	1,000			



<sup>\*</sup>Shank diameter is 0.150". NOTE: T = thread length, S = shank length.



3/8" - 16 Threaded Studs\* (Factory Mutual Listing-see below)

Length	Model	Pack	Carton	Compati	ble Tools
(in.)	No.	Qty.	Qty.	Simpson Strong-Tie	Others
% - 16 Knurled (T-1 1/4, S-3/4)	PSLV3-12575K	100	1,000	PT-27HDA	DX-600 and most other %" barrel tools
% - 16 (T-1 ¼, S-1)	PSLV3-125100	100	1,000		
3% - 16 (T-11⁄4, S-11⁄4)	PSLV3-125125**	100	1,000		





APPROVED

### **Metric Fasteners**

### 8mm-Headed Fasteners with 3.68mm Shank Diameter

Longth	Model	Pack	Carton	Compati	ole Tools
Length (in.)	No.	Qty.	Qty.	Simpson Strong-Tie	Others
½ Knurled	PHN-14K	100	1,000		
% Knurled	PHN-16K	100	1,000		
3/4 Knurled	PHN-19K	100	1,000		
7/8	PHN-22	100	1,000		DX-350 DX-36 DX-400E DX-440 DX-460 DX-A41 System 1
1	PHN-27	100	1,000	PTP-27L	
1 1/4	PHN-32	100	1,000	PTP-27S** PT-27	
1½	PHN-37	100	1,000	PT-22P**	
1%	PHN-42	100	1,000	PT-22A PT-22GS	
17/8	PHN-47	100	1,000	PT-22HA*	DX-351 and
2	PHN-52	100	1,000		8mm tools
21/4	PHN-57	100	1,000		
2½	PHN-62	100	1,000		
27/8	PHN-72	100	1,000		



<sup>\*</sup>Shank diameter is 0.205". NOTE: T = thread length, S = shank length.

<sup>\*\*</sup>Factory Mutual Listing 3031724

<sup>\*</sup>Up to 21/2"

<sup>\*\*</sup>Up to 11/2"



### **Metric Fasteners**

8mm-Headed Fasteners with 3.68mm Shank Diameter and 1" Metal Washers

Longth	Model	Pack	Carton	Compati	ble Tools
Length (in.)	No.	Qty.	Qty.	Simpson Strong-Tie	Others
1	PHNW-27	100	1,000		
1 1/4	PHNW-32	100	1,000		DX-350 DX-36 DX-400E DX-A40 DX-A41 DX-460 System1 DX-351 and
1 ½	PHNW-37	100	1,000	PTP-27L	
1 5/8	PHNW-42	100	1,000	PTP-27S* PT-27	
1 1/8	PHNW-47	100	1,000	PT-22P	
2	PHNW-52	100	1,000	PT-22A PT-22GS	
21/4	PHNW-57	100	1,000	PT-22HA	
21/2	PHNW-62	100	1,000		8mm tools
27/8	PHNW-72	100	1,000		



C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

8mm-Headed Tophat Fasteners with 3.68mm Shank Diameter

Length	Model	Pack	Carton Qty.	Compati	ble Tools
(in.)	No.	Qty.		Simpson Strong-Tie	Others
5% Knurled	PHNT-16K	100	1,000	PTP-27	DX-35 DX-350 DX-460 and most 8mm tools
3/4 Knurled	PHNT-19K	100	1,000	PTP-27L PTP-27S PT-27	
7/8	PHNT-22	100	1,000	PT-22P PT-22A PT-22GS PT-22HA	
1	PHNT-27	100	1,000		



<sup>\*</sup>Up to 2"

### Concrete Forming Pin – 0.187"-Headed with 0.145" Shank Diameter

Length Mo	Model	Pack		Compatible Tools	
(in.)	No.	Qty.		Simpson Strong-Tie	Others
3/16 X 21/2 Concrete Forming Pin	PKP-250	100	1,000	PTP-27L, PT-27 PT-22P, PT-22A PT-22GS, PT-22HA	DX-Series and 8mm tools

Note: Lengths in inches are for reference only and may not be exact.





### Miscellaneous

### 1/4"-Headed Hammer Drive Fastener with 3/8" Metal Washer

Length	Model	Pack	Carton	Compatible Tools				
(in.)	No.	Qty.		Simpson Strong-Tie	Others			
3/4	PHD-75	100	1,000		HT-38, R-260, R-375,			
1	PHD-100	100	1,000	PHT-38	XL-143 and other hammer drive tools			
1 1/4	PHD-125	100	1,000					





(not for use with powder loads)



Warning: Do not use powder loads with this tool. This is a hammer drive tool only. Use of powder loads with this tool may result in injury or death.

### Powder-Actuated Tool Repair and Maintenance Kits

Tool	Kit Model No.	Description	Contents
			5 Shear Clips (Part No. PT-301011)
			1 Annular Spring (Part No. PT-301014)
			1 Piston Stop (Part No. PT-301012)
PT-27	PT-27PK1	Normal wear part replacement kit	3 Ball Bearings (Part No. PT-301013)
		,	1 Piston (Part No. PT-301903)
			2 Piston Rings (Part No. PT-301208)
			1 Nosepiece (Part No. PT-301010)
			1 Cleaning Brush - Wire (Part No. BRUSH 125)
			1 Cleaning Brush 3/4" Diameter (Part No. BRUSH 25)
			1 Cleaning Brush 1/4" Diameter (Part No. BRUSH 75)
All	PT-MK1	Tool cleaning kit	1 PAT Tool Lubricant – 4 oz. spray bottle (Part No. PT-MTL4.0)
			(1) 1/8" Hex Wrench (Part No. MW-18)
			(1) 3/16" Hex Wrench (Part No. MW-316)
			(1) 5mm Hex Wrench (Part No. MW-5)
All	PT-MTL2.0	Tool lubricant	2 oz. spray bottle



PAT and Gas-Actuated Fasteners — Allowable Tension Loads in Normal-Weight Concrete

IBC	1



Direct		Shank	Minimum	Minimum	IVIIIIIIIIIIIIII		А	Allowable Tensio	n Load — lb. (k	N)	
Fastening Type	Model No.		Penetration In. (mm)	Edge Distance In. (mm)	Spacing In. (mm)	f' <sub>c</sub> ≥ 2,000 psi (13.8 MPa) Concrete	$\begin{array}{l} \text{f'}_\text{c} \geq 2{,}500 \text{ psi} \\ \text{(17.2 MPa)} \\ \text{Concrete} \end{array}$	$\begin{array}{c} {f'}_c \geq 3{,}000 \text{ psi} \\ (20.7 \text{ MPa}) \\ \text{Concrete} \end{array}$	f' <sub>c</sub> ≥ 4,000 psi (27.6 MPa) Concrete	$\begin{array}{c} \text{f'}_\text{c} \geq 5{,}000 \text{ psi} \\ \text{(34.5 MPa)} \\ \text{Concrete} \end{array}$	f' <sub>c</sub> ≥ 6,000 psi (41.3 MPa) Concrete
			<b>3/4</b> (19)	<b>3.5</b> (89)	<b>5</b> (127)	_	<b>110</b> (0.49)	<b>110</b> (0.49)	<b>110</b> (0.49)	_	<b>110</b> (0.49)
	PDPA PDPAT	0.157	<b>1</b> (25)	<b>3.5</b> (89)	<b>5</b> (127)	_	<b>210</b> (0.93)	<b>240</b> (1.07)	<b>310</b> (1.38)	_	<b>160</b> (0.71)
	PDPAW PDPAWL	(4.0)	<b>1 1/4</b> (32)	<b>3.5</b> (89)	<b>5</b> (127)	_	<b>320</b> (1.42)	<b>340</b> (1.51)	<b>380</b> (1.69)	_	<b>365</b> (1.62)
			<b>1 ½</b> (38)	<b>3.5</b> (89)	<b>5</b> (127)	_	<b>375</b> (1.67)	<b>400</b> (1.78)	<b>450</b> (2.00)	_	<b>465</b> (2.07)
Powder Actuated	PDPWL-SS	<b>0.145</b> (3.7)	<b>1</b> (25)	<b>3</b> (76)	<b>4</b> (102)	<b>60</b> (0.27)	_	_	_	_	_
		<b>0.145</b> (3.7)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)	_	_		<b>60</b> (0.27)	_	_
	PHN		<b>1</b> (25)	<b>3</b> (76)	<b>4</b> (102)	<b>45</b> (0.20)	<b>70</b> (0.31)	<b>100</b> (0.44)	<b>150</b> (0.67)	_	<b>150</b> (0.67)
			<b>1 1/4</b> (32)	<b>3</b> (76)	<b>4</b> (102)	<b>140</b> (0.62)	<b>195</b> (0.87)	<b>255</b> (1.13)	<b>370</b> (1.65)	_	<b>370</b> (1.65)
	PSLV3	<b>0.205</b> (5.2)	<b>1 1/4</b> (32)	<b>4</b> (102)	<b>6</b> (152)	_	<b>260</b> (1.16)	_	_	_	_
	GDP	0.106	<b>5%</b> (16)	<b>3</b> (76)	<b>4</b> (102)	<b>25</b> (0.11)	<b>25</b> (0.11)	<b>30</b> (0.13)	<b>45</b> (0.20)	<b>45</b> (0.20)	_
Gas	GDP	(2.7)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)	<b>30</b> (0.13)	<b>30</b> (0.13)	<b>30</b> (0.13)	<b>30</b> (0.13)	<b>30</b> (0.13)	_
Actuated	GW-75 GW-100	0.125	<b>5/8</b> (16)	<b>3</b> (76)	<b>4</b> (102)	<b>60</b> (0.27)	<b>65</b> (0.29)	<b>70</b> (0.31)	<b>95</b> (0.42)	_	_
	GTH	(3.2)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)	<b>85</b> (0.38)	<b>95</b> (0.42)	<b>105</b> (0.47)	<b>190</b> (0.85)	_	_

- 1. The fasteners must not be driven until the concrete has reached the designated minimum compressive strength.
- 2. Minimum concrete thickness must be three times the fastener embedment into the concrete.
- 3. The allowable tension and shear values are only for the fastener in the concrete. Members connected to the concrete must be investigated in accordance with accepted design criteria.

### PAT and Gas-Actuated Fasteners — Allowable Shear Loads in Normal-Weight Concrete



Direct		Shank	Minimum	Minimum	Minimum		Allowable Shear Load — lb. (kN)						
Fastening Type	Model No.	Diameter In. (mm)		Edge Distance In. (mm)	Spacing In. (mm)	$\begin{array}{l} {f'}_c \geq 2,\!000 \; psi \\ (13.8 \; MPa) \\ Concrete \end{array}$	$\begin{array}{l} {f'}_c \geq 2{,}500 \text{ psi} \\ {(17.2 \text{ MPa})} \\ {Concrete} \end{array}$	$\begin{array}{c} {f'}_c \geq 3{,}000 \text{ psi} \\ (20.7 \text{ MPa}) \\ \text{Concrete} \end{array}$	$\begin{array}{l} {f'}_c \geq 4{,}000 \; psi \\ (27.6 \; MPa) \\ Concrete \end{array}$	$\begin{array}{l} \text{f'}_\text{c} \geq 5,\!000 \text{ psi} \\ \text{(34.5 MPa)} \\ \text{Concrete} \end{array}$	$\begin{array}{c} \text{f'}_\text{c} \geq 6,\!000 \text{ psi} \\ \text{(41.3 MPa)} \\ \text{Concrete} \end{array}$		
			<b>3/4</b> (19)	<b>3.5</b> (89)	<b>5</b> (127)	_	<b>120</b> (0.53)	<b>125</b> (0.56)	<b>135</b> (0.60)	_	<b>130</b> (0.58)		
	PDPA PDPAT	0.157	<b>1</b> (25)	<b>3.5</b> (89)	<b>5</b> (127)	_	<b>285</b> (1.27)	<b>290</b> (1.29)	<b>310</b> (1.38)	_	<b>350</b> (1.56)		
	PDPAW PDPAWL	(4.0)	<b>1</b> 1/4 (32)	<b>3.5</b> (89)	<b>5</b> (127)	_	<b>360</b> (1.60)	<b>380</b> (1.69)	<b>420</b> (1.87)	_	<b>390</b> (1.73)		
Powder			1 ½ (38)	<b>3.5</b> (89)	<b>5</b> (127)		<b>405</b> (1.80)	<b>430</b> (1.91)	<b>485</b> (2.16)		<b>495</b> (2.20)		
Actuated	PDPWL-SS	<b>0.145</b> (3.7)	<b>1</b> (25)	<b>3</b> (76)	<b>4</b> (102)	<b>195</b> (0.87)	_				_		
	PHN	<b>0.145</b> (3.7)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)		_	_	<b>95</b> (0.42)	_	_		
			<b>1</b> (25)	<b>3</b> (76)	<b>4</b> (102)	<b>120</b> (0.53)	<b>140</b> (0.62)	<b>165</b> (0.73)	<b>205</b> (0.91)		<b>205</b> (0.91)		
			<b>1 1/4</b> (32)	<b>3</b> (76)	<b>4</b> (102)	<b>265</b> (1.18)	<b>265</b> (1.18)	<b>265</b> (1.18)	<b>265</b> (1.18)		<b>265</b> (1.18)		
	GDP	0.106	<b>5%</b> (16)	<b>3</b> (76)	<b>4</b> (102)	<b>25</b> (0.11)	<b>25</b> (0.11)	<b>25</b> (0.11)	<b>25</b> (0.11)	<b>25</b> (0.11)	_		
Gas	GDF	(2.7)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)	<b>45</b> (0.20)	<b>50</b> (0.22)	<b>55</b> (0.24)	<b>75</b> (0.33)	<b>75</b> (0.33)	_		
Actuated	GW-75 GW-100	0.125	<b>5%</b> (16)	<b>3</b> (76)	<b>4</b> (102)	<b>55</b> (0.24)	<b>60</b> (0.27)	<b>65</b> (0.29)	<b>95</b> (0.42)	_	_		
	GTH	(3.2)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)	<b>120</b> (0.53)	<b>135</b> (0.60)	<b>145</b> (0.64)	<b>215</b> (0.96)	_	_		

- 1. The fasteners must not be driven until the concrete has reached the designated minimum compressive strength.
- 2. Minimum concrete thickness must be three times the fastener embedment into the concrete.
- 3. The allowable tension and shear values are only for the fastener in the concrete. Members connected to the concrete must be investigated in accordance with accepted design criteria.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



PAT and Gas-Actuated Assemblies — Allowable Tension Loads in Normal-Weight Concrete



Direct	Shank Minimum Minimum Minimum			Allowable Tension Load — lb. (kN)							
Fastening Type	Model No.		Penetration In. (mm)		Spacing In. (mm)	$\begin{array}{c} f'_c \geq 2,\!000 \; psi \\ (13.8 \; MPa) \\ Concrete \end{array}$	$\begin{array}{c} f'_c \geq 2{,}500 \; psi \\ (17.2 \; MPa) \\ Concrete \end{array}$	$\begin{array}{c} f'_c \geq 3,\!000 \; psi \\ (20.7 \; MPa) \\ Concrete \end{array}$	$\begin{array}{c} f'_{\text{C}} \geq 4,\!000 \text{ psi} \\ (27.6 \text{ MPa}) \\ \text{Concrete} \end{array}$	$\begin{array}{c} f'_c \geq 5{,}000 \; psi \\ (34.5 \; MPa) \\ Concrete \end{array}$	$\begin{array}{c} f'_{\text{C}} \geq 6,\!000 \text{ psi} \\ (41.3 \text{ MPa}) \\ \text{Concrete} \end{array}$
	PCLDPA	0.157	<b>1</b> (25)	<b>3.5</b> (89)	<b>5</b> (102)	<b>175</b> (0.78)	_	_	<b>180</b> (0.80)	_	<b>190</b> (0.85)
	TOLDIA	(4.0)	<b>1 1/4</b> (32)	<b>3.5</b> (89)	<b>5</b> (102)	<b>210</b> (0.93)	_	_	<b>210</b> (0.93)	_	<b>190</b> (0.85)
Powder Actuated	PECLDPA	<b>0.157</b> (4.0)	<b>1</b> (25)	<b>3.5</b> (89)	<b>5</b> (102)	<b>180</b> (0.80)	_	_	<b>155</b> (0.69)	_	<b>180</b> (0.80)
	PTRHA3	PTRHA3 <b>0.157</b>	<b>1</b> (25)	<b>3.5</b> (89)	<b>5</b> (102)	<b>180</b> (0.80)	_	_	<b>190</b> (0.85)	_	<b>180</b> (0.80)
	PTRHA4	(4.0)	<b>1 1/4</b> (32)	<b>3.5</b> (89)	<b>5</b> (102)	<b>185</b> (0.82)	_	_	<b>220</b> (0.98)	_	<b>190</b> (0.85)
Gas	GRH25 GRH37	<b>0.125</b> (3.2)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)	_	<b>85</b> (0.38)	<b>115</b> (0.51)	<b>160</b> (0.71)	<b>165</b> (0.73)	<b>165</b> (0.73)
Actuated	GAC	<b>0.125</b> (3.2)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)	_	<b>105</b> (0.47)	<b>120</b> (0.53)	<b>150</b> (0.67)	<b>170</b> (0.76)	<b>195</b> (0.87)

- 1. The fasteners must not be driven until the concrete has reached the designated minimum compressive strength.
- $2. \, \hbox{Minimum concrete thickness must be three times the fastener embedment into the concrete}.$
- 3. The allowable tension values are only for the fastener in the concrete. Members connected to the concrete must be investigated in accordance with accepted design criteria.

### PAT and Gas-Actuated Assemblies — Allowable Oblique Loads in Normal-Weight Concrete



AT and das-Actuated Assemblies — Allowable Oblique Loads ITTNOTTIAL Weight Obliciete — — — —												
		Shank	Minimum	Minimum	Minimum	Allowable Oblique Load — lb. (kN)						
Direct Fastening Type	Model No.			Edge Distance In. (mm)			f' <sub>c</sub> ≥ 2,500 psi (17.2 MPa) Concrete	f' <sub>c</sub> ≥ 3,000 psi (20.7 MPa) Concrete	f' <sub>c</sub> ≥ 4,000 psi (27.6 MPa) Concrete	f' <sub>c</sub> ≥ 5,000 psi (34.5 MPa) Concrete	f' <sub>c</sub> ≥ 6,000 psi (41.3 MPa) Concrete	
	PCLDPA	0.157	<b>1</b> (25)	<b>3.5</b> (89)	<b>5</b> (102)	<b>255</b> (1.13)	_	_	<b>240</b> (1.07)	_	<b>245</b> (1.09)	
Powder Actuated	Powder	(4.0)	<b>1 1/4</b> (32)	<b>3.5</b> (89)	<b>5</b> (102)	<b>250</b> (1.11)	_	_	<b>265</b> (1.18)	_	<b>265</b> (1.18)	
	PECLDPA	<b>0.157</b> (4.0)	<b>1</b> (25)	<b>3.5</b> (89)	<b>5</b> (102)	<b>225</b> (1.00)	_	_	<b>230</b> (1.02)	_	<b>255</b> (1.13)	
Gas Actuated	GAC	<b>0.125</b> (3.2)	<b>3/4</b> (19)	<b>3</b> (76)	<b>4</b> (102)	_	<b>130</b> (0.58)	<b>135</b> (0.60)	<b>145</b> (0.64)	<b>155</b> (0.69)	<b>175</b> (0.78)	

- 1. The fasteners must not be driven until the concrete has reached the designated minimum compressive strength.
- 2. Minimum concrete thickness must be three times the fastener embedment into the concrete.
- 3. The allowable oblique values are only for the fastener in the concrete. Members connected to the concrete must be investigated in accordance with accepted design criteria.
- 4. Oblique load direction is 45° from the concrete member surface.

**Direct** Fastening

# Gas- and Powder-Actuated Pins Design Information - Concrete



PAT Fasteners — Allowable Tension and Shear Loads for Attachment of Wood Sill Plates to Normal-Weight Concrete









		Overall	Nominal Head	Shank	Washer	Washer	f' <sub>c</sub> ≥ 2,000 psi (13.8 MPa)		f' <sub>c</sub> ≥ 2,500 psi (17.2 MPa)	
Direct Fastening Type	Model No.	Length In. (mm)	Diameter In. (mm)	Diameter In. (mm)	Thickness In. (mm)	Bearing Area In <sup>2</sup> (mm <sup>2</sup> )	Allow. Tension Load lb. (kN)	Allow. Shear Load Ib. (kN)	Allow. Tension Load lb. (kN)	Allow. Shear Load Ib. (kN)
	PDPAW-287	<b>2</b> % (73)	<b>0.300</b> (7.6)	<b>0.157</b> (4.0)	<b>0.070</b> (1.8)	<b>0.424</b> (274)	_	_	<b>200</b> (0.89)	<b>205</b> (0.91)
Powder Actuated	PDPAWL-287 PDPAWL-287MG	<b>2</b> % (73)	<b>0.300</b> (7.6)	<b>0.157</b> (4.0)	<b>0.070</b> (1.8)	<b>0.767</b> (495)	_	_	<b>200</b> (0.89)	<b>205</b> (0.91)
	PHNW-72	<b>2</b> % (73)	<b>0.315</b> (8.0)	<b>0.145</b> (3.7)	<b>0.070</b> (1.8)	<b>0.770</b> (497)	<b>125</b> (0.56)	<b>150</b> (0.67)	_	_

- 1. The fasteners must not be driven until the concrete has reached the designated minimum compressive strength.
- 2. Minimum concrete thickness must be three times the fastener embedment into the concrete.
- 3. The allowable tension and shear values are only for the fastener in the concrete. Members connected to the concrete must be investigated in accordance with accepted design criteria.
- 4. Minimum concrete edge distance is 1¾ inches.
- 5. Only mechanically galvanized fasteners may be used to attach preservative-treated wood to concrete.
- 6. Minimum spacing shall be 4" on center.

### Spacing of PAT Fasteners for Attachment of Wood Sill Plates to Normal-Weight Concrete



·					
Direct Fastening Type	Model No.	Overall Length In.	Nominal Head Diameter In.	Shank Diameter In.	Maximum Spacing In. (mm)
		(mm)	(mm)	(mm)	Interior Nonstructural Walls <sup>2</sup>
	PHNW-72 <sup>3</sup>	<b>2</b> 7/8 (73)	<b>0.315</b> (8.0)	<b>0.145</b> (3.7)	<b>36</b> (914)
Powder Actuated	PDPAW-287 <sup>4</sup> PDPAWL-287 <sup>4</sup> PDPAWL-287MG <sup>4</sup>	<b>2</b> % (73)	<b>0.300</b> (7.6)	<b>0.157</b> (4.0)	<b>48</b> (1219)

- Spacings are based upon the attachment of 2-inch (nominal thickness) wood sill plates, with specific gravity of 0.50 or greater, to concrete floor slabs or footings.
- 2. All walls shall have fasteners placed at 6 inches from ends of sill plates, with maximum spacing as shown in the table.
- 3. Fasteners shall not be driven until the concrete has reached a compressive strength of 2,000 psi. Minimum edge distance is 1% inches.
- 4. Fasteners shall not be driven until the concrete has reached a compressive strength of 2,500 psi. Minimum edge distance is 1% inches.
- 5. The maximum horizontal transverse load on the wall shall be 5 psf.
- 6. The maximum wall height shall be 14 feet.
- 7. For exterior walls and interior structural walls, this table is not applicable and allowable loads must be used .
- 8. Walls shall be laterally supported at the top and the bottom.
- 9. Minimum spacing shall be 4" on center.
- 10. Only mechanically galvanized fasteners may be used to attach preservative-treated wood to concrete.

<sup>\*</sup> See page 12 for an explanation of the load table icons.



PAT and Gas-Actuated Fasteners — Allowable Tension Loads in Sand-Lightweight Concrete over Metal Deck

IBC		<b>~</b>	*

					Allowat	ole Tension Loa	d — lb. (kN)	
Direct Fastening Type	Model No.	Shank Diameter In. (mm)	Minimum Penetration In. (mm)	Installed in Concrete <sup>4</sup>	Installed Thru. 3" "W" Deck with 31/4" Concrete Fill <sup>5</sup>		Installed Thru. 1.5" "B" Deck with 21/4" Concrete Fill <sup>7</sup>	Installed Thru. 1.5" "B" Deck with 2" Concrete Fill <sup>8</sup>
					f' <sub>c</sub> ≥ 3,0	00 psi (20.7 MI	Pa) Concrete	
			<b>3/4</b> (19)	<b>85</b> (0.38)	<b>105</b> (0.47)	_	_	<b>160</b> (0.71)
	PDPA PDPAT	0.157	<b>1</b> (25)	<b>150</b> (0.67)	<b>145</b> (0.64)	_	_	<b>210</b> (0.93)
	PDPAW PDPAWL	(4.0)	<b>1</b> 1/4 (32)	<b>320</b> (1.42)	<b>170</b> (0.76)	_	_	<b>265</b> (1.18)
Powder Actuated			<b>1 ½</b> (38)	<b>385</b> (1.71)	<b>325</b> (1.45)	_	_	_
	PHNT	<b>0.145</b> (3.7)	<b>7/8</b> (22)	<b>185</b> (0.82)	<b>165</b> (0.73)	_	_	_
	PSLV3	<b>0.205</b> (5.2)	<b>1 1/4</b> (32)	_	<b>225</b> (1.00)	_	_	_
	PSLV4	<b>0.150</b> (3.8)	<b>1</b> (25)	<u>—</u>	<b>80</b> (0.36)	<u>—</u>	<del>_</del>	_
	GDP	0.106	<b>5%</b> (16)	<b>75</b> (0.33)	_	<b>60</b> (0.27)	<b>65</b> (0.29)	_
Gas Actuated	GDP	(2.7)	<b>3/4</b> (19)	<b>105</b> (0.47)	_	<b>60</b> (0.27)	<b>130</b> (0.58)	_
uas Actuated	GW-75	0.125	<b>5/8</b> (16)	<b>60</b> (0.27)		<b>35</b> (0.16)		_
	GW-100 GTH	(3.2)	<b>3/4</b> (19)	<b>115</b> (0.51)	_	<b>55</b> (0.24)	_	_

- 1. The fastener shall not be driven until the concrete has reached the designated compressive strength.
- The allowable tension values are for the fastener only. Members connected to the steel must be investigated separately in accordance with accepted design criteria.
- 3. Metal deck must be minimum 20 gauge and have a minimum yield strength of 38,000 psi.
- 4. The minimum fastener spacing is 4". The minimum edge distances are 3½" and 3" for powder-actuated fasteners and gas-actuated fasteners, respectively.
- 5. The fastener shall be installed minimum 11/2" from the edge of flute and 4" from the end of the deck. The minimum fastener spacing is 4".
- 6. The fastener shall be installed minimum 1" from the edge of flute and 3" from the end of the deck. The minimum fastener spacing is 4". For GW and GTH fasteners, the fastener must be a minimum of 1%" from the edge of flute.
- 7. The fastener shall be installed minimum 7%" from the edge of flute. For inverted 1.5" "B" deck configuration, the fastener must be a minimum of 1" from the edge of flute. Fastener must be installed minimim 3" from the end of the deck. The minimum fastener spacing is 4".
- 8. The fastener shall be installed minimum %" from the edge of flute and 4" from the end of the deck. The minimum fastener spacing is 4".



PAT and Gas-Actuated Fasteners — Allowable Shear Loads in Sand-Lightweight Concrete over Metal Deck

IBC	
o. (kN)	
	Installed Thru. 1.5" "B" Deck with 2" Concrete Fill <sup>8</sup>
noroto	

	Model No.	Shank Diameter In. (mm)		Allowable Shear Load — lb. (kN)					
Direct Fastening Type			Minimum Penetration In. (mm)	Installed in Concrete <sup>9</sup>	Installed Thru. 3" "W" Deck with 31/4" Concrete Fill <sup>5</sup>		Installed Thru. 1.5" "B" Deck with 21/4" Concrete Fill <sup>7</sup>		
					f' <sub>c</sub> ≥ 3,000	0 psi (20.7 MPa	) Concrete		
			<b>3/4</b> (19)	<b>105</b> (0.47)	<b>280</b> (1.25)	_	_	<b>275</b> (1.22)	
	PDPA PDPAT PDPAW PDPAWL	PAT <b>0.157</b> AW (4.0)	<b>1</b> (25)	<b>225</b> (1.00)	<b>280</b> (1.25)	_	_	<b>370</b> (1.65)	
Powder Actuated			<b>1</b> 1/4 (32)	<b>420</b> (1.87)	<b>320</b> (1.42)	_		<b>460</b> (2.05)	
			<b>1½</b> (38)	<b>455</b> (2.02)	<b>520</b> (2.31)	_	_	_	
	PHNT	<b>0.145</b> (3.7)	<b>7/8</b> (22)	<b>275</b> (1.22)	<b>400</b> (1.78)	_	_	_	
	GDP	0.106	5 <b>%</b> (16)	<b>35</b> (0.16)	_	<b>180</b> (0.80)	<b>195</b> (0.87)	_	
	GDF	(2.7)	<b>3/4</b> (19)	<b>140</b> (0.62)	_	<b>180</b> (0.80)	<b>270</b> (1.20)	_	
Gas Actuated	GW-75 GW-100 GTH	GW-100 0.125	<b>5/8</b> (16)	<b>110</b> (0.49)	_	<b>215</b> (0.96)	_	_	
			<b>3/4</b> (19)	<b>130</b> (0.58)	_	<b>235</b> (1.05)	_	_	

- 1. The fastener shall not be driven until the concrete has reached the designated compressive strength.
- 2. The allowable shear values are for the fastener only. Members connected to the steel must be invesigated separately in accordance with
- 3. Metal deck must be minimum 20 gauge and have a minimum yield strength of 38,000 psi.
- 4. Shear values are for loads applied toward edge of flute.
- 5. The fastener shall be installed minimum 11/2" from the edge of flute and 4" from the end of the deck. The minimum fastener spacing is 4".
- 6. The fastener shall be installed minimum 1" from the edge of flute and 3" from the end of the deck. The minimum fastener spacing is 4". For GW and GTH fasteners, the fastener must be a minimum of 11/8" from the edge of flute.
- 7. The fastener shall be installed minimum 7/6" from the edge of flute. For inverted 1.5" "B" deck configuration, the fastener must be a minimum of 1" from the edge of flute. Fastener must be installed miminim 3" from the end of the deck. The minimum fastener spacing is 4".
- 8. The fastener shall be installed minimum 1/8" from the edge of flute and 4" from the end of the deck. The minimum fastener spacing is 4".
- 9. The minimum fastener spacing is 4". The minimum edge distances are 31/2" and 3" for powder-actuated fasteners and gas-actuated fasteners, respectively.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.



PAT and Gas-Actuated Assemblies – Allowable Tension Loads in Sand-Lightweight Concrete over Metal Deck







		Shank Diameter In. (mm)	Penetration	Allowable Tension Load — lb. (kN)				
Direct Fastening Type	Model No.			Installed Thru. 3" "W" Deck with 2½" Concrete Fill <sup>4</sup>	Installed Thru. 3" "W" Deck with 2¼" Concrete Fill <sup>5</sup>	Installed Thru. 1.5" "B" Deck with 21/4" Concrete Fill <sup>6</sup>	Installed Thru. 1.5" "B" Deck with 2" Concrete Fill <sup>7</sup>	
			, ,		f' <sub>c</sub> ≥ 3,000 psi (20	0.7 MPa) Concrete		
	PTRHA3	0.157	<b>1</b> (25)	<b>160</b> (0.71)	_	_	<b>175</b> (0.78)	
	PTRHA4	(4.0)	<b>1</b> 1/4 (32)	<b>160</b> (0.71)	_	_	<b>175</b> (0.78)	
Powder Actuated	PCLDPA	<b>0.157</b> (4.0)	<b>1</b> (25)	<b>140</b> (0.62)	_	_	<b>160</b> (0.71)	
			<b>1</b> 1/4 (32)	<b>160</b> (0.71)	_	_	<b>180</b> (0.80)	
	PECDLPA	<b>0.157</b> (4.0)	<b>1</b> (25)	<b>120</b> (0.53)	_	_	<b>135</b> (0.60)	
Gas Actuated	GRH25 GRH37	<b>0.125</b> (3.2)	<b>3/4</b> (19)	_	<b>95</b> (0.42)	<b>95</b> (0.42)	_	
Gas Actuated	GAC	<b>0.125</b> (3.2)	<b>3/4</b> (19)	_	<b>105</b> (0.47)	<b>90</b> (0.40)	_	

- 1. The fastener shall not be driven until the concrete has reached the designated compressive strength.
- The allowable tension values are for the fastener only. Members connected to the steel must be investigated separately in accordance with accepted design criteria.
- 3. Metal deck must be minimum 20 gauge and have a minimum yield strength of 38,000 psi.
- 4. The fastener shall be installed minimum 11/2" from the edge of flute and 4" from the end of the deck. The minimum fastener spacing is 4".
- 5. The fastener shall be installed minimum 1" from the edge of flute and 3" from the end of the deck. The minimum fastener spacing is 4".
- 6. The fastener shall be installed minimum 7/8" from the edge of flute and 3" from the end of the deck. The minimum fastener spacing is 4".
- 7. The fastener shall be installed minimum 7/8" from the edge of flute and 4" from the end of the deck. The minimum fastener spacing is 4".

PAT and Gas-Actuated Assemblies – Allowable Oblique Loads in Sand-Lightweight Concrete over Metal Deck







C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

	Model No.	Shank Diameter In. (mm)	Minimum Penetration In. (mm)	Allowable Oblique Load — lb. (kN)					
Direct Fastening Type				Installed Thru. 3" "W" Deck with 2½" Concrete Fill <sup>4</sup>	Installed Thru. 3" "W" Deck with 21/4" Concrete Fill <sup>5</sup>	Installed Thru. 1.5" "B" Deck with 21/4" Concrete Fill <sup>6</sup>	Installed Thru. 1.5" "B" Deck with 2" Concrete Fill <sup>7</sup>		
					f' <sub>c</sub> ≥ 3,000 psi (20	0.7 MPa) Concrete			
	PCLDPA	0.157	<b>1</b> (25)	<b>175</b> (0.78)	_	_	<b>240</b> (1.07)		
Powder Actuated		(4.0)	<b>1 1/4</b> (32)	<b>185</b> (0.82)	_	_	<b>280</b> (1.25)		
	PECDLPA	<b>0.157</b> (4.0)	<b>1</b> (25)	<b>145</b> (0.64)	_	_	<b>175</b> (0.78)		
Gas Actuated	GAC	<b>0.125</b> (3.2)	<b>3/4</b> (19)	_	<b>120</b> (0.53)	<b>90</b> (0.40)	_		

- 1. The fastener shall not be driven until the concrete has reached the designated compressive strength.
- 2. The allowable oblique values are for the fastener only. Members connected to the steel must be investigated separately in accordance with accepted design criteria.
- 3. Metal deck must be minimum 20 gauge and have a minimum yield strength of 38,000 psi.
- 4. The fastener shall be installed minimum 11/2" from the edge of flute and 4" from the end of the deck. The minimum fastener spacing is 4".
- 5. The fastener shall be installed minimum 1" from the edge of flute and 3" from the end of the deck. The minimum fastener spacing is 4".
- 6. The fastener shall be installed minimum 1/8" from the edge of flute and 3" from the end of the deck. The minimum fastener spacing is 4".
- 7. The fastener shall be installed minimum 1/8" from the edge of flute and 4" from the end of the deck. The minimum fastener spacing is 4".
- 8. Oblique load direction is 45° from the concrete member surface.

<sup>\*</sup> See page 12 for an explanation of the load table icons



PAT and Gas-Actuated Fasteners — Allowable Tension and Shear Loads in Hollow CMU



		Shank Diameter	r Minimum Penetration In.	Minimum Edge	Minimum	8-inch Hollow CMU Loads Based on CMU Strength	
Direct Fastening Type	Model No.	In. (mm)		Distance In.	Spacing In.	Tension Load	Shear Load
.,,,,,			(mm)	(mm)	(mm)	Allowable lb. (kN)	Allowable lb. (kN)
Powder Actuated	PDPA PDPAT PDPAW PDPAWL	<b>0.157</b> (4.0)	<b>13/4</b> (44)	<b>4</b> (102)	<b>8</b> (203)	<b>125</b> <sup>1</sup> (0.56)	<b>210</b> <sup>1</sup> (0.93)
Gas Actuated	GDP	<b>0.106</b> (2.7)	<sup>5</sup> / <sub>8</sub> (16)	<b>3</b> (76)	<b>8</b> (203)	<b>35</b> ¹ (0.16)	<b>50</b> <sup>1</sup> (0.22)
das Actualeu	GW-75 GW-100 GTH	<b>0.125</b> 3.2)	<b>5</b> /8 (16)	<b>3</b> (76)	<b>8</b> (203)	<b>55</b> <sup>2</sup> (0.24)	<b>65</b> <sup>2</sup> (0.29)

Values for 8-inch-thick lightweight concrete masonry units conforming to ASTM C90. Values for 8-inch-thick medium-weight concrete masonry units conforming to ASTM C90.

### PAT and Gas-Actuated Fasteners — Allowable Tension Loads in Steel<sup>1</sup>



**Direct** Fastening

Direct		Shank	Minimum	Minimum			Allow	able Tensio	n Load — II	b. (kN)	
Fastening Type	Model No.	Diameter <sup>10</sup> In. (mm)	Edge Distance In. (mm)	Spacing In. (mm)	Minimum Steel Strength <sup>3</sup>	1/8" Thick Steel	3/16" Thick Steel	1/4" Thick Steel	%" Thick Steel	½" Thick Steel	¾" Thick Steel
	PDPA PDPAT	0.157	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>260</b> (1.16)	<b>370</b> (1.65)	<b>380</b> <sup>7</sup> (1.69)	<b>530</b> <sup>7</sup> (2.36)	<b>195</b> <sup>4</sup> (0.87)
	PDPAW PDPAWL	(4.0)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A572 Gr. 50 or ASTM A992	_	<b>305</b> (1.36)	<b>335</b> (1.49)	<b>355</b> <sup>7</sup> (1.58)	<b>485</b> <sup>5</sup> (2.16)	<b>170</b> <sup>6</sup> (0.76)
	PHN	<b>0.145</b> (3.7)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>155</b> (0.69)	_	_	_	_
Powder	PHN Knurled <sup>11</sup>	<b>0.145</b> (3.7)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>155</b> (0.69)	<b>440</b> (1.96)	_	_	_
Actuated	PHNT	<b>0.145</b> (3.7)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	<b>40</b> (0.18)	<b>50</b> (0.22)	<b>250</b> (1.11)	_	_	_
	PSLV3	<b>0.205</b> (5.2)	<b>1</b> (25)	<b>1 ½</b> (38)	ASTM A36	_	<b>270</b> (1.20)	<b>680</b> (3.02)	_	_	_
	PSLV3- 12575K	<b>0.205</b> (5.2)	<b>1</b> (25)	<b>1 ½</b> (38)	ASTM A36	_	<b>270</b> (1.20)	<b>870</b> (3.87)	_	_	_
	PSLV4	<b>0.150</b> (3.8)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>200</b> (0.89)	<b>420</b> (1.87)	_	_	_
	GDP	0.106	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	<b>125</b> (0.56)	<b>210</b> (0.93)	<b>220</b> (0.98)	_	_	_
	GDP	(2.7)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A572 Gr. 50 or ASTM A992	_	<b>225</b> (1.00)	<b>185</b> (0.82)	_	_	_
Gas	GDPS	0.118/0.102	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36		<b>95</b> (0.42)	<b>170</b> (0.76)	<b>165</b> <sup>8</sup> (0.73)	<b>145</b> <sup>8</sup> (0.64)	_
Actuated	GDPS	(3.0/2.6)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A572 Gr. 50 or ASTM A992	_	<b>110</b> (0.49)	<b>170</b> (0.76)	<b>155</b> <sup>8</sup> (0.69)	_	_
	GW-50	0.128/0.110	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>225</b> (1.00)	<b>275</b> (1.22)	<b>245</b> <sup>9</sup> (1.09)	_	_
	GVV-30	(3.3/2.8)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A572 Gr. 50 or ASTM A992	_	<b>240</b> (1.07)	<b>215</b> <sup>9</sup> (0.96)	<b>280</b> <sup>9</sup> (1.25)	_	_

- 1. The entire pointed portion of the fastener must penetrate through the steel to obtain the tabulated values, unless otherwise indicated.
- The allowable tension values are for the fastener only. Members connected to the steel must be investigated separately in accordance with accepted design criteria.
- 3. Steel strength must comply with the minimum requirements of ASTM A 36 ( $F_y$  = 36 ksi,  $F_u$  = 58 ksi), ASTM A 572, Grade 50 ( $F_y$  = 50 ksi,  $F_u$  = 65 ksi), or ASTM A992 ( $F_y$  = 50 ksi,  $F_u$  = 65 ksi).
- 4. Based upon minimum penetration depth of 0.46" (11.7 mm).

- 5. Based upon minimum penetration depth of 0.58" (14.7 mm).
- 6. Based upon minimum penetration depth of 0.36" (9.1 mm).
- The fastener must be driven to where the point of the fastener penetrates through the steel.
- 8. Based upon minimum penetration depth of 0.35" (8.9 mm).
- 9. Based upon minimum penetration depth of 0.25" (6.4 mm).
- 10. For stepped shank fasteners: (Diameter of shank above the step)/(Diameter of shank below the step.)
- 11. PHN-16K or longer.

Minimum penetration is measured from the outside face of the concrete masonry unit. No more than one fastener may be installed in an individual hollow CMU cell.

<sup>\*</sup> See page 12 for an explanation of the load table icons.









### PAT and GAS Fasteners — Allowable Shear Loads in Steel<sup>1</sup>

Direct			Minimum Ctaal		Allow	able Sheai	r Load — I	b. (kN)			
Fastening Type	Model No.	In. (mm)	In. (mm)	In. (mm)	Strength <sup>3</sup>	1/8" Thick Steel	3/16" Thick Steel	1/4" Thick Steel	%" Thick Steel	½" Thick Steel	3/4" Thick Steel
	PDPA, PDPAT,	0.157	0.5	1	ASTM A36	_	<b>410</b> (1.82)	<b>365</b> (1.62)	<b>385</b> <sup>7</sup> (1.71)	<b>385</b> <sup>7</sup> (1.71)	<b>325</b> <sup>4</sup> (1.45)
	PDPAW, PDPAWL	(4.0)	(13)	(25)	ASTM A572 Gr. 50 or ASTM A992	_	<b>420</b> (1.87)	<b>365</b> (1.62)	<b>290</b> <sup>7</sup> (1.29)	<b>275</b> <sup>7</sup> (1.22)	<b>275</b> <sup>7</sup> (1.22)
	PHN	<b>0.145</b> (3.7)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>395</b> (1.76)	_	_	_	_
Powder	PHN Knurled <sup>11</sup>	<b>0.145</b> (3.7)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>395</b> (1.76)	_	_	_	_
Actuated	PHNT	<b>0.145</b> (3.7)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	<b>440</b> (1.96)	<b>620</b> (2.76)	<b>620</b> (2.76)	_	_	_
	PSLV3	<b>0.205</b> (5.2)	<b>1</b> (25)	<b>1 ½</b> (38)	ASTM A36	_	<b>770</b> (3.43)	<b>1,120</b> (4.98)	_	_	_
	PSLV3-12575K	<b>0.205</b> (5.2)	<b>1</b> (25)	<b>1½</b> (38)	ASTM A36	_	<b>930</b> (4.14)	<b>1,130</b> (5.03)	_	_	_
	PSLV4	<b>0.150</b> (3.8)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>630</b> (2.80)	<b>690</b> (3.07)	_	_	_
	GDP	0.106	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	<b>285</b> (1.27)	<b>225</b> (1.00)	<b>205</b> (0.91)	_	_	_
	GDF	(2.7)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A572 Gr. 50 or ASTM A992	_	<b>250</b> (1.11)	<b>145</b> (0.64)	_	_	_
Gas	GDPS	0.118/0.102	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>180</b> (0.80)	<b>265</b> (1.18)	<b>225</b> <sup>8</sup> (1.00)	<b>225</b> <sup>8</sup> (1.00)	_
Actuated	GDP5	(3.0/2.6)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A572 Gr. 50 or ASTM A992	_	<b>205</b> (0.91)	<b>305</b> (1.36)	<b>205</b> <sup>8</sup> (0.91)	_	_
	GW-50	0.128/0.110	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A36	_	<b>400</b> (1.78)	<b>345</b> (1.53)	<b>310</b> <sup>9</sup> (1.38)	_	_
	uw 50	(3.3/2.8)	<b>0.5</b> (13)	<b>1</b> (25)	ASTM A572 Gr. 50 or ASTM A992	_	<b>380</b> (1.69)	<b>325</b> <sup>9</sup> (1.45)	<b>350</b> <sup>9</sup> (1.56)	_	_

- 1. The entire pointed portion of the fastener must penetrate through the steel to obtain the tabulated values, unless otherwise indicated.
- 2. The allowable shear values are for the fastener only. Members connected to the steel must be investigated separately in accordance with accepted design criteria.
- 3. Steel strength must comply with the minimum requirements of ASTM A 36 (F<sub>y</sub> = 36 ksi, F<sub>u</sub> = 58 ksi), ASTM A 572, Grade 50 (F<sub>y</sub> = 50 ksi, F<sub>u</sub> = 65 ksi), or ASTM A992 (F<sub>y</sub> = 50 ksi, F<sub>u</sub> = 65 ksi).
- 4. Based upon minimum penetration depth of 0.46" (11.7 mm).
- 5. Based upon minimum penetration depth of 0.58" (14.7 mm).
- 6. Based upon minimum penetration depth of 0.36" (9.1 mm).
- 7. The fastener must be driven to where the point of the fastener penetrates through the steel.
- 8. Based upon minimum penetration depth of 0.35" (8.9 mm).
- 9. Based upon minimum penetration depth of 0.25" (6.4 mm).
- 10. For stepped shank fasteners: (Diameter of shank above the step)/(Diameter of shank below the step).
- 11. PHN-16K or longer.



### Spiral Knurl Pin Allowable Tension and Shear Loads in Cold-Formed Steel Studs, 33 ksi Minimum Yield Strength

	Shank	Minimum Edge Dist. in. (mm)	Minimum	Designation	Allowable Loads		
Model No.	Diameter in. (mm)		Spacing in. (mm)	Thickness mils (gauge)	Tension lb. (kN)	Shear lb. (kN)	
GDPSK-138	0.109	13/ <sub>16</sub> (2.1)	<b>4</b> (102)	<b>33</b> (20)	<b>30</b> (0.13)	<b>70</b> (0.31)	
	(2.8)			<b>43</b> (18)	<b>48</b> (0.21)	<b>89</b> (0.40)	

- 1. Entire pointed portion of the fastener must penetrate through the steel to obtain tabulated values.
- 2. The allowable tension and shear values are for the fastener only. Members connected to the steel must be investigated separately in accordance with accepted design criteria.
- 3. Fastener is to be installed in the center of the stud flange.

### Spiral Knurl Pin Allowable Tension and Shear Loads in Cold-Formed Steel Studs. 50 ksi Minimum Vield Strength

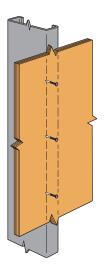
teel Studs, 50 ksi Miriimum Yield Strength								
	Shank	Minimum	Minimum	Designation	Allowable Loads			
Model No.	Diameter in. (mm)	Edge Dist. in. (mm)	Spacing in. (mm)	Thickness mils (gauge)	Tension lb. (kN)	Shear lb. (kN)		
GDPSK-138	0.109	<sup>13</sup> / <sub>16</sub> (2.1)	<b>4</b> (102)	<b>54</b> (16)	<b>92</b> (0.41)	<b>150</b> (0.67)		
	(2.8)			<b>68</b> (14)	<b>73</b> (0.32)	<b>218</b> (0.97)		

- 1. Entire pointed portion of the fastener must penetrate through the steel to obtain tabulated values.
- 2. The allowable tension and shear values are for the fastener only. Members connected to the steel must be investigated separately in accordance with accepted design criteria.
- 3. Fastener is to be installed in the center of the stud flange.

### PHN Fasteners Attaching Light-Gauge Steel Channels — Allowable Shear Loads in Normal-Weight Concrete

Model	Shank Diameter	eter Penetration Steel Channel		Allowable Shear Load lb. (kN)	
No.	in. (mm)	in. (mm)	Thickness gauge	$f'_c \ge 2,000 \text{ psi (13.8 MPa)}$ Concrete	
DUN	0.145	7/8	20	<b>160</b> (0.71)	
PHN	(3.7)	(22)	18	<b>135</b> (0.60)	

<sup>1.</sup> The fasteners shall not be driven until the concrete has reached the designated compressive strength. Minimum concrete thickness is three times the faster embedment into the concrete.



Typical GDPSK Installation

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

<sup>\*</sup> See page 12 for an explanation of the load table icons.

# **Restoration Solutions**







Simpson Strong-Tie offers a line of products designed for structural and architectural rehabilitation of concrete and masonry.

Our restoration solutions provide reliable, easy-to-use products for a variety of applications, including structural restoration, pick-proof sealing and water-intrusion prevention.







# **ETI** Injection Epoxy

ETI injection epoxies are two-component, high-solids formulations for the injection into cracks in concrete. Dispensed through a static mixing nozzle using either a manual, battery-powered or a pneumatic dispensing tool, these epoxies provide a waterproof, high strength (structural) repair.

### **Features**

- Bonds chemically to concrete, providing structural repair (meets the requirements of ASTM C 881 for structural repair epoxy)
- Formulated for maximum penetration under pressure (all viscosities)
- Seals out moisture, protecting rebar in the concrete from corrosion and flooring from moisture damage
- Reliable mixing and ratio control when used with the Simpson Strong-Tie<sup>®</sup>
   Optimix<sup>®</sup> static mixing nozzle (included with cartridge)
- Suitable for pressure injection or gravity-feed applications
- Non-shrink material resists oils, salts and mild chemicals
- Final product color: ETI-SLV dark purple / black; ETI-LV amber; ETI-GV – gray

### ETI-SLV Super-Low-Viscosity Epoxy

- Super-low viscosity (350 cP) repairs hairline cracks (0.002") and cracks up to 1/4" in width
- Penetrates smallest cracks
- Meets or exceeds AASHTO M-235 and ASTM C881 Type I and IV, Grade 1, Class B and C

### **ETI-LV Low-Viscosity Epoxy**

- Repairs fine to medium cracks 1/64" to 1/4" in width
- Offers low surface tension to effectively penetrate narrow cracks
- Approved under NSF/ANSI standard 61
- Meets or exceeds AASHTO M-235 and ASTM C881 Type I and IV, Grade 1, Class C

### ETI-GV Gel-Viscosity Epoxy

- Gel-viscosity (non-sag) epoxy repairs medium cracks 3/2" − 1/4" in width
- Decreases in viscosity under pressure, increasing flow
- Suitable for use as pick-proof sealant around doors, windows and fixtures
- Meets or exceeds AASHTO M-235 and ASTM C881 Type I and IV, Grade 3, Class C

### **Application Considerations**

- Suitable for repairing non-moving cracks in concrete walls, floors, slabs, columns and beams.
- ETI can be used to inject cracks in damp or wet conditions (non-seeping or non-leaking conditions only) with excellent results.
- Apply to concrete 60°F or above. For best results, warm material to 60°F or above prior to application.
- Mixed material in nozzle and injection fitting hardens in 15 minutes (ETI-SLV), and in 60 minutes (ETI-LV, ETI-GV) at temperatures of 40°F or above

Shelf Life: 24 months from date of manufacture in unopened cartridge Storage Conditions: For best results, store between 45°F and 95°F Injection Instructions: See pages 293–297.





**ETI-SLV** 



ETI-LV



ETI-GV

# **ETI** Injection Epoxy



Property	Test Method	ETI-SLV Results*	ETI-LV Results*	ETI-GV Results*
Viscosity (75°F)	ASTM D2556	350 cP	1,790 cP	Non-sag gel
Bond Strength (moist cure) @ 2 days	ASTM C882	3,100 psi	2,500 psi	1,110 psi
@ 14 days	3	3,900 psi	2,530 psi	3,990 psi
Tensile Strength	ASTM D638	10,200 psi	7,470 psi	_
Tensile Elongation at Break	ASTM D638	2.1%	4.8%	_
Compressive Yield Strength	ASTM D695	16,500 psi	12,500 psi	11,600 psi
Compressive Modulus	ASTM D695	569,000 psi	342,000 psi	403,000 psi
Heat Deflection Temperature	ASTM D648	140°F	130°F	131°F
Water Absorption (24-hour soak)	ASTM D570	0.25%	0.76%	0.58%
Linear Coefficient of Shrinkage	ASTM D2556	0.0035	0.0040	0.0000
Gel Time (60-gram mass)	ASTM C881	16 min.	68 min.	135 min.
Volatile Organic Compounds (VOC)	EPA Method 24 ASTM D2369	23 g/L	6 g/L	4 g/L
Initial Cure	_	24 hours	24 hours	24 hours
Mixing Ratio by Volume (Part A:Part B)	_	2:1	1:1	1:1

<sup>\*</sup>Material and curing conditions: 73  $\pm\,2^{\circ}\text{F}$ 

### ETI Cartridge System<sup>1</sup>

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

0 ,				
Model No.	Capacity ounces (cubic in.)	Dispensing Tool	Mixing Nozzle	
ETISLV	16.5 (29.8)			
ETILV22	22	EDT22S	EMN022 (included)	
ETIGV22	(39.7)			

<sup>1.</sup> Bulk containers also available. Contact Simpson Strong-Tie for details.

<sup>2.</sup> Use only appropriate Simpson Strong-Tie® mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair epoxy performance.

<sup>3.</sup> EDT22s tool must be configured for 2:1 cartridge ratio.

# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# Crack-Pac® Injection Epoxy



The Crack-Pac® injection epoxy is designed to repair cracks in concrete ranging from 1/64" to 1/4" wide in concrete walls, floors, slabs, columns and beams. The mixed adhesive has the viscosity of a light oil and a low surface tension, allowing it to penetrate fine to medium-width cracks in dry, damp or wet conditions with excellent results. Resin is contained in the cartridge and hardener is contained in the nozzle.

### **Features**

- Dispenses with a standard caulking tool, no special dispensing tool needed
- · Clean and easy to mix
- Seals out moisture, protecting rebar in the concrete from corrosion and flooring from moisture damage
- Chemically bonds with the concrete to restore strength
- Non-shrink material resistant to oils, salts and mild chemicals
- Meets the requirements of AASHTO M-235 and ASTM C881, Type IV, Grade 1, Class C

### **Application Considerations**

- Suitable for repair of cracks ranging from 1/64" to 1/4" wide in concrete walls, floors, slabs, columns and beams
- Can be used to inject cracks in dry, damp or wet conditions with excellent results. Not for use in actively leaking cracks.
- In order for components to mix properly, the resin and hardener must be conditioned to 60°F–80°F before mixing

Shelf Life: 24 months from date of manufacture, unopened

**Storage Conditions:** For best results, store between 45°F and 95°F

**Injection Instructions:** See pages 293–297.

### **Complementary Products**

Crack-Pac® injection epoxy is also available in the Crack-Pac Injection Kit. (ETIPAC10KT). The kit includes everything needed to pressure inject approximately 8 lineal feet of cracks (assumes a concrete thickness of 4" and 1/16" crack width).

- 2 Crack-Pac cartridge/nozzle sets
- 12 E-Z-Click injection ports
- 2 E-Z-Click injection fittings with 12" tubing
- 1 pint of ETR paste-over epoxy (8 oz. of resin + 8 oz. of hardener)
- 4 disposable wood paste-over applicators
- 1 pair latex gloves
- Installation video



Crack-Pac® Injection Epoxy (ETIPAC10)
Dispensing Systems: U.S. Patents 6,737,000 and
6,896,001 B2



Crack-Pac® Kit (ETIPAC10KT)



Crack-Pac® Kit Components

### **Complementary Products**



Crack-Pac®
Injection Epoxy
9 oz. Cartridge

CDT10S

Manual dispensing tool for acrylic adhesive dispensing cartridges (page 128)

# Crack-Pac® Injection Epoxy



Property	Test Method	Results*
Viscosity	ASTM D2556	1,400 cP
Bond Strength (moist cure) @ 2 days	ASTM C882	2,010 psi
@ 14 days	ASTM C882	3,830 psi
Tensile Strength	ASTM D638	5,860 psi
Tensile Elongation at Break	ASTM D638	14.0%
Compressive Yield Strength	ASTM D695	11,300 psi
Compressive Modulus	ASTM D695	319,000 psi
Flexural Strength	ASTM D790	8,020 psi
Water Absorption (24-hour soak)	ASTM D570	0.08%
Linear Coefficient of Shrinkage	ASTM D2556	0.0020
Gel Time (60-gram mass)	ASTM C881	16 min.
Full, Mixed Cartridge	_	30 min.
Volatile Organic Compounds (VOC)	EPA Method 24 ASTM D2369	7 g/L
Initial Cure	_	24 hours
Mixing Ratio by Volume (Part A:Part B)	_	8:1
*Motorial and ouring conditions: 72 ± 0°E		

<sup>\*</sup>Material and curing conditions: 73  $\pm\,2^{\circ}\text{F}$ 

### Crack-Pac® Cartridge System

Model No.	Capacity ounces (cubic in.)	Cartridge Type	Carton Quantity	Dispensing Tool
CPFH09	9 (16.2)	single	12	CDT10S or standard caulking tool
CPFH09KT	18 (32.4)	single	2 (kits)	

# Crack-Pac® Flex-H<sub>2</sub>O™ Polyurethane Crack Sealer



The Crack-Pac® Flex-H<sub>2</sub>O™ polyurethane injection resin seals leaking cracks, voids or fractures from ½" to ¼" wide in concrete or solid masonry. Designed to perform in applications where water is seeping or mildly leaking from the crack, the polyurethane is packaged in the cartridge and an accelerator is packaged in the nozzle. When the resin encounters water as it is injected into the crack, it becomes an expanding foam that provides a flexible seal in leaking and non-leaking cracks.

### **Features**

- Can be dispensed with a standard caulking tool
- Can also be used on dry cracks if water is introduced to affected area
- Can be used with a reduced amount or without accelerator to slow down reaction time
- · Expands to fill voids and seal the affected area
- Fast reacting reaction begins within 1 minute after exposure to moisture; expansion may be completed within 3 minutes (depending on the amount of moisture and the ambient temperature)
- 20:1 expansion ratio (unrestricted rise) means less material needed

### **Application Considerations**

- Suitable for sealing cracks ranging from ½2" to ¼" wide in concrete and solid masonry.
- Suitable for repair of cracks in dry, damp and wet conditions with excellent results. Designed to perform in applications where water is seeping or mildly leaking from the crack.
- In order for components to mix properly, the resin and hardener must be conditioned to 60°F–90°F before mixing.

Shelf Life: 12 months from the date of manufacture, unopened

Usage Temperature: 60°F to 90°F

**Storage Conditions:** For best results, store in a dry area between 45°F and 90°F. Product is very moisture sensitive.

Installation Instructions: See pages 293–297.

**Accessories:** See page 289 for information on mixing nozzles and for crack repair accessories.

### Additional Components Needed for Crack Repair

Condition	Paste-Over Material	Ports	
Dry Crack	ETR or		
Wet Crack	CIP-F*	EIP-EZA Flush-Mount	
Seeping Crack	Hydraulic Cement		
Mildly Leaking Crack		EIPX-EZ Drill-In	

<sup>\*</sup>CIP-F requires EIP-EZA port.



### Crack-Pac® Flex-H<sub>2</sub>O™ Crack Sealer

Dispensing System: U.S. Patents 6,737,000 and 6,896,001 B2

### Crack-Pac® Flex-H<sub>2</sub>O™ Cartridge System

Model No.	Capacity Ounces	Carton Quantity
CPFH09	9	12
CPFH09KT	18	2 (kits)

### Crack-Pac® Flex-H<sub>2</sub>O™ Bulk Packaging

Model No.	Description	Capacity	
FH05*	Flex-H <sub>2</sub> O Resin	5 Gallons	
FNUO	Flex-H <sub>2</sub> O Catalyst	16 Ounces	

<sup>\*</sup>For standard reaction time, use a 30:1 resin: catalyst ratio. For a faster reaction time, add more catalyst, for a slower reaction time, use less.

### Complementary Products



### Crack-Pac<sup>®</sup> Flex-H<sub>2</sub>O<sup>™</sup> Kit (CPFH09KT)

- 2 Crack-Pac Flex-H<sub>2</sub>0 cartridge/nozzle sets
- 12 E-Z-Click injection ports
- 2 E-Z-Click injection fittings with 12" tubing



# Crack-Pac<sup>®</sup> Flex-H<sub>2</sub>O<sup>™</sup> Kit Components

- 1 pint of ETR paste-over epoxy (8 oz. of resin + 8 oz. of hardener)
- 4 disposable wood pasteover applicators
- 1 pair latex gloves

# **Crack Repair Accessories**







**E-Z-Click** Injection Fitting



CIP-F

## Crack Injection Paste-Over in Cartridge Delivery System

Model No.	Capacity ounces	Carton Quantity
CIP-F	22	10

### Crack Repair Accessories Product Data

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

Description	Model No.	Package Qty.	Carton Qty. (ea.)
6 Optimix® mixing nozzles for ETI epoxies (61½" long, 3/6" square). Includes retaining nuts.1	EMNO22-RP6	6	30 (5 Packs)
100 E-Z-Click flush-mount injection ports and 1 E-Z- Click injection fitting	EIP-EZA	_	100
20 E-Z-Click flush-mount injection ports and 1 E-Z-Click injection fitting (compatible with all Simpson Strong-Tie paste-overs)	EIP-EZAKT	_	5 Kits
20 E-Z-Click corner mount/drilled-in injection ports <sup>2</sup>	EIPX-EZ-RP20	20	100 (5 Packs)
20 E-Z-Click corner mount/drilled-in injection ports and 1 E-Z-Click injection fitting <sup>2</sup>	EIPX-EZKT	_	5 Kits
E-Z-Click injection fitting	EIF-EZ	1	10
ETR Kit containing 1 8-oz. canister of resin and 1 8-oz. canister of hardener	ETR16	_	4 Kits

<sup>1.</sup> Use only an appropriate Simpson Strong-Tie® mixing nozzle in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair epoxy performance.

<sup>2.</sup> EIPX intended for use as a surface mount port in corners and a drilled-in port on flat surfaces. All accessories compatible with ETI-SLV, ETI-LV and ETI-GV epoxies.

# **Heli-Tie**<sup>™</sup> Helical Wall Tie

Strong-1

The Heli-Tie™ is a stainless-steel helical tie used to anchor building façades to structural members or to stabilize multiple-wythe brick walls.

The helical design allows the tie to be driven quickly and easily into a predrilled pilot hole (or embedded into mortar joints in new construction) to provide a mechanical connection between a masonry façade and its backup material or between multiple wythes of brick. As it is driven, the fins of the tie undercut the masonry to provide an expansion-free anchorage that will withstand tension and compression loads.

The Heli-Tie wall tie is installed using a proprietary setting tool that is used with an SDS-PLUS shank rotohammer to drive and countersink the tie. Heli-Tie wall ties perform in concrete and masonry as well as wood and steel studs.



#### **Features**

- Installs quickly and easily with the rotohammer in hammer mode, the tie installs faster than competitive products.
- Provides an inconspicuous repair that preserves the appearance of the building. After installation, the tie is countersunk up to 1/2" below the surface, allowing the tie location to be patched.
- Larger core diameter provides higher torsional capacity, resulting in less deflection due to "uncoiling" under load.
- Fractionally sized anchor no metric drill bits required.
- Patented manufacturing process results in a more uniform helix along the entire tie, allowing easier driving and better interlock with the substrate.

Material: Type-304 stainless steel (Type 316 available by special order—contact Simpson Strong-Tie for details)

Test Criteria: CSA A370

#### Installation

- Drill pilot hole through the facade material and into the backup material to the specified embedment depth + 1" using appropriate drill bit(s). Drill should be in rotation-only mode when drilling into soft masonry or into hollow backing material.
- Position blue end of the Heli-Tie<sup>™</sup> fastener in the installation tool and insert the tie into the pilot hole.
- With the SDS-PLUS rotohammer in hammer mode, drive the tie until the tip of the installation tool enters the exterior surface of the masonry and countersinks the tie below the surface. Patch the hole in the façade.

Heli-Tie™ Product Data

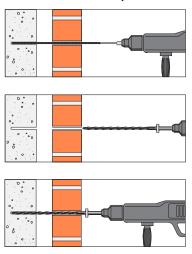
Size	Model	Drill Bit Dia.	Qua	ntity
(in.)	No.	(in.)	Box	Carton
3/8 x 7	HELI37700A		50	400
3/8 x 8	HELI37800A		50	400
3% x 9	HELI37900A		50	400
3% x 10	HELI371000A		50	200
3% x 11	HELI371100A	7/32	50	200
3/8 x 12	HELI371200A	or 1⁄4	50	200
3/8 x 14	HELI371400A	/4	50	200
3% x 16	HELI371600A		50	200
3% x 18	HELI371800A		50	200
% x 20	HELI372000A		50	200

# Heli-Tie™ Helical Wall Tie

U.S. Patent 7,269,987



## Installation Sequence



Special-order lengths are also available; contact Simpson Strong-Tie for details.



#### Heli-Tie™ Fastener Installation Tool -Model HELITOOL37A

Required for correct installation of Heli-Tie wall ties. Speeds up installation and automatically countersinks the tie into the façade material.

# Heli-Tie™ Design Information



#### Guide Tension Loads in Various Base Materials

				Min.		Tension Load <sup>1</sup>	
Size in. (mm)	in. Base Material	Anchor Location	Drill Bit Dia. in.	Embed. Depth in. (mm)	Ultimate <sup>2</sup> lb. (kN)	Load at Max. Permitted Displ. <sup>3</sup> lb. (kN)	Standard Deviation lb. (kN)
		Mortar	7/32		<b>570</b> (2.5)	<b>240</b> (1.1)	<b>79</b> (0.4)
	Solid	Bed Joint	1/4		<b>365</b> (1.6)	<b>130</b> (0.6)	<b>46</b> (0.2)
	Brick <sup>4</sup>	Brick	7/32		<b>1,310</b> (5.8)	<b>565</b> (2.5)	<b>84</b> (0.4)
		Face	1/4	<b>3</b> (76)	<b>815</b> (3.6)	<b>350</b> (1.6)	<b>60</b> (0.3)
		Mortar Bed Joint	7/32		<b>530</b> (2.4)	<b>285</b> (1.3)	<b>79</b> (0.4)
	Hollow Brick <sup>5</sup>	Brick	7/32		<b>775</b> (3.4)	<b>405</b> (1.8)	<b>47</b> (0.2)
		Face	1/4		<b>510</b> (2.3)	<b>185</b> (0.8)	<b>20</b> (0.1)
		Center of	7/32		<b>1,170</b> (5.2)	<b>405</b> (1.8)	<b>79</b> (0.4)
	Grout-Filled CMU <sup>6</sup>	Face Shell	1/4		<b>830</b> (3.7)	<b>350</b> (1.6)	<b>60</b> (0.3)
		Web	7/32		<b>1,160</b> (5.2)	<b>440</b> (2.0)	<b>56</b> (0.2)
3/8			1/4		<b>810</b> (3.6)	<b>330</b> (1.5)	<b>100</b> (0.4)
(9.0)		Mortar	7/32	<b>2</b> 3/4 (70)	<b>720</b> (3.2)	<b>320</b> (1.4)	<b>71</b> (0.3)
		Bed Joint	1/4		<b>530</b> (2.4)	<b>205</b> (0.9)	<b>58</b> (0.3)
		Center of	7/32		<b>790</b> (3.5)	<b>305</b> (1.4)	<b>56</b> (0.2)
	Hollow	Face Shell	1/4		<b>505</b> (2.2)	<b>255</b> (1.1)	<b>46</b> (0.2)
	CMU <sup>7</sup>	Web	7/32		<b>1,200</b> (5.3)	<b>445</b> (2.0)	<b>50</b> (0.2)
		vven	1/4		<b>675</b> (3.0)	<b>385</b> (1.7)	<b>96</b> (0.4)
	Normal-Weight		7/32	<b>1 3/4</b> (44)	<b>880</b> (3.9)	<b>410</b> (1.8)	<b>76</b> (0.3)
	Concrete <sup>8</sup>	_	1/4	<b>2</b> 3/ <sub>4</sub> (70)	<b>990</b> (4.4)	<b>380</b> (1.7)	<b>96</b> (0.4)
	2x4 Wood	Center of	7/32	23/4	<b>590</b> (2.6)	<b>370</b> (1.6)	<b>24</b> (0.1)
	Stud <sup>9,11</sup>	Thin Edge	1/4	(70)	<b>450</b> (2.0)	<b>260</b> (1.2)	<b>6</b> (0.0)
	Metal Stud <sup>10,11</sup>	Center of	7/32	1 (05)	<b>200</b> (0.9)	<b>120</b> (0.5)	<b>8</b> (0.0)
	IVICIAI SILIU 5	Flange	1/4	(25)	<b>155</b> (0.7)	<b>95</b> (0.4)	<b>2</b> (0.0)

Caution: Loads are guide values based on laboratory testing. On-site testing shall be performed for verification of capacity since base material quality can vary widely.

- Tabulated loads are guide values based on laboratory testing. Onsite testing shall be performed for verification of capacity since base material quality can vary widely.
- Ultimate load is average load at failure of the base material. Heli-Tie<sup>™</sup> fastener average ultimate steel strength is 3,885 pounds and does not govern.
- Load at maximum permitted displacement is average load at displacement of 0.157 inches (4 mm). The designer shall apply a suitable factor of safety to these numbers to derive allowable service loads.
- Solid brick values for nominal 4-inchwide solid brick conforming to ASTM C62/C216, Grade SW. Type N mortar is prepared in accordance with IBC Section 2103.8.
- Hollow brick values for nominal 4-inchwide hollow brick conforming to ASTM C216/C652, Grade SW, Type HBS, Class H40V. Mortar is prepared in accordance with IBC Section 2103.8.
- Grout-filled CMU values for 8-inch-wide lightweight, medium-weight and normal-weight concrete masonry units. The masonry units must be fully grouted. Values for 8-inch-wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry, f'<sub>m</sub>, at 28 days is 1,500 psi.
- Hollow CMU values for 8-inch-wide lightweight, medium-weight and normal-weight concrete masonry units.
- Normal-weight concrete values for concrete with minimum specified compressive strength of 2,500 psi.
- 2x4 wood stud values for nominal 2x4 Spruce-Pine-Fir.
- 10. Metal stud values for 20-gauge C-shape metal stud.
- 11. For new construction. Anchor one end of tie into backup material. Embed other end into veneer mortar joint. Not for retrofits due to difficulty of locating center of 2x4 or metal stud flange.

## Compression (Buckling) Loads<sup>1</sup>

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

Size in. (mm)	Unsupported Length in. (mm)	Ultimate Compression Load <sup>1</sup> Ib. (kN)
<b>%</b> (9.0)	<b>1</b> (25)	<b>1,905</b> (8.5)
	<b>2</b> (50)	<b>1,310</b> (5.8)
	<b>4</b> (100)	<b>980</b> (4.4)
	<b>6</b> (150)	<b>785</b> (3.5)

The Designer shall apply a suitable factor of safety to these numbers to derive allowable service loads.



HELITEST37A

HELIKEY37A

#### Heli-Tie<sup>™</sup> Wall Tie Tension Tester - Model HELITEST37A

Recommended equipment for onsite testing to accurately determine load values in any specific structure, the Heli-Tie wall tie tension tester features a key specifically designed to grip the Heli-Tie fastener and provide accurate results.

Replacement test keys sold separately (Model HELIKEY37A).

# Heli-Tie™ Helical Stitching Tie



The Simpson Strong-Tie® Heli-Tie™ helical stitching tie provides a unique solution to the preservation and repair of damaged brick and masonry structures. Ties are grouted into existing masonry to repair cracks and increase strength with minimum disturbance. Made of Type-304 stainless steel, the Heli-Tie stitching tie features radial fins formed on the steel wire via cold rolling process, increasing the tensile strength of the tie.



#### **HELIST254000**

#### **Features**

- Helical design distributes loads uniformly over a large surface area
- Installs into the mortar joint to provide an inconspicuous repair and preserve the appearance of the structure
- Type-304 stainless steel offers superior corrosion resistance to original reinforcement
- Patented manufacturing process results in consistent, uniform helix configuration (U.S. Patent 7,269,987)
- Batch number printed on each tie for easy identification and inspection

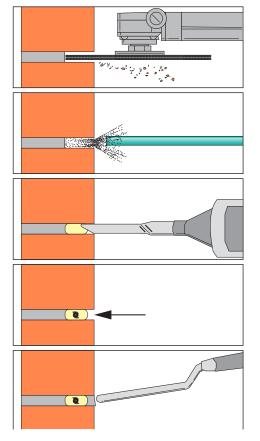
**HELIST254000:** ¼" x 40" stitching tie **Material:** Type-304 stainless steel

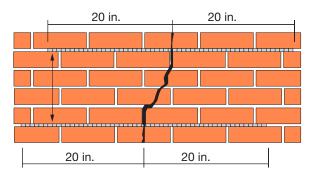
Ordering Information: Sold in tubes of 10

#### Installation Instructions

- Chase bed joint 20" on either side of the affected area to a depth of approximately 11/4" with a rotary grinding wheel. Vertical spacing of installation sites should be 12" for red brick or "every other course" for concrete masonry units.
- Clear bed joint of all loose debris.
- Mix non-shrink repair grout or mortar per product instructions and place into the prepared bed joint, filling the void to approximately two-thirds of its depth. Simpson Strong-Tie FX-263 repair mortar may be used.
- Embed the tie at one-half the depth of the void. Trowel displaced grout to fully encapsulate the tie.
- Fill any remaining void and vertical cracks with non-shrink repair grout or other repair mortar to conceal repair site.

# Installation Sequence







Important: These instructions are intended as recommended guidelines. Due to the variability of field conditions, selection of the proper material for the intended application and installation is the sole responsibility of the applicator.

Epoxy injection is an economical method of repairing non-moving cracks in concrete walls, slabs, columns and piers and is capable of restoring the concrete to its pre-cracked strength. Prior to doing any injection it is necessary to determine the cause of the crack. If the source of cracking has not been determined and remedied, the concrete may crack again.

#### **Materials**

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

- ETI-SLV for repair of hairline cracks (0.002") and those up to ¼" in width.
- ETI-LV for repair of fine to medium-width cracks (Suggested width range: 1/4"-1/4").
- ETI-GV for repair of medium-width cracks (Suggested width range: 3/2"-1/4")
- Crack-Pac® injection epoxy for repair of fine to medium non-structural cracks (Suggested width range: 1/64"-1/4")
- CIP-F and ETR are recommended for paste-over of crack surface and installation of injection ports.
   ET-HP, EDOT™, ETR or SET adhesives may also be used as a substitute. (SET is the only paste-over epoxy approved for NSF/ANSI Standard 61.)
- E-Z-Click<sup>™</sup> injection ports, fittings and other suitable accessories.

# Estimating Guide for Epoxy Crack Injection

Width of Crack (in.)	Concrete Thickness (in.)	Approx. Coverage per 22 oz. Cartridge (linear ft.)	Approx. Coverage per 16.5 oz. Cartridge (linear ft.)	Approx. Coverage per 9 oz. Cartridge (linear ft.)
	4	47.7	35.7	18.4
1/	6	31.8	23.8	12.3
1/64	8	23.8	17.9	9.2
	10	19.1	14.3	7.4
	4	23.8	17.9	9.2
1/32	6	15.9	11.9	6.1
//32	8	11.9	8.9	4.6
	10	9.5	7.1	3.7
	4	11.9	8.9	4.6
1/	6	7.9	6.0	3.1
1/16	8	6.0	4.5	2.3
	10	4.8	3.6	1.8
	4	6.0	4.5	2.3
1/8	6	4.0	3.0	1.5
/8	8	3.0	2.2	1.2
	10	2.4	1.8	0.9
	4	4.0	3.0	1.5
2/	6	2.6	2.0	1.0
3/16	8	2.0	1.5	0.8
	10	1.6	1.2	0.6
	4	3.0	2.2	1.2
1/.	6	2.0	1.5	1.8
1/4	8	1.5	1.1	0.6
	10	1.2	0.9	0.5

Coverage listed is approximate and will vary depending on waste and condition of concrete.

# SIMPSON Strong-Tie

#### Preparation of the Crack for Injection

Clean the crack and the surface surrounding it to allow the paste-over to bond to sound concrete. At a minimum, the surface to receive paste-over should be brushed with a wire brush. Oil, grease or other surface contaminant must be removed in order to allow the paste-over to bond properly. Take care not to impact any debris into the crack during cleaning. Using clean, oil-free compressed air, blow out the crack to remove any dust, debris or standing water. Best results will be obtained if the crack is dry at the time of injection. If water is continually seeping from the crack, the flow must be stopped in order for epoxy injection to yield a suitable repair. Other materials such as polyurethane resins may be required to repair an actively leaking crack.

For many applications, additional preparation is necessary in order to seal the crack. Where a surfacing material has been

removed using an acid or chemical solvent, prepare the crack as follows:

- 1. Using clean, compressed air, blow out any remaining debris and liquid.
- 2. Remove residue by high-pressure washing or steam cleaning.
- 3. Blow any remaining water from the crack with clean compressed air.

If a coating, sealant or paint has been applied to the concrete, it must be removed before placing the paste-over epoxy. Under the pressure of injection, these materials may lift and cause a leak. If the surface coating is covering the crack, it may be necessary to route out the opening of the crack in a "V" shape using a grinder in order to get past the surface contamination.

# Sealing of the Crack and Attachment of E-Z-Click™ Injection Ports

1. To adhere the port to the concrete, apply a small amount of pasteover around the bottom of the port base (Picture 1). Place the port at one end of the crack and repeat until the entire crack is ported (Picture 2). As a rule of thumb, injection ports should be placed 8" apart along the length of the crack.

**Important:** Do not allow paste-over to block the port or the crack under it; this is where the injection epoxy must enter the crack.

- 2. Using a putty knife or other paste-over tool, generously work paste-over along the entire length of the crack (Picture 3). Take care to mound the paste-over around the base of the port to approximately ¼" thick extending 1" out from the base of the port and to work out any holes in the material. It is recommended that the paste-over should be a minimum of ¾6" thick and 1" wide along the crack. Insufficient paste-over will result in leaks under the pressure of injection. If the crack passes completely through the concrete element, seal the back of the crack, if possible. If not, epoxy may be able to run out the back side of the crack, resulting in an ineffective repair.
- 3. Allow the paste-over to harden before beginning injection. Note: CIP-F and ETR epoxies are fast-cure materials and may harden prematurely if left in a mixed mass on the mixing surface while installing ports. Spreading paste-over into a thin film (approximately 1/s") on the mixing surface will slow curing by allowing the heat from the reaction to dissipate.

# Injection Procedure for ETI-SLV, ETI-LV, ETI-GV and Crack-Pac® Injection Epoxy

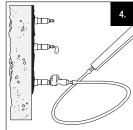
- 1. Follow cartridge preparation instructions on the cartridge label. Verify that the material flowing from the Optimix® mixing nozzle is a uniform and consistent color: for ETI-SLV, the mixed product is black; ETI-LV is transparent amber; and ETI-GV is grey. For Crack-Pac® injection epoxy, verify that the mixed material in the cartridge is a transparent amber color.
- Attach the E-Z-Click™ fitting to the end of the nozzle by pushing the tubing over the barbs at the end of the nozzle. Make sure that all ports are pushed in to the open position.
- 3. Attach the E-Z-Click™ injection fitting to the first E-Z-Click™ port until it clicks into place. Make sure that the heads of all the ports are pushed in to the open position. In vertical applications, begin injection at the lowest port and work your way up. In a horizontal application, start at one end of the crack and work your way to the other end.
- 4. Inject epoxy into the first port until it will no longer flow into the crack. If epoxy shows at the next port and the first port still accepts material, close the second port and continue to inject into the first port until it accepts no more epoxy. Continue closing ports where epoxy appears until the first port refuses epoxy. When the first port reaches the point of refusal, brace the base of the port and pull out gently on the head of the port to close it. Pulling too hard may dislodge the port from the surface of the concrete, causing a leak. Depress the metal tab on the head of the E-Z-Click fitting and remove it from the port.
- 5. Go to the last port where epoxy appeared while injecting the first port, open it, and continue injection at this port. If the epoxy has set up and the port is bonded closed, move to the next clean port and repeat the process until every portion of the crack has refused epoxy.











While this method may appear to leave some ports uninjected, it provides maximum pressure to force the epoxy into the smaller areas of the crack. Moving to the next port as soon as epoxy appears will allow the epoxy to travel along the wider parts of the crack to the next ports rather than force it into the crack before it travels to the next ports.

# SIMPSON Strong-Tie

#### **INJECTION TIPS**

- If using a pneumatic dispensing tool, set the tool at a low setting when beginning injection and increase pressure if necessary to get the epoxy to flow.
- For narrow cracks, it may be necessary to increase the
  pressure gradually until the epoxy begins to flow. It may also
  be necessary to wait for a few minutes for the epoxy to fill the
  crack and travel to the next port.
- If desired, once the injection epoxy has cured, remove the injection ports and paste-over. An epoxy-based paste-over can be removed with a chisel, scraper or grinder. The paste-over can
- be simply peeled off if CIP-F is used. Using a heat gun to soften the epoxy is recommended when using a chisel or scraper.
- Mixing nozzles can be used for multiple cartridges as long as the epoxy does not harden in the nozzle. For injection epoxies in side-by-side cartridges, care must be taken to ensure the level of material is the same on both parts of the cartridge. This can be done by checking for air in the cartridge and the positions of the wipers in the back of the cartridge. If the liquid levels are off by more than 1/8", then Step 1 from the injection procedures must be repeated.

#### TROUBLESHOOTING

# Epoxy is flowing into the crack, but not showing up at the next port.

This can indicate that the crack either expands and/or branches off under the surface of the concrete. Continue to inject and fill these voids. In situations where the crack penetrates completely through the concrete element, and the back-side of the concrete element cannot be sealed (e.g., basement walls, or footings with backfill), longer injection time may not force the epoxy to the next port. This most likely indicates that epoxy is running out the unsealed back side of the crack. In this case, the application may require a gel viscosity injection epoxy (ETI-GV) or may not be suitable for epoxy injection repair without excavation and sealing of the back side of the crack.

# Epoxy is leaking from the pasted-over crack or around injection ports.

Stop injecting. If using a fast-cure paste-over material (ETR or CIP), wipe off the leaking injection epoxy with a cotton cloth and reapply the paste-over material. Wait approximately 10–15 minutes to allow the epoxy to begin to harden. If the leak is large (e.g., the port broke off of the concrete surface), it is a good idea to wait approximately 30 minutes, or longer as necessary, to allow the paste-over to cure more completely. Check to see that the epoxy is hard before reinjecting, or the paste-over or ports may leak. Another option for small leaks is to clean off the injection epoxy and use paraffin or crayon to seal the holes.

#### More epoxy is being used than estimated.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

This may indicate that the crack either expands or branches off below the surface. Continue to inject and fill these voids. This may also indicate that epoxy is running out the back side of the crack. If the crack penetrates completely through the concrete element and cannot be sealed, the application may require a gel viscosity injection epoxy (ETI-GV) or may not be suitable for injection repair.

# Back pressure is preventing epoxy from flowing. This can indicate several situations:

- The crack is not continuous, and the portion being injected is full. (See above instructions about injection after the port has reached refusal.)
- The port is not aligned over the crack properly.
- The crack is blocked by debris.
- The injection epoxy used has too high a viscosity.
- If the mixing nozzle has been allowed to sit for a few minutes full of epoxy, the material may have hardened in the nozzle. Attach the E-Z-Click™ fitting to a port at another uninjected location on the crack and attempt to inject. If the epoxy still won't flow, chances are the epoxy has hardened in the nozzle. If so, replace the nozzle.

#### Less epoxy is being used than estimated.

This may indicate that the crack is shallower than originally thought, or the epoxy is not penetrating the crack sufficiently before moving to the next port. Reinject some ports with a lower-viscosity epoxy to see if the crack will take more epoxy. Another option is to heat the epoxy to a temperature of 80–100°F, which will reduce its viscosity and allow it to penetrate into small cracks easier. The epoxy should be heated uniformly; do not overheat cartridge.

# C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

# **Crack Injection Guide**

# SIMPSON Strong-Tie

## Injection Procedure for Crack-Pac® Flex-H<sub>2</sub>0™ Crack Sealer

- 1. Follow cartridge preparation instructions on the cartridge label. Verify that the material flowing from the nozzle is a uniform green color.
- Attach the E-Z-Click<sup>™</sup> fitting to the end of the nozzle by pushing the tubing over the barbs at the end of the nozzle. Make sure that all ports are pushed into the open position.
- 3. Attach the E-Z-Click injection fitting to the first E-Z-Click port until it clicks into place. Make sure that the head of the port is pushed into the open position. In vertical applications, begin injection at the lowest port and work your way up. In a horizontal application, start at one end of the crack and work your way to the other end.
- 4. Inject polyurethane into the first port until material shows at the next port. Remove the E-Z-Click fitting by bracing the base of the port and pulling out gently on the head of the port to close it. Pulling too hard may dislodge the port from the surface of the concrete, causing a leak. Depress the metal tab on the head of the E-Z-Click fitting and remove it from the port.
- Move to the next port and repeat until all ports have been injected.

#### Injection Tips for Crack-Pac® Flex-H<sub>2</sub>O Crack Sealer

- For narrow cracks, it may be necessary to increase the pressure gradually until the polyurethane begins to flow. It may also be necessary to wait a few minutes for the material to fill the crack and travel to the next port.
- If desired, once the polyurethane has cured, remove the injection ports and paste-over epoxy or hydraulic cement. The paste-over can be removed with a chisel, scraper or grinder.

## Troubleshooting for Crack-Pac® Flex-H<sub>2</sub>O Crack Sealer

# Polyurethane is flowing into the crack, but not showing up at the next port.

This can indicate that either the crack expands and/or branches off under the surface of the concrete. Continue to inject and fill these voids.

#### Back pressure is preventing polyurethane from flowing.

This can indicate several situations:

- The crack is not continuous and the portion being injected is full.
- The port is not aligned over the crack properly.
- The crack is blocked by debris.

# Polyurethane is leaking from the pasted-over crack or around injection ports.

Stop injecting. If using a fast cure paste-over material (ETR or CIP), wipe off the leaking injection epoxy with a cotton cloth and reapply the paste over material. Wait a approximately 10–15

minutes to allow the paste-over to begin to harden. If the leak is large (e.g., the port broke off of the concrete surface), it is a good idea to wait approximately 30 minutes, or longer as necessary, to allow the paste-over to cure more completely. Check to see that the paste-over is hard before reinjecting or the paste-over or ports may leak.

Another option for small leaks is to clean off the injection adhesive and use paraffin or crayon to seal the holes.

#### More polyurethane is being used than estimated.

This may indicate that the crack either expands or branches off below the surface. Continue to inject and fill these voids.

#### Less polyurethane is being used than estimated.

This may indicate that the crack is shallower than originally thought, or the polyurethane is not penetrating the crack sufficiently before moving to the next port.



#### **GRAVITY-FEED PROCEDURE**

In some horizontal applications where complete penetration isn't a requirement, cracks can be repaired using the gravity-feed method.

- 1. Follow cartridge preparation instructions on the cartridge label. Verify that the material flowing from the Optimix® mixing nozzle is a uniform and consistent color: For ETI-SLV, the mixed product is black, while ETI-LV is transparent amber. For Crack-Pac® injection epoxy, verify that the mixed material in the cartridge is a transparent amber color.
- 2. Starting at one end of the crack, slowly dispense epoxy into the crack, moving along the crack as it fills. It will probably be necessary to do multiple passes in order to fill the crack. It is possible that the epoxy will take some time to run into the crack, and the crack may appear empty several hours after the initial application. Reapply epoxy until the crack is filled.
- 3. In situations where the crack completely penetrates the member (e.g., concrete slab), the material may continue to run through the crack into the subgrade. It may be possible to use a small amount of coarse, dry sand to act as a barrier for the injection epoxy. Place the sand in the crack to a level no more than ¼" thickness of the member and apply the injection epoxy as described in step 2. The epoxy level will drop as it penetrates the sand, but should cure and provide a seal to the bottom of the crack. Reapply the epoxy until the crack is filled. In some cases, application of sand is impractical or not permitted and epoxy repair may not provide a complete and effective repair. Use of a gel viscosity injection epoxy (ETI-GV) may permit a surface repair to the crack with partial penetration.

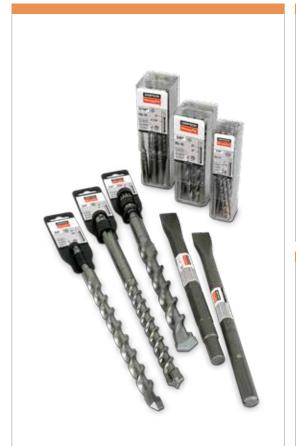
# **Carbide Drill Bits**





Simpson Strong-Tie offers a complete line of premium-quality drill bits, core bits and chisels to handle any drilling demolition and concrete preparation need. Our carbide products are manufactured to demanding tolerances and are designed to maximize production on the jobsite.

Our carbide-tipped drill bits are premium-quality, professional-grade tools manufactured in Germany to the highest industry standards. They are designed to meet precise ANSI tolerance requirements and incorporate proprietary features that enhance durability, drilling speed and usability. Regular and quad-head bit and solid-tipped tip configurations are available. Shank styles include SDS-PLUS, SDS-Max, Spline, and Straight.







# C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

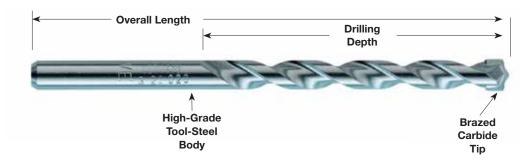
# Carbide Drill Bits for Concrete and Masonry



# Carbide Drill Bit Selection Information

Our carbide-tipped drill bits are premium-quality, professional-grade tools manufactured in Germany to the highest industry standards for Simpson Strong-Tie.

They are designed to meet precise ANSI tolerance requirements and incorporate proprietary features that enhance durability and drilling speed, while improving ease of use. Regular and quad-head bit tip and solid-tipped configurations are available. Shank styles include SDS-PLUS, SDS-MAX, spline and straight.



#### Features and Benefits

- Uniformly brazed carbide inserts result in longer bit life
- Most bits contain a centering tip that facilitates easy spot drilling
- Chromium-nickel-molybdenum steel alloy body ensures hammering quality and extended service life
- Heat-treatment procedures and shot-peened finish increase surface hardness and drilling speed, reduce drill bit wear and improve resistance to bending forces
- Drill bits conform to ANSI Standard B212.15

# Additional Features for SDS-MAX, Spline and Select SDS-PLUS Bits:

- Chisel-shaped drill bit head penetrates the material and directs concrete dust into the multi-flute spiral
- Patented, high-volume, multi-flute spiral quickly channels concrete dust from the hole to improve drilling speed
- 4 x 90° head geometry crushes through rebar and prevents sticking in reinforced concrete



Solid-tip carbide drill bit

#### **Quad-Head Feature**

(Available in SDS-PLUS, SDS-MAX and spline shank)

All the features of single cutter bits and the quad-head dual-cutter are designed to improve durability and drilling speed. The high-volume, double-helix design of the quad-head bit comes with the patented, high-performance, reinforced core flute to maximize energy transfer.

# Simpson Strong-Tie® drill bits come in various shank styles to fit virtually any drill or rotohammer.



# Carbide Drill Bits for Concrete and Masonry



# Drill Bit Tool Selection Guide

#### SDS-PLUS

Fits all current and older SDS-PLUS rotohammers from AEG, Black & Decker, Bosch, DeWalt, Hitachi, Hilti, Kango, Makita, Metabo, Milwaukee, Porter Cable, Ramset, Red Head, Ryobi, Skil

#### SDS-MAX

Fits all current and older SDS-MAX rotohammers from Black & Decker, Bosch, DeWalt, Hitachi, Hilti, Kango, Makita, Metabo, Milwaukee

#### Spline

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

Fits all current and older Spline rotohammers from AEG, Black & Decker, Bosch, DeWalt, Hitachi, Kango, Makita, Metabo, Milwaukee, Ramset, Red Head, Ryobi

#### The following are registered trademarks of the respective holders:

AEG® – AEG Power Tool Corp.
Bosch® – Robert Bosch Power Tool Corp.
SDS-PLUS and SDS-MAX are registered trademarks of Robert Bosch Power Tool Corp.
B&D® – Black and Decker US, Inc.
Hilti® – Hilti of America, Inc.
Hitachi® – Hitachi Power Tools USA, Ltd.
Kango® – Kango Wolf Power Tools, Inc.

Makita® – Makita USA, Inc.
Metabo® – Metabo Corp.
Milwaukee® – Milwaukee Electric Tool Corp.
Porter Cable® – Porter Cable Corporation
Ramset® – Illinois Tool Works
Red Head® – Illinois Tool Works
Ryobi® – Ryobi America Corporation



# **SDS-PLUS** Drill Bits

# SIMPSON Strong-Tie

# SDS-PLUS Shank Bits

SDS-PLUS		0	
Dia.	Drilling Depth	Overall Length	Model
(in.)	(in.)	(in.)	No.
5/	2	41/4	MDPL01504
5/32	4	61/4	MDPL01506
	2	41/4	MDPL01804
	4	61/4	MDPL01806
3/16	6	81/4	MDPL01808
/16	8	10	MDPL01810
	10	12	MDPL01812
	12	14	MDPL01814
	4	61/4	MDPL02106
	6	81⁄4	MDPL02108
7/32	11	8¾	MDPL02111
	14	16	MDPL02116
	18	20	MDPL02120
	2	41/4	MDPL02504
	4	61/4	MDPL02506
1/4	6	81/4	MDPL02508
	9	11	MDPL02511
	12	14	MDPL02514
	14	16	MDPL02516
5/16	4	61/4	MDPL03106
	10	12 61/4	MDPL03112
	8	101/4	MDPL03706 MDPL03710
3/8	10	121/4	MDPL03710
78	16	18	MDPL03712
	22	24	MDPL03724
	4	61/4	MDPL04306
7/16	10	121/4	MDPL04312
	4	61/4	MDPL05006
	8	101/4	MDPL05010
1/2	10	121/4	MDPL05012
	16	18	MDPL05018
	22	24	MDPL05024
	4	61/4	MDPL05606
9/16	10	121/4	MDPL05612
	16	18	MDPL05618
	6	8	MDPL06208
5/8	10	12	MDPL06212
/8	16	18	MDPL06218
	22	24	MDPL06224
11/16	6	8	MDPL06808
	6	8	MDPL07508
	8	10	MDPL07510
3/4	10	12	MDPL07512
	16	18	MDPL07518
40.1	22	24	MDPL07524
13/16	6	8	MDPL08108
27/32	6	8	MDPL08408
7/	6	8	MDPL08708
7/8	10	121/4	MDPL08712
	16	18	MDPL10010
1	8 16	10 18	MDPL10010 MDPL10018
	10	10	MINLFIGUIQ

#### SDS-PLUS Shank Bit SDS-PLUS bits use an asymmetrical-parabolic flute for efficient energy transmission and dust removal.



## SDS-PLUS Solid-Tip Carbide Drill Bits

Diameter (in.)	Total Length (in.)	Drilling Depth (in.)	Model No.
3/16	41/4	2	MDPL01804S
3/16	61/4	4	MDPL01806S
3/16	81/4	6	MDPL01808S
3/16	12	10	MDPL01812S
1/4	61/4	4	MDPL02506S
1/4	81/4	6	MDPL02508S
1/4	12	10	MDPL02512S
5/16	61/4	4	MDPL03106S
5/16	12	10	MDPL03112S
3/8	61/4	4	MDPL03706S
3/8	121/4	10	MDPL03712S
1/2	61/4	4	MDPL05006S
1/2	121/4	10	MDPL05012S
9/16	6	4	MDPL05606S
9/16	12	10	MDPL05612S

### SDS-PLUS Quad Head Drill Bits

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Model No.
	6	8	MDPL06208Q
5/8	10	12	MDPL06212Q
	16	18	MDPL06218Q
	6	8	MDPL07508Q
3/4	10	12	MDPL07512Q
	16	18	MDPL07518Q
	6	8	MDPL08708Q
7/8	10	12	MDPL08712Q
	16	18	MDPL08718Q
1	8	10	MDPL10010Q
ı	16	18	MDPL10018Q
41/	8	10	MDPL11210Q
11/8	16	18	MDPL11218Q
1 1/4	16	18	MDPL12518Q



Solid-tip carbide drill bit



Quad Head

# **SDS-PLUS** Drill Bits

# SDS-PLUS Shank Bits — Retail Packs

ODO-1 EOO OHAHR BITS — HETAIH LACKS				
Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Quantity (per pack)	Model No.
5/32	4	61/4	25	MDPL01506-R25
	2	41/4	25	MDPL01804-R25
	4	61/4	25	MDPL01806-R25
3/16	6	81/4	25	MDPL01808-R25
716	8	10	25	MDPL01810-R25
	10	12	25	MDPL01812-R25
	12	14	25	MDPL01814-R25
	4	61/4	25	MDPL02106-R25
7/32	6	81/4	25	MDPL02108-R25
	8¾	11	25	MDPL02111-R25
	2	41/4	25	MDPL02504-R25
1/4	4	61/4	25	MDPL02506-R25
74	6	81/4	25	MDPL02508-R25
	8¾	11	25	MDPL02511-R25
5/16	4	61/4	25	MDPL03106-R25
	4	61/4	25	MDPL03706-R25
3/8	8	101/4	25	MDPL03710-R25
	10	121/4	25	MDPL03712-R25
	4	61/4	25	MDPL05006-R25
1/2	8	101/4	25	MDPL05010-R25
	10	121/4	25	MDPL05012-R25
5/8	6	8	20	MDPL06208-R20



**SDS-PLUS Retail Packs** 



Stop Bit

# Fixed Depth Drill Bits

Model No	odel No Drill Bit Diameter   Drill Depth (In.)		Drop-In Anchor (in.)			
	Standard Drop-I	n Anchors				
MDPL037DIA	3/8	1 1/16	1/4			
MDPL050DIA	1/2	1 11/16	3/8			
MDPL062DIA	5/8	21/16	1/2			
	Short Drop-In Anchors					
MDPL050DIAS	1/2	1 11/16	3/8			
MDPL062DIAS	5/8	21/16	1/2			

# Titen® Screw Drill Bit/Driver Product Data

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	For Screw Dia. (in.)	Model No.
	23/8	5	3/16	MDPL01505H
5/32	31/8	6	3/16	MDPL01506H
	41/8	7	3/16	MDPL01507H
	23/8	5	1/4	MDPL01805H
3/16	31/8	6	1/4	MDPL01806H
	41/8	7	1/4	MDPL01807H
	41/8	,	1/4	MDPL01807H

Product is sold individually.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.



Special hex adaptor (included with the Titen® Screw installation kit) allows the Titen installation tool to slide over the bit and lock in, ready to drive Titen concrete and masonry screws. Rotohammer must be in rotation-only mode before driving screws.

# Titen Screw Drill Bit/Driver — Bulk Packs

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	For Screw Dia. (in.)	Model No.
5/	23/8	5	3/16	MDPL01505H-R25
5/32	41/8	7	3/16	MDPL01507H-R25
3/16	23/8	5	1/4	MDPL01805H-R25
716	41/8	7	1/4	MDPL01807H-R25

### Titen® Drill Bit/Driver — Bulk Packs of 25

Size (in.)	Drilling Depth (in.)	Overall Length (in.)	For Screw Dia. (in.)	Model No.
5⁄32 X 5	21/4	5	3/	MDBP15500HB
5⁄32 X 7	41/4	7	3/16	MDBP15700HB
3∕16 X 5	21/4	5	1/4	MDBP18500HB
3∕16 X 7	41/4	7	74	MDBP18700HB

# SIMPSON Strong-Tie

# SDS-PLUS and SDS-MAX Drill Bits

# SDS-MAX and SDS-MAX Quad Head Shank Bits

SDS-MAX and	SDS-MA	X Quad He	ad Shank Bits
Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Model No.
3/8	71/2	13	MDMX03713
1/2	71/2	13	MDMX05013
72	15½	21	MDMX05021
<sup>9</sup> / <sub>16</sub>	71/2	13	MDMX05613
716	15½	21	MDMX05621
	71/2	13	MDMX06213Q
5/8	151/2	21	MDMX06221Q
	301/2	36	MDMX06236Q
11/16	15½	21	MDMX06821Q
	8	13	MDMX07513Q
3/4	17	21	MDMX07521Q
	31	36	MDMX07536Q
13/16	17	21	MDMX08121Q
	8	13	MDMX08713Q
7/8	17	21	MDMX08721Q
	31	36	MDMX08737Q
	8	13	MDMX10013Q
1	17	21	MDMX10021Q
	31	36	MDMX10036Q
1 1/16	18	23	MDMX10623Q
	12	17	MDMX11217Q
1 1/8	17	21	MDMX11221Q
	31	36	MDMX11236Q
13/16	18	23	MDMX11823Q
	10	15	MDMX12515Q
1 1/4	18	23	MDMX12523Q
	31	36	MDMX12536Q
13/8	12	17	MDMX13717Q
1 7/8	18	23	MDMX13723Q
1 ½	18	23	MDMX15023Q
13/4	18	23	MDMX17523Q
2	18	23	MDMX20023Q
Managed and an arranged to the second			1

Model numbers ending with "Q" denote Quad Head.



Quad Head
Model numbers ending with
"Q" denote Quad Head bits.



SDS-MAX Shank Bit

# SIMPSON Strong-Tie

# Spline Shank Bits

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Model No.
	5	10	MDSP03710
3/8	8	13	MDSP03713
	11	16	MDSP03716
7/16	8	13	MDSP04313
	5	10	MDSP05010
	8	13	MDSP05013
	11	16	MDSP05016
1/2	17	22	MDSP05022
	24	29	MDSP05029
	31	36	MDSP05036
	8	13	MDSP05613
9/16	11	16	MDSP05616
	18	23	MDSP05623
	5	10	MDSP06210
	8	13	MDSP06213
F.	11	16	MDSP06216
5/8	17	22	MDSP06222
	24	29	MDSP06229
	31	36	MDSP06236
11/	8	13	MDSP06813
11/16	11	16	MDSP06816
	5	10	MDSP07510
	8	13	MDSP07513
3/4	11	16	MDSP07516
94	17	22	MDSP07522
	24	29	MDSP07529
	31	36	MDSP07536
	11	16	MDSP08716
7/8	17	22	MDSP08722
	31	36	MDSP08736
	11	16	MDSP10016
1	17	22	MDSP10022
	31	36	MDSP10036
11/8	11	16	MDSP11216
1 /0	17	22	MDSP11222
11/4	11	16	MDSP12516
1 /4	17	22	MDSP12522
13/8	11	16	MDSP13716
. , 5	17	22	MDSP13722
11/2	11	16	MDSP15016
	17	22	MDSP15022
13/4	17	22	MDSP17522
2	17	22	MDSP20022



Spline shank bits continued on the next page.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# Spline/Straight Shank Drill Bits

# SIMPSON StrongTie

# Spline Shank Quad Head Bits

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Model No.
	5	10	MDSP06210Q
	11	16	MDSP06216Q
5/8	17	22	MDSP06222Q
	24	29	MDSP06229Q
	31	36	MDSP06236Q
11/16	11	16	MDSP06816Q
	5	10	MDSP07510Q
	11	16	MDSP07516Q
3/4	17	22	MDSP07522Q
	24	29	MDSP07529Q
	31	36	MDSP07536Q
7/	11	16	MDSP08716Q
7/8	17	22	MDSP08722Q
	11	16	MDSP10016Q
1	17	22	MDSP10022Q
	31	36	MDSP10036Q
11/8	11	16	MDSP11216Q
I 78	17	22	MDSP11222Q
	11	16	MDSP12516Q
1 1/4	17	22	MDSP12522Q
	31	36	MDSP12536Q
13/8	11	16	MDSP13716Q
1 78	17	22	MDSP13722Q
1½	17	22	MDSP15022Q
13⁄4	18	23	MDSP17523Q
2	18	23	MDSP20023Q



Spline Shank Bit

# 'A' Taper Shank Bits

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Model No.
1/2	7	9	MDA05007
5/8	7	9	MDA06207
3/4	16	18	MDA07516



**Quad Head** 



'A' Taper Bit

# Spline/Straight Shank Drill Bits

# SIMPSON Strong-Tie

# Straight Shank Bits

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Model No.
1/8	13/8	3	MDB01203
3/16	1 %16	31/2	MDB01803
916	4	6	MDB01806
	21/8	4	MDB02504
1/4	4	6	MDB02506
	10	12	MDB02512
5/16	23/4	43/4	MDB03104
716	4	6	MDB03106
3/8	4	6	MDB03706
9/8	10	12	MDB03712
7/16	4	6	MDB04306
	4	6	MDB05006
1/2	10	12	MDB05012
	22	24	MDB05024
	31/2	6	MDB06206
5/8	10	12	MDB06212
	22	24	MDB06224
3/	4	6	MDB07506
3/4	10	12	MDB07512
7/8	4	6	MDB08706
'/8	10	12	MDB08712
1	4	6	MDB10006
ı	10	12	MDB10012

Bits have recessed shank to fit Titen® screws and other masonry screw installation tools. They also work in three-jaw-style chucks.



Straight Shank Bit

# Straight Shank Bits - Retail Packs

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Quantity (per pack)	Model No.
1/8	1%	3	25	MDB01203-R25
3/	1 %16	31/2	25	MDB01803-R25
3/16	4	6	25	MDB01806-R25
1/	21/8	4	25	MDB02504-R25
1/4	4	6	25	MDB02506-R25
5/	23/4	43/4	25	MDB03104-R25
5/16	4	6	25	MDB03106-R25
3/8	4	6	25	MDB03706-R25
1/2	4	6	25	MDB05006-R25
5/8	4	6	20	MDB06206-R20



# **Rebar Cutters/Adaptors**

# Rebar Cutters\*\*

When hole placement conflicts with rebar or wire mesh, these bits enable the rebar to be removed so the hole can be drilled to the proper depth. Rebar cutters are separate from shanks. Shanks work with all sizes of rebar cutters. Overall length is approximately 15".

\*\* After drilling through the reinforcement or plate, remove debris from the hole and resume drilling with carbide tipped drill bit.

Dia. (in.)	Drilling Depth (in.)	Model No.
1/2	12	MCR05012
5/8	12	MCR06212
3/4	12	MCR07512
7/8	12	MCR08712
1	12	MCR10012

#### Plate Cutters\*\*

Similar to rebar cutters, these bits are designed for cutting through steel base plates when it is necessary to enlarge the fixture hole. These bits can also be used as rebar cutters. Plate cutters are separate from shanks. Shanks work with all sizes of plate cutters.

\*\* After drilling through the reinforcement or plate, remove debris from the hole and resume drilling with carbide-tipped drill bit.

Dia. (in.)	Drilling Depth (in.)	Model No.
1/2	12	MCP05012
5%	12	MCP06212
3/4	12	MCP07512
7/8	12	MCP08712
1	12	MCP10012

#### Shanks for Rebar and Plate Cutters

Shank Style	Model No.	Description
Straight	MC	For use in drills with jawed chucks. Use in rotation mode only.
SDS-PLUS	MCSDP	For use in SDS-PLUS style drills. Use in rotation mode only.
SDS-MAX	MCSDM	For use in SDS-MAX style drills. Shank design allows rotation only.
Spline	MCS	For use in spline-style drills. Shank design allows rotation only.



**Rebar Cutter Detail** 

#### **Rebar Cutter**





**Plate Cutter Detail** 





SDS-PLUS Shank



Spline Shank

# **Rebar Cutters/Adaptors**



Drill Bit Shank Adaptors

Description (shank style to bit type)	Model No.
SDS-MAX to SDS-PLUS Adaptor	ADMX2PL
Spline to SDS-PLUS Adaptor	ADSP2PL
SDS-top to SDS-PLUS Adaptor	ADST2PL



# **Demolition Chisels and Bits**

Strong-Tie

Simpson Strong-Tie® chisels are made of toughened steel with special surface treatment that improves performance. The superior tempering process creates a hardened surface that is more wear resistant and allows the working point to be re-sharpened, which extends the life of the tool.

Simpson Strong-Tie® demolition chisels and bits come in various shank styles to fit virtually any demolition tool.



SDS-MAX



**SDS-PLUS** 



**Spline** (Design disables rotohammer rotation.)



3/4" Hex

# **Scrapers**

Removing Tiles, Flooring and Other Materials

Shank Type	Head Width (in.)	Overall Length (in.)	Model No.
SDS-PLUS	3/4	10	CHPLF07510
3D3-FLU3	1 ½	10	CHPLSC15010
SDS-MAX	2	12	CHMXSCP20012
Spline	2	12	CHSPSCP20012



Scraper

# Flat Chisels General Concrete and Masonry Demolition

Shank Type	Head Width (in.)	Overall Length (in.)	Model No.
SDS-MAX	1	12	CHMXF10012
2D2-IVIAX	1	18	CHMXF10018
Calina	1	12	CHSPF10012
Spline	1	18	CHSPF10018
2/11.11	1	12	CHHF10012
3/4" Hex	1	18	CHHF10018



Flat Chisel

# **Demolition Chisels and Bits**

# Strong-Tie

### **Bull Point Chisels**

General Concrete and Masonry Demolition

Shank Type	Overall Length (in.)	Model No.
SDS-PLUS	10	CHPLBP10
CDC MAY	12	CHMXBP12
SDS-MAX	18	CHMXBP18
Spline	12	CHSPBP12
	18	CHSPBP18
3⁄4" Hex	12	CHHBP12
	18	CHHBP18



# **Asphalt Cutters**

Asphalt, Hardpan and Compacted Soil Cutting

Shank Type	Head Width (in.)	Overall Length (in.)	Model No.
SDS-MAX	31/2	16	CHMXAC35016
3/4" Hex	31/2	16	CHHAC35016



**Asphalt** Cutter

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

**Clay Spades**Clay and Other Rock-Free Soil Cutting

Shank Type	Head Width (in.)	Overall Length (in.)	Model No.
Spline	5%	16	CHSPCS53716
Clay Spade	5%	16	CHHCS53716



Clay Spade

# **Demolition Bits**

# Strong-Tie

### **Scalers**

Removing Large Quantities of Material

Shank Type	Head Width (in.)	Overall Length (in.)	Model No.
	1 ½	12	CHMXSC15012
SDS-MAX	2	12	CHMXSC20012
	3	12	CHMXSC30012
	1 ½	12	CHSPSC15012
Spline	2	12	CHSPSC20012
	3	12	CHSPSC30012
9/11.11	2	12	CHHSC20012
3⁄4" Hex	3	12	CHHSC30012



Scaler

# **Ground Rod Drivers**

Driving in Ground Rods

Shank Type	Head Width (in.)	Overall Length (in.)	Model No.
SDS-MAX	7/8	101/4	CHMXRD08710
Spline	7/8	101/4	CHSPRD08710



**Ground Rod** Driver

Bushing Tools One Piece Concrete and Asphalt Surface Roughening

Shank Type	Head Width (in.)	Overall Length (in.)	Model No.
SDS-MAX	13/4	91/2	CHMXBT17509
Spline	13⁄4	91/4	CHSPBT17509
Bushing Tool	13/4	91/4	CHHBT17509



**Bushing Tool** Head

# **Core Bits**

# SIMPSON Strong-Tie

### Core Bits

Simpson Strong-Tie® Core Bits are made to the same exacting standards as our standard carbide-tipped drill bits. They utilize a centering bit to facilitate accurate drilling in combination hammer/drill mode.

# One-Piece Core Bits with Centering Bit – SDS-MAX Shank

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Model No.
1½	61/4	11%	CBMX15011
1 72	0 74	22	CBMX15022
2	61/4	11%	CBMX20011
2	0 1/4	22	CBMX20022
05/	01/	11%	CBMX26211
2%	61/4	22	CBMX26222
01/	0.17	11%	CBMX31211
31/8	61/4	22	CBMX31222
31/2	61/4	22	CBMX35022
4	01/	11%	CBMX40011
4	4 61/4	22	CBMX40022
5	5 04/	11%	CBMX50011
Э	61/4	22	CBMX50022
6	61/4	22	CBMX60022

NOTE: With 1-piece bits, once coring is begun, the centering bit must be removed using ejector pin. Core bit bodies are  $2^{11/16}$ " deep.

# One-Piece Core Bits with Centering Bit – Spline Shank

Dia. (in.)	Drilling Depth (in.)	Overall Length (in.)	Model No.
11/2	61/4	11%	CBSP15012
1 1/2	0 74	22	CBSP15022
2	61/4	11%	CBSP20011
	0 74	22	CBSP20022
25/8	61/4	11%	CBSP26211
2%8	0 74	22	CBSP26222
31/8	61/4	11%	CBSP31211
3 78	0 74	22	CBSP31222
31/2	61/4	11%	CBSP35011
3 1/2	0 74	22	CBSP35022
4	61/	11%	CBSP40011
4	4 61/4	22	CBSP40022
5	61/.	11%	CBSP50011
3	5 61/4	22	CBSP50022



One-piece core bit transfers energy efficiently

## Core Bit Replacement Parts

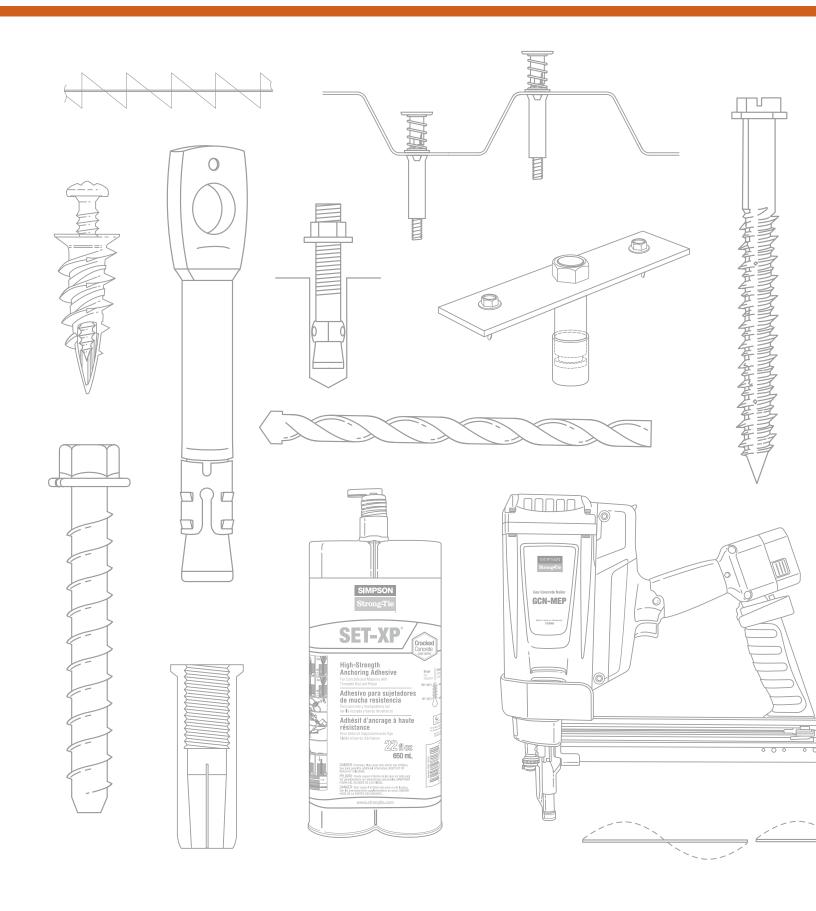
Core Bit Center Pilot Bit

Dia. (in.)	Overall Length (in.)	Model No.
7/16	43/4	CTRBTF04304

# Ejector Key

Dia.	Model
(in.)	No.
3/8	CDBEJKEY

# Appendix - Supplemental Topics





# To keep you as informed as possible, the following topics are included in this Appendix:

Page
316
316
316
318
318
322
322
323
324









# I. Base Materials

"Base material" is a generic industry term that refers to the element or substrate to be anchored to. Base materials include concrete, brick, concrete block (CMU) and structural tile, to name a few. The most common type of base material where adhesive and mechanical anchors are used is concrete.

Concrete – Concrete can be cast-in-place or precast concrete. Concrete has excellent compressive strength, but relatively low tensile strength. Cast-in-place (or sometimes called "poured in place") concrete is placed in forms erected on the building site. Cast-in-place concrete can be either normal-weight or lightweight concrete. Lightweight concrete is often specified when it is desirable to reduce the weight of the building structure.

Lightweight concrete differs from normal-weight concrete by the weight of aggregate used in the mixture. Normal-weight concrete has a unit weight of approximately 150 pounds per cubic foot compared to approximately 115 pounds per cubic foot for lightweight concrete.

The type of aggregate used in concrete can affect the tension capacity of an adhesive anchor. Presently, the relationship between aggregate properties and anchor performance is not well understood. Test results should not be assumed to be representative of expected performance in all types of concrete aggregate.

Prefabricated concrete is also referred to as "precast concrete". Precast concrete can be made at a prefabricating plant or site-cast in forms constructed on the job. Precast concrete members may be solid or may contain hollow cores. Many precast components have thinner cross sections than cast in place concrete. Precast concrete may use either normal or lightweight concrete. Reinforced concrete contains steel bars, cable, wire mesh or random glass fibers. The addition of reinforcing material enables concrete to resist tensile stresses which lead to cracking.

The compressive strength of concrete can range from 2,000 psi to over 20,000 psi, depending on the mixture and how it is cured. Most concrete mixes are designed to obtain the desired properties within 28 days after being cast.

Concrete Masonry Units (CMU) – Block is typically formed with large hollow cores. Block with a minimum 75% solid cross section is called solid block even though it contains hollow cores. In many parts of the country building codes require steel reinforcing bars to be placed in the hollow cores, and the cores to be filled solid with grout.

In some areas of the eastern United States, past practice was to mix concrete with coal cinders to make cinder blocks. Although cinder blocks are no longer made, there are many existing buildings where they can be found. Cinder blocks require special attention as they soften with age.

Brick – Clay brick is formed solid or with hollow cores. The use of either type will vary in different parts of the United States. Brick can be difficult to drill and anchor into. Most brick is hard and brittle. Old, red clay brick is often very soft and is easily over-drilled. Either of these situations can cause problems in drilling and anchoring. The most common use of brick today is for building facades (curtain wall or brick veneer) and not for structural applications. Brick facade is attached to the structure by the use of brick ties spaced at intervals throughout the wall. In older buildings, multiple widths, or "wythes" of solid brick were used to form the structural walls. Three and four wythe walls were common wall thicknesses.

Clay Tile – Clay tile block is formed with hollow cores and narrow cavity wall cross sections. Clay tile is very brittle, making drilling difficult without breaking the block. Caution must be used in attempting to drill and fasten into clay tile.

# II. Anchor Failure Modes

Four different tension failure modes and three different shear failure modes are generally observed for post-installed anchors under tension loading.

#### Failure Modes

Tension	Shear
Steel Fracture Breakout Pullout (Mech. Anch.) Bond Failure (Adhesive Anch.)	Steel Fracture Breakout Pryout

Breakout Failure – Breakout failure occurs when the base material ruptures, often producing a cone-shaped failure surface when anchors are located away from edges, or producing a spall when anchors are located near edges. Breakout failure can occur for both mechanical and adhesive anchors and is generally observed at shallower embedment depths, and for installations at less than critical spacings or edge distances.

**Pullout Failure** – Pullout failure occurs when a mechanical anchor pulls out of the drilled hole, leaving the base material otherwise largely intact.

Bond Failure – Bond failure occurs when an adhesive anchor pulls out of the drilled hole due to an adhesion failure at the adhesive-to-base-material interface, or when there is a cohesive failure within the adhesive itself. When bond failure occurs, a shallow cone-shaped breakout failure surface will often form near the base material surface. This breakout surface is not the primary failure mechanism.

**Pryout Failure** – Pryout failure occurs for shallowly embedded anchors when a base material failure surface is pried out "behind" the anchor, opposite the direction of the applied shear force.

Steel Fracture – Steel fracture occurs when anchor spacings, edge distances and embedment depths are great enough to prevent the base-material-related failure modes listed above and the steel strength of the mechanical anchor or adhesive anchor insert is the limiting strength.

# III. Corrosion Resistance

Many environments and materials can cause corrosion, including ocean salt air, fire-retardants, fumes, fertilizers, preservative-treated wood, de-icing salts, dissimilar metals and more. Metal fixtures, fasteners and anchors can corrode and lose load-carrying capacity when installed in corrosive environments or when installed in contact with corrosive materials.

The many variables present in a building environment make it impossible to accurately predict if, or when, corrosion will begin or reach a critical level. This relative uncertainty makes it crucial that specifiers and users are knowledgeable about the potential risks and select a product suitable for the intended use. It is also prudent that regular maintenance and periodic inspections are performed, especially for outdoor applications.

It is common to see some corrosion in outdoor applications. Even stainless steel can corrode. The presence of some corrosion does not mean that load capacity has been affected or that failure is imminent. If significant corrosion is apparent or suspected, then the fixtures, fasteners and connectors should be inspected by a qualified engineer or qualified inspector. Replacement of affected components may be appropriate.

**Chemical Attack** - Chemical attack occurs when the anchor material is not resistant to a substance with which it is in contact. Chemical-resistance information regarding anchoring adhesives is found on page 320.

# Simpson Strong-Tie® Anchoring and Fastening Systems for Concrete and Masonry

Some wood-preservative chemicals and fire-retardant chemicals and retentions pose increased corrosion potential and are more corrosive to steel anchors and fasteners than others. Additional information on this subject is available at www.strongtie.com.

We have attempted to provide basic knowledge on the subject of corrosion here, but it is important to fully educate yourself by reviewing our technical bulletins on the topic (www.strongtie.com/info) and also by reviewing information, literature and evaluation reports published by others.

Galvanic Corrosion - Galvanic corrosion occurs when two electrochemically dissimilar metals contact each other in the presence of an electrolyte (such as water) that acts as a conductive path for metal ions to move from the more anodic to the more cathodic metal. In the galvanic couple, the more anodic metal will corrode preferentially. The Galvanic Series of Metals table provides a qualitative guide to the potential for two metals to interact galvanically. Metals in the same group (see table) have similar electrochemical potentials. The farther the metals are apart on the table, the greater the difference in electrochemical potential, and the more rapidly galvanic corrosion will occur. Corrosion also increases with increasing conductivity of the electrolyte.

Good detailing practice, including the following, can help reduce the possibility of galvanic corrosion of anchors:

- Use of anchors and metals with similar electrochemical potentials
- · Separating dissimilar metals with insulating materials
- Ensuring that the anchor is the cathode, when dissimilar materials are present.
- Preventing exposure to and pooling of electrolytes

#### Galvanic Series of Metals

Corroded End (Anode)
Magnesium Magnesium alloys Zinc
Aluminum 1100 Cadmium Aluminum 2024-T4 Iron and Steel
Lead Tin Nickel (active) Inconel Ni-Cr alloy (active) Hastelloy alloy C (active)
Brasses Copper Cu-Ni alloys Monel
Nickel (passive)
304 stainless steel (passive) 316 stainless steel (passive) Hasteloy alloy C (passive)
Silver Titanium Graphite Gold Platinum
Protected End (Cathode)

#### Hydrogen-Assisted Stress-Corrosion Cracking

Some hardened fasteners may experience premature failure if exposed to moisture as a result of hydrogen-assisted stress-corrosion cracking. These fasteners are recommended specifically for use in dry, interior locations.

#### **Guidelines for Selecting Corrosion-Resistant Anchors and Fasteners**

#### **Evaluate the Application**

Consider the importance of the connection.

#### Evaluate the Exposure

Consider these moisture and treatment chemical exposure conditions:

- Dry Service: Generally INTERIOR applications and includes wall and ceiling cavities, raised floor applications in enclosed buildings that have been designed to prevent condensation and exposure to other sources of moisture. Prolonged exposure during construction should also be considered, as this may constitute a Wet Service or Elevated Service Condition.
- Wet Service: Generally EXTERIOR construction in conditions other than Elevated Service. These include Exterior Protected and Exposed and General Use Ground Contact as described by the AWPA UC4A.
- Elevated Service: Includes fumes, fertilizers, soil, some preservativetreated wood (AWPA UC4B and UC4C), industrial zones, acid rain and other corrosive elements.
- Uncertain: Unknown exposure, materials or treatment chemicals.
- Ocean/Water Front: Marine environments that include airborne chlorides and some splash. Environments with de-icing salts are included.
- Treatment Chemicals: See AWPA Use Category Designations. The preservative-treated wood supplier should provide all of the pertinent information about the wood being used. The information should include Use Category Designation, wood species group, wood treatment chemical and chemical retention. See appropriate evaluation reports for corrosion effects of treatment chemicals and fastener corrosion resistance recommendations.

## Use the Simpson Strong-Tie® Corrosion Classification Table

If the treatment chemical information is incomplete, Simpson Strong-Tie recommends the use of a 300-series stainlesssteel product. Also if the treatment chemical is not shown in the Corrosion Classification Table, then Simpson Strong-Tie has not evaluated it and cannot make any recommendations other than the use of coatings and materials in the Severe category. Manufacturers may independently provide test results of other product information; Simpson Strong-Tie expresses no opinion regarding such information.

#### Minimum Corrosion Resistance Recommendations

Corrosion Resistance Classification	Material or Coating	
Low	Zinc plated	
	Mechanically galvanized (ASTM B695-Class 55) <sup>1</sup>	
Medium	Hot-dip galvanized (ASTM A153-Class C)	
	Type 410 stainless steel with protective top coat	
High	Type 302, 303 or 304 stainless steel	
Severe	Type 316 stainless steel	
Severe	Hot-dip galvanized	

1. Mechanically galvanized Titen HD® anchors are recommended only for temporary outdoor service.

**Appendix** 



Corrosion Resistance Classifications

			Mate	rial To Be Fastened			
Environment	Untreated	Preservative-Treated Wood					
Environment	Wood or Other Material	SBX-DOT Zinc Borate	Chemical Retention ≤ AWPA, UC4A	Chemical Retention > AWPA, UC4A	ACZA	Other or Uncertain	FRT Wood
Dry Service	Low	Low	Low	High	High	High	Med
Wet Service	Med	N/A	Med	High	High	High	High
Elevated Service	High	N/A	Severe	Severe	High	Severe	N/A
Uncertain	High	High	High	Severe	High	Severe	High
Ocean/Waterfront	Severe	N/A	Severe	Severe	Severe	Severe	N/A

- These are general guidelines that may not consider all application criteria. Refer to product-specific information for additional guidance.
- Type 316/305/304 stainless-steel products are recommended where preservative-treated wood used in ground contact has chemical retention level greater than those for AWPA UC4A; CA-C, 0.15 pcf; CA-B, 0.21 pcf; micronized CA-C, 0.14 pcf; micronized CA-B, 0.15 pcf; ACQ-Type D (or C), 0.40 pcf.
- 3. Testing by Simpson Strong-Tie following ICC-ES AC257 showed that mechanical galvanization (ASTM B695, Class 55), Quik Guard coating, and Double Barrier coating will provide corrosion resistance equivalent to hot-dip galvanization (ASTM A153, Class D) in contact with chemically treated wood in dry service and wet service exposures (AWPA UC1 UC4A, ICC-ES AC257 Exposure Conditions 1 and 3) and will perform adequately subject to regular maintenance and periodic inspection.
- Mechanical galvanizations C3 and N2000 should not be used in conditions that would be more corrosive than AWPA UC3A (exterior, above ground, rapid water run off).
- 5. If uncertain about Use Category, treatment chemical, or environment, use Types 316/305/304 stainless steel, silicon bronze or copper fasteners.
- 6. Some treated wood may have excess surface chemicals making it potentially more corrosive than lower retentions. If this condition is suspected, use Types 316/305/304 stainless steel, silicon bronze or copper fasteners.
- 7. Types 316/305/304 stainless steel, silicon bronze or copper fasteners are the best recommendation for ocean salt-air and other chloride-containing environments. Hot-dip galvanized fasteners with at least ASTM A153, Class C protection can also be an alternate for some applications in environments with ocean air and/or elevated wood moisture content.

# IV. Mechanical Anchors

#### **Pre-Load Relaxation**

Expansion anchors that have been set to the required installation torque in concrete will experience a reduction in pre-tension (due to torque) within several hours. This is known as pre-load relaxation. The high compression stresses placed on the concrete cause it to deform which results in a relaxation of the pre-tension force in the anchor. Tension in this context refers to the internal stresses induced in the anchor as a result of applied torque and does not refer to anchor capacity. Historical data shows it is normal for the initial tension values to decrease by as much as 40–60% within the first few hours after installation. Retorquing the anchor to the initial installation torque is not recommended or necessary.

# V. Adhesive Anchors

#### Installation into Green Concrete

The strength design data for adhesive anchors in this catalog are based on installations into concrete that is at least 21 days old. Anchors may be installed in concrete less than 21 days old, provided a reduction factor is applied to bond strength:

Products	Concrete Age When Installed	Concrete Age When Loaded	Bond Strength Factor
ΛT	1.4 daya	21 days	1.0
AT-XP		7 days	0.9
ET-HP SET SET-XP	7 daya	21 days	1.0
SEI-AF	7 days	7 days	0.7

#### **Oversized Holes**

The performance data for adhesive anchors are based upon anchor tests in which holes were drilled with carbide-tipped drill bits of the same diameter listed in the product's load table. Additional static tension tests were conducted to qualify anchors installed with SET, SET-XP®, ET-HP® and AT adhesives for installation in holes with diameters larger than those listed in the load tables. The tables indicate the acceptable range of drilled hole sizes and the corresponding tension-load reduction factor (if any). The same conclusions also apply to the published shear load values. Drilled holes outside of the accepted range shown in the charts are not recommended.

#### SET Adhesive – Acceptable Hole Diameter

Insert Diameter (in.)	Acceptable Hole Diameter Range (in.)	Acceptable Load Reduction Factor
3/8	1/2 - 3/4	1.0
1/2	5/8 - 1 5/16	1.0
5/8	3/4 - 11/8	1.0
3/4	7/8 — 1 5/ <sub>16</sub>	1.0
7/8	1 – 1 ½	1.0
1	1 1/8 - 1 11/16	1.0
1 1/8	11/4 - 17/8	1.0
1 1/4	13/8 - 21/16	1.0
1 %	11/2 - 21/4	1.0

#### SET-XP and ET-HP Adhesives – Acceptable Hole Diameter

Insert Diameter (in.)	Acceptable Hole Diameter Range (in.)	Acceptable Load Reduction Factor
1/2	5/8 — 3/4	1.0
5/8	<sup>3</sup> / <sub>4</sub> - <sup>15</sup> / <sub>16</sub>	1.0
3/4	<sup>7</sup> / <sub>8</sub> − 1 ½	1.0
7/8	1 - 15/16	1.0
1	11/8 - 11/2	1.0
1 1/4	1% - 1%	1.0



## AT Adhesive - Acceptable Hole Diameter

Insert Diameter (in.)	Acceptable Hole Diameter Range (in.)	Acceptable Load Reduction Factor
3/8	7/16 - 1/2	1.0
1/2	9∕ <sub>16</sub> − 5⁄ <sub>8</sub>	1.0
5/8	11/16 - 3/4	1.0
3/4	<sup>13</sup> / <sub>16</sub> — <sup>7</sup> / <sub>8</sub>	1.0
7/8	1	1.0
1	11/16 - 11/8	.75 for 1 1/8 only

#### Core-Drilled Holes

The performance data for adhesive anchors are based upon anchor tests in which holes were drilled with carbide-tipped drill bits. Additional static tension tests were conducted to qualify anchors installed with SET and AT anchoring adhesives for installation in holes drilled with diamond-core bits. In these tests, the diameter of the diamond-core bit matched the diameter of the carbide-tipped drill bit recommended in the product's load table. The test results showed that no reduction of the published allowable tension load for SET and AT anchoring adhesives is necessary for this condition. The same conclusions also apply to the published allowable shear loads.

# Installation in Damp, Wet and Submerged Environments

SET-XP, ET-HP and AT-XP: The performance data for adhesive anchors using SET-XP, ET-HP and AT-XP adhesives are based upon tests according to ICC-ES AC308. This criteria requires adhesive anchors that are to be installed in outdoor environments to be tested in water-saturated concrete holes that have been cleaned with less than the amount of hole cleaning recommended by the manufacturer. A product's sensitivity to this installation condition is considered in determining the product's "Anchor Category" (strength reduction factor). SET-XP, ET-HP and AT-XP may be installed in dry or water-saturated concrete.

#### Based on Reliability Testing per ICC-ES AC308

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

- Dry Concrete Cured concrete whose moisture content is in equilibrium with surrounding non-precipitate atmospheric conditions.
- Water-Saturated Concrete Cured concrete that is covered with water and water saturated.
- Submerged Concrete Cured concrete that is covered with water and water saturated.
- Water-Filled Hole Drilled hole in water-saturated concrete that is clean yet contains standing water at the time of installation.

SET, EDOT and AT: The performance data for adhesive anchors using SET, EDOT and AT adhesives are based upon tests in which anchors are installed in dry holes. Additional static tension tests were conducted for some products in damp holes, water-filled holes and submerged holes. The test results show that no reduction of the published allowable tension load is necessary for SET, EDOT and AT adhesives in damp holes, or for SET and AT adhesives in water-filled holes. For SET and AT adhesives in submerged holes, the test results show that a reduction factor of 0.60 is applicable. The same conclusions also apply to the published allowable shear load values.

#### Based on Reliability Testing per ICC-ES AC58

- Dry Concrete Cured concrete whose moisture content is in equilibrium with surrounding non-precipitate atmospheric conditions.
- Damp Hole A damp hole, as defined in ASTM E1512 and

- referenced in ICC-ES AC58, is a drilled hole that has been properly drilled, cleaned and then is filled with standing water for seven days. After seven days, the standing water is blown out of the hole with compressed air and the adhesive anchor is installed.
- Water-Filled Hole A water-filled hole is defined similarly to a damp hole; however, the standing water is not blown out of the hole. Instead, the adhesive is injected directly into the water-filled hole (from the bottom of the hole up) and the insert is installed.
- Submerged Hole A submerged hole is similar to a water-filled hole with one major exception – in addition to standing water within the hole, water also completely covers the surface of the base material. Note that drilling debris and sludge should be removed from the drilled hole prior to installation. ICC-ES AC58 does not address this condition.

#### **Elevated In-Service Temperature**

The performance of all adhesive anchors is affected by elevated base material temperature. The in-service temperature sensitivity table provided for each adhesive provides the information necessary to apply the appropriate load adjustment factor to either the allowable tension based on bond strength or allowable shear based on concrete edge distance for a given base material temperature. While there is no commonly used method to determine the exact load-adjustment factor, there are a few guidelines to keep in mind when designing an anchor that will be subject to elevated base-material temperature. In any case, the final decision must be made by a qualified design professional using sound engineering judgment:

- When designing an anchor connection to resist wind and/or seismic forces only, the effect of fire (elevated temperature) may be disregarded.
- The base-material temperature represents the average internal temperature and, hence, the temperature along the entire bonded length of the anchor.
- The effects of elevated temperature may be temporary. If the inservice temperature of the base material is elevated such that a load-adjustment factor is applicable but, over time, the temperature is reduced to a temperature below which a load-adjustment factor is applicable, the full allowable load based on bond strength is still applicable. This is applicable provided that the degradation temperature of the anchoring adhesive (350°F for SET-XP®, SET, ET-HP®, AT-XP® and AT adhesives) has not been reached.

#### Creep Under Long-Term Loads

Creep is the slow, continuous deformation of a material under constant stress. Creep occurs in many construction materials, including concrete and steel when the stress is great enough. The creep characteristics of adhesives are product-dependent. Adhesive anchors that are not creep-resistant can pull out slowly over time when sustained tensile loads are applied.

Because of the creep phenomenon, it is important for Designers to consider the nature of the applied tension loads and to determine whether the tension loads will be continuously applied to the anchor over the long term. If this is the case, a product that is suitable for resisting sustained loads over the long term must be selected.

All Simpson Strong-Tie® anchoring adhesives (SET-XP, SET, ET-HP, EDOT, AT-XP and AT) have been qualified for resisting long-term loads through ICC-ES AC58 or ICC-ES AC308 "creep tests" in which an anchor is loaded and monitored for movement over time. According to AC58 and AC308, anchors that pass the creep test are determined to be suitable for resisting long-term tensile loads.



#### **Chemical Resistance of Adhesive Anchors**

Samples of Simpson Strong-Tie® anchoring adhesives were immersed in the chemicals shown below until they exhibited minimal weight change (indicating saturation) or for a maximum of three months. The samples were then tested according to ASTM D 543 Standard Practices for Evaluating the Resistance of Plastics to Chemical Changes, Procedures I & II, and either ASTM D 790 Standard Test Method for Flexural Properties of Unreinforced and Reinforced Plastics and Electrical Insulating Materials or ASTM D 695 Standard Test Method for Compressive Properties of Rigid Plastics. In cases where mild chemicals were evaluated, the exposure was accelerated per ASTM D 3045 Standard Practice for Heat Aging of Plastics Without Load.

Samples showing no visible damage and demonstrating statistically equivalent strength and elastic modulus as compared to control samples were classified as "Resistant" (R). These adhesives are considered suitable for continuous exposure to the identified chemical when used as a part of an adhesive anchor assembly.

Samples exhibiting slight damage, such as swelling or crazing, or not demonstrating both statistically equivalent strength and elastic modulus as compared to control samples were classified as "Non-Resistant" (NR). These adhesives are considered suitable for periodic exposure to the identified chemical if the chemical will be diluted and washed away from the adhesive anchor assembly after exposure, or if only emergency contact with the chemical is expected and subsequent replacement of the anchor would be undertaken. Some manufacturers refer to this as "limited resistance" or "partial resistance" in their literature.

Samples that were completely destroyed by the chemical, or that demonstrated a significant loss in strength after exposure were classified as "Failed" (F). These adhesives are considered unsuitable for exposure to the identified chemical.

Note: In most actual service conditions, the majority of the anchoring adhesive is not exposed to the chemical and thus some period of time is required for the chemical to saturate the entire adhesive. An adhesive anchor would be expected to maintain bond strength and creep resistance until a significant portion of the adhesive is saturated.

Chemical	Concentration	AT-XP	SET-XP	ET-HP	AT	SET
	Glacial	NR	F	F	F	F
Acetic Acid	5%	R	F	F	R	F
Acetone	100%	F	F	F	_	
Aluminum Ammonium	10070	'	'	'		
Sulfate (Ammonium Alum)	10%	R	R	R	R	R
Aluminum Chloride	10%	R	R	R	_	_
Aluminum Potassium Sulfate (Potassium Alum)	10%	R	R	R	R	R
Aluminum Sulfate (Alum)	15%	R	R	R	R	R
Ammonium Hydroxide	28%	NR	R	NR	R	R
(Ammonia)	10%	R	R	R	R	R
` ′	pH=10	R	R	R	_	_
Ammonium Nitrate	15%	R	R	R	R	R
Ammonium Sulfate	15%	R	R	R	R	R
Automotive Antifreeze	50%	R	R	R		
Aviation Fuel (JP5)	100%	R	R	R		
Brake Fluid (DOT3)	100%	R	NR	F	_	_
Calcium Hydroxide	10%	R	R	R	_	_
Calcium Hypochlorite (Chlorinated Lime)	15%	R	R	R	R	R
Calcium Oxide (Lime)	5%	R	R	R	R	R
Carbolic Acid	10%	NR	F	F	_	_
oarbone Acid	5%	NR	F	F	_	_
Carbon Tetrachloride	100%	R	R	R	_	_
Chromic Acid	40%	R	NR	NR	_	_
Citric Acid	10%	R	R	R	_	_
Copper Sulfate	10%	R	R	R	_	_
Detergent (ASTM D543)	100%	R	R	R	_	_
Diesel Oil	100%	R	R	NR	_	_
Ethanol, Aqueous	95%	NR	F	F	_	
	50%	NR	NR	NR	_	_
Ethanol, Denatured	100%	R	F	F	_	_
Ethylene Glycol	100%	R	R	R		
Fluorosilicic Acid	25%	R	R	R	R	R
Formic Acid	Concentrated	F	F	F		
	10%	R	F	F		_
Gasoline	100%	R	R	R		_
	Concentrated	NR -	F	F	R	F
Hydrochloric Acid	10%	R	NR	F	R	NR
	pH=3	R	R	R	_	_
Hydrogen Peroxide	30%	R R	F R	F R	R	F
Iron (II) Chloride	3% 15%	R	R	R	R R	NR R
(Ferrous Chloride)  Iron (III) Chloride	15%	R	R	R	R	NR
(Ferric Chloride)  Iron (III) Sulfate	10%	R	R	F		
(Ferric Sulfate)				•		
Isopropanol	100%	R	F	F		
Lactic Acid	85%	R	F	F		
Machine Oil	10%	R	F	F		
Machine Oil	100%	R	R	R F		
Methanol  Methyl Ethyl Ketana	100%	NR		-		
Methyl Ethyl Ketone	100%	NR	F	F		

# Strong-Tie

# **Supplemental Topics for Anchors**

Chemical	Concentration	AT-XP	SET-XP	ET-HP	AT	SET
Methyl Isobutyl Ketone	100%	NR	NR	NR	_	_
Mineral Oil	100%	R	R	R	_	_
Mineral Spirits	100%	R	R	R	_	
Mixture of Amines <sup>1</sup>	100%	R	F	F	_	_
Mixture of Aromatics <sup>2</sup>	100%	NR	NR	R		
Motor Oil (5W30)	100%	R	R	R		
N,N-Diethyaniline	100%	R	R	R		
14,14 Dietityariiirie	Concentrated	F	F	F	F	F
	40%	NR	F	F	F	F
Nitric Acid	10%	R	R	F	R	NR
	pH=3	R	R	R	_	_
	85%	R	F	F	F	F
Dhaanharia Aaid	40%	R	F	F	R	NR
Phosphoric Acid	10%	R	F	F	R	NR
	pH=3	R	R	R	_	_
	40%	NR	R	NR		_
Potassium Hydroxide	10%	NR	R	R		
	pH=13.2	R	R	R		
Potassium Permanganate	10%	R	R	R	R	R
Propylene Glycol	100%	R	R	NR	_	_
Seawater (ASTM D1141)	100%	R	R	R	_	_
Soap (ASTM D543)	100%	R	R	R	_	_
Sodium Bicarbonate	10%	R	R	R	R	R
Sodium Bisulfite	15%	R	R	R	R	NR
Sodium Carbonate	15%	R	R	R	R	R
Sodium Chloride	15%	R	R	R	R	R
Sodium Fluoride	10%	R	R	R	R	R
Sodium Hexafluorosilicate (Sodium Silicon Fluoride)	5%	R	R	R	R	R
Sodium Hydrosulfide	10%	R	R	R	_	_
-	60%	R	R	R	_	_
O a di conse la la colona di di a	40%	R	R	R	_	_
Sodium Hydroxide	10%	R	R	R	_	_
	pH=10	R	R	R	_	_
Sodium Hypochlorite	25%	R	R	R	R	R
(Bleach)	10%	R	R	R	R	R
Sodium Nitrate	15%	R	R	R	R	R
Sodium Phosphate (Trisodium Phosphate)	10%	R	R	R	R	R
Sodium Silicate	50%	R	R	R	R	R
	Concentrated	F	F	F	F	F
Sulfuric Acid	30%	R	NR	F	R	NR
	3%	R	NR	F	R	NR
TI	pH=3	R	R	R		
Toluene	100%	NR -	F	NR -		
Triethanol Amine	100%	R	NR	R		_
Turpentine	100%	R	R	R	_	_
Water	100%	R	R	R	R	R
Xylene	100%	NR	NR	R	_	_

<sup>&</sup>quot;R" - Resistant, "NR" - Non-Resistant, "F" - Failed, "-" - Not tested

<sup>1.</sup> triethanol amine, n-butylamine, N,N-dimethylamine

<sup>2.</sup> toluene, methyl naphthalene, xylene

# Allowable Stress Design (ASD) Method



In allowable stress design (ASD), the Designer must size the anchorage such that the service load does not exceed the allowable load for any anchor:

$$T_{service} \le T_{allowable}$$
 $V_{service} \le V_{allowable}$ 

The Designer must read the allowable load from the applicable table and adjust the allowable load for all applicable design parameters for the anchor, such as spacing, edge distance, in-service temperature or allowable-stress increase for short-term loads. Load-adjustment factors for anchors are applied cumulatively. For adhesive anchors, the designer must also ensure that the service load does not exceed the allowable load of the steel insert.

For anchors subjected to simultaneous tension and shear loading, the following equation must be satisfied, where the value of n is product-specific. Use a value of n=1 unless otherwise specified in the applicable products' load table.

$$\left(\frac{T_{\text{service}}}{T_{\text{allowable}}}\right)^n + \left(\frac{V_{\text{service}}}{V_{\text{allowable}}}\right)^n \le 1.0$$

Linear interpolation of allowable loads between embedment depths and/or compressive strengths shown in the load tables is permitted. Linear interpolation of load-adjustment factors in the edge distance and spacing tables is also permitted.

The allowable loads in this catalog are derived from full-scale testing, calculations, and/or experience. In general, the allowable load is determined by taking the average ultimate load from full scale tests and dividing by a safety factor  $(\Omega)$ .

$$T_{allowable} = \frac{\overline{T}_{ultimate}}{\Omega}$$
;  $V_{allowable} = \frac{\overline{V}_{ultimate}}{\Omega}$ 

For some anchors, the average ultimate load and/or allowable load is also controlled by anchor displacement limits.

The allowable loads for steel inserts used with adhesive anchors is determined as follows:

For threaded rod:  $T_{allowable} = 0.33F_uA_a$ ;  $V_{allowable} = 0.17F_uA_a$ 

For Grade 60 rebar:  $T_{allowable} = (24,000 \ psi) A_g$  ;  $V_{allowable} = 0.17 (90,000 \ psi) A_g$ 

Where:

 $A_q$  = Gross cross-sectional area of the insert

Threaded Insert Steel Type	Fu (psi)
F1554, Grade 36	58,000
A193, Grade B7	125,000
304/316 Stainless (Diam. ≤ 5/8")	100,000
304/316 Stainless (Diam ≥ 3/4")	85,000

Where:

 $F_u$  = Ultimate tensile strength of steel insert

# Strength Design (SD) Method (Under ACI 318 APPENDIX D, ICC-ES AC193, and ICC-ES AC308)

In strength design (SD), the Designer must size the anchorage such that the required strength (i.e. factored load) does not exceed the lowest design strength of the anchor or anchor group considering all possible failure modes.

$$N_{ua} \le \varphi N_n$$
  
 $V_{ua} \le \varphi V_n$ 

Calculations are performed in accordance with the applicable design standards: ICC-ES AC193 and ACI 318 Appendix D for mechanical anchors and ICC-ES AC308 for adhesive anchors. The additional design provisions of AC308 are shown elsewhere in this catalog.

The nominal strengths and design data in this catalog are derived from testing and calculations in accordance with ACl 355.2. ACl 355.4, ICC-ES AC193 and ICC-ES AC308. In general, nominal strengths are 5% fractile strengths calculated using the average ultimate load, and standard deviation of full-scale test results. A 5% fractile strength is the nominal strength for which there is a 90% confidence that there is a 95% probability of the actual strength exceeding the nominal strength.

For anchors that are designed using ACI 318 Appendix D, AC193, or AC308, it is possible to convert design strengths (i.e.  $\phi N_n$  or  $\phi V_n$ ) to allowable loads using the following approach from AC193:

$$T_{allowable, \, ASD} = \frac{\phi N_n}{\alpha}$$
 and  $V_{allowable, \, ASD} = \frac{\phi V_n}{\alpha}$ 

Where:

 $T_{allowable,ASD}$  = Allowable tension load

 $V_{allowable,ASD}$  = Allowable shear load

 $\phi N_n$  = Lowest design strength of an anchor or anchor group in tension as determined per ACI 318 Appendix D, AC193, AC308 and the IBC.

 $\phi V_n$  = Lowest design strength of an anchor or anchor group in shear as determined per ACI 318 Appendix D, AC193, AC308 and the IBC.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

 $\alpha$  = Conversion factor calculated as a weighted average of the load factors for the controlling load combination. In addition,  $\alpha$  shall include all applicable factors to account for non-ductile failure modes and required over-strength.

Interaction shall be calculated as follows:

For tension loads, T  $\leq$  0.2 $T_{allowable'}$  the full allowable load in shear shall be permitted.

For shear loads, V  $\leq$  0.2  $V_{\it allowable}$  the full allowable load in tension shall be permitted.

For all other cases: 
$$\frac{T}{T_{allowable}} + \frac{V}{V_{allowable}} \le 1.2$$

# **AC308 Modifications to ACI 318**



# 4.2.1 Replace Section D.5.5.5, and add Sections D.5.3.7 and D.8.6.1 to ACI 318 as follows:

**4.2.2 D.5.5.5** – The modification factor for adhesive anchors designed for uncracked concrete in accordance with D.5.5.2 without supplementary reinforcement to control splitting,  $\psi_{\textit{CP},\textit{Na}}$ , shall be computed as:

If 
$$c_{a,min} \ge c_{ac}$$
 then  $\psi_{cp,Na} = 1.0$  (D-26)

If 
$$c_{a,min} < c_{ac}$$
 then  $\psi_{cp,Na} = \frac{c_{a,min}}{c_{ac}}$  (D-27)

#### where

 $c_{ac}$  shall be determined in accordance with Eq. (D-27a) for anchor diameters up to 1¼ inches and for characteristic bond strengths in uncracked concrete less than or equal to 3,000 psi, and Eq. (D-27b) for anchor diameters larger than 1¼ inches or for characteristic bond strengths in uncracked concrete greater than 3,000 psi.

$$c_{ac} = h_{ef} \cdot \left(\frac{\tau_{k,uncr}}{1160}\right)^{0.4} \cdot \left[3.1 - 0.7 \frac{h}{h_{ef}}\right]$$
 (D-27a)

$$c_{ac} = h_{ef} \cdot \left(\frac{\tau_{k,uncr}}{664}\right)^{0.4} \cdot \left[3.1 - 0.7 \frac{h}{h_{ef}}\right]$$
 (D-27b)

#### where

$$\left\lceil \frac{h}{h_{ef}} \right\rceil$$
 need not be taken as larger than 2.4; and

 $au_{k,uncr}$  = characteristic bond strength stated in the Evaluation Service Report whereby  $au_{k,uncr}$  need not be taken as larger than:

$$\tau_{k,uncr} = \frac{k_{uncr} \sqrt{h_{ef} f'_{c}}}{\pi \cdot d}$$

In no case shall  $\psi_{CP,Na}$  determined from Eq. (D-27) be taken as less than  $c_{Na}$  /  $c_{ac}$ . For all other cases,  $\psi_{CP,Na}$  shall be taken as 1.0.

NOTE: Bond strength determination: Bond strength values are a function of the special-inspection level provided and installation conditions. Bond strength values must be modified with the factor  $K_{\it sat}$  for cases where the holes are drilled in water-saturated concrete as follows:

Special Inspection Level	Permissible Installation Condition	Bond Strength	Associated Strength Reduction Factor
Continuous	Dry Concrete	$ au_k$	$\Phi_{ extit{dry,ci}}$
Continuous	Water-saturated	τ <sub>k</sub> x K <sub>sat,ci</sub>	$\Phi_{\mathit{sat,ci}}$
Periodic	Dry Concrete	$\tau_k$	$\Phi_{ extit{dry,pi}}$
Periodic	Water-saturated	τκ X Ksat,pi	$\Phi_{\mathit{sat,pi}}$

Where applicable, the modified bond strengths must be used in lieu of  $\tau_{\textit{k,cr}}$  or  $\tau_{\textit{k,uncr}}$  in ACI 318. The resulting nominal bond strength must be multiplied by the strength-reduction factor for the special-inspection level listed above.

# **Example Calculations** Adhesive Anchors (Traditional ASD)



# Example calculation for a grouping of adhesive anchors using ASD:

Design a connection comprised of four %" diameter all-thread rods installed in  $f'_{\rm C}=2,000$  psi concrete using SET adhesive as shown. The anchor grouping is subject to an applied tension load of 3,000 lb. and an applied shear load of 1,000 lb. acting simultaneously.

#### ADDITIONAL DATA:

- All-thread rod material: ASTM A1554 Grade 36.
- All-thread rod embedment depth: 63/4"
- All-thread rod spacing: S1=S3=8", S2=11.3" (use 11")
   (S<sub>critical</sub> = 27" > S<sub>actual</sub>, therefore reduced efficiency.)
- All-thread rod edge distance: C1=C2=3" (C<sub>critical</sub> = 101/s" > C<sub>actual</sub>, therefore reduced efficiency.)

#### SOLUTION:

Unadjusted allowable tension loads:

Based on adhesive bond strength =  $T_{bond}$  = 10,525 lbs. Based on steel strength =  $T_{steel}$  = 8,460 lbs.

Unadjusted allowable shear loads:

Based on concrete strength = Vconc = 6,310 lbs. Based on steel strength =  $V_{steel}$  = 4,360 lbs.

Calculate reduced efficiency factors for all-thread rod installed at an edge distance of 3" using tables on pages 116–117:

Tension: C1=C2=3",  $f_{\rm C}$  = 0.56 from  $f_{\rm C}$  - Tension Table Shear: C1=C2=3",  $f_{\rm C}$  = 0.29 from  $f_{\rm C}$  - Shear Table

Calculate reduced efficiency factors for all-thread rod installed at a spacing of 8" using tables on pages 118–119:

Tension: S1=S3=8",  $f_S$  = 0.91 from  $f_S$  - Tension Table S2=11",  $f_S$  = 0.925 from  $f_S$  - Tension Table Shear: S1=S3=8",  $f_S$  = 0.95 from  $f_S$  - Shear Table S2=11",  $f_S$  = 1.00 from  $f_S$  - Shear Table

Reduce allowable tension value based on bond strength. The reduction factors are cumulative due to the influence of two reduced edge distance conditions and three reduced spacing conditions:

 $(T_{bond})$ net =  $(f_c)(f_s)(T_{bond})$ =  $(0.56 \times 0.56)(0.91 \times 0.91 \times 0.925)(10,525 \text{ lbs.})$ = 2,528 lbs.

Allowable tension value is the lesser of:

Tension based on net bond strength = 2,528 lbs. (governs) or Tension based on steel strength = 8,460 lbs.

For a group of 4 anchors the combined allowable tension value is: = (4 anchors)(2,528 lbs./anchor) = 10,112 lbs. > 3,000 lbs. (design tension) O.K.

(Note: If high in-service temperature is expected, the allowable based on bond/concrete should be multiplied by a strength reduction factor found in the adhesive's temperature sensitivity table.)

Reduce allowable shear value based on concrete strength. The reduction factors are cumulative due to the influence of two reduced edge-distance conditions and three reduced spacing conditions:

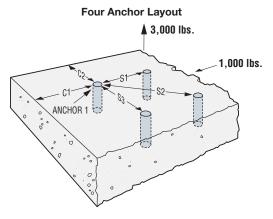
 $(V_{conc})$ net =  $(f_c)(f_s)(V_{conc})$ =  $(0.29 \times 0.29)(.95 \times .95 \times 1.00)(6,310 \text{ lbs.})$ = 478 lbs.

Allowable shear value is the lesser of:

Shear based on net concrete strength = 478 lbs. (governs) or Shear based on steel strength = 4,360 lbs.

For a group of 4 anchors the combined allowable shear value is: = (4 anchors)(478 lbs./anchor) = 1,912 lbs. > 1,000 lbs. (design shear) O.K.

(Note: If high in-service temperature is expected, the allowable shear based on bond/concrete should be multiplied by a strength reduction factor found in the adhesive's temperature sensitivity table.)



The allowable tension (or shear) value for a group of anchors is equal to the lowest (minimum) tension (or shear) value for a single anchor within the group multiplied by the number of anchors within the group.

#### CHECK COMBINED TENSION AND SHEAR INTERACTION:

For adhesive anchors, use the straight-line method (n=1.0, see Figure 1) when calculating the interaction of both tension and shear upon the anchor per the following equation:

(Design shear/allowable shear)^n + (Design tension/allowable tension)^n  $\leq 1.0,\, n{=}1.0$ 

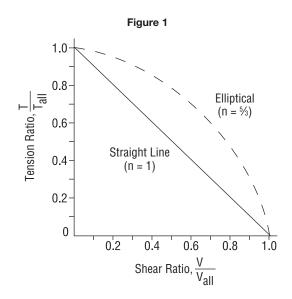
Design shear (V) = 1,000 lbs.

Allowable shear  $(V_{all}) = 1,912$  lbs.

Design tension (T) = 3,000 lbs.

Allowable tension  $(T_{all}) = 10,112$  lbs.

 $(1,000/1,912)^{1.0} + (3,000/10,112)^{1.0} = 0.82 \le 1.0$  O.K.



## **Example Calculations** Mechanical Anchors (Traditional ASD)



# Example calculation for a group of (2) Titen HD<sup>®</sup> anchors using ASD:

Design a connection comprised of two (2) 3/4" diameter Titen HD® anchors installed in the face of an 8" normal weight grouted CMU wall as shown. The anchor group has an applied tension load of 600 lbs. and an applied shear load of 500 lbs. acting simultaneously.

#### ADDITIONAL DATA:

- Embedment depth = 51/2"
- Spacing =  $S_{act}$  = S1 = 8"
- Critical spacing for  $\frac{3}{4}$ " dia. anchor at embedment =  $S_{cr}$  = 12"
- $S_{act} < S_{cr}$  therefore use spacing reduction factor for S1.
- End distance =  $C_{act}$  = C1 = 4"
- Edge distance =  $C_{act}$  = C2 = 12"
- Critical edge distance = C<sub>cr</sub> = 12"
- Critical end distance = C<sub>cr</sub> = 12"
- C1 <  $C_{cr}$ , therefore use perpendicular-to-edge reduction factor for C1.
- C2 > C<sub>cr</sub>, therefore no edge reduction factor for C2.

#### SOLUTION:

#### Tension

Determine uninfluenced allowable tension load in the face of an 8" normal wt. concrete grouted CMU wall:

Uninfluenced allowable tension = 1.600 lbs.

Calculate reduced efficiency factors for Edge Distance:

 $C_{act} = C1 = 4$ "

 $C_{act} = C2 = 12$ "

 $f_{cC1} = 0.66 = \text{Load adjustment factor (pages 198-199)}$ 

Calculate reduced efficiency factor for spacing:

 $S_{act} = S1 = 8$ "

 $f_{sS1} = 0.67 = \text{Load adjustment factor (page 200)}$ 

Calculate allowable tension load per anchor:

Allowable tension = (uninfluenced allowable tension) ( $f_{CC1}$ )( $f_{SS1}$ ) Allowable tension = (1,600 lbs.)(0.66)(0.67)= 708 lbs. per anchor

For a group of 2 anchors the combined allowable tension value is: = (2 anchors)(708 lbs./anchor) = 1,416 lbs. > 600 lbs.

### (design tension) O.K.

#### Shear

Determine uninfluenced allowable shear load in the face of an 8" normal wt. concrete grouted CMU wall:

Uninfluenced allowable shear = 3,000 lbs.

Calculate reduced efficiency factor for end distance:

 $C_{act} = C1 = 4$ "

 $C_{act} = C2 = 12$ "

 $f_{cC1} = 0.21 = \text{Load adjustment factor (pages 198-199)}$ 

Calculate reduced efficiency factor for spacing:

 $S_{act} = S1 = 8"$ 

 $f_{sS1} = 0.75 = \text{Load adjustment factor (page 200)}$ 

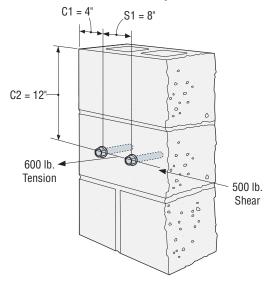
Calculate allowable shear load per anchor:

Allowable shear = (uninfluenced allowable shear) ( $f_{cC1}$ )( $f_{sS1}$ ) Allowable shear = (3,000 lbs.)(0.21)(0.75) = 473 lbs. per anchor

For a group of 2 anchors the combined allowable shear value is: = (2 anchors)(473 lbs./anchor) = **945 lbs.** > **500 lbs.** 

(design shear) O.K.

#### Two Anchor Layout



The allowable tension (or shear) value for a group of anchors is equal to the lowest (minimum) tension (or shear) value for a single anchor within the group multiplied by the number of anchors within the group.

#### CHECK COMBINED TENSION AND SHEAR INTERACTION:

For the Titen  $HD^{\otimes}$  in grouted CMU, use the straight-line method (n=1, see Figure 1) when calculating the interaction of both tension and shear upon the anchor per the following equation:

(Design shear/Allowable shear) $^{n}$  + (Design tension/Allowable tension) $^{n}$   $\leq 1.0, n = 1$ 

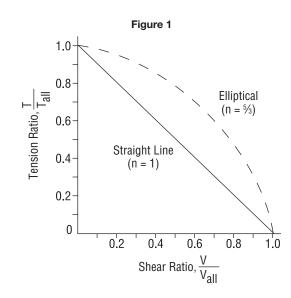
Design shear (V) = 500 lbs.

Allowable shear  $(V_{all}) = 945$  lbs.

Design tension (T) = 600 lbs.

Allowable tension  $(T_{all}) = 1,416$  lbs.

 $(600/1,416)^1 + (500/945)^1 = 0.95 \le 1.0$  **O.K.** 



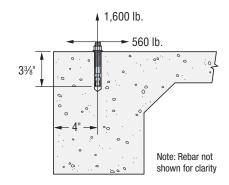
### Example Calculations Mechanical Anchors (ACI 318 App. D / ICC-ES AC193)



# Example calculation for a single Strong-Bolt™ 2 anchor using SD:

Determine if a single ½" diameter carbon-steel Strong-Bolt™ 2 torque-controlled expansion anchor with a minimum 3½" embedment ( $h_{ef} = 3\%$  inches) installed 4" from the edge of a 12" deep spandrel beam is adequate for a strength level tension load of 1,600 lb. for wind and a reversible strength level shear load of 560 lb. for wind. The anchor will be in the tension zone, away from other anchors in  $f'_{C} = 3,000$  psi normal-weight concrete.

Reference the appropriate tables in this catalog for Strong-Bolt 2 anchor performance values as determined from testing in accordance with ACI 355.2 and ICC-ES AC193.



#### CALCULATIONS AND DISCUSSION

#### REFERENCE

Note: Calculations are performed in accordance with ACI 318-11.

1. Determine the factored tension and shear design loads:

ACI 318, 9.2.1

$$N_{Ua} = 1.0W = 1.0 \times 1,600 = 1,600 \text{ lb.}$$

$$V_{ua} = 1.0W = 1.0 \times 560 = 560 \text{ lb.}$$

2. Design considerations:

D.4.1.1

This is a combined tension and shear interaction problem where values for both  $\phi N_n$  and  $\phi V_n$  need to be determined.  $\phi N_n$  is the lesser of the design tension strength controlled by: steel  $(\phi N_{sa})$ , concrete breakout  $(\phi N_{cb})$ , or pull-out  $(\phi n N_{pn})$ .  $\phi V_n$  is the lesser of the design shear strength controlled by: steel  $(\phi V_{sa})$ , concrete breakout  $(\phi V_{cb})$ , or pryout  $(\phi V_{cb})$ , or pryout  $(\phi V_{cb})$ .

3. Steel capacity under tension Loading:

D.5.1

 $\phi N_{sa} \ge N_{ua}$ 

D.4.1.1

 $N_{sa} = 12,100 \text{ lb.}$ 

This catalog

 $\phi = 0.75$ 

This catalog ψ

n = 1 (single anchor)

Calculating for  $\phi N_{sa}$ :

 $\phi N_{sa} = 0.75 \times 1 \times 12,100 = 9,075 \text{ lb.} > 1,600 \text{ lb.}$  **O.K.** 

#### CALCULATIONS AND DISCUSSION

#### REFERENCE

4. Concrete breakout capacity under tension loading:

D.5.2 D.4.1.1

$$\phi N_{CD} \ge N_{Ua}$$

$$N_{cb} = \frac{A_{Nc}}{A_{Nco}} \ \psi_{ed,N} \, \psi_{c,N} \, \psi_{cp,N} \, N_b$$

Eq. (D-3);

where:

$$N_b = k_c \lambda_a \sqrt{f'_c} h_{ef}^{1.5}$$

Eq. (D-6)

substituting:

$$\phi N_{cb} = \phi \frac{A_{Nc}}{A_{Nco}} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} K_c \lambda_a \sqrt{f'_c} h_{ef}^{1.5}$$

where:

 $k_C = k_{Cr} = 17$ 

This catalog

(Anchor is installed in a tension zone, therefore, cracking is assumed at service loads

 $\lambda = 1.0$  for normal-weight concrete 8.6.1

 $\psi_{CD,N} = 1.0$ 

D.5.2.7

$$\psi_{ed,N} = 0.7 + 0.3 \ \frac{c_{a,min}}{1.5 h_{ef}} \ \ \text{when} \ c_{a,min} < 1.5 \ h_{ef}$$

Eq. (D-10)

by observation,  $c_{a,min} = 4 < 1.5 h_{ef}$ 

$$\psi_{ed,N} = 0.7 + 0.3 \frac{(4)}{1.5(3.375)} = 0.94$$

 $\psi_{c,N} = 1.0$  assuming cracking

D.5.2.6

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

at service loads ( $f_t > f_r$ )  $\phi = 0.65$  for Condition B

This catalog

(no supplementary reinforcement provided)

Eq. (D-5)

 $A_{Nco} = 9h_{ef}^2$ = 9(3.375)<sup>2</sup> = 102.52 in.<sup>2</sup>

 $A_{Nc} = (c_{a1} + 1.5h_{ef})(2 \times 1.5h_{ef})$ =  $(4 + 1.5(3.375))(2 \times 1.5(3.375))$  Fig. RD.5.2.1(a)

= 91.76 in.<sup>2</sup>

$$\frac{A_{Nc}}{A_{Nco}} = \frac{91.76}{102.52} = 0.90$$

Calculating for  $\phi N_{cb}$ :

$$\phi N_{cb} = 0.65 \times 0.90 \times 0.94 \times 1.0 \times 1.0 \times 17 \times 1.0 \times \sqrt{3,000} \times (3.375)^{1.5} = 3,175 \text{ lb.} > 1,600 \text{ lb.}$$
 **O.K.**

### Continued on next page

Would you like help with these calculations?
Visit www.strongtie.com to download the Simpson Strong-Tie® Anchor Designer™ software.

### Example Calculations Mechanical Anchors (ACI 318 App. D / ICC-ES AC193)



REFERENCE

# **CALCULATIONS AND DISCUSSION**5. Pullout capacity under tension loading:

#### REFERENCE

D.5.3

Pullout capacity,  $N_{p,cr}$ , is established by reference tests in cracked concrete by the reliability test of ACI 355.2. Data from the anchor prequalification testing must be used. Reference Strong-Bolt® 2 anchor "characteristic tension design values" table for the 5 percent fractile value,  $N_{p,cr}$ .

$$N_{p,cr} = 3,735 \times \left(\frac{3,000}{2,500}\right)^{0.5} = 4,091 \text{ lb.}$$
 This catalog

$$\phi = 0.65$$
 This catalog

$$\phi N_{pn} = 0.65 \times 4,091 = 2,659 \text{ lb.} > 1,600 \text{ lb.}$$
 **O.K.**

Summary:

Steel capacity = 9,075 lb. Concrete breakout capacity = 3,175 lb.

Pullout capacity = 2,659 lb. ← Controls

#### $\therefore \phi N_n = 2,659$ lb. as pullout capacity controls

7. Steel capacity under shear loading: D.6.1 
$$\phi V_{sa} \geq V_{ua} \qquad \qquad D.4.1.1 \\ V_{sa} = 7,235 \text{ lb.} \qquad \qquad This \ catalog \\ \phi = 0.65 \qquad \qquad This \ catalog$$

Calculating for 
$$\phi V_{sa}$$
:

$$\phi V_{SA} = 0.65 \times 7,235 = 4,703 \text{ lb.} > 560 \text{ lb.}$$
 **O.K.**

$$\phi V_{cb} \ge V_{ua}$$

$$A...$$

$$D.4.1.1$$

$$V_{cb} = \frac{A_{Vc}}{A_{Vco}} \quad \Psi_{ed,V} \, \Psi_{c,V} \, \Psi_{h,v} \, V_b \qquad \qquad \textit{Eq. (D-30)}$$

where:

$$V_b = 7 \left(\frac{\ell_e}{d_{.}}\right)^{0.2} \sqrt{d_a} \, \lambda_a \sqrt{t'_c} \, c_{a1}^{1.5}$$
 Eq. (D-33)

substituting:

$$\phi V_{cb} = \phi \frac{A_{Vc}}{A_{Vco}} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,v} 7 \left(\frac{\ell_e}{d_a}\right)^{0.2} \sqrt{d_a} \lambda_a \sqrt{f'_c} C_{a1}^{1.5}$$

where:

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

$$\phi = 0.70$$
 for Condition B D4.4(c)(i)

(no supplementary reinforcement provided)

$$A_{Vco} = 4.5c_{a1}^2$$
 Eq. (D-32)  
=  $4.5(4)^2$ 

∴ 
$$A_{Vco} = 72 \text{ in.}^2$$

$$A_{VC} = 2(1.5c_{a1})(1.5c_{a1})$$
 Fig. RD.6.2.1(a)  
=  $2(1.5(4))(1.5(4))$ 

$$A_{Vc} = 72 \text{ in.}^2$$

$$\frac{A_{VC}}{A_{VCO}} = \frac{72}{72} = 1$$
 D.6.2.1

 $h_a = 12 \text{ in.}$ 

$$\psi_{h,v} = 1.0 \text{ since } h_a > 1.5 C_{a1}$$
 D.6.2.8  $\psi_{ed,V} = 1.0 \text{ since } c_{a2} > 1.5 c_{a1}$  Eq. (D-37)

 $\psi_{C,V} = 1.0$  assuming cracking

at service loads  $(f_t > f_r)$  D.6.2.7

 $d_a = 0.5 \text{ in.}$ 

$$\ell_{\rm e} = 3.375$$
 in. D.6.2.2  $\lambda_{\rm a} = 1.0$  for normal-weight concrete 8.6.1

 $c_{a1} = 4 \text{ in.}$ 

$$\phi V_{cb} = 0.70 \times 1 \times 1.0 \times 1.0 \times 1.0 \times 7 \times \left(\frac{3.375}{0.5}\right)^{0.2} \times \sqrt{0.5} \times 1.0$$

$$x \sqrt{3,000} x (4)^{1.5} = 2,224 \text{ lb.} > 560 \text{ lb.}$$
 **O.K.**

#### CALCULATIONS AND DISCUSSION

9. Concrete pryout strength: D.6.3

$$\phi n V_{CD} \ge V_{Ua}$$
 D.4.1.1 
$$V_{CD} = k_{CD} N_{Cb}$$
 Eq. (D-40)

where:

n = 1

$$k_{cp} = 2.0$$
 and  $\phi = 0.70$  This catalog

$$k_{cp} N_{cb} = 2.0 \times \frac{3,175}{0.65} = 9,769 \text{ lb.}$$
 D.6.3.1

$$\phi nV_{CD} = 0.70 \times 1 \times 9,769 = 6,838 \text{ lb.} > 560 \text{ lb.}$$
 **O.K.**

10. Check all failure modes under shear Loading: D.4.1.1

Summary:

Steel capacity = 4,703 lb.

Concrete breakout capacity = 2,224 lb. ← Controls

Pryout capacity = 6,838 lb.

#### $\therefore \phi V_n = 2,224$ lb. as concrete breakout capacity controls

11. Check interaction of tension and shear forces: D.7

If  $0.2 \phi V_n \ge V_{ua}$ , then the full tension

design strength is permitted. D.7.1

By observation, this is not the case.

If 0.2  $\phi N_n \ge N_{U\!a}$ , then the full shear design strength is permitted D.7.2

By observation, this is not the case.

Therefore:

$$\frac{N_{ua}}{\phi N_n} + \frac{V_{ua}}{\phi V_n} \le 1.2$$
 Eq. (D-42)

$$\frac{1,600}{2,659} + \frac{560}{2,224} = 0.60 + 0.25 = 0.85 < 1.2$$
 **O.K.**

#### 12. Summary

A single ½" diameter carbon-steel Strong-Bolt® 2 anchor at a 3%" embedment depth is adequate to resist the applied strength level tension and shear wind loads of 1,600 lb. and 560 lb., respectively.

### **Example Calculations** Adhesive Anchors (ACI 318 App.D / ICC-ES AC308)



#### Example calculation for a single SET-XP® epoxy adhesive anchor using SD:

Determine if a single 1/2" diameter ASTM A193 Grade B7 anchor rod in SET-XP® epoxy adhesive anchor with a minimum 41/2" embedment  $(h_{ef} = 4\frac{1}{2})$  installed 1\%" from the edge of a 12" deep spandrel beam is adequate for a strength level tension load of 1,040 lb. for wind and a reversible strength level shear load of 440 lb. for wind. The anchor will be in the tension zone, away from other anchors in  $f'_c = 3,000$ psi normal-weight concrete (dry). The anchor will be subjected to a maximum short-term temperature of 150°F and a maximum long-term temperature of 110°F. Continuous inspection will be provided

Reference the appropriate tables in this catalog for SET-XP epoxy adhesive anchor performance values as determined from testing in accordance with ACI 355.4 and ICC-ES AC308.

# 1,040 lb. 440 lb. 13/4" Note: Rebar not shown for clarity

#### CALCULATIONS AND DISCUSSION

#### REFERENCE

Note: Calculations are performed in accordance with ICC-ES AC308 and ACI 318-11.

1. Determine the factored tension and shear design loads:

ACI 318, 9,2,1

 $N_{ua} = 1.0W = 1.0 \times 1,040 = 1,040 \text{ lb.}$ 

 $V_{ua} = 1.0W = 1.0 \times 440 = 440 \text{ lb.}$ 

#### 2. Design considerations:

D.4.1.1

This is a combined tension and shear interaction problem where values for both  $\phi N_n$  and  $\phi V_n$  need to be determined.  $\phi N_n$  is the lesser of the design tension strength controlled by: steel ( $\phi N_{sa}$ ), concrete breakout ( $\phi N_{cb}$ ), or adhesive ( $\phi N_{a}$ ).  $\phi V_n$  is the lesser of the design shear strength controlled by: steel ( $\phi V_{sa}$ ), concrete breakout ( $\phi V_{cb}$ ), or pryout ( $\phi V_{cp}$ ).

3. Steel capacity under tension loading:

D.5.1 D.4.1.1  $\phi N_{sa} \ge N_{ua}$ 

 $N_{sa} = 17,750 \text{ lb.}$ 

This catalog

 $\phi = 0.75$ This catalog

n = 1 (single anchor)

Calculating for  $\phi N_{sa}$ :

 $\phi N_{sa} = 0.75 \times 1 \times 17,750 = 13,313 \text{ lb.} > 1,040 \text{ lb.}$  **O.K.** 

#### CALCULATIONS AND DISCUSSION REFERENCE

4. Concrete breakout capacity under tension loading: D.5.2

 $\phi N_{ch} \ge N_{ua}$ D.4.1.1

 $N_{cb} = \frac{A_{Nc}}{A_{Nco}} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ Eq. (D-3)

 $N_b = k_c \lambda_a \sqrt{f'_c} h_{ef}^{1.5}$ Eq. (D-6)

substituting:

$$\phi N_{cb} = \phi \frac{A_{Nc}}{A_{Nco}} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5}$$

where:

 $k_{c} = k_{cr} = 17$ This catalog

8.6.1  $\lambda_a = 1.0$  for normal-weight concrete

 $\psi_{CD,N} = 1.0$ D.5.2.7

 $\psi_{ed,N} = 0.7 + 0.3 \frac{c_{a,min}}{1.5h_{cf}}$  when  $c_{a,min} < 1.5h_{ef}$ Eq. (D-10)

by observation,  $c_{a,min} < 1.5 h_{ef}$ 

 $\psi_{ed,N} = 0.7 + 0.3 \frac{1.75}{1.5(4.5)} = 0.78$ 

D.5.2.6  $\psi_{C,N} = 1.0$ 

 $\phi = 0.65$  for Condition B This catalog

(no supplementary reinforcement provided)

 $A_{Nco} = 9h_{ef}^2$ Eq. (D-5)

 $= 9(4.5)^2$ 

 $= 182.25 \text{ in.}^2$ 

Fig. RD.5.2.1(a)  $A_{Nc} = (c_{a1} + 1.5h_{ef})(2 \times 1.5h_{ef})$  $= (1.75 + 1.5(4.5))(2 \times 1.5(4.5))$ 

= 114.75 in.<sup>2</sup>

 $\frac{A_{Nc}}{A_{Nc}} = \frac{114.75}{100} = 0.63$  $A_{Nco} = 182.25$ 

 $f'_{c} = 2,500 \text{ psi}$ ICC-ES ESR-2508 section 5.3

Calculating for  $\phi N_{cb}$ :

 $\phi N_{cb} = 0.65 \times 0.63 \times 1.0 \times 0.78 \times 1.0 \times 17 \times 1.0 \times 10^{-2}$ 

 $\sqrt{2,500}$  x (4.5)<sup>1.5</sup> = 2,592 lb. > 1,040 lb. **O.K.** 

D0449440

Would you like help with these calculations?

Visit www.stronatie.com to download the

Simpson Strong-Tie® Anchor Designer™ software.

ET-HIP

#### Continued on next page

### Example Calculations Adhesive Anchors (ACI 318 App.D / ICC-ES AC308)



REFERENCE

CALCULATIONS AND DISCUSSION	REFERENCE	CALCULATIONS AND DISCUSSION
5. Adhesive anchor capacity	D.5.5	8. Concrete breakout capacity under shear loa
under tension loading:		$\phi V_{CD} \ge V_{ua}$
$\phi N_a \geq N_{ua}$	D.4.1.1	$V_{cb} = \frac{A_{Vc}}{A_{Vc,v}} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,v} V_b$
$N_a = \frac{A_{Na}}{A_{Nao}} \Psi_{ed,Na} \Psi_{cp,Na} N_{ba}$	Eq. (D-18)	· VCO
$N_{ba} = \tau_{k,cr} \pi da_{hef} = 510(1.72)\pi(0.5)(4.5) = 6,200 \text{ lb.}$	Ea. (D-22)	where:
	-4· ()	$V_b = 7 \left(\frac{l_e}{d}\right)^{0.2} \sqrt{d_a} \lambda_a \sqrt{f'_c} C_{a1}^{1.5}$
$c_{Na} = 10d_a \sqrt{\frac{\tau_{k,uncr}}{1.100}}$	Eq. (D-21)	(G <sub>a</sub> )
11,100		substituting:
$c_{Na} = (10)(0.5)\sqrt{\frac{1,150(1.72)}{1,100}} = 6.70$ "		$\phi V_{cb} = \phi \frac{A_{Vc}}{A_{Vco}} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} 7 \left(\frac{\ell_{\theta}}{d_{a}}\right)^{0.2} \sqrt{d_{a}} \chi_{ed,V}$
$A_{N/20} = (2c_{N/2})^2 = (13.40)^2 = 179.56 \text{ in.}^2$	Ea. (D-20)	where:
$A_{Nao} = (20_{Na})^2 = (13.40)^2 = 179.30 \text{ m}.$	Eq. (D-20)	$\phi$ = 0.70 for Condition B
$A_{Na} = (c_{a1} + 2c_{Na})(2c_{Na}) = (1.75 + 6.70)(13.40) = 113.2$	23 in. <sup>2</sup>	(no supplementary reinforcement provided)
$\psi_{ed,Na} = \left(0.7 + 0.3 \frac{c_{a,min}}{c_{Na}}\right) \le 1.0 \text{ Since } c_{a,min} < c_{Na}$	Eq. (D-25)	$A_{VCO} = 4.5C_{a1}^{2}$ $= 4.5(1.75)^{2}$ $= 4.778 \text{ in } 2$
$\psi_{ed,Na} = \left(0.7 + 0.3 \frac{C_{a,min}}{C_{b,c}}\right) = \left(0.7 + 0.3 \frac{1.75}{6.70}\right) = 0.78$		$A_{VCO} = 13.78 \text{ in.}^2$
$\frac{\sqrt{ea}}{6.70} = \frac{1}{6.70} =$		$A_{Vc} = 2(1.5c_{a1})(1.5c_{a1})$ = 2(1.5(1.75))(1.5(1.75))
$\psi_{cp,Na} = 1.0$	D.5.5.5	$\therefore A_{VC} = 13.78 \text{ in.}^2$
$\phi = 0.65$ for dry concrete	This catalog	AVc 13.78 4
Calculating for $\phi N_a$ :		$\frac{AVc}{AVco} = \frac{13.78}{13.78} = 1$
$\phi N_a = 0.65 \times \frac{113.23}{179.56} \times 0.78 \times 1.0 \times 6,200 = 1,982 \text{ lb}$	. > 1,040 lb. <b>O.K.</b>	$h_a = 12 \text{ in.}$
		$\psi_{h,v} = 1.0 \text{ since } h_a > 1.5 c_{a1}$
6. Check all failure modes under tension loading:	D.4.1.1	$\psi_{ed,V} = 1.0 \text{ since } c_{a2} > 1.5c_{a1}$
Summary:		$\psi_{\text{C,V}} = 1.0$ for cracked concrete

Concrete breakout capacity = 2,592 lb. = 1,982 lb. ← **Controls** Adhesive capacity

∴  $\phi N_n = 1,982$  lbs. as adhesive capacity controls

7. Steel capacity under shear loading: D.6.1 D.4.1.1  $\phi V_{Sa} \ge V_{ua}$  $V_{sa} = 10,650 \text{ lb.}$ This catalog  $\phi = 0.65$ This catalog

= 13,313 lb.

Calculating for  $\phi V_{sa}$ :

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

Steel capacity

$$\phi V_{Sa} = 0.65 \text{ x } 10,650 = 6,923 \text{ lb.} > 440 \text{ lb. } \mathbf{O.K.}$$

oading: D.6.2

D.4.1.1

$$V_{cb} = \frac{A_{Vc}}{A_{Vco}} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,v} V_b$$
 Eq. (D-30)

$$V_b = 7 \left(\frac{\ell_e}{d}\right)^{0.2} \sqrt{d_a} \, \lambda_a \sqrt{f'_c} \, c_{a1}^{1.5}$$
 Eq. (D-33)

$$\phi V_{CD} = \phi \frac{A_{VC}}{A_{VCO}} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} 7 \left(\frac{\ell_e}{d_a}\right)^{0.2} \sqrt{d_a} \lambda_a \sqrt{f'_c} c_{a1}^{1.5}$$

D4.4(c)(i) Eq. (D-32)

Fig. RD.6.2.1(a)

$$\frac{AVc}{AV(c)} = \frac{13.78}{13.78} = 1$$
 D.6.2.1

D.6.2.8 Eq. (D-37) D.6.2.7  $d_a = 0.5 \text{ in.}$  $\ell_e = 8d_a = 8 (0.5) = 4$ " D.6.2.2  $\lambda = 1.0$  for normal-weight concrete 8.6.1

 $c_{a1} = 1.75$  in.

$$\phi V_{cb} = 0.70 \times 1 \times 1.0 \times 1.0 \times 1.0 \times 7 \times \left(\frac{4}{0.5}\right) 0.2 \times \sqrt{0.5} \times 1.0 \times \sqrt{3,000} \times (1.75) 1.5 = 666 \text{ lb.} > 440 \text{ lb. } \mathbf{O.K.}$$

9. Concrete pryout capacity under shear loading: D.6.3

 $V_{cp} = \min[k_{cp} N_a; k_{cp} N_{cb}]$ D.6.3.1

 $k_{cp} = 2.0 \text{ for } h_{ef} \ge 2.5$ "

 $N_a = 3,050$  lb. from adhesive-capacity calculation without  $\phi$  factor

 $N_{cb}$  = 3,988 lb. from concrete-breakout calculation without  $\phi$  factor

 $V_{CD} = (2.0)(3,050) = 6,100$  lb. controls

 $\phi = 0.7$ This catalog

 $\phi V_{CP} = (0.7)(6,100) = 4,270 \text{ lb.} > 440 \text{ lb.} \text{ O.K.}$ 

#### Continued on next page

#### CALCULATIONS AND DISCUSSION

#### REFERENCE

10. Check all failure modes under shear loading:

D.4.1.1

Example Calculations Adhesive Anchors (ACI 318 App.D / ICC-ES AC308)

Summary:

Steel capacity = 6,923 lb.

Concrete breakout capacity = 666 lb. ← Controls

Pryout capacity = 4,270 lb.

 $\therefore \phi V_n = 666$  lb. as concrete breakout capacity controls

11. Check interaction of tension and shear forces: D.7

lf

$$\frac{V_{ua}}{\phi V_n} \le 0.2$$

then the full tension design strength is permitted.

D.7.1

By observation, this is not the case.

Ιf

$$\frac{N_{ua}}{\phi N_n} \le 0.2$$

then the full shear design strength is permitted.

D.7.2

By observation, this is not the case.

Therefore:

$$\frac{N_{ua}}{\phi N_n} + \frac{V_{ua}}{\phi V_n} \le 1.2$$
 Eq. (D-42)

$$\frac{1,040}{1,982} + \frac{440}{666} = 0.52 + 0.66 = 1.18 < 1.2$$
 **O.K.**

12. Summary

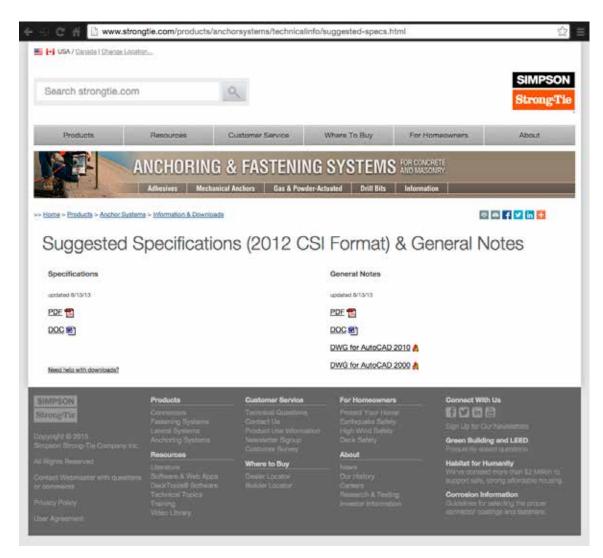
A single ½" diameter ASTM A193 Grade B7 anchor rod in SET-XP® epoxy adhesive at a 4½" embedment depth is adequate to resist the applied strength level tension and shear wind loads of 1,040 lb. and 440 lb., respectively.

C-A-2016 @2015 SIMPSON STRONG-TIE COMPANY INC.

### Suggested General Notes for Anchor Products



To download the full text of Suggested General Notes, please visit strongtie.com/products/anchorsystems/technicalinfo/suggested-specs.html.



### **Glossary**



ACI — American Concrete Institute

**ACRYLIC** — Polymer based on resins prepared from a combination of acrylic and methacrylic esters.

**ADHESIVE ANCHOR** — Typically, a threaded rod or rebar that is installed in a predrilled hole in a base material with a two-part chemical compound.

**ADMIXTURE** — A material other than water, aggregate or hydraulic cement used as an ingredient of concrete and added to concrete before or during its mixing to modify its properties.

**AERATED CONCRETE** — Concrete that has been mixed with airentraining additives to protect against freeze-thaw damage and provide additional workability.

**AGGREGATE** — A granular material, such as sand, gravel, crushed stone and iron blast-furnace slag, used with a cementing medium to form a hydraulic cement concrete or mortar.

AISC — American Institute of Steel Construction

**ALLOWABLE LOAD** — The maximum design load that can be applied to an anchor. Allowable loads for mechanical and adhesive anchors are based on applying a factor of safety to the average ultimate load.

**ALLOWABLE STRESS DESIGN (ASD)** — A design method in which an anchor is selected such that service loads do not exceed the anchor's allowable load. The allowable load is the average ultimate load divided by a factor of safety.

**AMINE CURING AGENT** — Reactive ingredient used as a setting agent for epoxy resins to form highly crosslinked polymers.

**ANCHOR CATEGORY** — The classification for an anchor that is established by the performance of the anchor in reliability tests such as sensitivity to reduced installation effort for mechanical anchors or sensitivity to hole cleaning for adhesive anchors.

ANSI — American National Standards Institute

ASTM — American Society for Testing and Materials

**BASE MATERIAL** — The substrate (concrete, CMU, etc.) into which adhesive or mechanical anchors are to be installed.

**BOND STRENGTH** — The mechanical interlock or chemical bonding capacity of an adhesive to both the insert and the base material.

**BRICK** — A solid masonry unit of clay or shale formed into a rectangular prism while plastic and burned or fired in a kiln that may have cores or cells comprising less than 25% of the cross sectional area.

**CAMA** — Concrete Anchor Manufacturer's Association

 $\begin{tabular}{ll} \textbf{CAST-IN-PLACE ANCHOR} & - \textbf{A} \text{ headed bolt, stud or hooked bolt} \\ \textbf{Installed into formwork prior to placing concrete.} \\ \end{tabular}$ 

**CHARACTERISTIC DESIGN VALUE** — The nominal strength for which there is 90% confidence that there is a 95% probability of the actual strength exceeding the nominal strength.

**CONCRETE** — A mixture of Portland cement or any other hydraulic cement, fine aggregate, coarse aggregate and water, with or without admixtures. Approximate weight is 150 pcf.

**CONCRETE BRICK** — A solid concrete masonry unit (CMU) made from Portland cement, water, and aggregates.

**CONCRETE COMPRESSIVE STRENGTH (f'<sub>c</sub>)** — The specified compressive load carrying capacity of concrete used in design, expressed in pounds per square inch (psi) or megapascals (MPa).

**CONCRETE MASONRY UNIT (CMU)** — A hollow or solid masonry unit made from cementitious materials, water and aggregates.

**CORE DRILL** — A method of drilling a smooth wall hole in a base material using a special drill attachment.

**CREEP** — Displacement under a sustained load over time.

**CURE TIME** — The elapsed time required for an adhesive anchor to develop its ultimate carrying capacity.

**DESIGN LOAD** — The calculated maximum load that is to be applied to the anchor for the life of the structure.

**DESIGN STRENGTH** — The nominal strength of an anchor calculated per ACI 318, ICC-ES AC193 or ICC-ES AC308 and then multiplied by a strength reduction factor ( $\phi$ ).

**DROP-IN ANCHOR** — A post-installed mechanical anchor consisting of an internally-threaded steel shell and a tapered expander plug. The bottom end of the steel shell is slotted longitudinally into equal segments. The anchor is installed in a pre-drilled hole using a hammer and a hand-setting tool. The anchor is set when the tapered expander plug is driven toward the bottom end of the anchor such that the shoulder of the hand-setting tool makes contact with the top end of the anchor. A drop-in anchor may also be referred to as a displacement controlled expansion anchor.

**DYNAMIC LOAD** — A load whose magnitude varies with time.

#### **EDGE DISTANCE:**

 $\mbox{\bf EDGE DISTANCE}$  (C) — The measure between the anchor centerline and the free edge of the concrete or masonry member.

**CRITICAL EDGE DISTANCE (C\_{cr} or C\_{ac})** — The least edge distance at which the allowable load capacity of an anchor is applicable without reductions.

**MINIMUM EDGE DISTANCE**  $(C_{min})$  — The least edge distance at which the anchors are tested for recognition.

**EFFECTIVE EMBEDMENT DEPTH** — The dimension measured from the concrete surface to the deepest point at which the anchor tension load is transferred to the concrete.

**EMBEDMENT DEPTH** — The distance from the top surface of the base material to the installed end of the anchor. In the case of a post-installed mechanical anchor, the embedment depth is measured prior to application of the installation torque.

 $\mbox{\bf EPOXY RESIN}-A$  viscous liquid containing epoxide groups that can be crosslinked into final form by means of a chemical reaction with a variety of setting agents.

**EXPANSION ANCHOR** — A mechanical fastener placed in hardened concrete or assembled masonry, designed to expand in a self-drilled or predrilled hole of a specified size and engage the sides of the hole in one or more locations to develop shear and/or tension resistance to applied loads without grout, adhesive or drypack.

**FATIGUE LOAD TEST** — A test in which the anchor is subjected to a specified load magnitude for  $2 \times 10^6$  cycles in order to establish the endurance limit of the anchor.

### **Glossary**



**GEL TIME** — The elapsed time at which an adhesive begins to increase in viscosity and becomes resistant to flow.

**GROUT** — A mixture of cementitious material and aggregate to which sufficient water is added to produce pouring consistency without segregation of the constituents.

#### GROUTED MASONRY (or GROUT-FILLED MASONRY) -

Hollow-unit masonry in which the cells are filled solidly with grout. Also, double or triple-wythe wall construction in which the cavity(s) or collar joint(s) is filled solidly with grout.

**HOT-DIP GALVANIZED** — A part coated with a relatively thick layer of zinc by means of dipping the part in molten zinc.

IAPMO UES — IAPMO Uniform Evaluation Service. An ISO 17065 ANSI-accredited company that issues evaluation reports expressing a professional opinion as to a product's building code compliance.

IBC — International Building Code.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

ICC-ES — ICC Evaluation Service. An ISO 17065 ANSI-accredited company that issues evaluation reports expressing a professional opinion as to a product's building code compliance.

**LEGACY ACCEPTANCE CRITERIA** — A past version of an ICC-ES anchor qualification criteria. These are no longer current standards, but are the basis for legacy allowable load data for anchors in concrete. These standards have been replaced by modern standards such as ICC-ES AC193 and AC308.

**LIGHTWEIGHT CONCRETE** — Concrete containing lightweight aggregate. The unit weight of lightweight concrete is not to exceed 115 pcf.

**MASONRY** — Brick, structural clay tile, stone, concrete masonry units or a combination thereof bonded together with mortar.

**MECHANICALLY GALVANIZED** — A part coated with a layer of zinc by means of mechanical impact. The thickest levels of mechanical galvanizing (ASTM B695, Class 55 or greater) are considered to be alternatives to hot-dip galvanizing and provide a medium level of corrosion resistance.

**MORTAR** — A mixture of cementitious materials, fine aggregate and water used to bond masonry units together.

**NOMINAL STRENGTH** — The strength of an element as calculated per ACI 318, ICC-ES AC193 or ICC-ES AC308.

**NORMAL WEIGHT CONCRETE** — Concrete containing normal weight aggregate. The unit weight of normal weight concrete is approximately 150 pcf.

**OBLIQUE LOAD** — A load that is applied to an anchor, which can be resolved into tension and shear components.

**PLAIN CONCRETE** — Structural concrete with no reinforcement or with less reinforcement than the minimum specified for reinforced concrete.

**PORTLAND CEMENT** — Hydraulic cement consisting of finely pulverized compounds of silica, lime and alumina.

**POST-INSTALLED ANCHOR** — Either a mechanical or adhesive anchor installed in a pre-drilled hole in the base material.

**POST-TENSION** — A method of prestressing in which tendons are tensioned after concrete has hardened.

**POT LIFE** — The length of time a mixed adhesive remains workable (flowable) before hardening.

**PRECAST CONCRETE** — A concrete structural element cast elsewhere than its final position in the structure.

**PRESTRESSED CONCRETE** — Structural concrete in which internal stresses have been introduced to reduce potential tensile stresses in concrete resulting from loads.

**PRETENSIONING** — A method of prestressing in which tendons are tensioned before concrete is placed.

**REBAR** — Deformed reinforcing steel which comply with ASTM A615.

**REINFORCED CONCRETE** — Structural concrete reinforced with no less than the minimum amount of prestressed tendons or nonprestressed reinforcement specified in ACI 318.

**REINFORCED MASONRY** — Masonry units and reinforcing steel bonded with mortar and/or grout in such a manner that the components act together in resisting forces.

**REQUIRED STRENGTH** — The factored loads and factored load combinations that must be resisted by an anchor.

**SCREEN TUBE** — Typically a wire or plastic mesh tube used with adhesives for anchoring into hollow base materials to prevent the adhesive from flowing uncontrolled into voids.

**SCREW ANCHOR** — A post-installed anchor that is a threaded mechanical fastener placed in a predrilled hole. The anchor derives its tensile holding strength from the mechanical interlock of the fastener threads with the grooves cut into the concrete during the anchor installation.

**SHEAR LOAD** — A load applied perpendicular to the axis of an anchor.

**SHOTCRETE** — Concrete that is pneumatically projected onto a surface at high velocity. Also known as gunite.

**SLEEVE ANCHOR** — A post-installed mechanical anchor consisting of a steel stud with nut and washer, threaded on the top end and a formed uniform tapered mandrel on the opposite end around which a full length expansion sleeve formed from sheet steel is positioned. The anchor is installed in a predrilled hole and set by tightening the nut by torquing thereby causing the expansion sleeve to expand over the tapered mandrel to engage the base material.

#### SPACING:

 $\ensuremath{\mathsf{SPACING}}$  (S) — The measure between anchors, centerline-to-centerline distance.

**CRITICAL SPACING (S\_{cr})** — The least anchor spacing distance at which the allowable load capacity of an anchor is applicable such that the anchor is not influenced by neighboring anchors.

**MINIMUM SPACING (S\_{min})** — The least anchor spacing at which the anchors are tested for recognition.

**STAINLESS STEEL** — A family of iron alloys containing a minimum of 12% chromium. Type-316 stainless steel provides greater corrosion resistance than Types 303 or 304.

**STANDARD DEVIATION** — As it pertains to this catalog, a statistical measure of how widely dispersed the individual test results were from the published average ultimate loads.

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

### **Glossary**

SIMPSON Strong-Tie

 $\ensuremath{\mathsf{STATIC}}\xspace \ensuremath{\mathsf{LOAD}}\xspace - \ensuremath{\mathsf{A}}\xspace$  load whose magnitude does not vary appreciably over time.

**STRENGTH DESIGN (SD)** — A design method in which an anchor is selected such that the anchor's design strength is equal to or greater than the anchor's required strength.

**STRENGTH REDUCTION FACTOR (** $\phi$ **)** — A factor applied to the nominal strength to allow for variations in material strengths and dimensions, inaccuracies in design equations, required ductility and reliability, and the importance of the anchor in the structure.

**TENDON** — In pretensioned applications, the tendon is the prestressing steel. In post-tensioned applications, the tendon is a complete assembly consisting of anchorages, prestressing steel, and sheathing with coating for unbonded applications or ducts with grout for bonded applications.

**TENSION LOAD** — A load applied parallel to the axis of an anchor.

**THIXOTROPIC** — The ability of a fluid to become less viscous (resistant to flow) under shear, then thicken when the shear force is removed.

**TORQUE** — The measure of the force applied to produce rotational motion usually measured in foot-pounds. Torque is determined by multiplying the applied force by the distance from the pivot point to the point where the force is applied.

**ULTIMATE LOAD** — The average value of the maximum loads that were achieved when five or more samples of a given product were installed and statically load tested to failure under similar conditions. The ultimate load is used to derive the allowable load by applying a factor of safety.

**UNDERCUT ANCHOR** — A post-installed anchor that develops its tensile strength from the mechanical interlock provided by undercutting of the concrete at the embedded end of the anchor.

**UNREINFORCED MASONRY (URM)** — A form of clay brick masonry bearing wall construction consisting of multiple wythes periodically interconnected with header courses. In addition, this type of wall construction contains less than the minimum amounts of reinforcement as defined for reinforced masonry walls.

**WEDGE ANCHOR** — A post-installed mechanical anchor consisting of a steel stud with nut and washer, threaded on the top end and a formed uniform tapered mandrel on the opposite end around which an expansion clip formed from sheet steel is positioned. The anchor is installed in a predrilled hole and set by tightening the nut by torquing, thereby causing the expansion clip to expand over the tapered mandrel to engage the base material. A wedge anchor may also be referred to as a torque controlled expansion anchor.

 $\ensuremath{\mathbf{WYTHE}}$  — A continuous vertical section of masonry one unit in thickness.

**ZINC PLATED** — A part coated with a relatively thin layer of zinc by means of electroplating.

# **Alphabetical Index of Products**



AD	Drill Bit Shank Adaptor	309
ADT	Acrylic Dispensing Tools	128
ADTA	Arcylic Battery-Powered and Pneumatic Dispensing Tools	128
AMN	Acrylic Mixing Nozzle	129
ARC	Adhesive Retaining Caps	132
AST	Adhesive Shear Tube	135
AT	Acrylic Adhesive	86–101
AT-XP	Acrylic Adhesive	20–37
ATS & ATSP	Acrylic Screens	133–134
BBMD	Blue Banger Hanger®	215
BBRD	Blue Banger Hanger®	216
		-
BBWF	Blue Banger Hanger®	214
CBMX	One-Piece Core Bit — SDS-MAX Shank	313
CBSP	One-Piece Core Bit – Spline Shank	313
CD	Crimp Drive® Anchor	242–243
CDBE	One-Piece Core Bit – Ejector Key	313
CDT10S	Adhesive Dispensing Tool	128, 287
СНН	Hex Shank Chisels and Demolition Bits	311–312
СНМХ	SDS-MAX Chisels and Demolition Bits	310–312
CHPL	SDS-PLUS Chisels and Demolition Bits	310–311
CHSP	Spline Shank Chisels and Demolition Bits	311
CIP-F	Crack Injection Paste Over	288–289, 293
CPFH	Crack-Pac® Flex-H20™ Crack Sealer	288
CSD	Countersunk Split Drive	244
CTRB	One-Piece Core Bit – Center Pilot Bit	313
DIA	Drop-In Anchor	229–235
DIAB	Drop-In Anchor	224–228
DIABST	Drop-In Anchor Setting Tool	225
DIAST	Drop-In Anchor Setting Tool	230
DSD	Duplex Head Split Drive	244
ED0T	General-Purpose Epoxy Anchoring Adhesive	122–123
EDT	Epoxy Dispensing Tools	128
EDTA	Epoxy Battery-Powered and Pneumatic Dispensing Tools	128
EIF	Injection Fitting	289
EIP	Injection Port	288–289
EMN	Epoxy Mixing Nozzle	129
ESA	Expansion Screw Anchor	240
ET-HP®	Epoxy Adhesive	62–85
ETB	Hole-Cleaning Brush	135
ETI	Crack Injection Epoxy	284–285
ETIPAC	Crack-Pac® Injection Epoxy	286
ETR	Epzoxy Paste	286, 288–289
ETS & ETSP	Epoxy Screens	133–134
EZAC	Easy-Set Pin-Drive Anchor	179
E-Z-Click	Injection System	286, 288–289
GAC	Gas Pins	251
GCC	Gas Pins	251

C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.

# SIMPSON Strong-Tie

# **Alphabetical Index of Products**

GCL	Gas Pins	251
GCN-MEP	Gas-Actuated Concrete Nailer	248
GCT	Gas Pins	251
GDP	Gas Pins	249
GDPS	Gas Pins	249
GDPSK	Spiral-Knurled Gas Pins	250
GFC	Gas Fuel Cell	250
GMR-2	Magnetic Ring	250
GRH	Gas Pins	251
GTH	Gas Pins	251
GTS	Gas Pins	251
GW	Gas Pins	251
GWL-100	Lathing Washer	250
HDIA	Hollow Drop-In Anchor	236–238
HELI	Heli-Tie Helical Wall and Stitching Tie	290–292
LSES	Lag Screw Expansion Shield	239
MC	Rebar Cutter Shank – Straight	308
MCP	Plate Cutter Head	308
MCR	Rebar Cutter Head	308
MCS	Rebar Cutter Shank – Spline	308
MCSDM	Rebar Cutter Shank – SDS-MAX	308
MCSDP	Rebar Cutter Shank – SDS-PLUS	308
MDA	"A" Taper Shank Drill Bits	306
MDB	Straight Shank Drill Bits	207, 307
MDBP	Titen Drill Bit / Driver	207, 303
MDMX	SDS-MAX & SDS-MAX Quad Head Bits	304
MDPL	SDS-PLUS Shank Bits	225, 230, 302
MDSP	Spline Shank Drill Bits	305–306
P22	.22 Cal. Powder Load – Single, Crimped	253, 265
P22LRSC	.22 Cal. Powder Load – Single, Straight Wall	253, 265
P25SL	.25 Cal. Powder Load — Strip	253, 265
P27LVL	.27 Cal. Powder Load — Single, Long	253, 265
P27SL	.27 Cal. Powder Load — Strip	253, 265
PBXDP	BX Cable Strap	253, 269
PCC	Conduit Clip	253, 269
PCLDPA	Ceiling Clip	253, 267
PDPA	0.157" Shank Diameter Drive Pin	253, 266
PDPAS	.157" Shank Diameter Drive Pin	253, 267
PDPAT	0.157" Shank Diameter Tophat Fastener	253, 267
PDPAW	0.157" Shank Diameter hopitat rasterior  0.157" Shank Diameter with ¾" Metal Washer	253, 266
PDPAWL	0.157" Shank Diameter with 1" Metal Washer	253, 266
PDPWLSS	0.145" Shank Diameter and 1" Metal Washer – Type-304 Stainless Steel	253, 268
PECLDPA	Ceiling Clip	253, 267
PEPT	Pole Tool / Accessories	252
PEPT-LR	Pole Tool / Accessories	252, 257, 259
PHBC	Highway Basket Clip	253, 269
PHD	Hammer Drive Pin	272
עוו ו	Hammor Dilye i III	212

# **Alphabetical Index of Products**

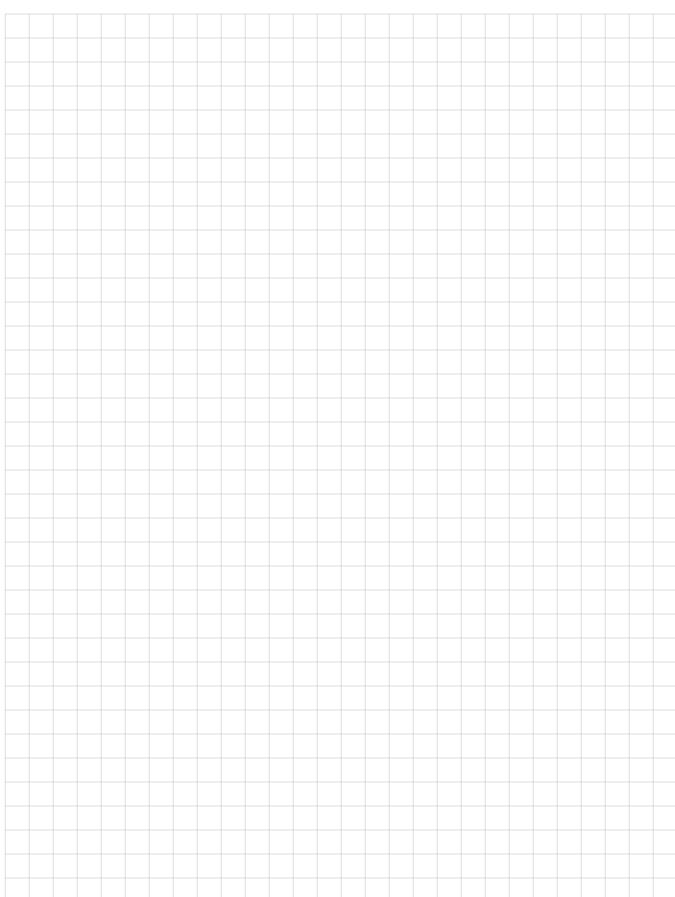
C-A-2016 @ 2015 SIMPSON STRONG-TIE COMPANY INC.



PHNW	8mm Headed Pin with 1" Washer	253, 271
PHT	Hammer Drive Tool	272
PINW	100 through 300 $-$ 0.300" Headed Pin with $1\%\ensuremath{\text{e}}$ Washer	253, 268
PINWP	100 through 300 $-$ 0.300" Headed Pin with $1\%\mbox{6}$ Plastic Washer	253, 268
PKP	Concrete Forming Pin	253, 272
PSLV3	%" Threaded Stud	253, 270
PSLV4	1/4" Threaded Stud	253, 269
PT-22A	.22 Cal. Powder-Actuated Tool	253, 255, 262
PT-22HA	Hammer-Activated Powder Tool	253, 255, 263
PT-22P	Powder-Actuated Tool	253, 255, 264
PT-27	.27 Cal. Powder-Actuated Tool	252, 253, 255, 261
PT-27HDA	Heavy-Duty Powder-Actuated Tool	253, 255, 260
PTP-27L	.27 Cal. Auto Powder-Actuated Tool	252–254, 256–257
PTP-27LMAGR	.27 Cal. Auto Powder-Actuated Tool with Magazine	252–254, 256–257
PTP-27S	.27 Cal. Auto Powder-Actuated Tool	252–254, 258–259
PTP-27SMAGR	.27 Cal. Auto Powder-Actuated Tool with Rotating Magazine	252–254, 258–259
PTRHA	0.157" Shank Diameter Threaded Rod Hanger	253, 267
RFB	Retrofit Bolt	135
RWH	Horizontal Wood Rod Hanger	212–213
RWV	Vertical Wood Rod Hanger	212–213
SET	Epoxy Adhesive	102–121
SET-XP®	Epoxy Adhesive	38–61
SL	Sleeve-All® Anchor	180–183
STB2	Strong-Bolt® 2 Wedge Anchor	144–163
SWN	Sure Wall Anchor – Nylon	245
SWZ	Sure Wall Anchor – Zinc	245
TCA	Torq-Cut™ Anchor	138–143
THD	Titen HD® Heavy-Duty Screw Anchor	184–199
THDB	Titen HD® Heavy-Duty Screw Anchor	184–199
THD RC	Titen HD® Rod Coupler	201–202
THD RH	Titen HD® Rod Hanger	208–211
TTN	Titen® Concrete and Masonry Screw	203–204
TTNSS	Titen® Concrete and Masonry Screw – Stainless Steel	205–206
TTNT	Titen® Screw Installation Tool	207
TW	Tie Wire Anchor	177–178
WA	Wedge-All® Anchor	164–176
ZN	Zinc Nailon™	241

### **Notes**

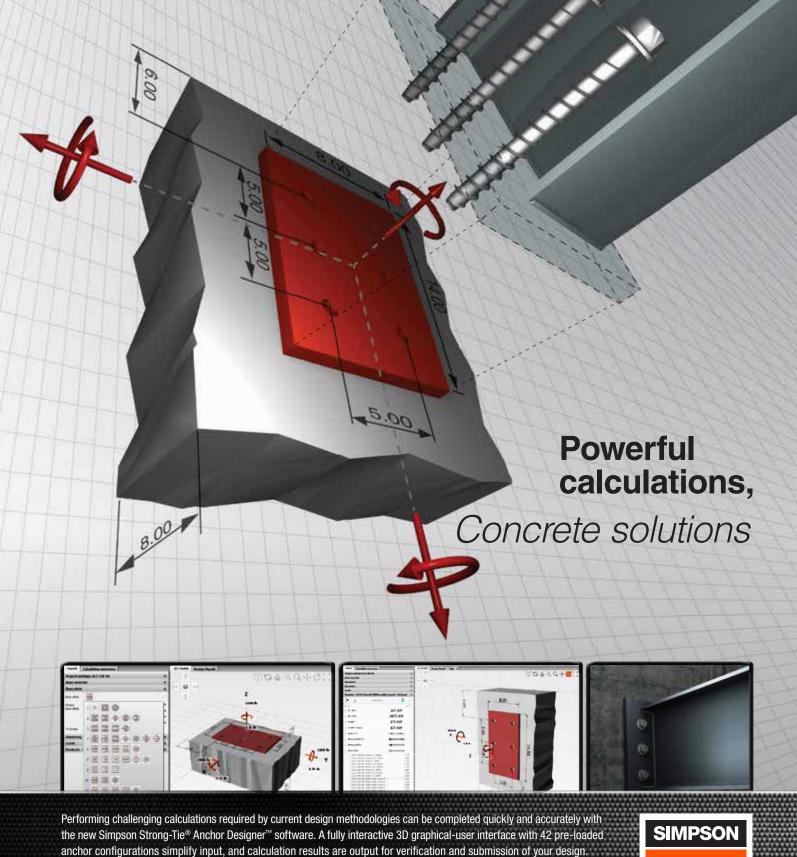




### **Notes**







Anchor Designer complies with current ACI 318, ETAG and CSA code requirements.

Call (800) 999-5099 to learn more and download the free software at strongtie.com/anchordesigner.

